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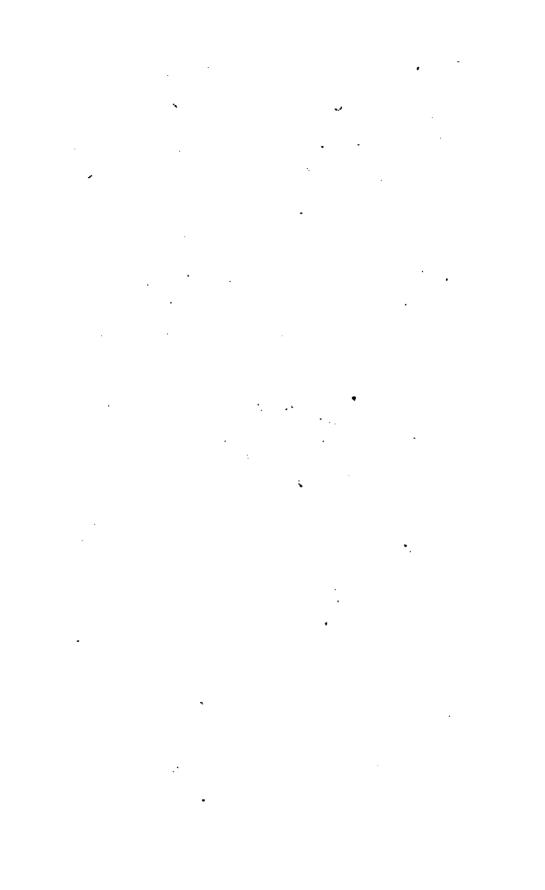






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#### THEORY AND PRACTICE

OF

# SURVEYING;

CONTAINING

All the Instructions requisite for the skilful practice of this Art.

6634

BY ROBERT GIBSON.

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THE WHOLE CORRECTED, NEWLY ARRANGED, AND GREATLY ENLARGED,

WITH USEFUL SELECTIONS.

AND A NEW SET OF ACCURATE

### **MATHEMATICAL TABLES**

BY D. P. ADAMS, TEAGHER OF THE MATHEMATICS

**NEW-YORK:** 

PUBLISHED BY EVERT DUYCKINCK.
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Bistrict of New-York, as.

BE IT REMEMBERED, that on the twenty-eighth day of March, in the thirty-fifth year of the Independence of the United States of America, Evert Dayckinck, of the said district, bath deposited in this office the title of a book, the right whereof he claims as proprietor, in the words following to wit:

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"The Theory and Practice of Surveying; containing all the Instructions requisite for the skilful practice of this Art. By Robert Gibson. Illustrated by Copper-Plates. The whole corrected, newly arranged, and greatly enlarged, with useful Selections, and anew set of accurate Mathematical Tables. By D. P. Adams, Teacher of the Mathematics."

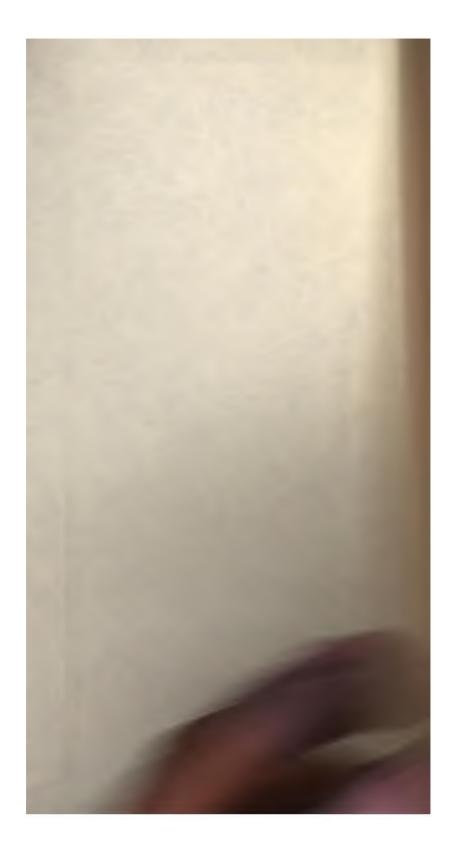
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CHARLES CLINTON, Clerk of the District of New-York

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Add 6.2 121.306 .75 2.7 and .0007 together. 121.06

.75

2.7

.0007

Sum = 130.9567

What is the sum of 6.57 1.026 .75 146.5 8.7 526. 3.97 and .0271?
Answer 693.5431.

What is the sum of 4.51 146.071 .507 .0006 132. 62.71 .507 7.9 and .10712?

Answer 354.31272.

#### SUBTRACTION OF DECIMALS.

Write the figures of the subtrahend beneath those of the minuend according to the denom nation of their places, as directed in the rule of addition; then, beginning at the right hand, subtract as in whole numbers, and place the decimal point in the difference exactly under the other two points.

#### EXAMPLES.

From 38.765 take 25.3741 25.3741

Difference = 13.3909.

From 2.4 take .8472 .8472

Diff. = 1.5528

From 71.45 take 8.4837248.

Difference = 62.9662752.

From 84 take 82.3412.

Diff. = 1.6588.

#### MULTIPLICATION OF DECIMALS.

Set the multiplier under the multiplicand without any regard to the situation of the decimal point; and having multiplied as in whole numbers, cut off as many places for decimals in the product, counting from the right hand towards the left, as there are in both the multiplicand and multiplier: but if there be not a sufficient number of places in the product, the defect may be supplied by prefixing ciphers thereto.

For the denominator of the product being an unit, prefixed to as many ciphers, as the denominators of the multiplier and multiplicand contain of ciphers, it follows, that the places of decimals in the product, will be as many as in the numbers

from whence it arose.

#### EXAMPLES.

Multiply 121.6 by 2.76 2.76

7296 8512 2432

Product = 335.616

Multiply .0089789 by 1085 Product=9.7421065

Multiply .248723 by .13587 Product = .03379399401.

#### DIVISION OF DECIMALS.

Divide as in whole numbers; observing that the divisor and quotient together must contain as many decimal places as there are in the dividend. therefore, the dividend have just as many places of decimals as the divisor has, the quotient will be a whole number without any decimal figures. If there be more places of decimals in the dividend, than there are in the divisor, point off as many figures in the quotient for decimals, as the decimal places in the dividend exceed those in the divisor; the want of places in the quotient being supplied by prefixing ciphers. But if there be more decimal places in the divisor, than in the dividend. annex ciphers to the dividend, so that the decimal places here may be equal, in number, to those in the divisor; and then the quotient will be a whole number, without fractions.

When there is a remainder, after the division has been thus performed, annex ciphers to this remainder, and continue the operation till nothing remains, or till a sufficient number of decimals shall be found in the quotient.

#### EXAMPLES.

Divide .144 by .12

.12).144(1.2=quotient.

Divide 63.72413456922 by 2718 2718)63.72413456922(.02344522979=quotient.

**3**6

There being II decimal figures in the dividited, and none in the divisor, II figures are to be cut off in the quotient; but as the quotient itself consists of but IO figures, prefix to them a cipher to complete that number.

Divide 1.728 by .012 .019)1.728(144 quotient.

59

48

40

Because the number of decimal figures in the divisor and dividend, are alike, the quotient will be integers.

Divide 2 by 3.1416

3.1416)2.0000,0(0.636618 + = quotient.

1 8849 6

115040 94248

> 907990 188496

> > 194240

188496

57440 31416

260240

251228

9012+ C What is the value of .6875 of a yard?

3 = number of feet in a [yard.

2.0625

12 = number of inches [in a foot.

.7500

12 = number of lines in [an inch.

9.0000

The answer here is 2 feet 9 lines.

What is the value of .084 of a furlong? Ans. 3 per. 1 yd. 2 ft. 11 in.

What is the value of .683 of a degree? Ans. 40

m. 58 sec. 48 thirds.

What is the value of .0053 of a mile? Ans. 1

per. 3 yds. 2 ft 5 in.+

What is the value of .036 of a day? Ans. 51' 50" 24".

# PROPORTION

### IN DECIMAL FRACTIONS.

Having reduced all the fractional parts in the given quantities to their corresponding decimals, and having stated the three known terms, so that the fourth, or required quantity, may be as much greater, or less than the third, as the second term is greater, or less than the first, then multiply the second and third terms together, and divide the product by the first term, and the quotient will be the answer;—in the same denomination with the third term.

# EXAMPLES.

If 3 acres 3 roods of land can be purchased for 93 dollars 60 ets. how much will 15 acres 1 rood cost at that rate?

```
3 \text{ acs. } 3 \text{ rds.} = 3.75 \text{ acres.}
       15 \text{ acs. } 1 \text{ rd} = 15.25 \text{ acres.}
     93, 60 cts. = 393.60
Then 3.75: 15.25:: 93.60:
                           468 00
                          18720
                        46800
                        9360
                 3.75)1427.4000(380.64=Answer.
                       1125
                        3024
                        3000
                           2400
                           2250
                             1500
                             1500
```

If a clock gain 14 seconds in 5 days 6 hours, flow much will it gain in 17 days 45 hours? Ans. 47 seconds.

If 187 dollars 85 cents gain 12 dollars 33 cents interest in a year, at what rate per cent is this interest? Ans. 6.56+

#### SECTION IL

# INVOLUTION AND EVOLUTION.

Involution is the method of raising any number, considered as the root, to any required power

Any number, whether given, or assumed at pleasure, may be called the root, or first power of this number; and its other powers are the products, that result from multiplying the number by itself, and the last product by the same number again; and so on to any number of multiplications.

The index, or exponent, is the number denoting the height, or degree of the power, being always greater by one, than the number of multiplications employed in producing the power. It is usually written above the root, as in the following EXAMPLE, where the method of involution is plainly exhibited.

Required the fifth power of 8 } = the root, or first first multiply by - - 8 } = power.

then multiply the product  $64 = 8^2 = \text{square}$ , or by 8 [second power.

&c.  $512 = 8^3 = \text{ cube, or third } 8$  [power.

4096 = 8' = biquadrate or [fourth power.

 $32768 = 8^5 =$ Answer.

#### EXAMPLES FOR EXERCISE.

What is the second power of 3.05? Ans. 9.3025 What is the third power of 85.3? Answer, 620650.477

What is the fourth power of .073? Answer, 090028398241

What is the eighth power of .09? Answer. .00.00.00,0043046721

Note. When two, or more powers are multiplied together, their product is that power, whose index is the sum of the indices of the factors, or powers multiplied.

EVOLUTION is the method of extracting any re-

quired root from any given power.

Any number may be considered as a power of some other number; and the required root of any given power is that number, which, being multiplied into itself a particular number of times, produces the given power; thus if 81 be the given number, or power, its square, or second root is 9; because 9×9=9°=81; and 3 is its biquadrate, or fourth root, because 3×3×3×3=34=81. Again, if 729 be the given power, and its cube root be required, the answer is 9, for 9×9×9=729; and if the sixth root of that number be required, it is found to be 3, for  $3 \times 3 \times 3 \times 3 \times 3 \times 3 = 729$ .

The required power of any given number, or root, can always be obtained exactly, by multiplying the number continually into it self; but there are many numbers, from which a proposed root can never be completely extracted ;-yet by approximating with decimals, these roots may be found as exact as necessity requires. The roots that are found complete, are denominated rational roots, and those, which cannot be found completed, or which only approximate, are called surd, or wrational roots.

Roots are usually represented by these characters or exponents;

v, or which signifies the square root; thus,

 $\sqrt{9}$ , or  $9\frac{1}{2} = 3$ 

or toube root;

\$64, or 644 =4

\*, or \* hiquadrate roof; 7 16, or 16 =2 &c

Likewise 8\* signifies the square root of 8 cubed; and, in general, the fractional indices imply, that the given numbers are to be raised to such powers as are denoted by their numerators, and that such roots are to be extracted from these powers, as are denoted by their denominators.

### RULE

# For extracting the Square Root.

Separate the given number into periods of two figures, by putting a point over the place of units, another over the place of hundreds, and so on, over every second figure, both toward the left hand in whole numbers, and toward the right hand in the Decimal places.—When the number of integral places is odd, the first, or left hand period will consist of one figure only.

Find the greatest square in the first period on the left hand, and write its root on the right hand of the given number, in the manner of a quotient

figure in division.

Subtract the square, thus found, from the said period, and to the remainder annex the two figures

of the next following period, for a dividend.

Double the root above mentioned for a divisor, and find how often it is contained in the said dividend, exclusive of its right hand figure, and set this quotient both in the place of the quotient and in the divisor.—The best way of doubling the root to form each new divisor, is to add the last figure always to the last divisor, as it is done in the subsequent examples.

Multiply the whole augmented divisor by this last quotient figure, and subtract the product from the said dividend, bringing down to it the next period of the given number for a new dividend.

Repeat the same operation again; that is, find another new divisor, by doubling all the figures now found in the root; from which, and the last dividend, find the next figure of the root as before; and so on through all the periods to the last.

- Nate 1. After the figures belonging to the given number are all exhausted, the operation may be continued in decimals, by annexing any number of periods of ciphers to the ramainder.
- 2. The number of integral places in the root, is always equal to the number of periods in the integral part of the resolvend.
- 3. When vulgar fractions occur in the given power, or number, they may be reduced to decimals, then the operation will be the same as before dictated.

#### EXAMPLES.

Required the square root of 1710864.

Required the square root of 16007.3104.

1   16007.3104(	126.52=Answer.
22   60 2   44	A STATE OF THE PARTY OF THE PAR
246   1607 6   1476	Service Fredry
2525   13131 5   12625	To be leaded to the
25302   50604   50604	TOTAL STATE

#### EXAMPLES FOR EXERCISE.

Required the square root of 298116. Ans. 546. Required the square root of 348.17320836. Ans. 18.6594.

Required the square root of 17.3056. Ans. 4.16. Required the square root of .000729. Ans. .027, Required the square root of 175. Ans. 4.168333+

## A GENERAL RULE

For extracting any Root whatever.

Find by trial a number, which, when involved to the power denoted by the index of the required root, shall come nearest to the given number, whether greater or less; and let that number be called the assumed root, and when thus involved, the assumed power,

Let the given power, or number be repre- sented by	G.
the index, or exponent, in the question by the assumed power, by	X.
the assumed root, by and the required root by	Q.

Then  $X+1 \times A + X-1 \times G : X+1 \times G + X-1 \times A$ :: Q: R.

That is, as the sum of X+1 times A and X-1 times G,

is to the sum of X+1 times G and X-1 times A,

so is the assumed root, Q,

to the required root, R,—nearly; and the operation may be repeated as many times, as we chuse, by using always the root last found for the assumed root, and this, involved according to the given index, for the assumed power.\*

#### EXAMPLES.

# 1. Required the Cube root of 789.

" "This is a very general approximating rule," says Dr. Hutton, "of which that for the cube root is a particular case, and is the best adapted for practice and for memory, of any that I have yet seen. It was first discovered in this form by myself, and the investigation and use of it were given at large in my Tracts—page 45 &c."

Here G=789, X=3, Q=9, A=9<sup>3</sup> =729, X+1
=4 and X-1=2.
And 4×729=2916 4×789=3156
2×789=1578 2×729=1458

Then 4494 : 4614 :: 9: 9.240+
9
4494)41526(9.2403+ [Ans. 40446

10800
8988

18120
17976

14400
13482

918 &c.

In the foregoing example the answer is strictly correct in its integral part and also in the three first decimal places; but if more decimals were wanted, and if their exactness were likewise requisite, the present answer might be taken for the assumed root, and the whole operation should be repeated.

2. Required the biquadrate root of 2.0743.

Here G=2.0743, Q=1.2, A= $\overline{1.2}^{\circ}$  =2.0736, X=4,  $\overline{X+1}$ =5, and  $\overline{X-1}$ =3. And  $5\times2.0736$ =10.3680  $5\times2.0743$ =10.3715  $3\times2.0743$ = 6.2229  $3\times2.0736$ = 6.2208 Then 16.5909 : 16.5923 [:: 1.2 : 1,2001+Ans.

Required the fifth root of 21035.8 Ans.=7.3213+ Required the sixth root of 21035.8 Ans.=5.2540+ Required the cube root of 999 Ans.=9.9966+ Required the cube root of 97.41 Ans.=3.1416 Required the cube root of .037 Ans.=.33322+ Required the cube root of 2 Ans.=1.2599+ Required the seventh root of 21035.8 Answer=

# SECTION III.

smirt aft like, beauty

# OF LOGARITHMS.

LOGARITHMS are a series of numbers, so contrived, that by them the work of mutiplication may be performed by addition; and the operation of division may be done by subtraction. Or,—Logarithms are the indices, or series of numbers in arithmetical progression, corresponding to another series of numbers in geometrical progression. Thus.

\$ 0, 1, 2, 3, 4, 5, 6, &c. Indices or Logarithms. 1, 2, 4, 8, 16, 32, 64, &c. Geometrical progression.

0, 1, 2, 3, 4, 5, 6, &c. Ind. or Log. 1, 3, 9, 27, 81, 243, 729, &c. Geometrical Series.

{ 0, 1, 2, 3, 4, 5, 6,&c.I.orL. 1, 10, 100, 1000, 10000, 100000, 100000, &c. Geometrical series,—where the same indices serve equally for any Geometrical series, or progression.

Hence it appears that there may be as many kinds of indices, or logarithms, as there can be taken kinds of geometrical series. But the Logarithms most convenient for common uses are those adapted to a geometrical series increasing in a tenfold progression, as in the last of the foregoing

examples.

In the geometrical series 1, 10, 100, 1000, &c. if between the terms 1 and 10, the numbers ?, 3, 4, 5, 6, 7, 8, 9 were interposed, indices might also be adapted to them in an arithmetical progression, suited to the terms interposed between 1 and 10, considered as a geometrical progression. Moreover, proper indices may be found to all the numbers, that can be interposed between any two terms of the Geometrical series.

But it is evident that all the indices to the numbers under 10, must be less than 1; that is, they must be fractions. Those to the numbers between 10 and 100, must fall between 1 and 2; that is, they are mixed numbers, consisting of 1 and some fraction. Likewise the indices to the numbers between 100 and 1000, will fall between 2 and 3; that is, they are mixed numbers, consisting of 2 and some fraction; and so of the other indices.

Hereafter the integral part only of these indices will be called the Index; and the fractional part will be called the Logarithm. The computation of these fractional parts, is called making Logarithms; and the most troublesome part of this work is to make the Logarithms of Prime Numbers, or those which cannot be divided by any other numbers than themselves and unity.

# RULE

For Computing the Logarithms of Numbers.

Let the sum of its proposed number and the next less number be called A. Divide 0.8685889638 × †

† The number 0.8685889638 + is the quotient of 2 divided by 2 302585093, which is the logarithm of 10, according to the first

by A, and reserve the quotient. Divide the reserved quotient by the square of A, and reserve this quotient. Divide the last reserved quotient by the square of A, reserving the quotient still; and thus proceed as long as division can be made. Write the reserved quotients orderly under one another, the first being uppermost. Divide these quotients respectively by the odd numbers 1, 3, 5, 7, 9, 11, &c.; that is, divide the first reserved quotient by 1, the second by 3, the third by 5, the fourth by 7, &c. and let these quotients be written orderly under one another; add them together and their sum will be a logarithm. To this logarithm add the logarithm of the next less number, and the sum will be the logarithm of the number proposed.

form of Lord Napier, the inventor of logarithms. The manner in which Napier's logarithm of 10 is found, may be seen in most books of Algebra, but it is here omitted, because students of Surveying are too generally unacquainted with the principles of that science, and the subject is too extensive for the present treatise. Those, however, who have not an opportunity for entering thoroughly into this subject, may with more propriety grant the truth of one number, and thereby be enabled to try the correctness of any logarithm in the tables, than receive those tables, as truly computed, without any means of examining their securacy.

The supplementation of the

#### EXAMPLE 1.

Required the Logarithm of the number 2.

Here the next less number is 1, and 2+1=3=A. and A<sup>2</sup>, or  $3^2=9$ ; then

3)0.868588964

9)0.289529654÷ 1=0.289529654

9)0.032169962÷ 3=0.010723321

9)0.003574440÷ 5=0.000714888

9)0.000397160÷ 7=0.000056737

9)0.000044129 ÷ 9=0.000004903

9)0.000004903÷11=0.000000446

9)0.000000545÷13=0.000000042

0.000000061÷15=0.000000004

To this Logarithm 0.301029995 addthe Logarithm of 1=0.000000000

Their Sum =0.301029995=Log. of 2.

The manner in which the division is here carried on, may be readily perceived by dividing, in the first place, the given decimal by A, and the succeeding quotients by A<sup>2</sup>; then letting these quotients remain in their situation, as seen in the example, divide them respectively by the odd numbers, and place the new quotients in a column by themselves. By employing this process, the operation is considerably abbreviated.

### EXAMPLE 2.

Required the Logarithm of the number 3.

Here the next less number is 2; and 3+2 5=A, and  $A^2=25$ .

5)0.868588964

25)0.173717793÷ 1=0.173717793

25)0.006948712÷ 3=0.002316237

25)0.000277948÷ 5=0.000055599

25)0.000011118÷ 7=0.000001588

25)0.000000445÷ 9=0.000000049

0.000000018+11=0.0000000002

To this Logarithm 0.176091259 add the Logarithm of 2=0.301029995

Their Sum=0.477121254=Log. of 3.

Then, because the sum of the logarithms of numbers, gives the logarithm of their product; and the difference of the logarithms, gives the logarithm of the quotient of the numbers: from the two preceding logarithms, and the logarithm of 10, which is 1, a great many logarithms can be easily made, as in the following examples.

Example 3. Required the Logarithm of 4.

Since 4=2×2, then to the Logarithm of 2=0.301029995 add the Logarithm of 2=0.301029995

The sum=Logarithm of 4=0.602059990

Example 4.	Required the Log	arithm of 5.
. –	=5, therefore from btract the Log. or	10=1.000000000
the remai	inder is the Log. of	5 = 0.698970005
Example 5.	Required the Lo	garithm of 6.
-	erefore to the Logard the Logarithm or	3=0.477191254
	their sum=Log. of	f 6=0.778151249
Example 6.	Required the Log	parithm of 8.
8=2 <sup>3</sup> , therefo	ore multiply the L	ogarithm of 2=0.301029995 by 3
The	e product=Log. of	8=0.903089985
Example 7.	Required the Log	garithm of 9.
$9=3^{\circ}$ , theref	ore the Logarithm	3 = 0.477121254

the product=Log. of 9=0.954242508

Example 8. Required the Logarithm of 7.

Here the next less number is 6, and 7+6=13=A, and  $A^{2}=169$ .

13)0.868588964

169)0.066814536÷1=0.066814536

169)0.000395352÷3=0.000131784

 $169)0.000002339 \div 5 = 0.000000468$ 

0.000000014 + 7 = 0.0000000002

To this Logarithm=0.066946790 add the Log. of 6=0.778151249

Their sum=0.845098039=Log. of 7.

of 19
of 14
of 15 is equal to the sum
of 16
of 18
of 20

of 20

of 7.

of 3 and 4.
of 7 and 2.
of 3 and 5.
of 4 and 4.
of 3 and 6.
of 4 and 5.

The Logarithms of the prime numbers, 11, 13, 17, 19, &c. being computed by the foregoing general Rule, the Logarithms of the intermediate numbers are easily found by composition and division. It may, however, be observed, that the operation is shorter in the larger prime numbers; for when any given number exceeds 400, the first quotient, being added to the Logarithm of its next lesser number, will give the Logarithm sought, true to 8, or 9 places; and therefore it will be very easy to examine any suspected Logarithm in the Tables.

For the arrangement of Logarithms in a Table, the method of finding the Logarithm of any natural number, and of finding the natural number corresponding to any given Logarithm, therein: likewise for particular rules concerning the Indices, the reader will consult Table 1, with its explanation, at the end of this Treatise.

### MULTIPLICATION.

Two, or more numbers being given, to find their product by Logarithms.

#### RULE.

Having found the Logarithms of the given numbers in the Table, add them together, and their sum is the Logarithm of the product; which Logarithm, being found in the Table, will give a natural number, that is, the product required

tural number, that is, the product required.

Whatever is carried from the decimal part of the

Whatever is carried from the decimal part of the Logarithm is to be added to the affirmative indices; but subtracted from the negative. Likewise the indices must be added together, when they are all of the same kind, that is, when they are all affirmative, or all negative; but when they are of different kinds, the difference must be found, which will be of the same denomination with the greater.

Example 1. Required the product of 86.25 multiplied by 6.48

Log. of 86.25=1.935759 Log. of 6.48=0.811575

Product=558.9=2.747334

Example 2. Required the product of 46.75 and 3275

Log. of 46.75= 1.669782 Log. of .3275=-1.515211

Product=15.31+ = 1.184993

Example 3. Required the product of 3.768, 2.053 and .007693.

Log. of 3.768= 0.576111 Log. of 2.053= 0.312389 Lc., of .007693=-3.886096

Product = .05951×=-2774596

Example 4. Required the product of 27.63 1.859, .7258 and 0.3591.

Log. of 27.63 = 1.441381Log. of 1.859 = 0.26979Log. of .7258 = -1.860317Log. of .03591 = -2.555215

Product nearly=1.339 = 0.126692

### DIVISION.

Two numbers being given, to find how many times one is contained in the other, by Legarithms.

#### RULE.

From the Logarithm of the Dividend subtracthe Logarithm of the Divisor, and the remainder will be the Logarithm, whose corresponding natural number will be the Quotient required.

In this operation, the Index of the Divisor mus be changed from affirmative to negative, or from negative to affirmative; and then the difference of the affirmative and negative Indices must be taken for the index to the Logarithm of the Quo tient. Likewise when one has been borrowed in the left hand place of the Decimal part of the Logarithm, add it to the Index of the Divisor, if affirmative; but subtract it, if negative; and let the

Index, thence arising, be changed and worked with, as before.

Example 1. Divide 558.9 by 6.48.

Log. of 558.9 = 2.747334

Log. of 6.48 = 0.811575

Quotient=86.25 = 1.935759

Example 2. Divide 15.31 by 46.75.

Log. of 15.31= 1.184975 Log. of 46.75= 1.669782

Quotient=.3275=-1.515193

Example 3. Divide .05951 by .007693,

Log. of .05951 =-2.774590

Log. of .007693=-3.886096

Quotient=7.735 = 0.888494

Example 4. Divide .6651 by 22.5.

Log. of .6651=-1.822887

Log. of 22.5 = 1.352183

Quotient=.02956=-2.470704

# PROPORTION,

Or the Rule of Three in Logarithms.

#### RULE.

Having stated the three given terms according to the rule in common Arithmetic, write them orderly under one another, with the signs of proportion; then add the Logarithms of the second and third terms together, and from their sum subtract the Logarithm of the first term, and the remainder will be the Logarithm of the fourth term, or Answer.

Or,-add together the Arithmetical Complement of the Logarithm of the first term, and the Logarithms of the second and third terms; the sum, rejecting 10 from the Index, will be the Logarithm

of the fourth term, or term required.

N. B. The Arithmetical Complement of a Logarithm is what it wants of 10,000000, or 20,000000. and the easiest way to find it is to begin at the left hand, and subtract every figure from 9, except the last, which should be taken from 10; but if the index exceed 9, it must be taken from 19 .- It is frequently used in the rule of Proportion and Trigonometrical calculations, to change Subtractions into Additions.

1st. If a clock gain 14 seconds in 5 days 18 hours, how much will it gain in 17 days 15 hours?

5.75 days : Log. = 0.759668

17.625 days :: Log.=1.246129 : Log. =1.146128 14 Seconds

2.392257

Answer=42", 91 =1.632589

Or thus; 5.75 days: Arith. Co. Log. = 9,240332

17.625 :: Log.=1.246129

14 Seconds: Log.=1.146128

=1.632589

2d. Find a fourth proportional to 9.485, 1.969 and 347.2.

98.45 : Log.=1.993216

347.2 :: Log.=2.540580 1.969 : Log.=0.294246

2.834826

Answer=6.944 = 0.841610

3d. What number will have the same proportion to .8538 as .3275 has to .0131

.0131 : Log.=--2.117271

.3275 :: Log.=—1.515211 .8538 : Log.=—1.931356

-1.446567

Answer=21.35= 1.329296

4th. Required a third proportional number to 9.642 and 4.821

9.642 : Log.=0.984167

4.821 :: Log.=0.683137 4.821 : Log.=0.683137

1.366274

Answer=2.411 =0.382107

### INVOLUTION.

To find any proposed power of a given number by Logarithms.

Rule. Multiply the Logarithm of the given number by the Index of the proposed power, and the

product will be the Logarithm, whose natural num-

ber is the power required.

When a negative Index is thus multiplied, its product is negative, but what was carried from the decimal part of the Logarithm must be allirmative; consequently the difference is the Index of the product, which difference must be considered of the same kind with the greater, or that which was made the minuend.

#### EXAMPLES.

1. What is the second power of 3.874?

Log. of 3.874=0.588160

Index = 2

Power required=15.01 =1.176320

2. Required the third power of the number 2.768. Log. of 2.768=0.442166

Log. of 2.708=0.442166 Index = 3

Answer=21.21=1.326498

3. Required the second power of the number .2857.

Log. of .2857=-1.455910 Index = 2

Answer=.08162=--2.911820

4. Required the third power of the number .7916.

Log. of .7916 = -1.898506Index = 3

Answer=.4961 --- 1.695518

### EVOLUTION.

To extract any proposed Root of a given number by Logarithms.

#### RULE.

Find the Logarithm of the given number, and divide it by the Index of the proposed root; the quotient is a Logarithm, whose natural number is

the root required.

When the index of the Logarithm to be divided, is negative, and does not exactly contain the divisor without some remainder, increase the index by such a number, as will make it exactly divisible by the index, carrying the units borrowed as so many tens to the left hand place of the decimal, and then divide as in whole numbers.

#### EXAMPLES.

1. Required the square root of 847. Index 2)2.927883=Log. of 847.

1.463941=Quot.=Log.of29.103+ = ans.

2. Required the cube root of 847. Index 3)2.927883=Log. of the given number.

0.975961=Quot.=Log.of9.462=ans.

[nearly.

3. Required the square root of .093. Index 2)—2.968483=Log. of .093.

-1.484241=Quot.=Log.of.304959= ans.

Required the cube root of 12345.
 Index 3)4.091491=Log. of 12345.

1,363830=Quot.=Log. of 23.116.= Ans.

#### SECTION IV.

#### ELEMENTS OF

### PLANE GEOMETRY.

#### DEFINITIONS.

### See PLATE I.

- 1. GEOMETRY is that science wherein we consider the properties of magnitude.
- 2. A point is that which has no parts, being of itself indivisible; as A.
- 3. A line has length but no breadth; as AB. figures 1 and 2.
- 4. The extremities of a line are points, as the extremities of the line AB are the points A and B. figures 1 and 2.
- 5. A right line is the shortest that can be drawn between any two points, as the line AB. fig. 1. but if it be not the shortest, it is then called a curve line, as AB. fig. 2.
- 6. A superficies or surface is considered only as having length and breadth, without thickness, as ABCD. fig. 3.
  - 7. The extremities of a superficies are lines.
- 8. The inclination of two lines meeting one another (provided they do not make one continued

line) or the opening between them, is called an angle. Thus in fig. 4, the inclination of the line AB to the line BC meeting each other in the point B, or the opening of the two lines BA and BC, is called an angle, as ABC.

- Note, When an angle is expressed by three letters, the middle one is that at the angular point.
- 9. When the lines that form the angle are right ones, it is then called a right-lined angle, as ABC, fig. 4. If one of them be right and the other curved, it is called a mixed-angle, as B. fig. 5. If both of them be curved it is called a curved-lined or spherical angle, as C. fig. 6.
- 10. If a right line, CD (fig. 7.) fall upon another right line, AB, so as to incline to neither side, but make the angles ADC, CDB on each side equal to each other, then those angles are called right angles, and the line CD a perpendicular.
- 11. An obtuse angle is that which is wider or greater than a right one, as the angle ADE. fig. 7. and an acute angle is less than a right one, as EDB. fig. 7.
  - 12. Acute and obtuse angles in general are called oblique angles.
  - 13. If a right line CB. (fig. 8.) be fastened at the end C, and the other end B, be carried quite round, then the space comprehended is called a circle; and the curve line described by the point B, is called the circumference or the periphery of the circle; the fixed point C, is called its centre.

- 14. The describing line CB. (fig. 8.) is called the semidiameter or radius, so is any line from the centre to the circumference; whence all radii of the same or of equal circles are equal.
- 15. The diameter of a circle is a right line drawn thro' the centre, and terminating in opposite points of the circumference; and it divides the circle and circumference into two equal parts, called semicircles; and is double the radius, as AB or DE. fig. 8.
- \*16. The circumference of every circle is supposed to be divided into 360 equal parts called degrees, and each degree into 60 equal parts called minutes, and each minute into 60 equal parts called seconds, and these into thirds, fourths, &c. these parts being greater or less as the radius is.
- 17. A chord is a right line drawn from one end of an arc or arch (that is, any part of the circumference of a circle) to the other; and is the measure of the arc. Thus the right line HG, is the measure of the arc HBG, fig. 8.
- 18. The segment of a circle is any part thereof, which is cut off by a chord: thus the space which is comprehended between the chord HG and the arc HBG, or that which is comprehended between the said chord HG and the arc HDAEG are called segments. Whence it is plaining fig. 8.
- That any chord will divide the circle into two segments.
- 2. The less the shord is, the more unequal are the acgments.

- 3. When the chord is greatest in becomes a manuter, and then the segments are equal; and each segment is a semicircle.
- 19. A sector of a circle is a part thereof less than a semicircle, which is contained between two radu and an arc: thus the space contained between the two radii CII, CB, and the arc HB is a sector, fig. 8.
- 20 The right sine of an arc, is a perpendicular bue let fall from one end thereof, to a diameter down to the other end: thus IIL is the right seed the arc IIB.

the sines on the same diameter increase till it y come to the centre, and so become the radius hence it is plain that the radius CD is the greatest possible sine, and thence is called the whole sine.

Since the whole sine CD (fig. 8.) must be perpendicular to the diameter (by def. 20.) therefore precincing DC to E the two diameters AB and DE cross one another at right angles, and thus the periphery is divided into four equal parts, as BD, DI, AE, and, EB; (by def. 10.) and so BD becomes a quadrant or the fourth part of the periphery: therefore the radius DC is always the size of a quadrant, or of the fourth part of the circle BD.

Sines are said to be of as many degrees as the are contains parts of 360; so the radius being the sine of a quadrant becomes the sine of 90 degrees, or the fourth part of the circle, which is 360 degrees.

- 21. The versed sine of an arc is that part of the diameter that lies between the right sine and the circumference: thus LB is the versed sine of the arc HB. fig. 8.
- 22. The tangent of an arc is a right line touching the periphery, being perpendicular to the end of the diameter, and is terminated by a line drawn from the centre through the other end: thus BK is the tangent of the arc HB. fig. 8.
- 23. And the line which terminates the tangent, that is, CK, is called the secant of the are HB. fig. 8.
- 24. What an arc wants of a quadrant is called the complement thereot: Thus DH is the complement of the arc HB. fig. 8.
- 25. And what an arc wants of a semicircle is called the supplement thereof: thus AH is the supplement of the arc HB. fig. 8.
- 26. The sine, tangent, or secant of the complement of any arc, is called the co-sine, co tangent, or co-secant of the arc itself: thus FH is the sine, DI the tangent, and CI the secant of the arc DH: or they are the co-sine, co-tangent, or co-secant of the arc HB. fig. 8.
- 27. The sine of the supplement of an arc, is the same with the sine of the arc itself; for drawing them according to del. 20, there results the self-same line; thus HL is the sine of the arc HB, or of its supplement ADH. fig. 8.
- 28. The measure of a right-lined angle, is the arc of a circle swept from the angular point, and

contained between the two lines that form the angle: thus the angle HCB (fig. 8.) is measured by the arc HB, and is said to contain so many degrees as the arc HB does; so if the arc HB is 60 degrees, the angle HCB is an angle of 60 degrees.

Hence angles are greater or less according as the arc described about the angular point, and terminated by the two sides, contains a greater or less number of degrees of the whole circle.

- 29. The sine, tangent, and secant of an arc, is also the sine, tangent, and secant of an angle whose measure the arc is: thus because the arc HB is the measure of the angle HCB, and since HL is the sine, BK the tangent, and CK the secant, BL the versed sine, HF the co-sine, DI the co-tangent, and CI the co-secant, &c. of the arc BH; then HL is called the sine, BK the tangent, CK the secant, &c. of the angle HCB, whose measure is the arc HB. fig. 8.
- 30. Parallel lines are such as are equi-distant from each other, as AB, CD. fig. 9.
- 31. A figure is a space bounded by a line or lines. If the lines be right it is called a rectilineal figure, if curved it is called a curvilineal figure; but if they be partly right and partly curved lines, it is called a mixed figure.
- 32. The most simple rectilineal figure is a triangle, being composed of three right lines, and is considered in a double capacity; 1st, with respect to its sides; and 2d, to its angles.
- 33. In respect to its sides it is either equilateral, having the three sides equal, as A, fig. 10.

- 34. Or isosceles, having two equal sides, as B. fig. 11.
- 35. Or scalene, having the three sides unequal. as C. fig. 12.
- 36. In respect to its angles, it is either rightangled, having one right angle, as D. fig. 13.
- Or obtuse angled, having one obtuse angle, as E. fig. 14.
- 38. Or acute angled, having all the angles acute, as F. fig. 15.
- S9. Acute and obtuse angled triangles are in general called oblique angled triangles, in all which any side may be called the base, and the other two the sides.
- 40. The perpendicular height of a triangle is a line drawn from the vertex to the base perpendicularly: thus if the triangle ABC, be proposed, and BC be made its base, then if from the vertex A the perpendicular AD be drawn to BC, the line AD will be the height of the triangle ABC, standing on BC as its base. Fig. 16.

Hence all triangles between the same parallels have the same height, since all the perpendiculars are equal from the nature of parallels.

- Any figure of four sides is called a quadrilateral figure.
- 42. Quadrilateral figures, whose opposite sides are parallel, are called parallelograms: thus

ABCD is a parallelogram. Fig. 3. 17, and AB fig. 18 and 19.

- 43. A parallelogram whose sides are all equal and angles right, is called a square, as ABCD. fig. 17.
- 44. A parallelogram whose opposite sides are equal and angles right, is called a rectangle, or an oblong, as ABCD. fig. 3.
- 45. A rhombus is a parallelogram of equal sides, and has its angles oblique, as A fig. 18. and is an inclined square.
- 46. A rhomboides is a parallelogram whose opposite sides are equal and angles oblique; as B. fig. 19. and may be conceived as an inclined rectangle.
- 47. Any quadrilateral figure that is not a parallelogram, is called a trapezium. Plate 7. fig. 3.
- 48. Figures which consist of more than four sides are called polygons; if the sides are all equal to each other, they are called regular polygons. They sometimes are named from the number of their sides, as a five-sided figure is called a pentagon, one of six sides a hexagon, &c. but if their sides are not equal to each other, then they are called irregular polygons, as an irregular pentagon, hexagon, &c.
- 49. Four quantities are said to be in proportion when the product of the extremes is equal to that of the means: thus if A multiplied by D, be equal to B multiplied by C, then A is said to be to B as C is to D.

### POSTULATES OR PETITIONS.

- 1. That a right line may be drawn from any one given point to another.
- 2. That a right line may be produced or continued at pleasure.
- 3. That from any centre and with any radius, the circumference of a circle may be d scribed.
- 4. It is also required that the equality of lines and angles to others given, be granted as possible: that it is possible for one right line to be perpendicular to another, at a given point or distance; and that every magnitude has its half, third, fourth, &c. part.

Note, Though these postulates are not always quoted the reader will easily perceive where, and in what sense they are to be understood.

# AXIOMS or self-evident TRUTIIS.

- 1. Things that are equal to one and the same thing, are equal to each other.
  - 2. Every whole is greater than its part.
- 3. Every whole is equal to all its parts taken together.
- 4. If to equal things, equal things be added, the whole will be equal.
- 5. If from equal things, equal things be deducted the remainders will be equal

- 6. If to or from unequal things, equal things be added or taken, the sums or remainders will be unequal.
  - 7. All right angles are equal to one another.
- 8. If two right lines not parallel, be produced towards their nearest distance, they will intersect each other.
- 9. Things which mutually agree with each other, are equal.

### NOTES.

A theorem is a proposition, wherein something is proposed to be demonstrated.

A problem is a proposition, wherein something is to be done or effected.

A lemma is some demonstration, previous and necessary, to render what follows the more easy.

A corollary is a consequent truth, deduced from a foregoing demonstration.

 $\Lambda$  scholium, is a remark or observation made upon something going before.

### GEOMETRICAL THEOREMS.

#### THEOREM I.

PL. 1, fig. 20.

IF a right line falls on another, as AB, or EB, does on CD, it either makes with it two right angles, or two angles equal to two right angles.

- 1. If AB be perpendicular to CD, then (by def. 10.) the angles CBA, and ABD, will be each a right angle.
- 2. But if EB fall slantwise on CD, then are the angles DBE + EBC = DBE + EBA (= DBA) + ABC, or two right angles. 2. E. D.

Corollary 1. Whence if any numbers of right lines were drawn from one point, on the same side of a right line; all the angles made by these lines will be equal to two right lines.

2. And all the angles which can be made about a point, will be equal to four right angles.

#### THEO. 11.

### PL. 1. fig. 21.

If one right line cross another, (as AC does BD) the opposite angles made by those lines, will be equal to each other: that is, AEB to CED and BEC to AED.

By theorem 1. BEC + CED = 2 right angles. and CED + DEA = 2 right angles.

Therefore (by axiom 1.) BEC+CED=CED+

DEA: take CED from both, and there remains BEC = DEA. (by axiom 5.) 2. E. D.

After the same manner CED + AED = 2 right angles; and AED + AEB—two right angles; wherefore taking AED from both, there remains CED = AEB. 2. E. D.

#### THEO. III.

#### PL. 1. feg. 22.

If a right line cross two furallels, as GH does AB and CD. then,

- 1. Their external angles are equal to each other, that is, GEB = CFH.
- 2. The alternate angles will be equal, that is, AEF = EFD and BEF = CFE.
- 3. The external angle will be equal to the internet and opposite one on the same side, that is, GEB = EFD and AEG = CFE.
- 4. And the sum of the internal angles on the same side, are equal to two right angles; that is, BEF+DFE are equal to two right angles, and AEF+CFE are equal to two right angles.
- 1. Since AB is parallel to CD, they may be considered as one broad line, crossed by another line, as GII; (then by the last theo.) GEB=CFH, and AEG=IIFD.
- 2. Also GEB = AEF, and CFH = EFD; but GEB = CFH (by part 1. of this theo.) therefore AEF = EFD. The same way we prove FEB = EFC.
- 3. AEF = EFD; (by the last part of this theo.) but AEF = GEB (by theo. 2.) Therefore GEB = EFD. The same way we prove AEG = CFE.

4. For since GEB = EFD, to both add FEB, then (by axiom 4.) GEB + FEB = EFD + FEB, but GEB + FEB, are equal to two right angles (by theo. 1.) Therefore EFD + FEB are equal to two right angles: after the same manner we prove that AEF + CFE are equal to two right angles.  $\mathfrak{L}. E. D.$ 

#### THEO. IV.

### PL. 1. fig. 23.

In any triangle ABC, one of its legs, as BC, being produccd towards D, it will make the external angle ACD equal to the two internal opposite angles taken together. Viz. to B and A.

Through C, let CE be drawn parallel to AB; then since BD cuts the two parallel lines BA, CE; the angle ECD = B, (by part 3. of the last theo.) and again, since AC cuts the same parallels, the angle ACE = A (by part 2. of the last.) Therefore ECD + ACE = ACD = B + A. 2. E. D.

#### THEO. V.

### PL. 1. fig. 23.

In any triangle ABC, all the three angles, taken together, are equal to two right angles, viz. A+B+ACB=2 right angles.

Produce CB to any distance, as D, then (by the last) ACD=B+A; to both add ACB; then ACD+ACB=2 right angles (by theo. 1.); therefore the three angles A+B+ACB=2 right angles. Q. E. D.

Cor. 1. Hence if one angle of a triangle be known, the sum of the other two is also known: for since the three angles of every triangle contain two right ones, or 180 degrees, therefore 180

—the given angle will be equal to the sum of the other two; or 180—the sum of two given angles, gives the other one.

Cor. 2. In every right-angled triangle, the two acute angles are = 90 degrees, or to one right angle: therefore 90—one acute angle, gives the other.

#### THEO. VI.

#### PL. 1. fig. 24.

If in any two triangles, ABC, DEF, there be two sides, AB, AC in the one, severally equal to DE, DF in the other, and the angle A contained between the two sides in the one, equal to D in the other; then the remaining angles of the one, will be severally equal to those of the other, viz. B=E and C=F; and the base of the one BC, will be equal to EF, that of the other.

If the triangle ABC be supposed to be laid on the triangle DEF, so as to make the points A and B coincide with D and E, which they will do, because AB = DE (by the hypothesis); and since the angle A = D, the line AC will fall along DF, and inasmuch as they are supposed equal, C will fall in F; seeing therefore the three points of one coincide with those of the other triangle, they are manifestly equal to each other; therefore the angle B = E and C = F, and BC = EF. AC.

#### LEMMA.

#### PL. 1. fig. 11.

If two sides of a triangle a b c be equal to each other, that is, ac=cb the angles which are officiate to those equal sides, will also be equal to each other; viz. a=b.

For let the triangle abc be divided into two

triangles a c d, d c b, by making the angle a c d = d c b (by postulate 4) then because a c = b c, and cd common, (by the last) the triangle a d c = d c b; and therefore the angle a = b. 2. E. D.

Cor. Hence if from any point in a perpendicular which bisects a given line, there be drawn right lines to the extremities of the given one, they with it will form an isosceles triangle.

#### THEO. VII.

#### PL. 1. fig. 25.

The angle BCD at the centre of a circle ABED, is double she angle BAD at the circumference, standing upon the same arc BED.

Through the point A, and the centre C, draw the line ACE: then the angle ECD=CAD, +CDA; (by theo 4.) but since AC=CD being radii of the same circle, it is plain (by the preceding lemma) that the angles subtended by them will be also equal, and that their sum is double to either of them, that is, DAC+ADC is double to CAD, and therefore ECD is double to CAD; after the same manner BCE, is double to CAB, wherefore, BCE+ECD, or BCD is double to BAC+CAD or to BAD. Q, E, D.

Cor. 1. Hence an angle at the circumference is measured by half the arc it subtends or stands on.

### Fig. 26.

Cor. 2. Hence all angles at the circumference of a circle which stands on the same chord as AB, are equal to each other, for they are all measured by half the arc they stand on, viz. by half the arc AB.

### Fig. 26.

Cor. 3. Hence an angle in a segment greater than a semicircle is less than a right angle; thus ADB is measured by half the arc AB, but as the arc AB is less than a semicircle, therefore half the arc AB, or the angle ADB is less than half a semicircle, and consequently less than a right angle.

### Fig. 27.

Cor. 4. An angle in a segment less than a semicircle, is greater than a right angle, for since the arc AEC is greater than a semicircle, its half, which is the measure of the angle ABC, must be greater than half a semicircle, that is, greater than a right angle.

### Fig. 28.

Cor. 5. An angle in a semicircle is a right angle, for the measure of the angle ABD, is half of a semicircle AED, and therefore a right angle.

### THEO. VIII.

#### PL. 1. fig. 29.

If from the centre C of a circle ABE, there be let fall the perpendicular CD on the chord AB, it will bisect it in the point D.

Let the lines AC and CB be drawn from the centre to the extremities of the chord, then since CA=CB, the angles CAB=CBA (by the lemma.) But the triangles ADC, BDC are right angled ones, since the line CD is a perpendicular; and so the angle ACD=DCB; (by cor. 2. theo. 5.) then have we AC, CD, and the angle ACD in one triangle; severally equal to CB, CD, and the angle

**BCD** in the other: therefore (by theo. 6.) A = DB. 2. E. D.

Cor. Hence it follows, that any line bisecting a chord at right angles, is a diameter; for a line drawn from the centre perpendicular to a chord, bisects that chord at right angles; therefore, conversely, a line bisecting a chord at right angles must pass through the centre, and consequently be a diameter.

#### THEO. IX.

### PL. 1. fig. 29.

If from the centre of a circle ABE there be drawn a perpendicular CD on the chord AB, and produced till it meets the circle in F, that line CF, will bisect the arc AB in the point F.

Let the lines AF and BF be drawn, then in the triangles ADF, BDF; AD = BD (by the last;) DF is common, and the angle ADF = BDF being both right, for CD or DF is a perpendicular. Therefore (by theo. 6.) AF = FB; but in the same circle, equal lines are chords of equal arcs, since they measure them (by def. 19.): whence the arc AF = FB, and so AFB is bisected in F, by the line CF.

Cor. Hence the sine of an arc is half the chord of twice that arc. For AD is the sine of the arc AF, (by def. 92.) AF is half the arc, and AD half the chord AB (by theo. 8.) therefore the corollary is plain.

### THEO. X.

#### PL. 1. fig. 30.

In any triangle ABD, the half of each side is the sine of the sphosite angle.

Let the circle ADB be drawn through the points A, B, D; then the angle DAB is measured by half the arc BKD, (by cor. 1. theo. 7.) viz. the chord of BK is the measure of the angle BAD; therefore (by cor. to the last) BE the half of BD is the sine of BAD: the same way may be proved that half of AD is the sine of ABD, and the half of AB the sine of ADB. AB.

#### THEO. XI.

### PL. 1. fig. 22.

If a right line GH cut two other right lines AB, CD, so as to make the alternate angles AEF, EFD equal to each other, then the lines AB and CD will be parallel.

If it be denied that AB is parallel to CD, let IK be parallel to it; then IEF=(EFD)=AEF by par 2 theo. 3.) a greater to a less, which is absurd, whence IK is not parallel; and the like we can prove of all other lines but AB; therefore AB is parallel to CD. 2. E. D.

#### THEO. XII.

#### PL. 1. fig. 3.

If two equal and parallel lines AB, CD, be joined by two other lines AD, BC, those shall be also equal and parallel.

Let the diameter or diagonal BD be drawn, and we will have the triangles ABD, CBD: whereof AB in one is=to CD in the other. BD common to both, and the angle ABD=CDB (by part 2. theo. 3. ;) therefore (by theo. 6.) AD=CB, and the angle CBD=ADB, and thence the lines AD and BC are parallel, by the preceding theorem.

Cor. 1. Hence the quadrilateral figure ABCD is a parallelogram, and the diagonal BD bisects the

same, inasmuch as the triangle ABD=BCD, as now proved.

- Cor. 2. Hence also the triangle ABD on the same base AB, and between the same parallels with the parallelogram ABCD, is half the parallelogram.
- Cor. 3. It is hence also plain, that the opposite sides of a parallelogram are equal; for it has been proved that ABCD being a parallelogram. AB will be=CD and AD=BC.

### THEO. XIII.

### PL. 1. fig. 31.

All parallelograms on the same or equal bases and between the same parallels, are equal to one another, that is, if BD=GH, and the lines BH and AF parallel, then the parallelogram ABDC=BDFE=EFHG.

For AC=BD=EF (by cor. the last;) to both add CE then AE=CF. In the triangles ABE, CDF; AB=CD and AE=CF and the angle BAE = DCF (by part 3. theo. 3.;) therefore the triangle ABE = CDF, (by theo. 6.) let the triangle CKE be taken from both. and we will have the trapezium ABKC=KDFE; to each of these add the triangle BKD, then the parallelogram ABCD = BDEF; in like manner we may prove the parallelogram EFGH=B!DEF. Wherefore ABDC=BDEF=EFHG. 2. E. D.

Cor. Hence it is plain that triangles on the same or equal bases, and between the same parallels, are equal, seeing (by cor. 2. theo. 12.) they are the halves of their respective parallelogram.

#### THEO. XIV.

### PL. 1. fig. 32.

In every right-angled triangle, ABC, the square of the hypotheruse or longest side, BC, or BCMH, is equal to the sum of the squares made on the other two sides AB and AC, that is, ABDE and ACGF.

Through A draw AKL perpendicular to the hypothenuse BC, join AH, AM, DC and BG; in the triangles, BDC, ABH, BD=BA, being sides of the same square, and also BC=BH, and the included angles DBC=ABH, (for DBA=CBH being both right, to both add ABC, then DBC=ABH) therefore the triangle DBC=ABH (by theo. 6.) but the triangle DBC is half of the square ABDE (by cor. 2. theo. 12.) and the triangle ABH is half the parallelogram BKLH. The same way it may be proved, that the square ACGF, is equal to the parallelogram KCLM. So ABDE + ACGF the sum of the squares=BKLH+KCML, the sum of the two parallelograms or square BCMH; therefore the sum of the squares on AB and AC is equal to the square on BC. 2. E. D.

Cor. 1. Hence the hypothenuse of a right-angled triangle may he found by having the sides; thus, the square root of the sum of the squares of the base and perpendicular, will be the hypothenuse.

Cor. 2. Having the hypothenuse and one side given to find the other; the square root of the difference of the squares of the hypothenuse and given side, will be the required side.

#### THEO. XV .

# Pt. 1. fig. 33.

In all circles the chord of 60 degrees is always equal in tength to the radius.

Thus in the circle AEBO, if the arc AEB be an are of 60 degrees, and the chord AB be drawn; then AB=CB=AC.

In the triangle ABC, the angle ACB is 60 degrees, being measured by the arc AEB; therefore the sum of the other two angles is 120 degrees (by Cor. 1. theo. 5.) but since AC=CB, the angle CAB=CBA (by lemma preceding theo. 7.) consequently each of them will be 60, the half of 120 degrees, and the three angles will be equal to one another, as well as the three sides: wherefore AB=BC=AC. 2. E. D.

Cor. Hence the radius, from whence the lines on any scale are formed, is the chord of 60 degrees on the line of chords

# THEO. XVI.

### PL. 1. fig. 34.

If in two triangles ABC, abc, all the angles of one be each respectively equal to all the angles of the other, that is, A=a, B=b, C=c: then the sides opposite to the equal angles will be proportional, viz.

AB: ab:: AC: ac
AB: ab:: BC: bc
and AC: ac:: BC: bc

For the triangles being inscribed in two circles, it is plain since the angle A=a, the arc BDC= bdc, and consequently the chord BC is to bc, as the radius of the circle ABC is to the radius of the circle abc; (for the greater the radius is, the greater is the circle described by that radius; and consequently the greater any particular arc of that circle is, so the chord, sine, tangent, &c of that arc will be also greater. Therefore, in general, the chord, sine, tangent, &c. of any arc is proportional to the radius of the circle;) the same way the chord

AB is to the chord ab, in the same proportion. So AB:ab::BC:bc; the same way the rest may be proved to be proportional.

#### THEO, XVII.

### PL. 1. fig. 35.

If from a point A without a circle DBCE there be drawn two lines ADE, ABC, each of them cutting the circle in two points; the product of one whole line into its external part viz. AC into AB, will be equal to that of the other line intoits external part, viz. AE into AD.

Let the lines DC, BE, be drawn in the two triangles ABE, ADC; the angle AEB=ACD (by cor. 2, theo. 7.) the angle A is common, and (by cor. 1, theo. 5.) the angle ADC=ABE; therefore the triangles ABE, ADC, are mutually equiangular, and consequently (by the last) AC: AE: AD: AB; wherefore AC multiplied by AB, will be equal to AE multiplied by AD. 2. E. D.

#### THEO. XVIII.

## PL. 2. fig. 1.

Triangles ABC, BCD, and parallelograms ABCF and BDEC, having the same altitude, have the same proportion between themselves as their bases BA and BD.

Let any aliquot part of AB be taken, which will also measure BD: suppose that to be Ag, which will be contained twice in AB, and three times in BD, the parts Ag, gB, Bh, hi, and iD being all equal, and let the lines gC, hC, and iC, be drawn: then (by cor. to theo. 13.) all the small triangles AgC, gCB, BCh, &c. will be equal to each other; and will be as many as the parts into which their bases were divided; therefore it will be as the sum of the parts in one base, is to the sum of those in

the other, so will be the sum of the small triangles in the first, to the sum of the small triangles in the second triangle; that is, AB:BD:ABC:BDC.

Whence also the parallelograms ABCF and BDEC, being (by cor. 2. theo. 12.) the doubles of the triangles, are likewise as their bases. 2. E. D.

Note. Wherever there are several quantities connected with the sign (: :) the conclusion is always drawn from the first two and last two proportionals.

### THEO. XIX.

### PL. 2. fig. 2.

Triangles ABC, DEF, standing whon equal bases AB and DE, are to each other as their altitudes CG and FH.

Let BI be perpendicular to AB and equal to CG, in which let KB = FH, and let AI and AK be drawn.

The triangle AIB = ACB (by cor. to theo. 13.) and AKB = DEF; but (by theo. 18.) BI: BK:: ABI: ABK. That is, CG: FH:: ABC: DEF. 2. E. D.

# THEO. XX.

### PL. 2. fig. 3.

If a right line BE be drawn parallel to one side of a triangle ACD, it will cut the two other sides proportionally, viz. AB: BC: : AE: ED.

Draw CE and BD; the triangles BEC and EBD being on the same base BE and under the same parallel CD, will be equal (by cor. to theo. 13.)

therefore (by theo. 18) AB:BC::(BEA:BEC or BEA:BED)::AE:ED. 2. E. D.

Cor. 1. Hence also AC: AB:: AD: AE:For AC: AB:: (AEC: AEB:: ABD: AEB):: AD: AE.

Cor. 2. It also appears that a right line, which divides two sides of a triangle proportionally, must be parallel to the remaining side.

Cor. 3. Hence also, theo. 16. is manifest; since the sides of the triangles *ABE*, *ACD*, being equiangular, are proportional.

### THEO. XXI.

### PL. 2. fig. 4.

If two triangles ABC, ADE, have an angle BAC, in the one, equal to an angle DAE, in the other, and the sides about the equal angles, proportional; that is, AB: AD: AC: AE; then the triangles will be mutually equiangular.

In AB take Ad = AD, and let de be parallel to BC, meeting AC in e.

Because (by the first cor. to the foregoing theo.) AB:Ad (or AD): AC:Ae, and (by the hypothesis, or what is given in the theorem) AB:AD:AC:AE; therefore Ae=AE seeing AC bears the same proportion to each; and (by theo. 6.) the triangle Ade=ADE, therefore the angle Ade=D and Aed=E, but since ed and BC are parallel (by part 3 theo. 3) Ade=B, and Aed=C, therefore B=D and C=E, QED.

#### THEO. XXII.

PL. 2. fig. 5.

Equiangular triangles ABC, DEF, are to one another in

a duplicate proportion of their homologous or like sides; or as the squares AK, and DM of their homologous sides.

Let the perpendiculars CG and FH be drawn as well as the diagonals BI and EL.

The perpendiculars make the triangles ACG and DFH equiangular, and therefore similar (by theo. 16.) for because the angle CAG=FDH and the right angel AGC=DHF, the remaining angle ACG=DFH, (by cor. 2. theo. 5.)

Therefore GC: FH:: (AC: DF::)AB: DE, or which is the same thing, GC: AB:: FH: DE for FH multiplied by AB = AB multiplied by FH.

By theo. 19. ABC: ABI:: (CG: AI or AB as before:: FH DE or DL::) DFE: DLE, therefore ABC: ABI:: DFE: DLE, or ABC: AK:: DFE: DM, for AK is double the triangle ABI, and DM double the triangle DEL, by cor. 2. theo. 12. Q. E. D.

### THEO. XXIII.

### PL. 2. Fix. 6.

Like polygons ABCDE, a b c d e, are in a duplicate proportion to that of the sides AB, a b, which are between the equal angles A and B and a and b, or us the squares of the sides AB, ab.

# Draw AD, AC, ad, ac.

By the hypothesis AB:ab::BC:bc, and thereby also the angle B=b; therefore (by theo. 21.) BAC=b a c; and ACB=a c b: in like manner EAD=e a d, and EDA=e d d. If therefore from the equal angles A, and a, we take the equal ones.

EAD+BAC=c a d, + b a c the remaining angle DAC=d a c, and if from the equal angles D and d, EDA=c d a, be taken, we shall have ADC=a d c: and in like manner if from C and c be taken BCA=b c a, we shall have ACD=a c d; and so the respective angles in every triangle, will be equal to those in the other.

By theo. 22. ABC: abc: the square of AC to the square of ac, and also ADC: adc: the square of AC, to the square of a c; therefore from equality of proportions ABC: abc: ADC: a dc: in like manner we may shew that ADC: a dc: EAD: e a d: Therefore it will be as one antecedent is to one consequent, so are all the antecedents to all the consequents. That is, ABC is to abc as the sum of the three triangles in the first polygon, is to the sum of those in the last. Or ABC will be to abc, as polygon to polygon.

The proportion of ABC to abc (by the foregoing theo.) is as the square of AB is to the square of ab, but the proportion of polygon to polygon, is as ABC to abc, as now shown: therefore the proportion of polygon to polygon is as the square of AB to the square of ab.

## THEO. XXIV .

# PL. 1. fig. 8.

Let DHB be a quadrant of a circle described by the radius CB; HB an arc of it, and DH its complement; HL or FC the sine, FH or CL its co-sine, BK its tangent, DI its cotangent; CK its secant, and CI its co-secant. Fig. 8.

1. The co-sine of an arc is to the sine, as the radius is to the tangent.

- 2. The radius is to the tangent of an arc, as the co-sine of it is to the sine.
- 3. The sine of an arc is to its co-sine, as the raclius to its co-tangent;
- 4. Or the radius is to the co-tangent of an arc, as its sine to its co-sine.
- 5. The co-tangent of an arc is to the radius, as the radius to the tangent.
- 6. The co-sine of an arc is to the radius, as the radius is to the secant.
- 7. The sine of an arc is to the radius, as the tangent is to the secant.

The triangles CLH and CBK, being similar, (by theo. 16.)

- 1. CL: LH: : CB : BK.
- 2. Or, CB: BK: :CL: LH.

The triangles CFH and CDI, being similar.

- 3. CF (or LH): FH:: CD: DI.
- 4. CD:DI::CF (or LH): FH.

The triangles CDI and CBK are similar: for the angle  $CI(\cdot) = KCB$ , being alternate ones (by part 2, theo. 3.) the lines CB and DI being parallel: the angle CDI = CBK being both right, and consequently the angle DCI = CKB, where one,

5. DI: CD:: CB: BK.

And again, making use of the similar triangle CLH and CBK.

6. CL : CB :: CH : CK.

7. HL: CH: BK: CK.

# GEOMETRICAL PROBLEMS.

PROB. I.

Pt. 2. fig. 7.

To make a triangle of three given right lines BO, LB, LO, of which any two must be greater than the third.

Lay BL from B to L; from B with the line BO, describe an arc, and from L with LO describe another arc; from O, the interesting point of those arcs, draw BO and OL, and BOL is the triangle required.

This is manifest from the construction.

PROB. II.

PL. 2. fig. 8.

At a point B in a given right line BC, to make an angle equal to a given angle A.

Draw any right line ED to form a triangle, as EAD, take BF = AD, and upon BF make the triangle BFG, whose side BG = AE, and GF = ED (by the last) then also the angle B = A; if we suppose one triangle be laid on the other, the sides

will mutually agree with each other, and therefore be equal; for if we consider these two triangles to be made of the same three given lines, they are manifestiy one and the same triangle.

Otherwise.

Upon the centres A and B, at any distance, let two arcs, DE,  $FG_2$  be described; make the arc FG=DE, and through B and G draw the line BG, and it is done.

For since the chords ED, GF, are equal, the angles A and B are also equal, as before (by def. 17.)

PROB. III.

P1. 2. fig. 9.

To bisect or divide into two equal parts, any given rightlined angle, BAC.

In the lines AB and AC, from the point A set off equal distances  $AE_{r}=AD$ , then, with any distance more than the half of  $DE_{r}$ , describe two ares to cut each other in some point  $F_{r}$ ; and the rightline  $AF_{r}$ , joining the points A and  $F_{r}$ , will bisect the given angle  $BAC_{r}$ .

For if DF and FE be drawn, the triangles ADF, AEF, are equilateral to each other viz. AD = AE, DF = FE, and AF common, wherefore DAF = EAF, as before.

PROB. IV.

Ps. 2. fig. 10.

To bisect a right-line. AB.

With any distance, more than half the line, from

A and B, describe two circles CFD, CGD, cutting each other in the points C and D; draw CD intersecting AB in E, then AE=EB.

For, if AC, AD, BC, BD, be drawn, the triangles ACD, BCD, will be mutually equilateral, and consequently the angle ACE=BCE: therefore the triangle ACE, BCE, having AC=BC, CE common, and the angle ACE=BCE; (by theo. 6.) the base AE the base BE.

Cor. Hence it is manifest, that CD not only bisects AB, but is perpendicular to it. (by def. 11.)

#### PROB. V.

### PL. 2. fig. 11.

On a given froint A, in a right line EF, to erect a perpendicular.

From the point A lay off on each side, the equal distances, AC, AD; and from C and D, as centres, with any interval greater than AC or AD, describe two arcs intersecting each other in B; from A to B draw the line AB, and it will be the perpendicular required.

For, let CB, and BD be drawn; then the triangles CAB, DAB, will be mutually equilateral and equiangular, so CAB = DAB, a right angle, (by def. 10.)

#### PROB. VI.

### PL. 2. fig. 12.

To raise a perpendicular on the end B of a right line AB.

From any point D not in the line AB, with the distance from D to B, let a circle be described cut-

ting AB in E; draw from E through D the right line EDC, cutting the periphery in C, and join CB; and that is the perpendicular required.

**EBC** being a semicircle, the angle **EBC** will be a right angle (by cor. 5. theo. 7.)

PROB. VII.

PL. 2. fig. 13.

From a given point A, to let fall a perpendicular upon a given right line BC.

From any point D, in the given line, take the distance to the given point A, and with it describe a circle AGE, make GE = AG, join the points A and E, by the line AFE, and AF will be the perpendicular required.

Let DA, DE, be drawn; the angle ADF = FDE, DA = DE, being radii of the same circle, and DF common; therefore (by theo. 6.) the angle DFA = DFE, and FA a perpendicular. (By def. 10.)

PROB. VIII.

PL. 2. fig. 14.

Through a given point A, to draw a right line AB, parallel to a given right line CD.

From the point A, to any point F, in the line CD, draw the line AF, with the interval FA, and one foot of the compasses in F, describe the arc AE, and with the like interval and one foot in A, describe the arc BF, making BF = AE; through A and B draw the line AB, and it will be parallel to CD.

By prob. 2. The angle BAF = AFE, and by theo. 11. BA and CD are parallel.

PROB. IX.

PL. 1. fig. 17.

Upon a given line AB to describe a square ABCD.

Make BC perpendicular and equal to AB; and from A and C, with the line AB, or BC, let two arcs be described, cutting each other in D; from whence to A and C, let the lines AD, DC be drawn; so is ABCD the square required.

For all the sides are equal by construction; therefore the triangles ADC and BAC, are mutually equilateral and equiangular, and ABCD is an equilateral parallelogram, whose angles are right. For B being right, D is also right, and DAC, DCA, BAC, ACB, each half a right angle (by lemma preceding theo. 7. and cor 2. theo 5.) whence DAB and BCD will each be a right angle, and (by def. 44.) ABCD is a square.

#### SCHOLITIM.

By the same method a rectangle or oblong, may be described, the sides thereof being given.

· PROB. X.

PL. 2. fig. 15.

To divide a given right line AB, into any proposed number of equal parts.

Draw the indefinite right line AP, making any angle with AB, also draw BQ parallel to AP, in

each of which, let there be taken as many equal parts AM, MN, &c. Bo, on, &c. as you would have AB divided into; then draw Mm, Nn, &c. intersecting AB in E, F, &c. and it is done.

For MN and mn being equal and parallel, FN will be parallel to EM; and in the same manner, GO to FN (by theo. 12.) therefore AM, MN, NO, being all equal by construction, it is plain (from theo. 10.) that AE, EF, FG, &c. will likewise be equal.

#### PROB. XI.

PL. 2. fig. 16.

To find a third proportional to two given right lines, A and B.

Draw two indefinite blank lines CE, CD, anywise to make any angle. Lay the line A, from C to F; and the line B, from C, to G; and draw the line FG; lay again the line A, from C to H; and through H, draw HI parallel to FG (by prob. 8.) so is CI the third proportional required.

For by cor. 1. theo. 20, CG: CH: CF: CI.

 $\mathbf{Or}, B:A:A:CI.$ 

PROB. XII.

PL. 2. fig. 17.

Three right lines A, B, C, given to find a fourth propertional.

Having made an angle DEF anywise, by two indefinite blank right lines, ED, EF, as before; lay the line A, from E to G; the line B, from E to I; and draw the line IG; lay the line C, from E to

H, and (by prob. 8.) draw HK parallel thereto, so will EK be the fourth proportional required.

For, by cor. 1. theo. 20. EG : EI : :EH : EK.

Or, A:B:C:EK

PROB. XIII.

PL. 3. fig. 1.

Two right lines, A and B, given to find a mean propertional.

Draw an indefinite blank line, as AF, on which lay the line A, from A to B, and the line B, from B to C, on the point B, which is the joining point of the lines A and B; erect a perpendicular BD (by prob. 5.) bisect AC in E (by prob. 4.) and describe the semicircle ADC; and from the point D, where the periphery cuts the perpendicular BD, d aw the line BD, and that will be the mean proportional required.

For if the lines AD, DC, be drawn, the angle ADC is a right angle (by cor. 5. theo. 7.) being an angle in a semicircle.

The angles ABD, DBC, are right ones (by def. 10.) the line BD being a perpendicular; wherefore the triangles ABD, DBC, are similar, thus the angle ABD=DBC, being both right, the angle DAC is the complement of BDA to a right angle (by cor. 2. theo. 5.) and is therefore equal to BDC, the angle ADC being a right angle as before; consequently (by cor. 1. theo. 5.) the angle ADB=DCB, wherefore (by theo. 16.)

AB:BD::BD:BC.Or, A:BD::BD:B

#### PROB. XIV.

### PL. 3. fig. 2.

To divide a right line AB, in the point E, so that AE shall have the same proportion to EB, as two given lines C and D have.

Draw an indefinite blank line, AF, to the extremity of the line AB, to make with it any angle; lay the line C, from A to C; and D, from C to D; and join the points B and D by the line BD; through C draw CE parallel to BD (by prob. 8.) so is E the point of division.

For, by cor. 1. theo. 90. AC : AD : : AE : AB. Or, C : D : : AE : EB.

### PROB. XV.

# P1. S. fig. 3.

To describe a circle about a triangle ABC, or (which is the same thing) through any three points, A, B, C, which are not situated in a right line.

By prob. 4. Bisect the line AC by the perpendicular DE, and also CB, by the perpendicular FG, the point of intersection H, of these perpendiculars, is the centre of the circle required, from which take the distance to any of the three points A, B, C, and describe the circle ABC, and it is done.

For, by cor. to theo. 8. The lines DE and FG, must each pass through the centre, therefore, their point of intersection H, must be the centre.

#### SCHOLIUM.

By this method the centre of a circle may be found, by having only a segment of it given.

#### PROB. XVI.

## PL. 3. fig. 4.

To make an angle of any number of degrees, at the foint A, of the line AB, suppose of 45 degrees.

From a scale of chords take 60 degrees, for 60° is equal to the radius (by cor. theo. 15) and with that distance from A, as a centre, describe a circle from the line AB; take 45 degrees, the quantity of the given angle, from the same scale of chords, and lay it on that circle from a to b, through A and b, draw the line AbC; and the angle A will be an angle of 45 degrees, as required.

If the given angle be more than 900, take its half (or divide it into any two parts less than 90) and lay them after each other on the arc, which is described with the chord of 60 degrees; through the extremity of which, and the centre, let a line be drawn, and that will form the angle required, with the given line.

#### PROB. XVII.

# PL. 3. fig. 5.

#### To measure a given angle, ABC.

If the lines which include the angle, be not as long as the chord of 60° on your scale, produce them to that or a greater length, and between them so produced, with the chord of 60° from B, describe the arc e d; which distance e d, measured on the same line of chords, gives the quantity of the angle BAC, as required; this is plain from def. 17

### PROB. XVIII.

### PL. 3. fig. 6.

To make a triangle BCE equal to a given quadrilateral figure ABCD.

Draw the diagonal AC, and parallel to it (by prob. 8.) DE, meeting AB produced in E; then draw CE, and ECB will be the triangle required.

For the triangles ADC, AEC, being upon the same base AC, and under the same parallel ED, (by cor. to theo. 13.) will be equal, therefore if ABC be added to each, then ABCD = BEC.

### PROB. XIX.

### PL. 3. fig. 7.

To make a triangle DFH, equal to a given five-sided figure ABCDE.

Draw DA and DB, and also EH and CF, parallel to them (by prob. 8.) meeting AB produced in :H and F; then draw DH, DF, and the triangle HDF is the one required.

For the triangle DEA = DHA, and DBC = DFB (by cor. to then. 13.) therefore by adding these equations, DEA + DBC = DHA + DFB if to each of these ADB be added; then DEA + ADB + DBC = ABCDE = (DHA + ABD + DFB, = DHF.

#### PROB. XX.

### PL 3. fig. 8:

To project the lines of chords, sines, tangents and secantswith any radius.

On the line AB, let a semicircle ADB be described; let CDF be drawn perpendicular to this line from the centre C; and the tangent BE perpendicular to the end of the diameter; let the quadrants, AD, DB, be each divided into 9 equal parts, every one of which will be 10 degrees; if then from the centre C. lines be drawn through 10, 20, 30, 40, &c. the divisions of the quadrant BD, and continued to BE, we shall there have the tangents of 10, 20, 30, 40, &c. and the secants C 10, C 20, C 30, &c. are transferred to the line CF, by describing the arcs 10, 10: 20, 20: 30, 30, &c. If from 10, 20,30,&c. the divisions of the quadrant BD, there be let fall perpendiculars, let these be transferred to the radius CB, and we shall have the sines of 10, 20, 30, &c. and if from A we describe the arcs 10, 10: 20, 20: 30, 30, &c. from every division of the arc AD; we shall have a line of chords. The same way we may have the sine, tangent, &c. to every single degree on the quadrant, by subdividing each of the 9 former divisions into 10 equal parts. By this method the sines, tangents, &c. may be drawn to any radius; and then, after they are transferred to lines on a rule, we shall have the scales of sines, tangents, &c. ready for use.

# MATHEMATICAL

# DRAWING INSTRUMENTS.

The strictness of geometrical demonstration admits of no other instruments, than a rule and a pair of compasses. But, in proportion as the practice of geometry was extended to the different arts, either connected with, or dependent upon it, new instruments became necessary, some to answer peculiar

purposes, some to facilitate operation, and others to

promote accuracy.

As almost every artist, whose operations are connected with mathematical designing, furnishes himself with a case of drawing instruments suited to his peculiar purposes, they are fitted up in various modes, some containing more, others, tewer instruments. The smallest collection put into a case, consists of a plane scale, a pair of compasses with a moveable leg, and two spare points, which may be applied occasionally to the compasses; one of these points is to hold ink; the other, a porte crayon, for holding a piece of black-lead pencil.

What is called a full pocket case, contains the

following instruments.

A pair of large compasses with a moveable point, an ink point, a pencil point, and one for dotting; either of those points may be inserted in the compasses, instead of the moveable leg.

A pair of plain compasses somewhat smaller than

those with the moveable leg.

A pair of bow compasses.

A drawing pen with a protracting pin in the upper part.

A sector.

A plain scale.

A protractor.

A parallel rule.

A pencil and screw-driver.\*

\* Large collections are called, magazine cases of instru-

ments; these generally contain

A pair of six inch compasses with a moveable leg, an ink point, a dotting point, the crayon point, so contrived as to hold a whole pencil, two additional pieces to lengthen occasionally one leg of the compasses, and thereby enable them to measure greater extents, and describe circles of a larger radius.

A pair of hair compasses.

A pair of bow compasses.

A pair of triangular compasses.

In a case with the best instruments, the protractor and plain scale are always combined. The instruments in most general use are those of six inches; instruments are seldom madelonger, but often smaller. Those of six inches are, however, to be preferred, in general, before any other size; they will effect all that can be performed with the shortest ones, while, at the same time, they are better adapted to large work.

#### OF DRAWING COMPASSES.

Compasses are made either of silver or brass, but with steel points. The joints should always be framed of different substances; thus, one side, or part, should be of silver or brass, and the other of

A sector.

A parallel rule.

A protrac or.

A pair of proportional compasses, either with or without an adjusting screw.

A pair of wholes and halves.

Two drawing pens, and .. pointril.

A pair of small hair compasses, with a head similar to those of the bow compasses.

A knife, a file, key, and screw-driver or the compasses in one piece.

A small set of fine water colours.

To these some of the following instruments are often added.

A pair of beam compasses.

A pair of gunners callipers. A pair of elliptical compasses.

A pair of spiral ditto.

A pair of perspective compasses.

A pair of compasses with a micrometer screw.

A rule for drawing lines, tending to a centre at a great distance.

A protractor and parallel rule.

One or more parallel rules.

A pantographer, or Pentagraph.

A pair of sectoral compasses, forming, at the same time, a pair of beam and calliper compasses.

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an obtuse angle with the paper or plane, on which

they are used.

The ink and crayon points have a joint just under that part which fits into the compasses, by this they may be always so placed as to be set nearly perpendicular to the paper; the end of the shank of the best compasses is framed so as to form a strong spring, to bind firmly the moveable points, and prevent them from shaking. This is found to be a more effectual method than that by a screw.

Two additional pieces, are often applied to these compasses; these, by lengthening the leg, enable them to strike larger circles, or measure greater extents, than they would otherwise perform, and that without the inconveniences attending longer compasses. When compasses are furnished with this additional piece, the moveable leg has a joint that it may be placed perpendicular to the paper.

The bow compasses, are a small pair, usually with a point for ink; they are used to describe small arches or circles, which they do much more conveniently than large compasses, not only on account of their size, but also from the shape of the head, which rolls with great ease between the fingers.

of the drawing pen and protracting pin. The pen part of this instrument is used to draw strait lines; it consists of two blades with steel points fixed to a handle, the blades are so bent, that the ends of the steel points meet, and yet leave a sufficient cavity for the ink; the blades may be opened more or less by a screw, and, being properly set, will draw a line of any assigned thickness. One of the blades is framed with a joint, that the points may be separated, and thus cleaned more conveniently; a small quantity only of ink should be put at one time into the drawing pen, and this should be placed in the cavity, between the blades, by a common pen, or feeder; the drawing pen acts

better, if the pen, by which the ink is inserted, be made to pass through the blades. To use the drawing pen, first feed t with ink, then regulate it to the thickness of the required line by the screw. In drawing lines, incline the pen a small degree, taking care, however, that the edges of both the blades touch the paper, keeping the pen close to the rule and in the same direction during the whole operation: the blades should always be wiped very clean, before the pen is put away.

These directio is are equally applicable to the ink point of the compasses, only observing, that when an arch or circle is to be described, of more than an inch radius, the point should be so bent, that the blades of the pen may be nearly perpendicular to the paper, and both of them touch it at the same

time.

The protracting pin, is only a short piece of steel wire, with a very line point, fixed at one end of the upper part of the handle of the drawing pen. It is used to mark the intersection of lines, or to set off divisions from the plotting scale, and protractor.

#### OF THE SECTOR.

Amidst the variety of mathematical instruments that have been contrived to facilitate the art of drawing, there is none so extensive in its use, or of such general application as the sector. It is an universal scale, uniting, as it were angles and parallel lines, the rule and the compass, which are the only means that geometry makes use of for measuring, whether in speculation or practice. The real inventor of this valuable instrument is unknown; yet of so much merit has the invention appeared, that it was claimed by Galileo, and disputed by nations.

This instrument derives its name from the tenth definition of the third book of Euclid, where he defines the sector of a circle. It is formed of two equal rules called legs; these legs are moveable about the centre of a joint, and will; consequently, by their different openings, represent every possible variety of plane angles. The distance of the extremities of these rules are the subtenses or chords.

or the arches they describe.

Sectors are made of different sizes, but their length is usually denominated from the length of the legs when the sector is shut. Thus a sector of six inches, when the legs are close together, forms a rule of 12 inches when opened; and a foot sector is two feet long, when opened to its greatest extent. In describing the lines usually placed on this instrument, I refer to those commonly laid down on the best six-inch brass sectors. But as the principles are the same in all, and the differences little more than in the number of subdivisions, it is to be presumed that no difficulty will occur in the application of what is here said to sectors of a larger radius.

The scales, or lines graduated upon the faces of the instrument, and which are to be used as sectoral lines, proceed from the centre; and are, 1. Two scales of equal parts, one on each leg, marked LIN. or n. Each of these scales, from the great extensiveness of its use, is called the line of lines.

2. Two lines of chords, marked CHO. or c. 3. Two lines of secants marked SEC. or s. A line of polygons, marked POL. Upon the other face, the sectoral lines are, 1. Two lines of sines, marked sin or s. 2. Two lines of tangents, marked tan. 3. Between the lines of tangents and sines, there is another line of tangents to a lesser radius to supply the defect of the former, and extending from

450 to 759.

Each pair of these lines (except the line of polygons) is so adjusted as to make equal angles at the centre, and consequently at whatever distance the sector be opened, the angles will be always respectively equal. That is, the distance between 10 and 10 on the line of lines, will be equal to 60 and 60 on the line of chords, 90 and 90 on the line of sines, and 45 and 45 on the line of tangents.

Besides the sectoral scales, there are others on each face, placed parallel to the outward edges, and used as those of the common plain scale. There are on the one face, 1. A line of inches. 2. A line of latitudes. 3. A line of hours. 4. A line of inclination of meridians. 5. A line of chords. On the other face, three logarithmic scales, namely, one of numbers, one of sines, and one of tangents; these are used when the sector is fully opened, the legs forming one line.

To read and estimate the divisions on the sectoral lines. The value of the divisions on most of the lines are determined by the figures adjacent to them; these proceed by tens, which constitute the divisions of the first order, and are numbered accordingly; but the value of the divisions on the line of lines, that are distinguished by figures, is entirely arbitrary, and may represent a ly value that is given to them; hence the figures 1, 2, 3, 4, 3cc. may denote either 10, 20, 30, 40; or 100, 200, 300, 400, and so on.

The line of lines is divided into ten equal parts, numbered 1, 2, 3, to 10; these may be called divisions of the first order; each of these are again subdivided into 10 other equal parts, which may be called divisions of the second order; and each of these is divided into two equal parts, forming divisions of the third order.

The divisions on all the scales are contained between four parallel lines; those of the first order extend to the most distant; those of the third, to the least; those of the second to the intermediate

parallel.

When the whole line of lines represents 100, the divisions of the first order, or those to which the figures are annexed, represent tens; those of the second order, units; those of the third order, the halves of these units. If the whole line represents ten, then the divisions of the first order are units; those of these cond, tenths, and the thirds, twentieths.

In the line of tangents, the divisions to which the numbers are affixed, are the degrees expressed by those numbers. Every fifth degree is denoted by a line somewhat longer than the rest; between every number and each fifth degree, there are four divisions, longer than the intermediate adjacent ones, these are whole degrees; the shorter ones, or those of the third order, are 30 minutes.

From the centre, to 60 degrees, the line of sines is divided like the line of tangents; from 60 to 70, it is divided only to every degree; from 70 to 80, to every two degrees; from 80 to 90, the division

must be estimated by the eye.

The divisions on the line of chords are to be es-

timated in the same manner as the tangents.

The lesser line of tangents is graduated every two degrees from 45 to 50; but from 50 to 60, to every degree; from 60 to the end, to half degrees.

The line of secants from 0 to 10, is to be estimated by the eye; from 20 to 50 it is divided to every two degrees; from 50 to 60, to every degree; and from 60 to the end, to every half degree.

The solution of questions on the sector is said to be *simple*, when the work is begun and ended on the same line; *compound*, when the operation begins on one line, and is finished on the other.

The operation varies also by the manner in which the compasses are applied to the sector. If a measure be taken on any of the sectoral lines, beginning at the centre, it is called a lateral distance. But if the measure be taken from any point in one line, to its corresponding point on the line of the same denomination, on the other leg, it is called a transverse or parallel distance.

The divisions of each sectoral line are bounded by three parallel lines; the incrmost of these is that on which the points of the compasses are to be placed, because this alone is the line which goes to the centre, and is alone, therefore, the sectoral

line.

We shall now proceed to give a few general instances of the manner of operating with the sector.

Multiplication by the line of lines. Make the lateral distance of one of the factors the parallel distance of 10; then the parallel distance of the

other factor is the product.

Example. Multiply 5 by 6, extend the compasses from the centre of the sector to 5 on the primary divisions, and open the sector till this distance become the parallel distance from 10 to 10 on the same divisions; then the parallel distance from 6 to 6, extended from the centre of the sector, shall reach to 3, which is now to be reckoned 30. At the same opening of the sector, the parallel distance of 7 shall reach from the centre to 35, that of 8 shall reach from the centre to 40, &c.

Division by the line of lines. Make the lateral distance of the dividend the parallel distance of the divisor, the parallel distance of 10 is the quotient. Thus, to divide 30 by 5, make the lateral distance of 30, viz. 3 on the primary divisions, the parallel distance of 5 of the same divisions; then the parallel distance of 10, extended from the centre,

shall reach to 6.

Proportion by the line of lines. Make the lateral distance of the second term the parallel distance

of the first term; the parallel distance of the third

term is the fourth proportional.

Example. To find a fourth proportional to 8, 4, and 6, take the lateral distance of 4, and make it the parallel distance of 8; then the parallel distance of 6, extended from the centre, shall reach to

the fourth proportional 3.

In the same manner a third proportional is found to two numbers. Thus, to find a third proportional to 8 and 4, the sector remaining as in the former example, the parallel distance of 4, extended from the centre, shall reach to the third proportional 2. In all these cases, if the number to be made a parallel distance be too great for the sector, some aliquot part of it is to be taken, and the answer multiplied by the number by which the first number was divided. Thus, if it were required to find a fourth proportional to 4, 8, and 6; because the lateral distance of the second term 8 cannot be made the parallel distance of the first term 4, take the lateral distance of 4, viz. the half of 8, and make it the parallel distance of the first term 4; then the parallel distance of the third term 6, shall reach from the centre to 6, viz. the half of 12. Any other aliquot part of a number may be used in the same way. In like manner, if the number proposed be too small to be made the parallel distance, it may be multiplied by some number, and the answer is to be divided by the same number.

To protract angles by the line of Chords. Case
1. When the given degrees are under 60. 1. With
any radius on a centre, describe the arch. 2. Make
the same radius a transverse distance between 60
and 60 on the line of chords. 3. Take out the
transverse distance of the given degrees, and lay
this on the arch, which will mark out the angular

distance required

Case 2. When the given degrees are more than

60. 1. Open the sector, and describe the arch as before. 2. Take 4 or 4 of the given degrees, and take the transverse distance of this 4 or 4, and lay it off twice, if the degrees were halved, three times if the third was used as a transverse distance.

Case 3. When the required angle is less than 6 degrees; suppose 3. 1. Open the sector to the given radius, and describe the arch as before. 2. Set off the radius. 3. Set off the chord of 57 degrees backwards, which will give the arc of three degrees.

Given the radius of a circle, (suppose equal to two inches, ) required the sine and tangent of 28°

30 to that radius.

Solution. Open the sector so that the transverse distance of 90 and 90 on the sines, or of 45 and 45 on the tangents, may be equal to the given radius, viz. two inches; then will the transverse distance of 38° 30', taken from the sines, be the length of that sine to the given radius; or if taken from the tangents; will be the length of that tangent to the given radius.

But if the secant of 28° 30' was required?

Make the given radius, two inches, a transverse distance to 0 and 0, at the beginning of the line of secants; and then take the transverse distance of the degrees wanted, viz. 28° 30'.

A tangent greater than 45° (suppose 60°) is

found thus.

Make the given radius, suppose two inches, a transverse distance to 45 and 45 at the beginning of the scale of upper tangents; and then the required number 60° 00' may be taken from this scale.

Given the length of the sine, tangent or secant of any degrees; to find the length of the radius to that

sine, tangent, or secant.

Make the given length a transverse distance to its given degrees on its respective scale: then, In the sines. The transverse distance of 90 and

90 will be the radius sought.

In the lower tangents. The transverse distance of 45 and 45, near the end of the sector, will be

the radius sought.

In the upper tangents. The transverse distance of 45 and 45, taken towards the centre of the sector on the line of upper tangents, will be the centre sought.

In the secant. The transverse distance of O and O, or the beginning of the secants, near the centre

of the sector, will be the radius sought.

Given the radius and any line representing a sine, tangent, or secant; to find the degrees corresponding to that line.

SOLUTION. Set the sector to the given radius, according as a sine, or tangent, or secant is concerned.

Take the given line between the compasses; apply the two feet transversely to the scale concerned, and slide the feet along till they both rest on like divisions on both legs; then will those divisions shew the degrees and parts corresponding to the given line.

To find the length of a versed sine to a given number of degrees, and a given radius.

Make the transverse distance of 90 and 90 on the

sines, equal to the given radius.

Take the transverse distance of the sine comple-

ment of the given degrees.

If the given degrees are less than 90, the difference between the sine complement and the radius gives the versed sine.

If the given degrees are more than 90, the sum of the sine complement and the radius gives the versed

sine

To open the legs of the sector, so that the corres-

ponding double scales of lines, chords, sines, and

tangents, may make each a right angle.

On the lines, make the lateral distance 10, a distance between eight on one leg, and six on the other leg.

On the sines, make the lateral distance 90 a transverse distance from 45 to 45; or from 40 to 50; or from 30 to 60; or from the sine of any degrees to their complement.

Or on the sines, make the lateral distance of 45

a transverse distance between 30 and 30.

#### OF THE PLAIN SCALE.

The divisions laid down on the plain scale are of two kinds, the one having more immediate relation to the circle and its properties, the other being merely concerned with dividing straight lines.

Though arches of a circle are the most natural measures of an angle, yet in many cases right lines are substituted, as being more convenient; for the comparison of one right line with another, is more natural and easy, than the comparison of a right line with a curve; hence it is usual to measure the quantities of angles not by the arch itself, which is described on the angular point, but by certain lines described about that arch.

The lines laid down on the plain scales for the measuring of angles, or the protracting scales, are, 1. A line of chords marked CHO. 2. A line of sines marked SIN. of tangents marked TAN. of semitantangents marked SIN. and of secants marked SIC. this last is often upon the same line as the sines, because its gradations do not begin till the sines end.

There are two other scales, namely, the rhumbs, marked Ru. and longitudes, marked Lon. Scales of latitude and hours are sometimes put upon the plain scale; but, as dialling is now but seldom studied,

they are only made to order.

The divisions used for measuring straight lines are called scales of equal parts, and are of various lengths for the convenience of delineating any figure of a large or smaller size, according to the fancy or purposes of the draughts-man. They are, indeed. nothing more than a measure in miniature for laying down upon paper, &c. any known measure, as chains, yards, feet, &c. each part on the scale answering to one foot, one yard, &c. and the plan will be larger or smaller, as the scale contains a smaller or a greater number of parts in an inch. Hence a variety of scales is useful to lay down lines of any required length, and of a convenient proportion with respect to the size of the drawing. If none of the scales happen to suit the purpose, recourse should be had to the line of lines on the sector; for, by the different openings of that instrument, a line of any length may be divided into as many equal parts as any person chooses.

Scales of equal parts are divided into two kinds,

the one simple, the other diagonally divided.

Six of the simply divided scales are generally placed one above another upon the same rule; they are divided into as many equal parts as the length of the rule will admit of; the numbers placed on the right hand, shew how many parts in an inch each scale is divided into. The upper scale is sometimes shortened for the sake of introducing another, called the line of chords.

The first of the larger, or primary divisions, on every scale is subdivided into 10 equal parts, which small parts are those which give a name to the scale: thus it is called a scale of 20, when 20 of these divisions are equal to one inch. If, therefore, these lesser divisions be taken as units, and each represents one league, one mile, one chain, or one yard,

&c. then will the larger divisions be so many tens; but if the subdivisions are supposed to be tens, the

larger divisions will be hundreds.

To illustrate this, suppose it were required to set off from either of the scales of equal parts \$4, 36, or 360 parts, either miles or leagues. Set one foot of your compasses on 3, among the larger or primary divisions, and open the other point till it falls on the 6th subdivision, reckoning backwards or towards the left hand. Then will this extent represent, \$4, 36, or 360 miles or leagues, &c. and bear the same proportion in the plan as the line measured does to the thing represented.

To adapt these scales to feet and inches, the first primary division is often duodecimally divided by an upper line; therefore, to lay down any number of feet and inches, as for instance, eight feet eight inches, extend the compasses from eight of the larger to eight of the upper small ones, and that distance laid down on the plan will represent eight feet

eight inches.

Of the scale of equal parts diagonally divided.

The use of this scale is the same as those already described. But by it a plane may be more accurately divided than by the former; for any one of the larger divisions may by this be subdivided into 100 equal parts; and, therefore, if the scale contains 10 of the larger divisions, any number under 1000 may

be laid down with accuracy.

The diagonal scale is seldom placed on the same side of the rule with the other plotting scale. The first division of the diagonal scale, if it be a foot long, is generally an inch divided into 100 equal parts, and at the opposite end there is usually half an inch divided into 100 equal parts. If the scale be six inches long, one end has commonly half an inch, the other a quarter of an inch subdivided into 100 equal parts.

The nature of this scale will be better understood by considering its construction. For this

purpose:

First: Draw eleven parallel lines at equal distances; divide the upper of these lines into such a number of equal parts, as the scale to be expressed is intended to contain; from each of these divisions draw perpendicular lines through the eleven parallels.

Secondly. Subdivide the first of these divisions into ten equal parts, both in the upper and lower

lines.

Thirdly. Subdivide again each of these subdivisions, by drawing diagonal lines from the 10th below to the 9th above; from the 8th below to the 7th above; and so on, till from the first below to the 0 above; by these lines each of the small divisions is divided into ten parts, and, consequently, the whole first space into 100 equal parts; for, as each of the subdivisions isone-tenth part of the whole first space or division, so each parallel above it is one-tenth of such subdivision, and, consequently, one-hundreth part of the whole first space; and if there be ten of the larger divisions, one-thousandth part of the whole space.

If, therefore, the larger divisions be accounted as units, the first subdivisions will be tenth parts of an unit, and the second, marked by the diagonal upon the parallels, hundreth parts of the unit. But, if we suppose the larger divisions to be tens, the first subdivisions will be units, and the second tenths. If the larger are hundreds, then will the

first be tens, and the second units.

The numbers therefore, 576, 57,6, 5,76, are all expressible by the same extent of the compasses: thus setting one foot in the number five of the larger divisions, extend the other along the sixth parallel to the seventh diagonal. For, if the five

darger divisions be taken for 500, seven of the first subdivisions will be 70, which upon the sixth parallel, taking in six of the second subdivisions for units, makes the whole number 576. Or, if the five larger divisions be taken for five tens, or 50, seven of the first subdivisions will be seven units, and the six second subdivisions upon the sixth parallel, will be six tenths of an unit. Lastly, if the five larger divisions be only esteemed as five units, then will the seven first subdivisions be seven tenths, and the six second subdivisions be the six hundredth parts of an unit.

Of the line of chords. This line is used to set off an angle from a given point in any right line, or to measure the quantity of an angle already laid

down.

Thus to draw a line that shall make with another line an angle, containing a given number of

degrees, suppose 40 degrees.

Open your compasses to the extent of 60 degrees upon the line of chords, (which is always equal to the radius of the circle of projection,) and setting one foot in the angular point, with that extent describe an arch; then taking the extent of 40 degrees from the said chord line, set it off from the given line on the arch described; a right line drawn from the given point, through the point marked upon the arch, will form the required angle.

The degrees contained in an angle already laid down, are found nearly in the same manner; for instance, to measure an angle. From the centre describe an arch with the chord of 60 degrees, and the length of the arch, contained between the lines measured on the line of chords, will give the num-

ber of degrees contained in the angle.

If the number of degrees are more than 90, they must be measured upon the chords at twice; thus, if 120 degrees were to be practised, 60 may be taken from the chords, and those degrees be laid of

twice upon the arch. Degrees taken from the chords are always to be counted from the beginning

of the scale.

Of the rhumb line. This is, in fact, a line of chords constructed to a quadrant divided into eight parts or points of the compass, in order to facilitate the work of the navigator in laying down a ship's course.

Of the line of longitudes. The line of longitudes is a line divided into sixty unequal parts, and so applied to the line of chords, as to shew by inspection, the number of equatorial miles contained in a degree on any parallel of latitude. The graduated line of chords is necessary, in order to shew the latitudes; the line of longitude shews the quantity of a degree on each parallel in sixtieth parts of an equatorial degree, that is, miles.

The lines of tangents, semitangents, and secants serve to find the centres and poles of projected circles in the stereographical projection of the sphere.

The line of sines is principally used for the ortho-

graphic projection of the sphere.

The lines of latitudes and hours are used conjointly, and serve very readily to mark the hour lines in the construction of dials; they are generally on the most complete sorts of scales and sectors; for the uses of which see treatises on dialling.

## OF THE PROTRACTOR.

This is an instrument used to protract, or lay down an angle containing any number of degrees, or to find how many degrees are contained in any given angle. There are two kinds put into cases of mathematical drawing instruments; one in the form of a semicircle, the other in the form of a parallelogram. The circle is undoubtedly the only natural measure of angles; when a straight line is therefore used, the divisions thereon are derived

from a circle, or its properties, and the straight line is made use of for some relative convenience: it is thus the parallelogram is often used as a protractor, instead of the semicircle, because it is in some cases more convenient, and that other scales, &c.

may be placed upon it.

The semicircular protractor, is divided into 180 equal parts or degrees, which are numbered at every tenth degree each way, for the conveniency of reckoning either from the right towards the left, or from the left towards the right; or the more easily to lay down an angle from either end of the line, beginning at each end with 10, 20, &c. and proceeding to 180 degrees. The edge is the diameter of the semicircle, and the mark in the middle points out the centre, in a protractor in the form of a parallelogram: the divisions are as in the semicircular one, numbered both ways; the blank side represents the diameter of a circle. The side of the protractor to be applied to the paper is made flat, and that whereon the degrees are marked, is chamfered or sloped away to the edge, that an angle may be more easily measured, and the divisions set off with greater exactness.

Application of the protractor to use. 1. A number of degrees being given, to protract, or lay down an angle, whose measure shall be equal thereto.

Thus, to lay down an angle of 60 degrees from the point of a line, apply the diameter of the protractor to the line, so that the centre thereof may coincide exactly with the extremity; then with a protracting pin make a fine dot against 60 upon the limb of the protractor; now remove the protractor, and draw a line from the extremity through that point, and the angle contains the given number of degrees.

2. To find the number of degrees contained in a

given angle.

Place the centre of the protractor upon the angular point, and the fiducial edge, or diameter, exactly upon the line; then the degree upon the limb that is cut by the line will be the measure of the given angle, which, in the present instance, is found to be 60 degrees.

S. From a given point in a line, to erect a per-

pendicular to that line.

Apply the protractor to the line, so that the centre may coincide with the given point, and the division marked 90 may be cut by the line, then a line drawn against the diameter of the protractor will be the perpendicular required.

#### OF PARALLEL BULES.

Parallel lines occur so continually in every species of mathematical drawing, that it is no wonder so many instruments have been contrived to delineate them with more expedition than could be effected by the general geometrical methods. For this purpose, rules of various constructions have been made; and particularly recommended by their inventors; their use however is so apparent as to need no explanation.

# GUNTER'S SCALE.

The scale generally used is a ruler of two feet in length, having drawn upon it equal parts, chords, sines, tangents, secants, &c. These are contained on one side of the scale, and the other side contains the logarithms of these numbers. Mr. Edmund Gunter was the first who applied the logarithms of numbers, and of sines and tangents to straight lines drawn on a scale or ruler; with which, proportions in common numbers, and trigonometry, may be solved by the application of a pair of compasses

only. The method is founded on this property, That the logarithms of the terms of equal ratios are equidifferent. This was called Gunter's Proportion, and Gunter's Line; hence the scale is generally called the Gunter.

Of the Logarithmical Lines, or Gunter's Scale. The logarithmical lines, on Gunter's scale, are the

eight following:

S. Rhumb, or fine rhumbs, is a line containing the logarithms of the natural sines of every point and quarter point of the compass, numbered from a brass pin on the right hand towards the left with 8, 7, 6, 5, 4, 3, 2, 1.

T\*Rhumb, or tangent rhumbs, also corresponds to the logarithm of the tangent of every point and quarter point of the compass. This line is numbered from near the middle of the scale with 1.2. 3. 4 towards the right hand, and back again with the numbers 5, 6, 7 from the right hand towards the left. To take off any number of points below four, we must begin at 1 and count towards the right hand; but to take off any number of points above four, we must begin at four and count towards the left hand.

Numbers, or the line of numbers, is numbered from the left hand of the scale towards the right with 1, 2, 3, 4, 5, 6, 7, 8, 9, 1 which stands exactly in the middle of the scale; the numbers then go on 2, 3, 4, 5, 6, 7, 8, 9, 10 which stands at the right hand end of the scale. These two equal parts of the scale are divided equally, the distance between the first or left hand 1, and the first 2, 3, 4, &c. is exactly equal to the distance between the middle 1 and the numbers 2, 3, 4, &c. which follow it. The subdivisions of these scales are likewise similar, viz. they are each one tenth of the primary divisions, and are distinguished by lines of about half the length of the primary divisions.

These subdivisions are again divided into ten parts, where room will permit; and where that is not the case, the units must be estimated, or guessed at, by the eye, which is easily done by a little

practice.

The primary divisions on the second part of the scale, are estimated according to the value set upon the unit on the left hand of the scale: If you call it one, then the first 1, 2, 3, &c. stand for 1, 2, 3, &c. the middle 1 is 10, and the 2. 3. 4. &c. following stand for 20, 30, 40, &c. and the ten at the right hand is 100: If the first 1 stand for 10, the first 2, 3, 4, &c. must be counted 20, 30, 40, &c. the middle 1 will be 100, the second 2, 3, 4, 5, &c. will stand for 200, 300, 400, 500, &c. and the ten at the right hand for 1000.

If you consider the first 1 as  $\frac{1}{10}$  of an unit, the 2, 3, 4, &c. following will be  $\frac{1}{10}$ ,  $\frac{1}{10}$ ,  $\frac{1}{10}$ , &c. the middle 1 will stand for an unit, and the 2, 3, 4, &c. following will stand for 2, 3, 4, &c. also the division at the right-hand end of the scale will stand for 10. The intermediate small divisions must be estimated according to the value set upon the primary ones.

Sine. The line of sines is numbered from the left hand of the scale towards the right, 1, 2, 3, 4, 5, &c. to 10; then 20, 30, 40, &c. to 90, where it terminates just opposite 10 on the line of numbers.

Versed sine. This line is placed immediately under the line of sines, and numbered in a contrary direction, viz. from the right hand towards the left 10, 20, 30, 40, 50, to about 169; the small divisions are here to be estimated according to the number of them to a degree. By comparing the line of versed sines with the line of sines, it will appear that the versed sines do not belong to the arches with which they are marked, but are the half versed sines of their supplements. Thus, what is marked the versed sine of 90 is only half the versed sine of 90,

the versed sine of 120° is half the versed sine of 60°, and the versed sine marked 100° is half the versed sine of 80°, &c.

The versed sines are numbered in this manner to render them more commodious in the solution of

trigonometrical, and astronomical problems.

Tangents. The line of tangents begins at the left hand, and is numbered 1, 2, 3, &c. to 10, then 20, 30, 45, where there is a little brass pin just under 90 in the line of sines; because the sine of 90° is equal to the tangent of 45°. It is numbered from 45° towards the left hand 50, 60, 70, 80, &c. The tangents of arches above 45° are therefore counted backward on the line, and are found at the same points of the line as the tangents of their complements.

Thus, the division at 40 represents both 40 and

50 the division at 30 serves for 30 and 60, &c.

Meridional Parts. This line stands immediately above a line of equal parts, marked Equal Pt. with which it must always be compared when used. The line of equal parts is marked from the right hand to the left with 0, 10, 20, 30, &c.; each of these large divisions represents 10 degrees of the equator, or 600 miles. The first of these divisions is sometimes divided into 40 equal parts, each re-

presenting 15' minutes or miles.

The extent from the brass pin on the scale of meridional parts to any division on that scale, applied to the line of equal parts, will give (in degrees) the meridional parts answering to the latitude of that division. Or the extent from any division to another, on the line of meridional parts, applied to the line of equal parts, will give the meridional difference of latitude between the two places denoted by the divisions. These degrees are reduced to leagues by multiplying by 20, or to miles by multiplying by 60.

The use of the logarithmical lines on Gunter's Scale. By these lines and a pair of compasses, all the problems of Trigonometry, &c. may be solved.

These problems are all solved by proportion; Now in natural numbers, the quotient of the first term by the second is equal to the quotient of the third by the fourth: therefore, logarithmically speaking, the difference between the first and second term is equal to the difference between the third and fourth, consequently on the lines on the scale, the distance between the first and second term will be equal to the distance between the third and fourth. And for a similar reason, because four proportional quantities are alternately proportional, the distance between the first and third terms, will be equal to the distance between the second and fourth. Hence the following

#### General Rule.

The extent of the compasses from the first term to the second, will reach, in this same direction, from the third to the fourth term. Or, the extent of the compasses from the first term to the third, will reach, in the same direction, from the second to the fourth.

By the same direction in the foregoing rule, is meant that if the second term lie on the right hand of the first, the fourth will lie on the right hand of the third, and the contrary. This is true, except the two first or two last terms of the proportion are on the line of tangents, and neither of them under 45°; in this case the extent on the tangents is to be made in a contrary direction: For had the tangents above 45° been laid down in their proper direction, they would have extended beyond the length of the scale towards the right hand; they are therefore as it were folded back up-

on the tangents below 45°, and consequently lie in a direction confrary to their proper and natural order.

If the two last terms of a proportion be on the line of tangents and one of them greater and the other less than 45°; the extent from the first term to the second, will reach from the third beyond the scale. To remedy this inconvenience, apply the extent between the two first terms from 45° backward upon the line of tangents, and keep the left hand point of the compasses where it falls; bring the right hand point from 45° to the third term of the proportion; this extent now in the compasses applied from 45° backward will reach to the fourth term, or the tangent required. For, had the line of tangents been continued forward beyond 45°, the divisions would have fallen above 45° forward; in the same manner as they fall under 45° backward.

#### SECTION V.

#### TRIGONOMETRY.

The word Trigonometry signifies the measuring of triangles. But, under this name is generally comprehended the art of determining the positions and dimensions of the several unknown parts of extension, by means of some parts, which are already known. If we conceive the different points, which may be represented in any space, to be joined together by right lines, there are three things offered for our consideration; I. the length of these lines; 2. the angles, which they form with one another; 3. the angles formed by the planes, in which these lines are drawn, or are supposed to be traced. On the comparison of these three objects.

depends the solution of all questions, that can be proposed concerning the measure of extension, and its parts; and the art of determining all these things from the knowledge of some of them, is reduced to the solution of these two general questions.

1. Knowing three of the six parts, the sides and angles—which constitute a rectilineal triangle; to

find the other three.

Knowing three of the six parts, which compose a spherical triangle; that is a triangle formed on the surface of a sphere by three arches of circles, which have their centre in the centre of the same

sphere-to find the other three.

The first question is the object of what is called Plane Trigonometry, because the six parts, considered here, are in the same plane: it is also denominated Rectilineal Trigonometry. The second question belongs to Spherical Trigonometry, wherein the six parts are considered in different planes. But the only object here is to explain the solutions of the former question: viz.

### PLANE TRIGONOMETRY.

Plane Trigonometry is that branch of geometry, which teaches how to determine, or calculate three of the six parts of a rectilineal triangle by having the other three parts given or known. It is usually divided into Right angled and Oblique angled Trigonometry, according as it is applied to the mensuration of Right or Oblique angled Triangles.

In every triangle, or case in trigonometry, three of the parts must be given, and one of these parts, at least, must be a side; because, with the same angles, the sides may be greater or less in any pro-

portion.

#### RIGHT ANGLED PLANE TRIGONOMETRY.

#### PL. 5. Fig. 1.

1. In every right-angled plane triangle ABC, if the hypothenuse AC be made the radius, and with it a circle, or an arc of one, be described from each end; it is plain (from def. 20.) that BC is the sine of the angle A, and AB is the sine of the angle C; that is, the legs are the sines of their opposite angles.

#### Fig. 2.

If one leg AB be made the radius, and with it, on the point A, an arc be described; then BC is the tangent, and AC is the secant of the angle A, by def. 22 and 25.

#### Fig. 3.

3. If BC be made the radius, and an arc be described with it on the point C; then is AB the tangent, and AC is the secant of the angle C, as before.

Because the sine, tangent, or secant of any given are in one circle, is to the sine, tangent, or secant of a like are (or to one of the like number of degrees) in another circle; as the radius of the one is to the radius of the other; therefore the sine, tangent, or secant of any are is proportional to the sine, tangent, or secant of a like are, as the radius of the given are is to 10.000000, the radius from whence the logarithmic sines, tangents, and secants, in most tables, are calculated, that is;

If AC be made the radius, the sines of the angle A and C, described by the radius AC, will be proportional to the sines of the like arcs, or angles in the circle, that the tables now mentioned were

calculated for. So if BC was required, having the angles and AB given, it will be,

Fig. 1.

As S.C : AB : : S.A : BC.

That is, as the sine of the angle C in the tables, is to the length of AB; (or sine of the angle C, in a circle whose radius is AC;) so is the sine of the angle A in the tables, to the length of BC. (or sine of the same angle, in the circle, whose radius is AC.)

In like manner, the tangents and secants represented by making either leg the radius, will be proportional to the tangents and secants of a like arc, as the radius of the given arc is to 10.000000.

the radius of the tables aforesaid.

Hence it is plain, that if the name of each side of the triangle be placed thereon, a proportion will arise to answer the same end as before: thus if AC be made the radius, let the word radius be written thereon; and as BC and AB, are the sines of their opposite angles; upon the first let S.A, or sine of the angle A, and on the other let S.C, or sine of the angle C, be written. Then,

When a side is required, it may be obtained by

this proportion, viz.

As the name of the side given

is to the side given,

So is the name of the side required

to the side required.

Thus, if the angles A and C, and the hypothenuse AC were given, to find the sides; the proportion will be

Fig. L.

1. R : AC :: S.A : BC.

That is, as radius is to AC, so is the sine of the angle A, to BC. And,

 $\mathbf{Q}. \quad \mathbf{R} : \mathbf{AC} : : \mathbf{S.C} : \mathbf{AB}.$ 

That is as radius is to AC, so is the sine of the angle C, to AB.

When an angle is required, we use this propor-

tion, viz.

As the side that is made the radius,

is to radius,

So is the other given side,

to its name.

Thus, if the legs were given to find the angle A, and if AB be made the radius, it will be

#### Fig. 2.

#### AB:R::BC:T.A.

That is, as AB, is to radius, so is BC, to the tangent of the angle A.

After the same manner, the sides or angles of all right angled plane triangles may be found, from

their proper data.

We here, in plate 4, give all the proportion requisite for the solution of the six cases in right-angled trigonometry; making every side possible the radius.

In the following triangles this mark — in an angle, denotes it to be known, or the quantity of degrees it contains to be given; and this mark' on a side, denotes its length to be given in feet, yards, perches, or miles, &c. and this mark', either in an angle or on a side, denotes the angle or side to be required.

From these proportions it may be observed; that to find a side, when the angles and one side are given, any side may be made the radius; and

to find an angle, one of the given sides must be made the radius. So that in the 1st, 2d, and 3d cases, any side, as well required as given may be made the radius, and in the first statings of the 4th, 5th, and 6th cases, a given side only is made the radius.

#### RIGHT ANGLED TRIANGLES.

#### CASE I.

The angles and hypothenuse given, to find the base and perpendicular.

#### PL. 5. Fgi. 4.

In the right angled triangle ABC, suppose the angle  $A=46^{\circ}$ . 30. and consequently the angle  $C=43^{\circ}$ . 30. (by cor. 2. theo. 5.); and AC 250 parts, (as feet, yards, miles, &c.) required the sides AB and BC.

#### Ist. BY CONSTRUCTION.

Make an angle of 46°. 30', in blank lines, (by prob. 16. geom.) as CAB; lay 250, which is the given hypothenuse, from a scale of equal parts, from A to C; from C, let fall the perpendicular (BC, by prob. 7. geom.) and that will constitute the triangle ABC. Measure the lines BC, and AB, from the same scale of equal parts that AC was taken from; and you have the answer.

### 2d. BY CALCULATION.

1. Making AC the radius, the required sides are found by these propositions, as in plate 4, case 1.

R:AC::S.A:BC.R:AC::S.C:AB.

That is, as radius, $=90^{\circ}$ is to $AC = 250^{\circ}$ So is the sine of $\Lambda = 46^{\circ}$ . So	10.000000 2.397940 9.860562
to BC, =181. 4	2,258502
As radius, $=90^{\circ}$ is to $AC$ , $=250$ So is the sine of $C=43^{\circ}$ , $30^{\circ}$	10.000000 2.397940 9.837812
to AB, =172. 1	2.235752

If from the sum of the second and third logs. that of the first be taken, the number will be the log. of the fourth; the number answering to which, will be the thing required; but when the first log. is radius, or 10.000000, reject the first figure of the sum of the other two logs. (which is the same thing as to subtract 10.000000;) and that will be the log. of the thing required.

# 2. Making AB the radius.

Secant A: AC: :R: AB. Secant A: AC: :T.A: BC.

That is, As the secant is to AC, So is the radius	of A=46° 30' =250 =90°	10.162188 2.397940 10.000000
		12.397940
to AB,	=172. 1	2.235762

As the secant of $A$ is to $AC$ , So is the tangent of $A$	=46° 30′ = 250 =46° 30′	10.162188 2.39794 <b>0</b> 10.02275 <b>0</b>
		12.420690
to <i>BC</i> ,	=181.34.	2.258502

# 3. Making BC the radius.

Sec. <i>C : AC : :</i>			4
Sec. $C:AC:$ :  That is, as the secant of is to $AC$ , . So is radius			10.139438 2.397940 10.000000
			12.397940
to $BC$ , As the secant of $C$ is to $AC$ , So is the tangent of $C$	=4. =	181.34 3° 30′ 250 3° 30′	2.258502 10.139438 2.397940 9.977950
			12.575190

to AB, = 172. 1 2.235752 Or, having found one side, the other may be obtained by cor. 2. theo. 14. sect. 4.

# 3d. By Gunter's scale.

The first and third terms in the foregoing proportions, being of a like nature, and those of the second and fourth being also like to each other; and the proportions being direct ones, it follows; that if the third term be greater or less than the first, the fourth term will be also greater or less

than the second; therefore the extent in your compasses, from the first to the third term, will reach from the second to the fourth.

Thus, to extend the first of the foregoing proportions;

- 1. Extend from 90° to 46° 30′, on the line of sines; that distance will reach from 250 on the line of numbers, to 181, for BC.
- 2. Extend from 90° to 43° 30′, on the line of sines; that distance will reach from 250 on the line of numbers, to 172, for AB.

If the first extent be from a greater to a less number; when you apply one point of the compasses to the second term, the other must be turned to a less; and the contrary.

By def. 20. sect. 4. The sine of 90° is equal to the radius; and the tangent of 45° is also equal to the radius; because if one angle of a right angled triangle be 45°, the other will be also 45°; and thence (by the lemma preceding theo. 7. sect. 4.) the tangent of 45° is equal to the radius: for this reason the line of numbers of 10.0000000, the sine of 90°, and tangent of 45° being all equal terminate at the same end of the scale.

The two first statings of this case, answers the question without a secant: the like will be also made evident in all the following cases.

4th. Solution by Natural Sines.

From the foregoing analogies, or statements, it

is obvious that if the hypothenuse be multiplied by the natural sine of either of the acute angles, the product will be the length of the side opposite to that angle; and multiplied by the natural co-sine of the same angle, the product will be the length of the other side, or that which is contiguous to the angle. Thus:

the	given	ang = 470	30'.
	The state of the state of	THE PERSON AS	

Nat. Sine=.725374 Hyp. = 250	Nat. Cos 688855	
36268700 1450748	34417750 1376710	
1 707 0/0500	T- 170 000770	

Perpend.=181.343500

Base=172.088750

#### CASE II.

The base and angles given; to find the perpendicular and hypothenuse.

## P1. 5. fig. 5.

In the triangle ABC there is the angle A 42° 201, and of course the angle C 47° 40′ (by cor. 2 theo. 5,) and the side AB 190, given; to find BC and AC.

## 1st. By Construction.

Make the angle CAB (by prob. 16. sect. 4.) in blank lines, as before. From a scale of equal parts lay 190 from A to B; on the point B, erect a perpendicular BC (by prob. 5. sect. 4.) the point where this cuts the other blank line of the angle, will be C: so is the triangle ABC constructed; let AC and BC be measured from the same scale of equal parts that AB was taken from, and the answers are found.

# 2d. By Calculation.

# 1. Making AC the radius.

S. C: AB:: R: AC. S. C: AB:: S. A: BC.

That is; as the sine of C =479 40' 9.868785 2.278754 is to AB, 190 So is radius 90° 10.000000 12.278754 257 to AC 2.409969 As the sine of C =47° 40' 9.868785 is to AB. 190 2.278754 So is the sine of  $A = 42^{\circ}$  20' 9.828301 12.107055 =173.1to BC, 2.238270

# 2. Making AB the radius,

R:AB::T.A:BC.R:AB::Sec. A:AC.

That is, as radius 90<sup>6</sup> 10.000000 2.278754 is to AB, 190 So is the tangent of  $A=42^{\circ}$  20' 9.959516 2.238270 =173. ] to  $BC_{1}$ As radius =9010.000000 2.278754 is to AB, =19010.131215 So is the secant of  $A = 42^{\circ} 20$ ? 2.409969 to AC, 257

# 3. Making BC the radius.

- T. C : AB : : Sec. C : AC.	
T. C: AB: R: BC.	
That is, as the tangent of C=47° 401	10.040484
is to $\Delta B_{\star} = 190$	2.278754
So is the Secant of C=47° 40/	10.171699
So is the Secant of C=47° 407	10.171099
	-
	12.450453
EUROCO OLLU SVEL	
to $AC_{2} = 257$	2.409969
The state of the s	10.040484
As the tangent of $C=47^{\circ} 40'$	III. THE REAL PROPERTY AND ADDRESS OF THE PERSON NAMED AND ADD
is to $AB$ , = 190	2.278754
So is the radius $=90^{\circ}$	10.000000
	12.278754
Minds and and the	10.010101
The same of the same of	0.000070
to $BC = 173.1$	2,238270

Or, having found one of the required sides, the other may be obtained, by one, or the other of the cors. to theo. 14. sect. 4.

# 3d. By Gunter's Scale.

# 1. When AC is made the radius.

Extend from  $47^{\circ}$  40', to  $90^{\circ}$  on the line of sines; that distance will reach from 190 to 257, on the line of numbers, for AC.

2. When AB is made the radius, the first stating

is thus performed,

Extend from 45° on the tangents (for the tangent of 45° is equal to the radius, or to the sine of 90° as before) to 42° 201; that extent will reach from 190, on the line of numbers, to 173, for BC.

3. When BC is made the radius, the second stating is thus performed.

Extend from  $47^{\circ}$  40' on the line of tangents, to  $45^{\circ}$ , or radius; that extent will reach from 190 to 173, on the line of numbers, for BC; for the tangent of  $47^{\circ}$  40', is more than the radius, therefore the fourth number must be less than the second, as before.

The two first statings of this case, answer the question without a secant.

4th. Solution by Natural Sines.

$$\frac{AB \times R.}{S \text{ of } C.} = AC; \text{ and } \frac{AB \times S \text{ of } A.}{S \text{ of } C.} = BC.$$

Nat. S of C, side  $AB \times R$ .

Thus .739239) 190.000000 (257.02 & c.= AC.

147.8478

421**5220 3**6961**95** 

5190250 5174673

> 1557700 147847**8**

and, .673443=Nat. S. of A. 190=side AB.

60609870

The

50,9027 5174673. 2283540 2217717

### CASE III.

The engles and perpendicular given; to find the base and hypothenues.

### Pt. 5. fg. 6.

In the triangle ABC, there is the angle A 40°, and consequently the angle C 50°, with BC 170, given: to find AC and AB.

## 1st. By Construction.

Make an angle CAB of  $40\circ$  in blank lines; (by prob. 16. sect. 4.) with BC 170, from a line of equal parts draw the lines EF parallel to AB (by prob. 8. sect. 4.) the lower line of the angle, and from the point where it cuts the other line in C, let fall a perpendicular BC (by prob. 7. sect. 4.) and the triangle is constructed: the measures of AC and AB, from the same scale that BC was taken, will answer the question.

What has been said in the two foregoing cases, is sufficient to render the operations in this, both by calculation, Gunter's scale, and Natural sines, so obvious, that it is needless to insert them; however, for the sake of the learner, we give for

Answers; AC 264. 5, and AB 202. 6.

#### CASE IV.

The base and hypothenuse given; to find the angles and perpendicular.

#### PL. 5. fig. 7.

In the triangle ABC, there is given, AB300 and AC500: the angles A and C, and the perpendicular BC, are required.

### 1st. By Construction.

From a scale of equal parts lay 300 from A to B; on B erect an indefinite blank perpendicular line, with AC500, from the same scale, and one foot at the compass, in A, cross the perpendicular line in C; and the triangle is constructed.

By prob. 17. sect. 4. measure the angle A, and let BC be measured from the same scale of equa parts that AC and AB were taken from; and the answers are obtained.

# 2d. By Calculation.

1. Making AC the radius.

AC: R: : AB: S.C. R: AC: : S.A.: BC.

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That is, as $AC$	==	<i>5</i> 00	2.598970
is to radius,	=	<b>90°</b>	10.000000
So is $AB$	=	<b>3</b> 00	2.477121
	•	,	12.477121
to the sine	of <i>C</i> ,=	36° 52′	9.778151
By cor. 2. theo. 5. angle $A$ .	90°—3	36° 52′ =	53° 08′ the
As radius =	90°		10.000000
is to $AC_{1} =$	<b>5</b> 00		2.698970
So is the sine of A	4 = 53°	08/	9.903108
to BC	, = 400		2.602078

# 2. Making AB the radius.

AB : R : AC : Sec. A.R : AB : TA : BC.

That is, as $AB$	=	<i>3</i> 00	2.477121
is to radiu	s =	90°	10.000000
So is $AC$	=	500	2.698970
			12.698970
to the seca	ant of A,	=53°. 08 <i>1</i>	10.221849
As radius	=	90°	10.000000
is to $AB$ ,	=	<i>3</i> 00	2.477121
So is the tange	ent of $A=$	=53°. 081	10.124990
to <i>BC</i> ,	22	400	2,602111

Or BC may be found from cor. 2. theo. 14. sect. 4.

## 3d. By Gunter's Scale.

# 1. Making AC the radius.

Extend from 500 to 300, on the line of numbers; that extent will reach from  $90^{\circ}$ , on the line of sines, to  $36^{\circ}$ .  $52^{\prime}$  for the angle C.

Again, extend from  $90^{\circ}$  to  $53^{\circ}$ . 08', on the line of sines, that extent will reach from 500 to 400, on the line of numbers, for BC.

2, Making AC the radius, the second stating is thus performed.

Extend from radius, or the tangent of  $45^{\circ}$ , to  $53^{\circ}$ . 08', that extent will reach from 300 to 400, for BC.

4th. Solution by Natural Sines.

$$\frac{R \times AB.}{AC} = S \text{ of } C; \text{ and } \frac{AC \times S \text{ of } A.}{R} = BC.$$
Thus,  $AC = AB$ 

$$5,00) 300.0000,00$$

$$600000 = \text{Nat. sine } 36^{\circ} 52^{\circ}$$

and.

Nat. sine of 
$$A = 53^{\circ}$$
 8' = .800034  
 $AC = 500$   
 $400.017000 = BC$ 

#### CASE V.

The perpendicular and hypothenuse given, to find the angles and base.

#### PL. 5. fig. 8.

In the triangle ABC there is BC 306, and AC 370 given; to find the angles A and C; and the base AB.

## 1st. By Construction.

Draw a blank line from any point, in which, at B, erect a perpendicular, on which lay BC 306, from a scale of equal parts: from the same scale, with AC 370, in the compasses, cross the first drawn blank line in A, and the triangle ABC is constructed.

Measure the angle A (by prob. 17. sect. 4.); and also AB, from the same scale of equal parts the other sides were taken from, and the answers are now found.

The operations by calculation, the square root, Gunter's scale, and Natural sines, are here omitted, as they have been heretofore fully explained: the statings, or proportions must also be obvious, from what has already been said.

Answers; The angle  $A 55^{\circ} 48'$ ; therefore the angle  $C 34^{\circ} 12'$ , and AB 208.

#### CASE VI.

The base and perpendicular given; to find the angles and hypothenuse.

PL. 5. fig. 9.

In the triangle ABC, there is AB 225, and BC 272, given; to find the angles A and C, and the hypothenuse AC.

## 1st. By Construction.

Draw a blank line, on which lay AB 225, from a scale of equal parts; at B, erect a perpendicular; on which lay BC, 272, from the same scale: join A and C, and the triangle is constructed.

As before, let the angle  $\mathcal{A}$ , and the hypothenuse  $\mathcal{AC}$  be measured; in order to find the answers.

## 2d. By Calculation.

1. Making AB the radius.

AB : R : BC : T.A.R. : AB : Sec. A : AC.

2. Making BC the radius.

BC:R::AB:T.C.R.:BC::Sec.C:AC.

By calculation; the answers from the foregoing proportions are easily obtained, as before.

But because AC, by either of the said proportions is found by means of a secant; and since there is no line of secants on Gunter's scale; after having

found the angles, as before, let us suppose AC the radius, and then

1. 
$$S.A:BC::R.:AC.$$
 or 2.  $S.C:AB::R:AC.$ 

These proportions may be easily resolved, either by calculation or Gunter's scale, as before; and thus the hypothenuse AC may be found without a secant.

From the two given sides, the hypothenuse may be easily obtained, from cor. 1. theo. 14. sect. 4.

Thus the square of 
$$AB = 50625$$
  
Add the square of  $BC = 73984$   

$$124609 (353 = AC)$$

$$9$$

$$65)346$$

$$325$$

$$703)2109$$

$$2109$$

From what has been said on logarithms, it is plain,

1. That half the logarithm of the sum of the squares of the two sides, will be the logarithm of the hypothenuse. Thus,

The sum of squ res, as before, is 124609; its log. is 5.095549, the half of which is 2.547774;

ŗ

and the corresponding number to this, in the tables, will be 353, for AC.

2. And that half of the logarithm of the difference of the squares of AC and AB, or of AC and BC, will be the logarithm of BC, or of AB.

The following examples are inserted for the exercise of the learner.

1. Given, 
$$\begin{cases} \text{the angle } C64^{\circ} 40' \\ AC & 3876 \end{cases} \begin{cases} AB \\ BC \end{cases}$$

2. Given, the angle 
$$C$$
 47° 20′  $AC$  required.

3 Given, the angle 
$$C$$
 28° 30′  $AB$  required.

4. Given, 
$$\begin{cases} AB & 2 \\ AC & 3 \end{cases}$$
 the angles required.

5. Given, 
$$\begin{cases} BC & 17 \\ AC & 21.6 \end{cases}$$
 the angles required.

6 Given, 
$$\begin{cases} AB & 2871.64 \\ BC & 3176.2 \end{cases}$$
 the angles required.

The answers are omitted, that the learner may resolve them for himself by the foregoing methods; by which means he will find and see more distinctly their mutual agreements: and become more expert, and better acquainted with the subject.

#### OBLIQUE ANGLED

## PLANE TRIGONOMETRY.

DEFORE we need to the solution of the four cases of Oblique singled triangles. It is necessary to premise the following theorems.

### THEO. I.

#### PL: 5.Ag. 10.

To any plane triungle ABC, the sides are proportional in the since of their opposite angles; that is, 8. C: AB:: 8. A: BC, and BAC: AB:: 8. A: BC, also 8. B: AC:: 8. A: BC.

By the sine of its opposite angle; but the sines of those angles, in tabular parts, are proportional to the sines of the same in any other measure; and therefore the sines of the angles will be as the halves of their opposite sides; and since the halves are as the wholes, it follows, that the sines of their angles are as their opposite sides; that is, S. C: AB::S.A:BC, &c. 2. E. D.

#### THEO. II.

#### Fig. 11.

In any plane triangle ABC, the sum of the two given sides AB and BC, including a given angle ABC, is to their difference, as the tangent of half the sum of the two unknown angles A and C is to the tangent of half their difference.

Produce AB and make HB=BC, and join HC: let fall the perpendicular BE, and that will bisect

the angle HBC (by theo. 9. sect. 4.) through B draw BD parallel to AC, and make HF=CC, and join BF; take BI=BA, and draw IG parallel to BD or AC.

It is then plain that AH will be the sum, and **HI** the difference of the sides AB and BC: and since HB=BC, and BE perpendicular to HC, therefore HE=EC (by theo. 8. sect 4.); and since BA=BI, and BD and IG parallel to AC, there are GD = DC = FH, and consequently HG = FD, and  $\frac{1}{2}HG = \frac{1}{2}FD$  or ED. Again EBC being half HBC, will be also half the sum of the angles A and C (by theo. 4. sect 4.) also, since HB, HF, and the included angle H, are severally equal to BC, CD, and the included angle BCD: therefore (by theo. 6. sect. 4.) HBF = DBC = BCA (by part 2. theo. 3. sect. 4.) and since HBD=A (by part. 3. then. 3. sect. 4.) and HBF=BCA: therefore BFD is the difference, and EBD, half the difference of the angles A and C: then making BE the radius, it is plain, that EC will be the tangent of half the sum, and ED the tangent of half the difference of the two unknown angles A and C: now Id being parallel to AC; AII: III: CH: GH. (by cor. 1. theo. 20 sect. 4.) But the wholes are as their halves, that is, AH: III: CE: ED, that is as the sum of the two sides AB and BC, is to their difference; so is the tangent of half the sum of the two unknown angles A and C, to the tangent of half their difference. 2. E. D.

#### THEO. III.

#### Fig. 12.

In any right lined plane triangle ABD; the base AD, will be to the sum of the other sides, AB, BD, as the difference of those sides, is to the difference of the segments of the base, made by the her her headicular BE; viz. the difference between AE and ED.

#### THEO. IV.

#### Fig. 13.

If to half the sum of two quantities, be added half their difference; the sum will be the greatest of them; and if from half the sum be subtracted half their difference; the remainder will be the least of them.

Let the two quantities be represented by AB and BC: (making one continued line;) whereof AB is the greatest, and BC the least; bisect the whole line AC in E; and make AD=BC; then

it is plain, that AC is the sum, and DB the difference of the two quantities; and AE or EC, their half sum, and DE or EBtheir half difference. Now if to AE we add EB, we shall have AB, the greatest quantity; and if from EC we take EB, we shall have BC the least quantity.  $\mathcal{Q}$ . E. D.

Cor. Hence, if from the greatest of two quantities, we take half the difference of them, the remainder will be half their sum; or if to half their difference be added the least quantity, their sum, will be half the sum of the two quantities.

### OBLIQUE ANGLED TRIANGLES.

#### CASE I.

TWO sides, and an angle opposite to one of them given; to find the other angles and side.

#### PL. 5. fig. 11.

In the triangle ABC, there is given AB 240, the angle A 46° 30', and BC 200; to find the angle C, being acute, the angle B, and the side AC.

## 1st. By Construction.

Draw a blank line, on which set AB 240, from a scale of equal parts; at the point A, of the line AB, make an angle of 46° 30′, by an indefinite blank line; with BC 200, from a like scale of equal parts that AB was taken, and one foot in B, describe the arc DC to cut the last blank line in the points D and C. Now if the angle C had been required obtuse, lines from D to B, and to A, would constitute the triangle; but as it is required acute,

draw the lines from C to B and to A, and the triangle ABC is constructed. From a line of chords let the angles B and C be measured; and AC from the same scale of equal parts that AB and BC were taken; and you will have the answers required.

### 2d. By Calculation.

This is performed by theo. 1. of this sect. thus;

As $BC$ = is to the sine of $A$ = So is $AB$ =	200 46°. 30′ 240	<b>2.3</b> 01 <b>030</b> 9.86056 <b>2</b> <b>2.3</b> 80211
	,	12 240773
to the sine of $C_{i}$	60°. 31′	9.939743

180°—the sum of the angles A and C, will give the angle B, by cor. 1. theo. 5. sect. 4.

180°—107°. 1'=72°. 59'=B.

As the sine of 
$$A = 46^{\circ}$$
 30' 9.860562 is to  $BC$ , = 200 2.301030 9.980555

So is the sine of  $B = 72^{\circ}$ . 59' 9.980555 12.281585 to  $AC$ , = 263. 7 2.421023

# 3d. By Gunter's Scale.

Extend from 200 to 240, on the line of numbers; that distance will reach from 46° 30′ on the line of sines, to 60° 31′ for the angle C.

. .

Extend from 46° 30', to 72° 59', on the line of sines; that distance will reach from 200 to 263.7 on the line of numbers, for AC.

Note. The method by Natural Sines will be obvious from the foregoing analogies.

#### CASE II.

Two angles and a side given; to find the other sides.

PL. 5. fig. 15.

In the triangle ABC, there is the angle A 46° 30' AB 230, and the angle B 37° 30', given to find AC and BC.

### 1st. By Construction.

Draw a blank line, upon which set AB 230, from a scale of equal parts; at the point A of the line AB, make an angle of 46° 30′, by a blank-line; and at the point B of the line AB make an angle of 37° 30′, by another blank line: the intersection of those lines gives the point C, then the triangle ABC is constructed. Measure AC and BC from the same scale of equal parts that AB was taken; and you have the answer required.

## 2d. By Calculation.

By (cor. 1. theo. 5. sect. 4.) 180°—the sum of the angles A and B=C.

A 46° 30' B 37. 30

 $180^{\circ} - 84^{\circ}$ .  $00' = 96^{\circ} 00' = C$ .

By def. 27. sect. 4. The sine of 96°=the sine of 84°, which is the supplement thereof; therefore instead of the sine of 96°, look in the tables for the sine of 84°.

# By theo. 1. of this sect.

ł	As the sine of is to AB, So is the sine	=	96° 00′ 230 46° 30′	9.997614 2.361728 9.860562
•				12.222290
•	to BC,	==	167.8	2.224676
-	As the sine of is to $AB$ , So is the sine	=	230	9.997614 <b>2.3</b> 61728 9.78444 <b>7</b>
				12.146175
•	to $AC$ ,	=	140.8	2.148561

# 3d. By Gunter's Scale.

Extend from 84° (which is the supplement of 96°) to 46° 30′ on the sines; that distance will reach from 230 to 168, on the line of numbers, for BC.

Extend from 84° to 37°. 30′, on the sines; that extent will reach from 230 to 141, on the line of numbers, for AC.

#### CASE III.

Two sides and a contained angle given; to find the other angles and side.

#### PL. 5. fig. 16.

In the triangle ABC, there is AB 240, the angle A 36° 40¢ and AC 180, given; to find the angles C and B, and the side BC.

### 1st. B. Construction.

Draw a blank line, on which from a scale of equal parts, lay  $AB \ 240$ ; at the point A of the line AB, make an angle of  $36^{\circ} \ 40'$ , by a blank line; on which from A, lay  $AC \ 180$ , from the same scale of equal parts; measure the angles C and B, and the the side BC, as before; and you have the answers required.

## 2d. By Calculation.

By cor 1. theo. 5. sect. 4.  $180^{\circ}$ —the angle A 36°.  $40' \approx 143^{\circ}$ . 20' the sum of the angles C and B: therefore half of  $143^{\circ}$ . 20', will be half the sum of the two required angles, C and B.

## By theo. 2. of this sect.

As the sum of the two sides AB and AC = 420 is to their difference, = 60

So is the tangent of half the sum of the two unknown angles C and B =  $71^{\circ}$  40° to the tangent of half their difference = 23° 20°

## By theo. 4.

To half the sum of the angles C and  $B=71^{\circ}$  40' Add half their difference as now found = 23 20.

The sum is the greatest angle, or ang. C=95 00

Subtract, and you have the least angle, or B=48 20

The angle C and B being found; BC is had, as before, by theo. 1. of this sect. Thus,

S. B: AC::S:A:BC. 48° 20': 180::36° 40:143.9.

3d. By Gunter's Scale.

Because the two first terms are of the same kind, extend from 420 to 60 on the line of numbers; lay that extent from 45° on the line of tangents, and keeping the left leg of your compasses fixed, move the right leg to 71°. 40; that distance laid from 45° on the same line will reach to 23°.30′, the half difference of the required angles. Whence the angles are obtained, as before.

The second proportion may be easily extended, from what has been already said.

CASE IV.

PL. 5. fig. 17.

The three sides given, to find the angles.

In the triangle APC, there is given, AB 64, AC 47, BC 34: the angles A, B, C, are required.

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## 1st. By Construction.

The construction of this triangle must be manifest, from prob. 1. sect. 4.

# 2d. By Calculation.

From the point C, let fall the perpendicular CD on the base AB; and it will divide the triangle into two right angled ones, ADC and CBD; as well as the base AB, into the two segments, AD and DB.

AC 47
BC 34
Sum 81
—
Difference 13

# By theo. 3. of this sect. -

As the base or the longest side, AB
is to the sum of the other sides, AC and BC, 81
So is the difference of those sides
to the difference of the segments of the base AD, DB.

64
16.46

## By theo. 4. of this sect.

To half the base, or to half the sum of the segments AD and DB.

Add half their difference, now found,

8.23

Their sum will be the greatest segment AD 40.23

Subtract, and their difference will be the least segment DB,

23.77

In the right angled triangle ADC, there is AC47, and AD40. 23, given, to find the angle A.

This is resolved by case 4. of right angled plane trigonometry, thus,

AD: R:: AC: Sec. A. 40.23: 90°:: 47: 31° 08'

Or it may be had by finding the angle ACD, the complement of the angle A; without a secant, thus,

AC: R:: AD: S. ACD. 44: 900:: 40, 23: 58° 52/

90-58° 52' = 31°. 08', the angle A.

Then by theo. I of this sect.

BC: S. A: : AC: S. B. 34: 31° 08': : 47: 45° 37.

By cor. 1. theo. 5. sect. 4.  $180^{\circ}$ —the sum of A and B=C.

A 31•.08 / B 45. 37

 $180^{\circ}$ —76.  $45 = 103^{\circ}$ . 15', the angle C.

# 3d. By Gunter's Scale,

The first proportion is extended on the line of numbers; and it is no matter whether you extend from the first to the third, or to the second term, since they are all of the same kind: If you extend to the second, that distance applied to the third, will give the fourth; but if you extend from the first to the third, that extent will reach from the second to the fourth.

The methods of extending the other proportions have been already fully treated of.

An example in each case of oblique angled triangles.

1. Given, 
$$\begin{cases} AC & 290 \\ C & 69^{\circ}.30^{\prime} \end{cases} \stackrel{A}{B}$$
 required.  $AB & 350 \end{cases} \stackrel{A}{B}C$ 

2. Given,  $\begin{cases} C & 24^{\circ}.20^{\prime} \\ B & 128^{\circ}.30 \\ AC & 3246 \end{cases} \stackrel{A}{B}C$ 

3. Given,  $\begin{cases} AC & 6 \\ C & 124^{\circ}.30^{\prime} \\ BC & 4.5 \end{cases} \stackrel{A}{A}B$  required.  $AC & 92 \\ BC & 52 \end{cases} \stackrel{A}{C}C$ 

### Additional Exercises with their Answers.

## QUESTIONS FOR EXERCISE.

1. Given the Hypothenuse 108 and the Angle opposite the Perpendicular 25° 36; required the Base and Perpendicular.

Answer. The Base is 97.4, and the Perpendicu-

lar 46.66.

2. Given the Base 96 and its opposite Angle 71° 45'; required the Perpendicular and the Hypothenuse.

Answer. The Perpendicular is 31.66 and the

Hypothenuse 101.1.

3. Given the Perpendicular 360 and its opposite Angle 58° 20'; required the Base and the Hypothenuse.

Answer. The Base is 222, and the Hypothenuse 423.

4. Given the Base 720 and the Hypothenuse 980; required the Angles and the Perpendicular.

Answer The Angles are 479 17 and 489 434

Answer. The Angles are 47° 17' and 42° 43',

and the Perpendicular 664.8

5. Given the Perpendicular 110.8 and the Hypothenuse 176.5; required the Angles and the Base.

Answer. The Angles are 38° 41' and 51° 19', and the Base 137.8.

Given the Base 360 and the Perpendicular480; required the Angles and the Hypothenuse.

Answer. The Angles are 53° 8' and 36° 52', and the Hypothenuse 600.

7. Given one Side 129, an adjacent Angle 56° 30′, and the opposite Angle 81° 36′: required the third Angle and the remaining Sides.

Answer. The third Angle is 41° 54, and the

remaining Sides are 108.7 and 87.08.

8. Given one Side 96.5, another Side 59.7, and the Angle opposite the latter Side 31° 30′: requir-

ed the remaining Angles and the third Side.

Answer. This Question is ambiguous; the given Side opposite the given Angle being less than the other given Side (see Rule I.;) hence, if the Angle opposite the Side 96.5 be acute, it will be 57° 38′, the remaining Angle 90° 52′, and the third Side 114.2; but if the Angle opposite the Side 96.5 be obtuse, it will be 122° 22′, the remaining Angle 26° 8′, and the third Side 50.32.

9. Given one Side 110, another Side 102, and the contained Angle 113° 36: required the remaining Angles and the third Side.

Answer. The remaining Angles are 3' and

31° 47', and the third Side is 177.5.

10 Given the three Sides respectively, 120.6, 125.5, and 146.7: required the Angles.

Answer. The Angles are 51° 53', 54° 58', and

73° 9 ′.

The student, who has advanced thus far in this work with diligence and active curiosity, is now prepared to study, with ease and pleasure, the following part; which comprehends all the necessary directions for the practice of Surveying.

#### PART II.

# Or the Practical Surveyor's Guide.

#### SECT. I.

Containing a particular Description of the several Instruments used in Surveying, with their respective Uses.

#### THE CHAIN.

HE stationary distance, or merings of ground, are measured either by Gunter's chain of four poles or perches, which consists of 100 links; (and this is the most natural division) or by one of 50 links, which contains two poles or perches: but because the length of a perch differs in many places, therefore the length of chains and their respective links will differ also.

The English statute-perch is  $5\frac{1}{2}$  yards, the two-pole chain is 11 yards, and the four pole one is 22 yards; hence the length of a link in a statute-chain is 7.92 inches.

There are other perches used in different parts of England, as the perch of woodland measure, which is 6 yards; that of church-land measure, which is 7 yards, and the forest measure perch, which is 8 yards.

For the more ready reckoning the links of a four-pole chain, there is a large ring, or sometimes a round piece of brass fixed at every 10 links; and at 50 links, or in the middle, there are two large rings. In such chains as have a brass piece at every 10 links, there is the figure I on the first piece, 2 on the second, 3 on the third, &c. to 9. By leading therefore that end of the chain forward, which has the least number next to it, he who carries the hinder end may easily determine any number of links : thus, if he has the brass piece number 8, next to him, and six links more in a distance, that distance is 86 links. After the same manner 10 may be counted for every large ring of a chain which has not brass pieces on it; and the number of links is thus readily determined.

The two-pole chain has a large ring at every 10 links, and in its middle, or at 25 links, there are 2 large rings; so that any number of links may be the more readily counted off, as before.

The surveyer should be careful to have his chain measured before he proceeds on business, for the rings are apt to open by frequently using it, and its length is thereby increased, so that no one can be too circumspect in this point.

In measuring a stationary distance, there is an object fixed in the extreme point of the line to be measured; this is a direction for the hinder chainman to govern the foremost one by, in order that the distance may be measured in a right line; for if the hinder chainman causes the other to cover the object, it is plain the foremost is then in a right line towards it. For this reason it is necessary to have a person that can be relied on, at the hinder

end of the chain, in order to keep the foremost man in a right line; and a surveyor who has no such person, should chain himself. The inaccuracies of most surveys arise from bad chaining, that is, from straying out of the right line, as well as from other omissions of the hinder chainman: no person, therefore, should be admitted at the hinder end of the chain, of whose abilities in this respect, the surveyor was not previously convinced; since the success of the survey, in a grest measure, depends on his care and skill.

In setting out to measure any stationary distance. the foreman of the chain carries with him 10 iron pegs pointed, each about ten inches long; and when he has stretched the chain to its full length, he at the extremity thereof sticks one of those pegs perpendicularly in the ground; and leaving it there, he draws on the chain till the hinder man checks him when he arrives at that peg: the chain being again stretched, the fore man sticks down another peg, and the hind man takes up the former ; and thus they proceed at every chain's length contained in the line to be measured, counting the surplus links contained between the last peg, and the object at the termination of the line, as before: so that, the number of pegs taken up by the hinder chainman, expresses the number of chains; to which, if the odd links be annexed, the distance line required in chains and links is obtained, which must be registered in the field book, as will hereafter be shewn.

If the distance exceeds 10, 20, 30, &c. chains, when the leader's pegs are all exhausted, the hinder chainman, at the extremity of the 10 chains, delivers him all the pegs; from whence they pro-

oced to measure as before, till the leader's pegs are again exhausted, and the hinder chainman at the extremity of these 10 chains again delivers him the pegs; from whence they proceed to measure the whole distance line in the like manner; then it is plain, that the number of pegs the hinder chainman has, being added to 10, if he had delivered all the pegs once to the leader, or to 20 if twice, or to 30 if thrice, &c. will give the number of chains in that distance; to which if the surplus links be added, the length of the stationary distance is known in chains and links.

It is customary, and indeed necessary, to have red, or other coloured cloth fixed to the top of each peg, that the hinder man at the chain may the more readily find them; otherwise, in chaining through corn, high grass, briars, rushes, &c. it would be extremely difficult to find the pegs which the leader puts down: by this means no time is lost, which otherwise must be, if no cloths are fixed to the pegs, as before.

It will be necessary here to observe, that all slant, or inclined surfaces, as sides of hills, are measured horizontally, and not on the plane or surface of the hill, and is thus affected.

# PL. 8. fig. 4.

Let ABC be a hill, the hindmost chainman is to hold the end of the chain perpendicularly over the point A (which he can the better effect with a plummet and line, then by letting a stone drop, which is most usual) as d is over A, while the leader puts down his peg at e: the eye can direct the horizontal position near enough, but if greater accuracy

end of the chain, in order man, in a right line; and such person, should chain case of most surveys arise to their other ormstons of the history or the chain of the right of the chain of the line of the chain of the chain of the chain of the survey, was not previous to the survey, the surveys of the surveys.

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# PROB. II.

e chains and links, to two-hole once.

o; to which annex the links, if o: but if they exceed 50, douone to them, and take 50 from mainder will be the links, thus,

four-pole chains, how many two-pole ones?

our-pole chains, how many -pole ones?

Wer.

# B. 111.

t links, to perches and decimals perch.

the hundreth part of a min and links be multiplied chain) the product will parts of a perch. To

Ch. L. s in 13. 64 of for

Answer 54, 56 perches,

of page on

m bintle

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or to 30

be atded,

the more through aid be exhe leader it, which the pegs,

measured ace of the

over the that a plant cop, which the brushes accurate

are measured by a statute chain, it will give you the miles English, but if by a plantation chain, the miles will be Irish. Hence an English mile contains 1760, and an Irish m le 2240 yards; and because 14 half yards is an Irish, and 11 half yards is an Linglish perche, therefore 11 Irish perches, or Irish miles, are equal to 14 English ones.

Since some surveys are taken by a four-pole, and others by a two-pole chain; and as ground for houses is measured by feet, we will shew how to reduce one to the other, in the following problems.

## PROB. I.

To reduce two-pole chains and links to four-pole ones.

If the number of chains be even, the half of them will be the four-pole ones, to which annex the given links, thus,

Ch. L.
1. In 16. 37 of two-pole chains, how many four-pole ones?

Ch. L. Answer 8. 37.

But if the number of chains be odd, take the half of them for chains, and add 50 to the links, and they will be four-pole chains and links, thus,

2. In 17. 42 of two-pole chains, how many four-pole ones?

Ch. L. Answer 8. 92.



### PROB. II.

To reduce four-pole chains and links, to two-pole ones.

Double the chains, to which annex the links, if they be less than 50; but if they exceed 50, double the chains, add one to them, and take 50 from the links, and the remainder will be the links, thus,

Ch. 1. In 8. 2	L. 37	of four-pole of	chains, how les?	many
16	.37		•	
-				

2. In 8. 82 of four-pole chains, how many 2. 50 two-pole ones?

17. 32 Answer.

#### PROB. III.

To reduce four-pole chains and links, to perches and decimals of a perch.

The links of a four-pole chain are decimal parts of it, each tink before the hundreth part of a chain; therefore if the chain and links be multipled by 4, (for 4 perches are a chain) the product will be the perches and decimal parts of a perch. Thus,

How many perches in 13. 64 of four-pole chains,

Answer 54. 56 perches,

### PROB. IV.

To reduce two-pole chains and links, to perches and decimals of a perch.

They may be reduced to four-pole ones (by prob. 1.) and thence to perches and decimals (by the last.) or,

If the links be multiplied by 4, carrying one to the chains, when the links are, or exceed 25; and the chains by 2, adding one, if occasion be: the product will be perches, and decimals of a perch. Thus,

Ch. L.

1. In 17. 21 of two-pole chains, how many
2. 4 perches.

Answer, 34. 84 perches.

Ch. L.

2. In 15. 38 of two-pole chains, how many

2. 4 perches?

Answer, 31. 52 perches.

#### PROB. V.

To reduce perches, and decimals of a perch, to four-pole chains and links.

Divide by 4, so as to have two decimal places in the quotient, and that will be four-pole chains and links. Thus, In 31. 52 perches, how many four-pole chairs and links?

Ch. L. 4)31.52(7. 88 Answer,

35

## PROB. VI.

To reduce perches and decimals of a perch, to two-pole chains and links.

The perches may be reduced to four-pole chains (by the last) and from thence to two-pole chains (by prob. 2.) or,

Divide the whole number by 2, the quotient will be chains; to the remainder annex the given decimals, and divide by 4, the last quotient will be the links. Thus,

In 31.52 perches, how many two-pole chains and links?

Ch. L. 2)31.52(15. 38 Answer.

11 4)152(38 32

### PROB. VII.

To reduce chains and links, to feet and decimal parts of a foot.

If they be two-pole chains, reduce them to fourpole ones: (by prob. 1.) these being multiplied by the feet in a four-pole chain, will give the feet and decimals of a foot. Thus,

Ch. L. In 17. 21 of two-pole chains, how many feet?

Ch. L.

8. 71 of four-pole chains. 66 feet = 1 chain.

5226. Feet Inches 5226 Answer 574. 104.

Feet 574.86

12

Inches 10.32

4.

1.28

## PROB. VIII.

To reduce feet and inches to chains and links.

Reduce the inches to the decimal of a foot, and annex that to the feet; that divided by the feet in a four-pole chain, will give the four-pole chains and links in the quotient: these may be reduced to twopole chains and links, if required, by prob. 2. Thus,

Feet. Inches.

In 217. 9 how many two-pole chains? 12)9.00.(75 the decimal of 9 inches.

60

66)217.75(3. 29 of four-pole chains, or

197 655 6. 29 61

How to take a Survey by the CHAIN only.

#### PROB. I.

To survey a piece of ground, by going round it, and the method of taking the angles of the field, by the chain only.

## P1. 6. fig. 6.

Let ABCDEFG be a piece of ground to be surveyed: beginning at the point A, let one chain be laid in a direct line from A, towards G, where let a peg be left, as at c; and again, the like distance from A in a direct line towards B, where another peg is also to be left, as at d: let the distance from d to c he measured, and placed in the field-book, in

the second column under the denomination of angles, in a line with station No. 1; and in the same line, under the title of distances, in the third column, let the measure of the line AB in chains and links be inserted. Being now arrived at B, let one chain be laid in a direct line from B towards A, where let a peg be left, as at f, and again, the like distance from B in a direct line towards C, where let also another peg be left, as at e; the distance from e to f is to be inserted in the field-book in the second column, under angles, in a line with station No. 2; and in the same line, under the title of distances in the third column, let the measure of the line BC, in chains and links, he inserted; after the same manner we may proceed from C to D, and thence to E; but because the angle at E, viz FED, is an external angle, after having laid one chain from E to h, and to g, the distance from g to his measured, and inserted in the column of angles, in a line with station No. 5, and on the side of the field-book against that station, we make an asterisk, thus \*, or any other mark, to signify that to be an external angle, or one measured out of the ground. Proceed we then as before, from E to F, to G, and thence to A, measuring the angles and distances, and placing them as before, in the field-book, opposite to their respective stations; so will the fieldbook be completed in manner following.

N. B. After this manner the angles for inaccessible distances may be taken, and the method of constructing or laying them down, as well as the construction of the map, from the following field-notes, must be obvious from the method of taking them.

The form of the field-book, with the title.

A field-book of part of the land of Grange, in the parish of Portmarnock, barony of Coolock, and county of Dublin; being part of the estate of L. P. Esq. let to C. D. farmer. Surveyed January, 30, 1782.

Taken by a four pole chain.

Remarks	No. Sta.	Angles Gh. L.	Distan. Ch. L.
Mr. J. D's part of Grange	1	1 80	17.65
Mr. L.P's partof Portmarnock	3	1.79 1.76	18.50 28.00
strand *	4 5	1.411	<b>20.00</b> 14.8 <b>3</b>
Widow J. G's part of Grange	6	1 14	19.41
		1 89	24.53

# Explanation of the remarks.

Mr. J. D's part of Grange bounds, or is adjacent to the surveyed land from the first to the third station; Mr. L. P's part of Portmarnock bounds it from the third to the fourth station; the strand then is the boundary from thence to the sixth, and from the sixth to the first station, the widow J. G's part of Grange is the boundary.

It is absolutely necessary to insert the persons' names, and town-lands, strands, rivers, bogs, rivulet's, &c. which bound or circumscribe the land which is surveyed, for these must be expressed in the map.

In a survey of a town-land, or estate, it is sufficient to mention only the circumjacent town-lands, without the occupiers' names: but when a part only of a town-land is surveyed, then it is necessary to insert the person or persons' names, who hold any particular parcel or parcels, of such townland, as bound the parts surveyed.

When an angle is very obtuse, as most in our present figure, are, viz. the angles at A, B, C, E, and G: it will be best to lay a chain from the angular point as at A, on each of the containing sides to c and to d; and any where nearly in the middle of the angle as at c: measuring the distances cc and ed; and these may be placed for the angle in the field book. Thus.

For when an angle is very obtuse, the chord line, as ed, will be nearly equal to the radii Ac and Ad; so if the arc ced be swept, and the chord line ed be laid on it, it will be difficult to determine exactly that point in the arc where ed cuts it; but if the angle be taken in two parts, as ce the arc, and the angle thence may be truly determined and constructed.

After the same manner any piece of ground may be surveyed by a two-pole chain.

#### PROB. II.

To take a survey of a piece of ground from any point within it, from whence all the angles can be seen; by the chain only.

#### PL. 6. fig. 6.

Let a mark be fixed at any point in the ground as at H, from whence all the angles can be seen; let the measures of the lines HA, HB, HC, &c. be taken to every angle of the field from the point H; and let those be placed opposite to No. 1, 2, 3, 4, &c. in the second column of the radii: the measures of the respective lines of the mearing, viz AB, BC, CO, DE &c. being placed in the third column of distances, will complete the field-book. Thus,

No. Ridii. Distan. Ch. L. Ch. L.
1 20.00 17.65
2 21.72 18 50
3 21 74 28 00
4 25.34 20.00
5 17.20 14.83
6 29.62 19.41
7 21.20 24.53

If any line of the field be inaccessible, as suppose CD to be, then by way of proof that the distance CD is true, let the measure of the angle CHD be taken by the line oo, with the chain: if this angle corresponds with its containing sides, the length of the line DC is truly obtained, and the whole work is truly taken.

Note, That in setting off an angle it is necessary to use the largest scale of equal parts, viz. that of the inch, which is diagonally divided into 100 parts, in order that the angle should be accurately laid down; or if two inches were thus divided for angles, it would be the more exact; for it is by no means necessary that the angles should be laid from the said scale with the stationary distances.

## PROB. III.

To take a survey by the chain only, when all the angles cannot be seen from one point within.

## PL. 6. fig. 7.

Let the ground to be surveyed be represented by 1, 2, 3, 4, & c. Since all the angles cannot be seen from one point, let us assume 3 points, as A, B, C, from whence they may be seen; at each of which let a mark be put, and the respective sides of the triangle be measured and set down in the field-book; let the distance from A to 1, and from B to 1, be measured, and these will determine the point I; let the other lines which flow from A, B, C, as well as the circuit of the ground, be then measured as the figure directs; and thence the map may be easily constructed.

There are other methods which may be used; as dividing the ground into triangles, and measuring the 3 sides of each; or by measuring the base and perpendicular of each triangle. But this we shall speak of hereafter.

### PROB. IV.

How to take any inaccessible distance by the chain only.

PL. 8. fig. 8.

Suppose AB to be the breadth of a river, or any other inaccessible distance, which may be required.

ŧ,

Let a staff or any other object be set at B, draw yourself backward to any convenient distance C, so that B may cover A: from B, lay off any other distance by the river's side to E, and complete the parallelogram EBCD: stand at D, and cause a mark to be set at F, in the direction of A; measure the distance in links from E to F, and FB will be also given. Wherefore EF:ED::FB:AB. Since it is plain (from part 1. theo. 3. sect. 4. and theo. 2. sect. 4.) the triangles EFDBFA. are mutually equiangular.

If part of the chain be drawn from B to C, and the other part from B to E; and if the ends at E and C be kept fast, it will be easy to turn the chain over to D, so as to complete a parallelogram; by reckoning off the same number of links you had in BC, from E to D, and pulling each part straight.

#### THE

### CIRCUMFERENTOR.

HIS instrument is composed of a brass circular box, about five or six inches in diameter; within which is a brass ring, divided on the top into 360 degrees, and numbered 10, 20, 30, &c. to 360: in the centre of the box is fixed a steel pin finely pointed, called a centre-pin, on which is placed a needle touched by a loadstone, which always retains the same situation; that is, it always points to the North and South points of the horizon nearly, when the instrument is horizontal, and the needle at rest.

The box is covered with a glass lid, in a brass rim, to prevent the needle being disturbed by wind or rain, at the time of surveying: there is also a brass lid or cover, which is laid over the former to preserve the glass in carrying the instrument.

This box is fixed by screws, to a brass index, or ruler, of about 14 or 15 inches in length, to the ends whereof are fixed brass sights, which are screwed to the index, and stand perpendicular thereto: in each sight is a large and a small aperture, or slit, one over the other; but these are changed, that is if the large aperture be uppermost in the one sight, it will be lowest in the other, and

so of the small ones: therefore the small aperture in one is opposite to the large one in the other; in the middle of which last, there is placed a horse hair, or fine silk thread.

The justrument is then fixed on a ball and socket; by the help of which and a screw, you can readily fix it horizontally in any given direction; the socket being fixed on the head of a three-legged staff, whose legs, when extended, support the instrument whilst it is used.

To take field notes by the Circumferentor-

Pt. 6. fig. 6.

Let your instrument be fixed at any angle, as A, your first station; and let a person stand at the next angle B, or cause a staff, with a white sheet, to be set there perpendicularly for an object to take your view to: then having placed your instrument horizontally (which is easily done by turning the box so that the ends of the needle may be equidistant from its bottom, and it traverses or plays freely) turn the flower-de-luce, or north part of the box, to your eye, and looking through the small aperture, turn the index about, till you cut the person or object in the next angle B, with the horse hair, or thread of the opposite sight: the degrees then cut by the south end of the needle, will give the number to be placed in the second column of your field-book in a line with station No. 1, and expresses the number of degrees the stationary line is from the north, counting quite round with the sun.

Most needles are pointed at the south end, and have a small ring at the north; such needles are

better than those which are pointed at each end, because the surveyor cannot mistake by counting to a wrong end; which error may be frequently committed, in using a two-pointed needle.

Two-pointed needles have sometimes a ring, but more usually a cross towards the north end: and the south end is generally bearded towards its extremity, and sometimes not, but its arm is a naked right line from the cap at the centre.

Having taken the degrees or bearing of the first stationary line AB, let the line be measured, and the length thereof in chains and links be inserted in the third column of your field-book, under the title of distances, opposite to station No. 1.

It is customary, and even necessary, to cause a sod to be dug up at each station, or place where you fix the instrument: to the end, that if any error should arise in the field-book, it may be the more readily adjusted and corrected, by trying over the former bearings and stationary distances.

Having done with your first station, set the instrument over the hole or spot where your object stood, as at B, for your second station, and send him forward to the next angle of the field, as at C; and having placed the instrument in an horizontal direction, with the sights directed to the object at C, and the north of the box next your eye, count your degrees to the south end of the needle, which register in your field-book, in the second column opposite to station No. 2; then measure the stationary distance BC, which insert in the third column, and thus proceed from angle to angle, sending your object before you, till you

return to the place where you began, and you will have the field-book complete; observing always to signify the parties names who hold the contiguous lands, and the names of the town-lands, rivers, roads, swamps, lakes, &c. that bound the land you survey, as before; and this is the manner of taking field-notes by what is called foresights.

But the generality of mearsmen frequently set themselves in disadvantageous places, so as often to occasion two or more stations to be made, where one may do, which creates much trouble and loss of time; we will therefore shew how this may be remedied, by taking back-sights, thus : let your object stand at the point where you begin your survey, as at A; leaving him there, proceed to your next angle B, where fix your instrument so, that you may have the longest view possible towards C. Having set the instrument in an horizontal position, turn the south part of the box next your eye, and having out your object at A, reckon the degrees to the south point of the needle, which will be the same as if they were taken from the object to the instrument, the direction of the index being the same. Let the degree be inserted in the fieldbook, and the stationary distance be measured and annexed thereto, in its proper column; and thus proceed from station to station, leaving your object in the last point you left, till you return to the first station A.

By this method your stations are laid out to the best advantage, and two men may do the business of three, for one of those who chain, may be your object; but in fore-sights, you must have an object before you, besides two chainmen. It was said before, that a surveyor should have a person with him to carry the hinder end of the chain, on whom he can depend: this person should be expert and ready at taking off-sets, as well as exact in giving a faithful return of the length of every stationary line. One who has such a person, and who uses back sights, will be able to go over near double the ground he could at the same time, by taking fore-sights, because of overseeing the chaining; for should he take back-sights, he must be obliged, after taking his degree, to go back to the foregoing station, to oversee the chaining, and by this means to walk three times over every line, which is a labour not be borne.

Or a back and a fore-sight may be taken at one station, thus; with the south of the box to your eye, observe from B the object A, and set down the degree in your field-book, cut by the south end of the needle. Again from B observe an object at C, with the north of the box to your eye, and set down the degree cut by the south point of the needle, so have you the bearings of the lines AB and BC; you may then set up your instrument at D, from whence take a back-sight to C, and a fore-sight to E: thus the bearings may be taken quite round, and the stationary distances being annexed to them, will complete the field-book.

But in this last method, care must be taken to see that the sights have not the least cast on either side; if they have, it will destroy all: and yet with the same sights you may take a survey by fore sights, or by back-sights only, with as great truth as if the sights were ever so erect, provided the same cast continues without any alteration; but upon the whole, back sights only will be found the readiest method.

If your needle be pointed at each end, in taking fore-sights, you may turn the north part of the box to your eye, and count your degrees to the south part of the needle, as before; or you may turn the south of the box to your eye, and count your degrees to the north end of the needle.

But in back-sights you may turn the north of the box to your eye, and count your degrees to the north point of the needle; or you may turn the south of the box to your eye, and count your degrees to the south end of the needle.

The brass ring in the box is divided on the side into 360 degrees, thus; from the north to the east into 90, from the north to the west into 90, from the south to the east into 90, and from the south to the west into 90 degrees; so the degrees are numbered from the north to the east or west, and from the south to the east or west.

The manner of using this part of the instrument is this; having directed your sights to the object, whether fore or back, as before, observe the two cardinal points of your compass, the point of the needle lies between, (the north, south, east and west being called the four cardinal points, and are graved on the bottom of the box) putting down those points, together by their initial letters, and thereto annexing the number of degrees, counting from the north or south, as before, thus; if the point of your needle lies between the north and east, north and west, south and east, or south and west points in the bottom of the box, then put down NE. NW, SE, or SW, annexing thereto the number of degrees cut by the needle on the side of the ring, counting from the north or south as before.

But if the needle point exactly to the north, south, east, or west, you are then to write down N, S, E, or W, without annexing any degree.

This is the manner of taking field notes, whereby the content of ground may be universally determined by calculation; and they are said to be taken by the quartered compass, or by the four mineties.

To find the number of degrees contained in any given angle.

Set up your instrument at the angular point, and thence direct the sights along each leg of the angle, and note down their respective bearings, as before; the difference of these bearings, if less than 180, will be the quantity of degrees contained in the given angle; but if more, take it from 360, and the remainder will be the degrees contained in the given angle.

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#### THE

### THEODOLITE.

HIS instrument is a circle, commonly of brass, of ten or twelve inches in diameter, whose limb is divided into 360 degrees, and those again are subdivided into smaller parts, as the magnitude of it will admit; sometimes by equal divisions, and sometimes by diagonals, drawn from one concentric circle of the limb to another.

In the middle is fixed a circumferentor, with a needle; but this is of little or no use, except in finding a meridian line, or the proper situation of the land.

Over the brass circle is a pair of sights, fixed to a moveable index, which turns on the centre of the instrument, and upon which the circumferentor box is placed.

This instrument will either give the angles of the field, or the bearing of every stationary distance line, from the meridian; as the circumferentor and quartered compass do.

To take the angles of the field.

PL. 6. fig. 6.

Lay the ends of your index to 360°, and 180°; turn the whole about with the 360 from you; direct

the sights from A to G, and screw the instrument fast ; direct them from A, to cut the object at B; the degree then cut by that end of the index which is opposite you, will be the quantity of the angle GAB, to place in your field-book; to which annex the measure of the line AB, in chains and links : set up your instrument at B, unscrew it, and lay the ends of your index to 360 and 180; turn the whole about with the 360 from you, or 180 next you, till you cut the object at A; screw the instrument fast, and direct your sights to the object at C. and the degree then cut by that end of the index which is opposite to you, will be the quantity of Thus proceed from station to the angle ABC. station, still laying the index to 360, turning it from you, and observing the object at the foregoing station, screwing the instrument fast, and observing the object at the following station, and counting the degrees to the opposite end of the index, will give you the quantity of each respective angle.

## LEMMA.

All the angles of any polygon, are equal to twice as many right angles as there are sides less by four. Thus, all the angles A, B, C, D, E, F, G, are equal to twice as many right angles as there are sides in the figure, less by four.

# PL. 6. fig. 6.

Let the polygon be disposed into triangles, by lines drawn from any assigned point H within it, as by the lines HA, HB, HC, &c. It is evident then (by theo. 2. sect. 4 part 1.) that the three angles of each triangle are equal to two right; and consequently, that the angles in all the triangles are twice as many right ones as there are sides:

but all the angles about the point H, are equal to four right (by cor. 2. theo. 1. sect. 4.); therefore the remaining angles are equal to twice as many right ones as there are sides in the figure, abating four. 2. E. D.

## SCHOLIUM.

Hence we may know if the angles of a survey be truly taken; for if their sum be equal to twice as many right angles, as there are stations, abating four right angles, you may conclude that the angles were truly taken, otherwise not.

If you take the bearing of any line with the circumferentor, that bearing will be the number of degrees the line is from the north; consequently the north must be a like number of degrees from the line, and thus the north, and of course the south, as well as the east and west, or the situation of the land, is obtained.

To take the bearing of each respective line from the meridian; or to perform the office of the circumferentor, or quartered compass by the theodolite.

Set your instrument at the first station, and lay the index to 360° and 180°, with the flower-de-luce of the box next 360; unscrew the instrument, and turn the whole about, till the north and south points of the needle cut the north and south points in the box; then screw it fast, and the instrument is north and south, if there be no variation in the needle; but if there be, and its quantity known, it may be easily allowed.

The circumferentor-box may then be taken off.

Direct the sights to the object at the second station and the degree cut by the opposite end of the polices will be the bearing of that line from the north, and the same that the circumferentor would

After having measured the stationary distance, set up your instrument at the second station ; unscrew it, and set either end of the index to the deoree of the last line, and turning the whole about with that degree towards you, direct your sights to an object at the foregoing station, and screw the instrument fast; it will then be parallel to its former situation, and consequently north and south; direct then your sights to an object at the following station, and the degree cut by the opposite end of index, will be the bearing of that line.

In like manner you may proceed through the whole.

If the brass circle be divided into four nineties, from 360 and 180, and the letters N, S, E, W, be applied to them; the bearings may be obtained by putting down the letters the far or opposite end of the index lies between, and annexing thereto the degrees from the N. or S; and this is the same as the quartered compass.

If you keep the compass box on, to see the mutual agreement of the two instruments; after having fixed the theodolite north and south, as before; turn the index about with the north end or flowerde-luce next your eye, and count the degree to the opposite, or south end of the index, and this will correspond with the degree cut by the south end of the needle.

At the second, or next station, unscrew the instrument, and set the south of the index to the degree of the last station; turn the whole about, with the south of the index to you, and cut the object at the foregoing station; screw the instrument fast, and with the north of the index to you, cut the object at the next following station, the degree then cut by the south of the index, will correspond with the degree cut by the south end of the needle, and so through the whole.

Some theodolites have a standing pair of sights fixed at 360 and 180, besides those on the moveable index; if you would use both, look through the standing sights, with the 180 next you, to an object at the foregoing station: screw the instrument fast, and direct the upper sights on the moveable index, to the object at the following station, and the degree cut by the opposite end of the index, will give you the quantity of the angle of the field.

Two pair of sights can be of no use in finding the angles from the meridian; and inasmuch as one pair is sufficient to find the angles of the field, the second can be of no use: besides, they obstruct the free motion of the moveable index, and therefore are rather an incumbrance than of any real use. Some will have it, that they are useful with the others, for setting off a right angle, in taking an off-set: and surely this is as easily performed by the one pair on the moveable index: thus, if you lay the index to 360 and 180, and cut the object either in the last or following station, screw the instrument fast, and turn the index to 90 and 270, and then it will be at right angles with the line. So that the small sights, at those of the circle, can be

of no additional use to the instrument, and therefore should be laid aside as useless.

This instrument may be used in windy and rainy weather, as well as in mountainous and hilly grounds; for it does not require an horizontal position to find the bearing, or angle, as the needle doth; and therefore is preferred to any instrument that is governed by the needle.

### THE SEMICIRCLE.

HIS instrument, as its name imports, is a half circle, divided from its diameter into 180 degrees, and from thence again, that is, from 0, to 360 degrees: it is generally made of brass, and is from 8 to 18 inches diameter.

On the centre there is a moveable index with sights, on which is placed a circumferentor-box, as in the theodolite.

This instrument may be used as the theodolite in all respects; but with this difference, when you are to reckon the degree to that end of the index which is off the semicircle, you may find it at the other end, reckoning the degree from 180 forwards.

#### THE

#### PLANE TABLE.

PLANE TABLE is an oblong of oak, or other wood, about 15 inches long, and 12 broad; they are generally composed of 3 boards, which are easily taken asunder, or put together, for the convenience of carriage.

There is a box frame, with 6 joints in it, to take off and put on as occasion serves; it keeps the table together, and is likewise of use to keep down a sheet of paper which is put thereon.

The outside of the frame is divided into inches and tenths, which serve for ruling parallels or squares on the paper, or for shifting it, when occasion serves.

The inside of the frame is divided into 360 degrees, which, though unequal on it, yet are the degrees of a circle produced from its centre, or centre of the table, where there is a small hole.

The degrees are subdivided as small as their distance will admit; at every tenth degree are two numbers, one the number of degrees, the other its complement to 360.

There is another centre hole about 1 of the table's breadth from one edge, and is in the mid-

dle between the two ends. To this centre hole on the other side of the frame, there are the divisions of a semicircle, or 180 degrees; and these again are subdivided into halves, or quarters, as the size of the instrument will admit.

That side of the frame on which the 360 degrees are, supplies the place of a theodolite, the other, that of a semicircle.

There is a circumferentor-box of wood, with a paper chart at the bottom, applied to one side of the table by a dove-tail joint, fastened by a screw. This box (besides its rendering the plane table capable of answering the end of a circumferentor) is very useful for placing the instrument in the same position every remove.

There is a brass ruler or index, of about two inches broad, with a sharp or fiducial edge, at each end of which is a sight; on the ruler are scales of equal parts, with and without diagonals, and a scale of chords; the whole is fixed on a ball and socket, and set on a three-legged staff.

## To take the angles of a field by the table.

Having placed the instrument at the first station, turn it about till the north end of the needle be over the meridian, or flower-de-luce of the box, and there screw it fast. Assign any convenient point, to which apply the edge of the index, so as through the sights you may see the object in the last station, and by the edge of the index from the point draw a line. Again, turn about the index with its edge to the same point, and through the sights ob-

serve the object in the second station, and from the point, by the edge of the index, draw another line; so is the angle laid down; on that last line set off the distance to the second station, in chains and links: apply your instrument to the second station, taking the angle as before; and after the like manner proceed till the whole is finished.

This method may be used in good weather, if the needle be well touched and play freely; but if it be in windy weather, or the needle out of order, it is better, after having taken the first angle as before, and having removed your instrument to the second station, and placed the needle over the meridian line as before, to lay the index on the last drawn line, and look backward through the sights; if you then see the object in the first station, the table is fixed right, and the needle is true; if not, turn the table about, the index lying on the last line, till through the sights you see the object in the first station: and then screw it fast, and keeping the edge of the index to the second station, direct your sights to the next; draw a line by the edge of the index, and lay off the next line; and prccced through the whole without using the needle, as you do with the theodolite.

If the sheet of paper on the table be not large enough to contain the map of the ground you survey, you must put on a clean sheet, when the other is full; and this is called shifting of paper, and is thus performed.

PL. 6. fig. 8.

Let ABCD represent the sheet of paper on the plane table, upon which the plot E, F, G, H, I,

K, L, M, is to be drawn; let the first station be E; proceed as before from thence to F, and to G; then proceeding to H, you find there is not room on your paper for the line GH; however, draw as much of the line GH, as the paper can hold, or draw it to the paper's edge. Move your instrument back to the first station E, and proceed the contrary way to M, and to L; but in going from thence to K, you again find your sheet will not hold it; however, draw as much of the line LK on the sheet as it can hold.

Take that sheet off the table, first observing the distance oo of the lines GH and LK, by the edge of the table; take off that sheet, and mark it with No. 1, to signify it to be the first taken off: Having then put on another sheet, lay that distance oo on the contrary end of the table, and so proceed as before, with the residue of the survey; from o to H, to K, and thence to o; so is your survey complete.

In the like manner you may proceed to take ofi, and put on, as many sheets as are convenient; and these may afterwards be joined together with mouth glue, or fine white wafer, very thin.

If the index be fixed to the first centre, using the 360 side, it will then serve as a theodolite, and when to the second centre, using the 180 side, it will serve as a semicircle; by either of which you may survey in rainy weather, when you cannot have paper on the table.

TO MEASURE ANGLES OF ALTITUDE BY THE CIRCUMFERINTOR, THEODOLITE, SEMICIRCLE, OR PLANE TABLE.

1. To take an angle of altitude, by the circumferentor.

LET the glass lid be taken off, and let the instrument be turned on one side, with the stem of the ball into the notch of the socket, so that the circle may be perpendicular to the plane of the horizon; let the instrument be placed in this situation before the object, so that the top thereof may be seen through the sights; let a plummet be suspended from the centre pin, and the object being then observed, the complement of the number of degrees, comprehended between the thread of the plummet, and that part of the instrument which is next your eye, will give the angle of altitude required.

2. If an angle of altitude is to be taken by the theodolite, or semicircle, let a thread be run through a hole at the centre, and a plummet be suspended by it; turn the instrument on one side, by the help of the ball and notch in the socket for that purpose, so that the thread may cut 90, having 360 degrees next you; screw it fast in that position, and through the sights cut the top of the objects; and the degrees then cut by the end of the index next you, are the degrees of elevation required. An angle of depression is taken the contrary way.

# 170 OF ANGLES OF ELEVATION, &c.

3. By the plane table an angle of altitude is taken in the like manner, by suspending a plummet from the centre thereof, having turned the table on one side, and fixed the index to the centre by a screw, so as to move freely, let the thread cut 90, look through the sights as before, and you have the angle of elevation, and on the contrary that of depression THE THE

# PROTRACTOR.

THE protractor is a semicircle annexed to a scale, and is made of brass, ivory, or horn; its diameter is generally about five or six inches.

The semicircle contains three concentric semicircles at such distances from each other, that the spaces between them may contain figures.

The outward circle is numbered from the right to the left hand, with 10, 20, 30, &c. to 180 degrees; the middlemost the same way, from 180 to 360 degrees; and the innermost from the upper edge of the scale both ways, from 10, 20, 30, &c. to 90 degrees.

It is easy to conceive that the protractor, though a semicircle, may be made to supply the place of a whole circle; for if a line be drawn, and the centre-hole of the protractor be laid on any point in that line, the upper edge of the scale corresponding with that line, the divisions on the edge of the semicircle will run from 0 to 180, from right to left; again, if it be turned the other way, or downwards, keeping the centre-hole thereof on the aforesaid point in the line, then the divisions will run from

in the con-

180 to 360, and so completes an entire circle with the former semicircle.

The use of the protractor is to lay off angles, and to delineate or draw a map, or plan, of any ground from the field notes; and is performed in the following manner.

To protract a field-book, when the ungles are taken from the meridian.

# Pr. 6. fig. 9.

On your paper rule lines parallel to each other, at an inch asunder (being most usual), or at any other convenient distance; on the left end of the parallels put N. for north, and on the right S. for south; put E. at the top for east, and W. at the bottom of your paper for west.

Then let the following field-book be that which is to be protracted, the bearings being taken from the meridian, whether by a circumferentor, theodolite, or semicircle, and measured with a two-pole chain.

No.	Bearing.	Ch. L.
16	2831	55.20
2	3483	12.36
3	317	29.20
4	12661011	55,20
115	193	40.00
6	124	76.00
17	684	87.02
Close at the first station		

Soul tout dist

Pitch upon any convenient point on your paper for your first station, as at 1, on which lay the centre-hole of your protractor, with a protracting-pin; then if the degrees be less than 180, turn the arc of your protractor downwards, or towards the west; but if more than 180, upwards, or towards the east.

Or if the right hand be made the north, and the left the south, the west will be then up, and the east down.

In this case, if the degree be less than 180, turn the arc of your protractor upwards, or towards the west; and if more, downwards, or towards the east.

By the foregoing field-book, the first bearing is 2834, turn the arc of your protractor upwards, keeping the pin in the centre-hole, move the protractor so that the parallel lines may cut opposite divisions, either on the ends of the scale, or on the degrees, and then it is parallel. This must be always first done, before you lay off your degrees.

Then by the edge of the semicircle, keeping the protractor steady, with the pin prick the first bearing 283 ½ and from the centre point, through that point or prick, draw a blank line with the pin, on which from a scale of equal parts, or from the scale's edge of the protractor, lay off the distance 55C. 20L. so is that station protracted.

At the end of the first station, or at 2, which is the beginning of the second, with the pin place the centre of the protractor, turning the arc up, because the bearing of the second station is more

than 180, viz. 348. Place your protractor parallel as before, and by the edge of the semicircle, with the pin prick at that degree, through which and the end of the foregoing station, draw a blank line, and on it set the distance of that station.

In the like manner proceed through the whole, only observe to turn the arc of your protractor down, when the degrees are less than 180.

If you lay off the stationary distances by the edge of the protractor, it is necessary to observe, that if your map is to be laid down by a scale of 40 perches to an inch, every division on the protractor's edge will be one two-pole chain; ‡ a division will be 25 links, and ‡ of a division will be 12½ links.

If your map is to be laid down by a scale of 20 perches to an inch, two divisions will be one two-pole chain; one division will be 25 links; \(\frac{1}{2}\) a division 12\(\frac{1}{2}\) links, and \(\frac{1}{2}\) of a division will be 6\(\frac{1}{2}\) links.

In general, if 25 links be multiplied by the number of perches to an inch, the map is to be laid down by, and the product be divided by 20 (or which is the same thing, if you cut off one and take the half), you will have the value of one division on the protractor's edge, in links and parts.

# EXAMPLES.

1. How many links in a division, if a map be laid down by a scale of 8 perches to an inch?

25 8 2|0)20|0 10 links. Answer.

2. How many links in a division, if a map be laid down by a scale of 10 perches to an inch?

25 10 2|0)25|0

12.5 or 121 links. Answer:

And so of any other.

To protract a field-book, taken by the angles of the field.

Note. We here suppose the land surveyed is kept on the right hand as you survey.

Draw a blank line with a ruler of a length greater than the diameter of the protractor; pitch upon any convenient point therein, to which apply the centre-hole of your protractor with your pin, turning the arc upwards if the angle be less than 180, and downwards if more; and observe to keep the upper edge of the scale, or 180 and 0 degrees upon the line: then prick off the number of degrees contained in the given angle, and draw a line from the first point through the point at the degrees; upon which lay the stationary distance. Let this line be lengthened forwards and backwards, keeping your first station to the right, and second to the left;

and lay the centre of your protractor over the second station, with your pin, turning the arc upwards, if the angle be less than 180, and downwards, if more; and keeping the 180 and 0 degrees on the line, prick off the number of degrees contained in the given angle, and through that point and the last station draw a line, on which lay the stationary distance: and in like manner proceed through the whole.

In all protractions, if the end of the last station falls exactly in the point you began at, the field-work and protraction are truly taken, and performed; if not, an error must have been committed in one of them: in such case make a second protraction; if this agrees with the former, and neither meet nor close, the fault is in the field-work, and not in the protraction; and then a re-survey must be taken.

#### REMARKS.

The accuracy of geometrical and trigonometrical mensuration, depends in a great degree on the exactness and perfection of the instruments made use of; if these are defective in construction, or difficult in use, the surveyor will either be subject to error, or embarrassed with continual obstacles. If the adjustments, by which they are to be rendered fit for observation, be troublesome and inconvenient, they will be taken upon trust, and the instrument will be used without examination, and thus subject the surveyor to errors, that he can neither account for, nor correct.

In the present state of science, it may be laid down as a maxim, that every instrument should be so contrived, that the observer may easily examine and rectity the principal parts; for however careful the instrument-maker may be, however perfect the execution thereof, it is not possible that any instrument should long remain accurately fixed in the position in which it came out of the maker's hand, and therefore the principal parts should be moveable, to be rectified occasionally by the observer.

# AN ENUMERATION OF INSTRUMENTS USEFUL TO A SURVEYOR;

Fewer or more of which will be wanted, according to the extent of his work, and the accuracy required.

A case of good pocket instruments.

A pair of beam compasses.

A set of feather-edged plotting scales.

Three or four parallel rules.

A pair of proportional compasses.

A pair of triangular ditto.

A pantagraph.

A cross staff.

A circumferentor.

An Hadley's sextant.

An artificial horizon.

A theodolite.

A surveying compass.

Measuring chains, and measuring tapes.

King's surveying quadrant.

A perambulator, or measuring wheel.

A spirit level with telescope.

Station staves, used with the level.

A protractor, with or without a nonius.

To be added for county and marine euroeying;

An astronomical quadrant, or circular instrument.

A good refracting and reflecting telescope.

A copying glass.

For marine surveying ;

A station pointer.
An azimuth compass.
One or two boat compasses.

Besides these, a number of measuring rods, iron pins, or arrows, &c. will be found very convenient, and two or three offset staves, which are straight pieces of wood, six feet seven inches long, and about an inch and a quarter square; they should be accurately divided into ten equal parts, each of which will be equal to one link. These are used for measuring offsets, and to examine and adjust the chain.

Five or six staves of about five feet in length, and one inch and an half in diameter, the upper part painted white, the lower end shod with iron, to be struck into the ground as marks.

Twenty or more iron arrows, ten of which are always wanted to use with the chain, to count the number of links, and preserve the direction of the chain, so that the distance measured may be really in a straight line.

The pocket measuring tapes, in leather boxes, are often very convenient and useful. They are made to the different lengths of one, two, three, four poles, or sixty-six feet and 100 feet; divided, on one side into feet and inches, and on the other into links of the chain. Instead of the latter, are sometimes placed the centesimals of a yard, or three feet into 100 equal parts.

#### SECTION II.

#### **MENSURATION**

#### OF HEIGHTS AND DISTANCES.

1st. Of Heights.

PL. 5. fig. 18.

HE instrument of least expense for taking heights, is a quadrant, divided into ninety equal parts or degrees; and those may be subdivided into halves, quarters, or eighths, according to the radius, or size of the instrument: its construction will be evident by the scheme thereof.

From the centre of the quadrant let a plummet be suspended by a horse hair: or a fine silk thread of such a length that it may vibrate freely, near the edge of its arc: by looking along the edge AC, to the top of the object whose height is required; and holding it perpendicular, so that the plummet may neither swing from it, nor lie on it; the degree then cut by the hair, or thread, will be the angle of altitude required.

If the quadrant be fixed upon a ball and socket on the three-legged staff, and if the stem from the ball be turned into the notch of the socket, so as to bring the instrument into a perpendicular position, the angle of altitude by this means, can be acquired with much greater certainty.

An angle of altitude may be also taken by any of the instruments used in surveying; as has been

particularly shown in treating of their description and uses.

Most quadrants have a pair of sights fixed on the edge AC, with small circular holes in them; which are useful in taking the sun's altitude, requisite to be known in many astronomical cases; this is effected by letting the sun's ray, which passes through the upper sight, fall upon the hole in the lower one; and the degree then cut by the thread, will be the angle of the sun's altitude; but those sights are useless for our present purpose, for looking along the quadrant's edge to the top of the object will be sufficient, as before.

### PROB. I.

#### PL. 5. fig. 19.

To find the height of a perpendicular object at one station, which is on an horizontal plane.

# A steeple.

Given, The angle of altitude, 53 degrees.

Distance from the observer to the foot of the steeple, or the base, 85 feet.

Height of the instrument, or of the observer, 5 feet.

Required, the height of the steeple.

The figure is constructed and wrought, in all respects, as case 2 of right-angled trigonometry; only there must be a line drawn parallel to, and beneath AB of 5 feet for the observer's hight, to represent the plane upon which the object stands;

to which the perpendicular must be continued, and that will be the height of the object.

Thus, AB s the base, A the angle of altitude, BC the height of the steeple from the instrument, or from the observer's eye, if he were at the foot of it; DC the height of the steeple above the horizontal surface.

Various statings for *BC*, as in case 2. of right angled plane trigonometry.

$$90^{\circ}$$
 $53=A$ .

 $37=C$ .

- 1. S. C: AB:: S. A: BC. 37° 85 53° 112.8.
- 2. R.: AB:: T. A: BC. 90° 85 53° 112.8.
- 3. T. C: AB :: R. : BC. 37° 85 90° 112.8.

Their sum is 117.8 or 118 feet, the height of the steeple required.

## OF HEIGHTS.

### PROB. II.

PL. 5. fig. 20.

To find the height of a perpendicular object, on an horizontal filane; by having the length of the shadow given.

Provide a rod, or staff, whose length is given, let that be set perpendicular, by the help of a quadrant, thus; apply the side of the quadrant AC, to the rod, or staff; and when the thread cuts 90°. it is then perpendicular; the same may be done by a carpenter's or mason's plumb.

Having thus set the rod or staff perpendicular; measure the length of its shadow, when the sun shines, as well as the length of the shadow of the object, whose height is required; and you have the proper requisites given. Thus,

ab, the length of the shadow of the staff, 15 feet, bc, the length of the staff, 10 feet.

AB, the length of the shadow of the steeple, or object, 135 feet.

Required BC, the height of the object.

The triangles abc, ABC, are similar, thus; the angle b=B, being both right; the lines ac, AC are parallel, being rays, or a ray of the sun; whence the angle a=A (by part 3. theo. 3. sect. 4.) and consequently c=C. The triangles being therefore mutually equiangular, are similar (by theo. 16. sect. 4.) it will be,

ab: bc: : AB: BC.
15 10 135 90. the steeple's height, required.

The foregoing method is most to be depended on; however, this is mentioned for variety's sake.

#### PROB. III.

PL. 5. fig. 21.

To take the altitude of a perfiendicular object, at the foot of a hill, from the hill's side.

Turn the centre  $\Lambda$  of the quadrant, next your eye, and look along the side  $\Lambda C$ , or 90 side, to the top and bottom of the object; and nothing down the angles, measure the distance from the place of observation to the foot of the object. Thus,

Given, Angle to the foot of the object, 55° \(\frac{1}{2}\) or 55°. 15'

Angle to the top of it, 31°\(\frac{1}{2}\) or 31°. 15'

Distance to the foot of it, 250 feet.

Required, the height of the object.

# By Construction.

Draw an indefinite blank line AD, at any point in which A make the angles EAB of 55°. 15′, and EAC of 31°. 15′; lay 250 from A to B; from B, draw the perpendicular BE (by prob. 7 of geometry) crossing AC in C; so will BC be the height of the object required.

In the triangle ABC there is given,

ABE the complement of EAB to 90°, which is 34°. 45′.

CAB the difference of the given angle 24°.00'.

The side AB, 250. Required, BC.

This is performed as case 2. of oblique angular trigonometry. Thus,

180—the sum of  $ABE 34^{\circ}$ . 45', and  $CAB 24^{\circ}$ . 00' =  $ACB 121^{\circ}$ . 15'. Then,

S. ACB: AB:: S. CAB: BC.
121°. 15/250 24°. 00' 119, the height required.

### PROB. IV.

### PL. 5. fig. 22.

To take the altitude of a perpendicular object, on the top of a hill, at one station; when the top and bottom of it can be seen from the foot of the hill.

As in prob. 1. take an angle to the top, and another to the bottom of the object; and mersure from the place of observation to the foot of the object, and you have all the given requisites. Thus,

### A Tower on a hill.

Given, Angle to the bottom, 48°. 30'.

Angle to the top, 67°. 00'.

Dist. to the foot of the object, 136 feet.

Required, the height of the object.

## By Construction.

Make the angle  $DAB=48\ 30$ , and lay 136 feet from A to B; from B, let fall the perpendicular BP; and that will be the height of the hill: produce BD upwards by a blank line: again, at A, make the angle  $DAC=67^{\circ}$  00' by a blank line, and from C where that crosses the perpendicular produced, draw the line CB, and that will be the height of the object required.

Let AC be drawn.

In the triangle ABC, there is given.

The angle ACD the complement of  $DAC = 23^{\circ}$ , 00  $^{\prime}$ .

CAB the difference between the two given angles=18°. 30'.

And the side AB 136. To find BC.

S. C:: AB:: S. CAB: BC. 23° 136 18°. 30′ 1104.

If BD were wanted, it is easily obtained, by the Arst case of right angled plane trigonometry.

#### PROB. V.

PL. 5. fig. 23.

To take an inaccessible perpendicular altitude, on a horizontal plane.

This is done at two stations, thus:

Bb

Let DC be a tower which cannot be approached by means of a moat or ditch, nearer than B; at B, take an angle of altitude, to C: measure any convenient distance backward to A, which note down; at A, take another angle to C; so have you the given requisites, thus:

Given, Stationary distance, 87 feet. Second angle, 379.00'.

The height of the tower CD, is required.

# By Construction.

Upon an indefinite blank line, lay off the stationary distance 87, from A to B; from B, set off your first; and from A, your second angle; from C, the point of intersection of the lines which form these angles, let fall the perpendicular CD; and that will be the height of the object required.

The external angle CBD, of the triangle ABC; is equal to the two internal opposite ones, A, and ACB (by theo. 4. sect. 4.): wherefore if one of the internal opposite angles be taken from the external angle, the remainder will be the other internal opposite one, thus;

# CBD 550-A 370-ACB 18°.

Therefore in the triangle ABC; we have the angles A, and AGB, with the side AB given to find BC.

S. ACB: AB:: S. A: BC. 18° 87 37° 169.4 Having found BC, we have in the triangle BCD the angle CBD 55°, consequently BCD 35°, and BC 169.4; to find DC.

This is performed by the first case of right angled trigonometry, three several ways; thus:

1. R: BC:: S. CBD: DC. 90° 169.4 55° 138.8. The height required.

2. Sec. CBD: BC: T. CBD: DC. 55° 169.4 55° 138.8. The height required.

3. Sec. BCD: BC:: R:CD.
35° 1694 90° 138.8.
The height required.

If BD, the breadth of the moat, were required; it may also be found, by three different statings, as in the first case of right angled plane trigonometry.

# PROB. VI.

PL. 5. fig. 24.

Let BC, a may-pole, whose height is 100 feet, be broken at D; the upper part of which, DC, falls upon an horizontal plane, so that its extremity, C, is 34 feet from the bottom or foot of the pole.

Required, the segments BD and DC.

# By Construction.

Lay 34 feet from A to B; on B erect the perpendicular BC of 100 feet; and draw AC; bisect

AC (by prob. 4. geom.) with the perpendicular line, EF; and from D, where it cuts the perpendicular BC, draw AD, which will be the upper segment; and DB will be the lower.

By cor. to lemma, preceding theo. 7. geom. AD=DC; and (by the lemma) the angle C=CAD.

In the triangle ABC, find C as in case 6, of right angled trigonometry, thus;

By theo. 4. geom. The external angle  $ABD = 37^{\circ} 34'$  or to twice the angle  $C_{1}$ , i. e. to  $C_{2}$  and  $C_{2}AD$ .

Then in the triangle ABD, there is ABD 37° 34' therefore also its complement DAB 52° 26' and AB 34, given, to find AD and BD.

By the second case of right-angled trigonometry.

These may be had from other statings, as in the second case aforesaid.

#### PROB. VII.

PL. 5. fig. 25.

To take the altitude of a perpendicalar object on a hill, from a plane beneath it.

This is done at two stations, thus:

Let the height DC, of a wind-mill on a hill be required.

From any part of the plane whence the foot of the object can be seen, let angles be taken to the foot and top; measure thence any convenient distance towards the object, and at the end thereof, take another angle to the top: and you have the proper requisites, thus;

First station. Angle to the foot DAB 21° 00'.

Angle to the top CAB 35° 00'.

Stationary distance AB 104 feet.

Second station.

Angle to the top 48° 30.

# DC required.

# By Construction.

On an indefinite blank line, lay the stationary distance AB 104 feet; from A, set off the second, and from B, the third given angle; and from the intersecting point C of the line formed by them, let fall the perpendicular CE; from A set off the first angle, and the line formed by it will determine the point D. Thus have we the height of the hill, as well as that of the wind-mill.

The angle CBE-A=ACB, as in the last prob.

In the triangle ABC, find AC thus;

S. ACB: AB:: S. ACB (or sup. of CBE): AC 13°, 30': 104:: 131°, 30': 333.6

The angle CAE-DAE=CAD.

The angle  $ACD = AED \times EAD$ , by theo. 4.

In the triangle CAD, find CD thus,

S. ADC: AC: : S. CAD: DC 111°.: 333.6:: 14: 86.46 required.

CE, BE, or DE, may be found by other various statings, as set forth in the first and second cases of right angled trigonometry.

# PROB. VIII.

PL. 5. fig. 26.

To find the length of an object, that stands obliquely on the top of a hill, from a plane beneath.

Let CD be a tree whose length is required.

This is done at two stations.

Make a station at B, from whence take an angle to the foot, and another to the top of the tree; measure any convenient distance backward to A, from whence also let an angle be taken to the foot, and another to the top; and you have the requisites given. Thus,

First station. Angle to the foot  $EBD = 36^{\circ}$ . 30'. Angle to the top  $EBC = 44^{\circ}$ . 30'. Stationary distance AB = 104 feet.

Second station. Angle to the foot  $EAP=24^{\circ}$ . 30'. Angle to the top  $EAC=32^{\circ}$ . 00'.

### Let DC and DE be required.

The geometrical constructions of this and the next problem are omitted; as what has been already said, and the figures are looked upon as sufficient helps.

EBC-A=ACB, or 44°. 30' - 32°.=12°. 30'.

In the triangle ABC, find BC. Thus,

1. S. ACB: AB:: S. A: BC. 12°. 80' 104 32° 254.7.

EBD-EAD=ADB, or 36°. 30′-24°. 30′=12° 00′

In the triangle ADB, find DB, thus;

2. S. ADB: AB:: S. DAB: DB. 12° 00′ 104 24°. 30′. 207.4.

CBE-DBE=CBD, or 44°. 30'-36°. 30'=8°00'

In the triangle CBD there is given, CB 254.7, DB 207.4, and the angle CBD 8° 00'; to find DC.

This is performed as case 3. of oblique angled trigonometry, thus;

# of Heightso

86° 00' +56° 40' +141° 40' - BDC. 86° 00' -55° 40' +50° 90' = BCD.

4. S. BCD: BD 17-6 CBD: DC.
30°, 20′ 907.4 8°. 00′ 57.15 length of

To find DE in the triangle DBE.

7 R.: BD:: S. DBE: DE, 900: 2074: 250° 2010 1934 height of the

# PROB. IX.

To find the height of an inaccessible object CD, on a hill BC, from ground that is not horizontal.

#### PL: 6. fig. 1.

From any two points, as G and A, whose distance GA, is measured, and therefore given; let the angles HGD, BAD, BAC, and EAG, be taken; because GH is parallel to EA (by part 2. theo. 3. geom.) the angle HGA=EAG; therefore EAG  $\times HGD=AGD$ ; and (by cor. 1. theo. 1. geom.) 180—the sum of EAG and BAD=GAD; and, (by cor. 1. theo. 5. geom.) 180—the sum of the angles AGD and GAD=GDA: thus we have the angles of the triangle AGD, and the side AG given; thence (by case 2. of obl. ang. trig.) AD may be easily found. The angle DAB—CAB=DAC, and  $90^{\circ}$ —BAD=ADC; and  $180^{\circ}$ —the sum of DAC and ADC=ACD: so have we the

several angles of the triangle ACD given, and the side AD; whence (by case 2 of obl. trig.) CD may be easily found. We may also find AC, which with the angle BAC, will give CB the height of the bill.

The solutions of the several problems in heights and distances, by Gunter's scale, are omitted; because every particular stating has been already shewn by it, in trigonometry.

#### 2d. OF DISTANCES.

HE principal instruments used in surveying, will give the angles or bearings of lines; which has been particularly shewn, when we treated of them.

### PROB. I.

### PL. 6. fig. 2.

Let  $\mathcal{A}$  and  $\mathcal{B}$  be two houses on one side of a river, whose distance asunder is 293 perches: there is a tower at C on the other side of the river, that makes an angle at  $\mathcal{A}$ , with the line  $\mathcal{A}\mathcal{B}$  of 53° 20'; and another at  $\mathcal{B}$ , with the line  $\mathcal{B}\mathcal{A}$  of 66° 20'; required the distance of the tower from each house. viz.  $\mathcal{A}C$  and  $\mathcal{B}C$ .

This is performed as case 2. of oblique angled trigonometry, thus;

1. S. C: AB:: S. A: BC. 60° 20′ 293 53° 20′ 270.5.

2. S. C: AB: : S. B: AC. 60° 20′ 293 66° 20′ 508.8.

#### PROB. II.

PL. 6. fig. 11.

Let B and C, be two houses whose direct distance asunder, BC, is inaccessible: however it is

known that a house at A is 252 perches from B, and 230 from C; and that the angle BAC, is found to be 70°. What is the distance BC, between the two houses?

This is performed as case 3. of oblique angled trigonometry, thus;

1. 
$$AB+AC:AB-AC::T. \text{ of } \frac{1}{2}C+B;$$
482 222 55°. 00'

 $55^{\circ}+3^{\circ}.44^{\prime}=58^{\circ}.44^{\prime}=C.55^{\circ}-3^{\circ}.44^{\prime}=51^{\circ},$  16=B.

2. S. C: AB:: S. A: BC. 58°.44' 252 70° 277.

#### PROB. III.

#### PL. 6. fig. 3.

Suppose ABC a triangular piece of ground, which by an old survey we find to be thus; AB 260, AC 160, BC 150 perches, the meaning lines AC and BC, are destroyed or plowed down, and the line AB, only remaining. What angles must be set off at A and B, to run new meanings by exactly where the old ones were?

This is performed as in case 4. of oblique angled trigonometry, thus;

130+5.96=135.96=AD. 130-5.96=124.04=DB.

- 2. AD: R:: AC: Sec. A. 136 90°:: 160 31°. 47′.
- 3. BC: S. A:: AC: S. B. 150 31°. 47′ 160 34°. 10.

#### PROB. IV.

PL. 6. fig. 4.

Let D and C, be two trees in a bog, to which you can have no nearer access than at A and B; there is given, DAB 100°, CAB 36°. 30′, CBA 121°. DBA 49°, and the line AB 113 perches. Required, the distances of the trees DC.

180°—the sum of DBA and DAB=ADB=31°. 180°—the sum of CAB and CBA=ACB=22. 30.

In the triangle ABD, find DB, thus;

1. S. ADB: AB:: S. DAB: DB. 31° 113::100° 216.

And in the triangle ABC, find BC, thus;

2. S. ACB: AB: : S: CAB: BC. 22° 30′ 113 36° 30′ 175.6.

In the triangle DBC, you have  $DBC=ABC-ABD=72^{\circ}$ ; likewise the sides BD, BC, as before found, given to find DC.

3.  $BD+BC: BD-BC: T. \text{ of } \pm DCB+CDB: 391.6 40.4 549$ 

#### T. of $\frac{1}{2}$ DCB—CDB.

8° 05'.

54°+8° 05'=62° 05'=DCB. 54°-8° 05'=45° 55'=CDB.

4. S. CDB: BC:: S. DBC: DC. 45° 55' 175.6 72° 232.5.

#### LEMMA.

#### PL. 6. fig. 12.

If from a point C, of a triangle ABC, inscribed in a circle, there be a perpendicular CD, let fall upon the opposite side AB; that perpendicular is to one of the sides, including the angle, as the other side, including the angle, is to the diameter of the circle, i. e. DC: AC: CB: CE.

Let the diameter CE be drawn and join EB; it is plain the angle CEB = CAB (by cor. 2. theo. 7. geom.) and CBE is a right angle (by cor. 5. theo. 7. geom.) and =ADC: whence ECB = ACD. The triangles CEB, CAD, are therefore mutually equiangular, and (by theo. 16. geom.) DC:AC:CB:CE, or DC:CB:AC:CE. 2. E. D.

#### PROB. V.

#### P.L. 6. fig. 5.

Let three gentlemen's seats, A, B, C, be situate in a triangular form: there is given, AB 2.5 miles, AC 2.3, and BC 2. It is required to build a church at E, that shall be equi-distant from the seats A, B, C. What distance must it be from each seat, and by what angle may the place of it be found?

# By Construction.

By prob. 15. geom. Find the centre of a circle that will pass through the points, A, B, C: and that will be the place of the church; the measure of which, to any of these points, is the answer for the distance: draw a line from any of the three points to the centre, and the angle it makes with either of the sides that contain the angle it was drawn to; that angle laid off by the direction of an instrument, on the ground, and the distance before found, being ranged thereon, will give the place of the church required.

# By Calculation.

### 1.25+.258=1.508=AD.

By cor. 2. theo. 14. geom. The square root of the difference of the squares of the hypothenuse AC, and given leg AD, will give DC.

That is, 5.29-2.274064=3.015936.

Its square root is 1.736=CD.

Then by the preceding lemma,

2. CD: AC: CB: the diameter. 1.736 2.3 2 2.65.

the half of which, viz. 1.325 is the semi-diameter, or distance of the church from each seat, that is, AE, CE, BE.

From the centre E, let fall a perpendicular upon any of the sides as EF, and it will bisect in E: (by theo. 8 geom.)

Wherefore  $AF=CF=\frac{1}{2}AC=1.15$ .

In the right angled triangle AFE, you have AF 1.15, and AE the radius 1.325 given, to find FAE, thus;

3. AF: R.:: AE: Sec. FAE. 1.15 90° 1.325 29° 47′.

Wherefore directing an instrument to make an angle of  $29^{\circ}47'$ , with the line AC; and measuring 1.325 on that line of direction, will give the place of the church, or the centre of a circle that will pass through A, B, and C.

The above angle FAE, may be had without a secant, as before, thus;

AE:R::AF:S.AEF. 1.325 90° .115 60°. 13'

Its complement 29°. 47', will give FAE, as before.

The questions that may be proposed on this head, being innumerable, we have chosen to give only a few of the most useful.

#### SECTION III.

MENSURATION OF AREAS, OR THE VARIOUS METHODS OF CALCULATING THE SUPERFICIAL CONTENT OF ANY FIELD.

#### DEFINITION.

HE area or content of any plane surface, in perches, is the number of square perches which that surface contains.

# PL. 7. fig. 1.

Let ABCD represent a rectangular parallelogram, or oblong: let the side AB, or DC, contain 8 equal parts; and the side AD, or BC. three of such parts; let the line AB be moved in the direction of AD, till it has come to EF; where AE, or BF (the distance of it from its first situation) may be equal to one of the equal parts. Here it is evident, that the generated oblong ABEF, will contain as many squares as the side AB contains equal parts, which are 8; each square having for its side one of the equal parts, into which AB, or AD, is divided. Again, let AB move on till it comes to GH, so as GE, or HF, may be equal to AE, or BF; then it is plain that the oblong AGHB, will contain twice as many squares as the side AB contains equal parts. After the same manner it will appear, that the oblong ADCB will contain three times as many squares as the side AB contains equal parts; and in general, that every rectangular parallelogram, whether square or oblong, contains as many squares as the product of the number of equal parts in the base, multiplied into the number of the same equal parts in the height, contains units, each square having for its side one of the equal parts.

Hence arises the solution of the following problems.

### PROB. I.

To find the content of a square piece of ground.

1. Multiply the base in perches, into the perpendicular in perches, the product will be the content in perches; and because 160 perches make an acre, it must thence follow, that

Any area, or content in perches, being divided by 160, will give the content in acres; the remaining perches, if more than 40, being divided by 40, will give the roods, and the last remainder, if any, will be perches,

### Or thus:

2. Square the side in four-pole chains and links, and the product will be square four-pole chains and links; divide this by 10, or cut off one more than the decimals, which are five in all, from the right towards the left: the figures on the left are acres; because 10 square four-pole chains make an acre, and the remaining figures on the right, are decimal parts of an acre. Multiply the five figures to the right by 4, cutting 5 figures from the product, and if any figure be to the left of them, it is a rood, or roods; multiply the last cut off figures by 40, cutting off five or (which is the same thing) by 4, cutting off four; and the remaining figures to the left, if any, are perches.

1. The first part is plain, from considering that a piece of ground in a square form, whose side is a perch, must contain a perch of ground; and that 40 such perches make a rood, and four roods an

acre; or which is the same thing, that 160 square perches make an acre, as before.

2. A square four-pole chain (that is, a piece of ground four poles or perches every way) must contain 160 square perches; and 160 perches make an acre, therefore 10 times 16 perches, or 10 square four-pole chains, make an acre.

Note. The chains given, or required, in any of the following problems, are supposed to be twopole chains, that chain being most commonly used; but they must be reduced to four-pole chains or perches for calculation, because the links will not operate with them as decimals.

#### EXAMPLES.

PL. 1. fig. 17.

Ch. L.

Let ABCD be a square field, whose side is 1429, required the content in acres.

Ch. L.

By problem 4. section 1. part 2. 14. 29 are equal to 29.16 perches. 29.16

17496
2916
26244
5832
A. R. P.
160)850.3056( 5. 1. 10. content. 40)50(1 rood.

· f0 perches.

#### Or thus:

Ch. L. 14. 29 are equal to 7. 29 of four-pole chains, by prob. 1. sect. 1. pt. 2. 7. 29

6561 1458 5103 A. R. P. Acres 5|31441 cont. as before 5. 1.10 4 Rood 1|25764 40 Perches 10|30560

It is required to lay down a map of this piece of ground, by a scale of twenty perches to an inch.

Take 29. 16 the perches of the given side, from the small diagonal on the common surveying scale, where 20 small, or two of the large divisions, are an inch: make a square whose side is that length (by prob. 9. geom.) and it is done.

# PROB. II.

To find the side of a square, whose content is given.

Extract the square root of the given content in perches, and you have the side in perches, and consequently in chains.

#### EXAMPLE.

It is required to lay out a square piece of ground which shall contain 12A. 3R. 16P. Required the number of chains in each side of the square; and to lay down a map of it, by a scale of 40 perches to an inch.

# To draw the map.

From a scale where 4 of the large, or 40 of the small divisions are an inch, take 45.34, the perches of the side, of which make a square.

### PROB. III.

To find the content of an oblong piece of ground.

Multiply the length by the breadth, for the content.

#### EXAMPLE.

PL. 1. fig. 3.

Let ABCD be an oblong piece of ground, whose length AB is 14C.25L, and breadth 8C.37L, required the content in acres, and also to lay down a map of it, by a scale of 20 perches to an inch.

Ch. L. Perches.

14.25=29.00 | 8.37 = 17.48 | By prob. 4. sect. 1. pt 2.

15732
3496

A. R. P.
160)506.9200(3. 0. 27. content.

26 perches, or near 27.

Or thus:
4 pole ch.

Ch. L. Ch. L.
14.25 = 7.25
8.37 = 4.37 | By prob. 1. sect, 1. pt. 2.

5075
2175
2900

Perches 26|9200

Acres 3|16825

Rood |67300

# To draw the map.

Make an oblong (by schol. to prob. 9. geom.) whose length, from a scale of 20 to an inch, may be 29 perches, and breadth, 17.48 perches.

# PROB. IV.

The content of an oblong piece of ground, and one side given, to find the other.

Divide the content in perches, by the given side in perches, the quotient is the side required in perches; and thence it may be easily reduced to chains.

#### EXAMPLE.

There is a ditch 14 Ch. 25 L. long, by the side of which it is required to lay out an oblong piece of ground, which shall contain 3A. 0R. 37P: what breadth must be laid off at each end of the ditch tenclose the 3A. 0R. 37P?

A. R. P. 3. 0. 27.  $\frac{4}{12}$   $\frac{40}{29)507(17.48 = 8.37. \text{ breadth}}$   $\frac{217}{140}$  $\frac{140}{240}$ 

8

The map is constructed like the last.

#### PROB. V.

To find the content of a piece of ground, in form of an oblique angular parallelogram; or of a rhombus; or rhomboides.

Multiply the base into the perpendicular height. The reason is plain from theo. 13. geom.

## Example.

Let ABCD be a piece of ground in form of a rhombus, whose base AB is 22 chains, and perpendicular DE, or FC, 20 chains. Required the content.

$$Ch. Ch.$$
 $22=11.0$ 
 $20=10.0$ 

Acres 11|0

Or,

The converse of this is done by prob. 4. and the map is drawn, by laying off the perpendicular on that part of the base from whence it was taken; joining the extremity thereof to that of the base by a right line, and thence completing the parallelogram.

PROB. VI.

To find the content of a triangular piece of ground.

Multiply the base by half the perpendicular, or the perpendicular by half the base; or take half the product of the base into the perpendicular.

The reason of this is plain, from cor. 2. theo. 12. geom.

PL. 1. fig. 16.

Let ABC be a triangular piece of ground, whose longest side or base BC, is 24C. 38L. and perpendicular AD, let fall from the opposite angle, is 18 C. 28L. Required the content.

Rood |78728

40

Perches 31|49120 A. R. P. Content 4. 0. 31.

Or 2dly. Perp. 6.78 of four-pole chains. \$\frac{1}{2}\text{base } 6.19

Or 3dly. Base 12.38 four-pole chains. Perp. 6.78

Or the base and perpendicular may be reduced to perches; and the content may be thence obtained, thus:

Ch. L. Perches. **Perp.** 13.28 = 27.12By prob.4.sect. 1.pt.2; Perches. Ch. L. 1. Base 49.52 = 24.381 perp. 13.56 20712 24760 14856 4952 \_\_\_\_\_A. R. P. 160)671 4912(4. 0. 31. 31 Perches. 2. Perp. 27.12 Half base 24.76 16272 18984 10848 5424 --- A, R. P. 671.4912 = 4, 0. 31.

But, square perches may be reduced to acres, &c. rather more commodiously, by dividing by 40 and 4, than by 160; thus,

4)16. 31

A. 4. 0. 31

Perches.

3. Base 49.52
Perp. 27.12

9904
4952
34664
9904

1342.9824
A. R. P.
671.4912 = 4. 0. 31.

The map may be readily drawn, having the distance from either end of the base, to the perpendicular given; as may be evident from the figure.

# PROB. FII.

The content of a triangular piece of ground, and the base given, to find the perpendicular.

Divide the content in perches, by half the base in perches; and the quotient will give you the perpendicular, in perches and so in chains.

# EXAMPLES.

## PL. 1. fig. 16.

Let *BC* be a ditch, whose length is 24*C*. 40*L*. by which it is required to lay out a triangular piece of ground, whose content shall be 4A. 1R. 10P. Required the perpendicular.

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Ch. L. Perches. Base 24.40 = 49.6Half the base = 24.8

A. R. P.
4. 1. 10.
4
17
40
Perches.
24.8)690(27.28
1940
2040
660
64

Perches. Ch. L. Answer perp. 27.28 = 13.45.

This perpendicular being laid on any part of the base, and lines run from its extremity to the ends of the base, will lay out the triangle (by cor. to theo. 13. geom.) so that the perpendicular may be set on hat part of the base which is most convenient and agreeable to the parties concerned.

#### LEMMA.

PL. 8. fig. 9.

If from half the sum of the sides of any plane triungle ABC, each particular side be taken; and if the half sum, and the three remainders be multiplied continually into each other, the square root of this product will be the area of the triangle.

**Bisect** any two of the angles, as A and B, with the lines AB, BD meeting in D; draw the perpendiculars DE, DF, DG.

In the same way if A and C were bisected, the same point D would be had; therefore a line from D to C will bisect C, and thus the triangles DFC, DGC will be also equal.

Produce CA to H, till AH=EB or GB; so will HC be equal to half the sum of the sides, viz. to  $\frac{1}{2}AB$ ,  $+\frac{1}{3}AC$  +  $\frac{1}{2}BC$ ; for FC, FA, EB, are severally equal to CG, AE, BG; and all these to gether are equal to the sum of the sides of the triangle; therefore FC + FA + EB or CH, are equal to half the sum of the sides.

FC=CH-AB, for AF=AE and HA=EB; therefore HF=AB; and AF=CH-BC; for CF

=CG, and AH=GB; therefore BC=HA+FC, and AH=CH-AH.

Continue DC, till it meets a perpendicular drawn upon H in K; and from K draw the perpendicular KI, and join AK.

Because the angles AHK and AIK are two right ones, the angles HIA and K together, are equal to two right; since the angles of the two triangles contain four right: in the same way FDE+FAE=(2 right angles=) FAE+IAH; let FAE be taken from both, then FDE=IAH, and of course FAE=K; the quadrilateral figures AFDE, and KHAI, are therefore similar, and have the sides about the equal angles proportional; and it is plain the triangles CFD and CHK are also proportional: hence,

FD: HA:: FA: HK FD: FC:: HK: HC

Wherefore by multiplying the extreme, and means in both, it will be the square of  $FD \times HK \times HC = FC \times FA \times HA \times HK$ ; let HK be taken from both, and multiply each side by CH; then the square of  $CH \times D$  by the square of  $FD = FC \times FA \times HA \times CH$ .

It is plain, by the foregoing problem, that  $\frac{1}{2}AB \times DE$ ,  $+\frac{1}{3}BC \times DG + \frac{1}{3}AC \times FD =$  the area of the triangle; or that half the sum of the sides, viz.  $CH \times FD =$  the triangle; wherefore the square of  $CH \times BD =$  the triangle; wherefore the square of  $CH \times BD =$  the triangle; wherefore the square of  $CH \times BD =$  the triangle of  $CH \times BD =$  the triangle of  $CH \times BD =$  the half sum multiplied continually into the differences between the half sum and each side, will be the square of the area of the triangle, and its root the area. 2. E. D.

Hence the following problem will be evident.

## PROB. VIII.

The three sides of a plane triangle given to find the area.

#### RULE.

From half the sum of the three sides subtract each side severally; take the logarithms of half the sum and three remainders, and half their total will be the logarithm of the area: or, take the square roo! of the continued product of the half sum and three remainders for the area.

#### EXAMPLES.

PL. 8. fig. 9.

# 1. In the triangle ABC, are

Given, 
$$\begin{cases}
AB=10.64 \\
AC=12.28 \\
CB=9.00
\end{cases}$$
 four-pole chains; required the area?

Sum 31.92

Half sum 15.96 Log. 1.203033

Remainders 
$$\begin{cases}
5.32 & -0.725912 \\
3.68 & -0.565848 \\
6.96 & -0.842609
\end{cases}$$
2)3.337402

Answer, Sqr. Ch. 46.63 Log. 1.668701 or, 4.663 Acres.

Or,  $15.96 \times 5.32 \times 3.68 \times 6.96 = 2174.71113216$ ;

the square root of which is 46.63, for the area as before.

2 What quantity of land is contained in a triangle, the 3 sides of which are, 80, 120 and 160 perches respectively? Answer 29A. 7P.

### PROB. IX.

Two sides of a fulane-triangle and their included angle given, to find the area.

#### RULE.

To the log sine of the given angle (or of its supplement to 180°, if obtuse) add the logarithms of the containing sides; the sum, less radius, will be the logarithm of the double area.

## Examples.

PL. 5. fig. 16.

Suppose two sides, AB, AC, of a triangular lot ABC, form an angle of 30 degrees, and measure one 64 perches, and the other 40.5 what must the content be?

Given angle Containing sides	30°. { 64. { 40.5	sine log. log.	9.6989 <b>70</b> 1.8061 <b>80</b> 1.6074 <b>55</b>
	2)1296.	log.	3.112605
,	160)648(4A. 8P. answer.		
	8		

- 2. Required the area of a triangle, two sides of which are 49.2 and 40.8 perches, and their contained angle 144 ½ degrees? Answer, 3A. 2R. 22P.
- 3. What quantity of ground is inclosed in an equilateral triangle, each side of which is 100 perches, either angle being 60 degrees? Answer, 27A. 10P.

# Demonstration of this problem.

#### PL. 11. fig. 3.

Let AH be perpendicular to AB and equal to AC, and HE, FCG, parallel to AB; then making AH (= AC) radius, AF (= CD) will be the sine of CAD, and the parallelograms ABEH (the product of the given sides) and ABGF the double area of the triangle) having the same base AB, are in proportion as their heights AH, AF; that is, as radius to the sine of the given angle; which proportion gives the operation as in the rule above.

## PROB. X.

To find the area of a trapezoid, viz. a figure bounded by four right lines, two of which are parallel, but unequal.

#### RULE.

Multiply the sum of the parallel sides by their perpendicular distance, and take half the product for the area.

Note. On this 16th problem are founded most of the calculations of differences by latitude and departure, and those by offsets, following in this treatise.

#### EXAMPLES.

1. Required the area of a trapezoid, of which the parallel sides are, respectively, 30 and 49 perches, and their perpendicular distance 61.6?

$$30+49 = \frac{61.6}{79.}$$
 Multiply. 2)4866.4

Answer, 2433.2=15A. 33.2P.

PL. 9. fig. 10.

2. In the trapezoid ABCD the parallel sides are, AD, 20 perches, BC, 30, and their perpendicular distance, AB, 26; required the content?

Answer, 4A. 36P.

### PROB. XI.

To find the Content of a trapezium.

#### RULE.

Multiply the diagonal, or line joining the remotest opposite angles, by the sum of the two perpendiculars falling from the other angles to that diagonal, and half the product will be the area.

#### EXAMPLE.

PL. 7. fig. 3.

Let ABCD be a field in form of a trapezium, the diagonal AC 64.4 perches, the perpendicular Bb 13.6 and Dd 27.2, required the content?

Note. The method of multiplying together the half sums of the opposite sides of a trapezium for the content is erroneous, and the more so the more oblique its angles are.

To draw the map set off Ab 28 perches and Ad 34.4, and there make the perpendiculars to their proper lengths, and join their extremities to those of the diagonal.

## PROB. XII.

To find the area of a circle, or an ellipsis.

#### RULE.

Multiply the square of the circle's diameter, or the product of the longest and shortest diameters of the ellipsis by .7854 for the area. Or, subtract 0.104909 from the double logarithm of the circle's diameter, or from the sum of the logarithms of those elliptic diameters, and the remainder will be the logarithm of the area.

Note. In any circle, the Diam. multi. by 3.14159, produces the Cir. Circum. div. by 3.14159, quotes the diam.

#### EXAMPLES.

1. How many acres are in a circle of a mile diameter?

1 Mile =320 per. log. 2.505150 2.505150 5.010300 0.104909 4|0)804?|5. log. 4.905391 4)2010.25 Answer, 502A. 2R. 25P.

2. A gentleman, knowing that the area of a circle is greater than that of any other figure of equal perimeter, walls in a circular deer park of 100 perches diameter, in which he makes an elliptical fish pond 10 perches long by 5 wide; required the length of his wall, content of his park, and area of his pond?

Answer, the wall 314.16 perches inclosing 49A. 14P. of which  $39\frac{1}{4}$  perches, or  $\frac{1}{4}$  of an acre nearly is appropriated to the pond.

## PROB. XIII.

The area of a circle given, to find its diameter

#### RULE.

To the logarithm of the area add 0.104909, and half the sum will be the logarithm of the diameter. Or, divide the area by .7854 and the square-root of the quotient will be the diameter.

#### EXAMPLES.

A horse in the midst of a meadow suppose,

Made fast to a stake by a line from his nose.

How long must this line be, that feeding all round,

Permits him to graze just an acre of ground?

Area in perches 160 log. 2.204120 0.104909 2)2.309029 Diameter 14.2733 log. 1.154514 Answer, 7.13665 per. = 117F. 9 In.

## PROB. XIV.

## Allowance for roads.

It is customary to deduct 6 acres out of 106 for roads; the land before the deduction is made may be termed the gross, and that remaining after such deduction, the neat.

## RULE.

The gross div. The neat mul. by 1.06, a quotes the neat. prod. the gross.

### EXAMPLES.

1. How much land must I inclose to have 850A. 2R. 20P. neat?

222

40|20. 4| 2.5 Acres. A. R. P. 850.625×1.06=901.6625=901.2.26. the ans.

2. How much neat land is there in a tract of 901A. 2R. 26P. gross?

40|26. 4| 2.65 Acres. A. R. P. 1.06)901.6625(850.625=850. 2. 20. the answ. 848 &c.

Note. These two operations prove each other.

## PROB. XV.

To find the area of a piece of ground be it ever so irregular by dividing it into triangles and trajecia.

### PL. 7. fig. 4.

We here admit the survey to be taken and protracted; by having therefore the map, and knowing the scale by which it was laid down, the content may be thus obtained.

Dispose the given map into triangles, by fine pencilled lines, such as are here represented in the scheme, and number the triangles with 1, 2, 3, 4, &c. Your map being thus prepared, rule a table with four columns; the first of which is for the number of the triangle, the second for the base of it, the third for the perpendicular, and the fourth for the content in perches.

Then proceed to measure the base of number 1, from the scale of perches the map was laid down, and place that in the second column of the table, under the word base; and from the angle opposite to the base, open your compasses so, as when one foot is in the angular point, the other being moved backwards and forwards, may just touch the base line, and neither go the least above or beneath it; that distance in the compasses measured from the same scale, is the length of that perpendicular, which place in the third column, under the word perpendicular.

If the perpendiculars of two triangles fall on one and the same base, it is unnecessary to put down the base twice, but insert the second perpendicular opposite to the number of the triangles in the table, and join it with the other perpendicular by a brace as No. 1 & 2, 4 & 5, 6 & 7, 9 & 10, &c.

Proceed after this manner, till you have measured all the triangles; and then by prob. 6. find the content in perches of each respective triangle, which severally place in the table opposite to the number of the triangle, in the fourth column, under the word content.

But where two perpendiculars are joined together in the table, by a brace having both one and the same base; find the content of each (being a trapezium) in perches, by prob. 11. which place opposite the middle of those perpendiculars, in the fourth column, under the word content.

Having thus obtained the content of each respective triangle and trapezium, which the map contains, add them all together, and their sum will be the content of the map in perches; which being divided by 160, gives the content in acres. Thus, for

## EXAMPLES.

No.	Base.	Perpend.	Content.
1	24.8	17.0	412.92
2 3	28.2	16.3 5	225.6
4	39.8	19.6	712.42
5	49.4	16.25	ILATE
7	49.4	29.0	1086.8
8	38.7	6.7	129.64
9	40.0	17.0	600.
11	42.8	10.2	481.5
12	000	12.3	11.00
13	26.2	17.9	234.49
15	24.0	10.0	259.2
Content in perches 4142.57			
Cont	ent in l	perches	4142.57

This being divided by 160, will give 25A. 3R. 22P. the content of the map.

Let your map be laid down by the largest scale your paper will admit, for then the bases and perpendiculars can be measured with greater accuracy than when laid down by a smaller scale, and if possible measure from scales divided diagonally.

If the bases and perpendiculars were measured by four-pole chains, the content of every triangle and trapezium, may be had as before, in problems 6, and 11, and consequently the whole content of the map.

If any part of your map has short or crooked bounds, as those represented in plate 7. fig. 5. then by the straight edge of a transparent horn, draw a fine pencilled line as AB to balance the parts taken and left out, as also another, BC: these parts when small, may be balanced very nearly by the eye, or they may be more accurately balanced by method the third. Join the points A and C by a line, so will the content of the triangle ABC, be equal to that contained between the line AC, and the crooked boundary from A to B, and to C: by this method the number of triangles will be greatly lessened, and the content become more certain; for the fewer operations you have, the less subject will you be to err: and if an error be committed, the sooner it may be discovered.

The lines of the map should be drawn small, and neat, as well as the bases; the compasses neatly pointed, and scale accurately divided; without all which you may err greatly. The multiplications should be run over twice at least, as also the addition of the column content.

From what has been said, it will be easy to survey a field, by reducing it into triangles, and measuring the bases and perpendiculars by the chain. To ascertain the content only, it is not material to know at what part of the base the perpendicular was taken: since it has been shewn (in cor. to theo. 13. geom.) that triangles on the same base, and between the same parallels are equal; but if you would draw a map from the bases and perpen-

diculars, it is evident that you must know at what part of the base the perpendicular was taken in order to set it off in its due position; and hence the map is easily constructed.

## PROB. XVI.

To determine the area of a piece of ground, having the map given, by reducing it to one triangle equal thereto, and thence finding its content.

# PL. 8. fig. 5.

Let A B C D E F G H be a map of ground, which you would reduce to one triangle equal thereto.

Produce any line of the map, as AH, both ways, lay the edge of a parallel ruler from A to C, having B above it; hold the other side of the ruler, or that next you fast; open till the same edge touches B, and by it, with a protracting pin, mark the point  $\delta$ , on the produced line, lay the edge of the ruler from  $\delta$  to D, having C above it, hold the other side fast, open till the same edge touches C, and by it mark the point c, on the produced line. A line drawn from c to D will take in as much as it leaves out of the map.

Again lay the edge of the ruler from H to F, having G above it, keep the other side fast, open till the same edge touches G, and by it mark the point g, on the produced line; lay the edge of the ruler from g to E, having F above it, keep the other side fast, open till the same edge touches F, and by it mark the point f, on the produced line. Lay the edge of the ruler from f to D, having E

above it, keep the other side fast, open till the same edge touches E, and by it mark the point e, on the produced line. A line drawn from D to e, will take in as much as it leaves out. Thus have you the triangle c D e, equal to the irregular polygon A B C D E F G H.

If when the ruler's edge be applied to the points  $\mathcal{A}$  and C, the point  $\mathcal{B}$  talls under the ruler, hold that side next the said points fast, and draw back the other to any convenient distance; then hold this last side fast, and draw back the former edge to  $\mathcal{B}$ , and by it mark b, on the produced line; and thus a parallel may be drawn to any point under the ruler, as well as if it were above it. It is best to keep the point of your protracting pin in the last point in the extended line, till you lay the edge of the ruler from it to the next station, or you may mistake one point for another.

This may also be performed with a scale, or ruler, which has a thin sloped edge, called a fiducial, edge; and a fine pointed pair of compasses. Thus,

Lay that edge on the points A and C, take the distance from the point B to the edge of the scale, so that it may only touch it, in the same manner as you take the perpendicular of a triangle; carry that distance down by the edge of the scale parallel to it, to b; and there describe an arc on the point b; and if it just touches the ruler's edge, the point b is in the true place of the extended line. Lay then the fiducial edge of the scale from b to b, and take a distance from b, that will just touch the edge of the scale; carry that distance along the edge, till the point which was in b, cuts the produced line in b; keep that foot in b; and describe an arc, and if

it just touches the ruler's edge, the point c is in the true place of the extended line. Draw a line from c to D, and it will take in and leave out equally: in like manner the other side of the figure may be balanced by the line c D.

Let the point of your compasses be kept to the last point of the extended line, till you lay your scale from it to the next station, to prevent mistakes from the number of points.

That the triangle c D e, is equal to the right-lined figure ABCDEFGH, will be evident from problems 18. 19. geom for thereby, if a line were drawn from b to C, it will give and take equally, and then the figure b C D E F G H, will be equal to the map. Thus the figure is lessened by one side, and by the next balance line will lessen it by two, and so on, and will give and take equally. In the same manner an equality will arise on the other side.

The area of the triangle is easily obtained, as before, and thus you have the area of the map.

It is best to extend one of the shortest lines of the polygon, because if a very long line be produced, the triangle will have one angle very obtuse, and consequently the other two very acute; in which case it will not be easy to determine exactly the length of the longest side, or the points where the balancing lines cut the extended one.

This method will be found very useful and ready in small enclosures, as well as very exact; it may be also used in large once, but great care must be taken of the points on the extended line, which will be crowded, as well as of not missing a station.

## PROB. XVII.

A map with its area being given, and its scale contied to be either drawn or mentioned; to find the scale.

CAST up the map by any scale whatsoever, and it will be

As the area found

Is to the square of the scale by which you cast up,
:: The given area of the map

To the square of the scale by which it was laid down.

The square roat of which will give the scale.

#### EXAMPLE.

A map whose area is 126A. 3R. 16P. being given; and the scale omitted to be either drawn or mentioned; to find the scale.

Suppose this map was cast up by a scale of 20 perches to an inch, and the content thereby produced be 31A. 2R. 34P.

As the area found, 31A. 2R. 34P.=5074P.

Is to the square of the scale by which it was cast up, that is to 20×20=400,

:: The given area of the map 126A. 3R. 16P. = 20296P.

To the square of the scale by which it was kild down.

5074: 400:: 20296: 1600 the square of the required scale.

Root. 1600(40 16 8(00

Answer. The map was laid down by a scale of 40 perches to an inch.

## PROB. XVIII.

How to find the true content of a survey, though it be taken by a chain that is too long or too short.

Let the map be constructed and its area found as if the chain were of the true length. And it will be,

As the square of the true chain
Is to the content of the map,
:: The square of the chain you surveyed by
To the true content of the map.

## EXAMPLE.

If a survey be taken with a chain which is 3 inches too long; or with one whose length is 42 feet 3 inches, and the map thereof be found to contain 920A. 2R. 20P. Required the true content.

As the square of 42F. OIn.=the square of 504 inches=254016.

Is to the content of the map 920A. 1R. 20P.= 147260P.

: The square of 42F. 3In.=the square of 507 inches=257049.

To the true content.

P. P. P. 250416: 147260: : 257049: 149019
A. R. P. 160)149019(931. 1. 19 Answer.

501

219

40)59(1R.

19P.

METHOD OF DETERMINING THE AREAS OF RIGHT-LINED FIGURES UNIVERSALLY, OR BY CALCULATION.

#### DEFINITIONS.

#### PL. 8. fig. 7.

- 1. MERIDIANS are north and south lines, which are supposed to pass through every station of the survey.
- 2. The difference of latitude, or the northing or southing of any stationary line, is the distance that one end of the line is north or south from the other end; or it is the distance which is intercepted on the meridian, between the beginning of the stationary line and a perpendicular drawn from the other end to that meridian. Thus, if N so be a meridian line passing through the point A of the line AB, then is Ab the difference of latitude or southing of that line.
- 3. The departure of any stationary line, is the nearest distance from one end of the line to a meridian passing through the other end. Thus Bb is the departure or easting of the line AB: but if CB be a meridian, and the measure of the stationary distance be taken from B to A; then is BC the difference of latitude, or northing, and AC the departure or westing of the line BA.

- 4. That meridian which passes through the first station, is sometimes called the first meridian; and sometimes it is a meridian passing on the east or west side of the map, at the distance of the breadth thereof, from east to west, set off from the first station.
- The meridian distance of any station is the distance thereof from the first meridian, whether it be supposed to pass through the first station, or on the east or west side of the map.

## THEO. I.

In every survey which is truly taken, the sum of the northings will be equal to that of the southings; and the sum of the eastings equal to that of the westings.

## PL. 9. fg. 1.

Let a, b, c, e, f, g, h, represent a plot or parcel of land Let a be the first station, b the second, c the third, &c. Let NS be a meridian line, then will all lines parallel thereto, which pass through the several stations, be meridians also; as ao, bs, cd, &c. and the lines bo, cs, de, &c. perpendicular to those, will be the east or west lines, or departures.

The northings, ei+go+hq=ao+bs+cd+fr the southings: for let the figure be completed; then it is plain that go+hq+rk=ao+bs+cd, and ei-rk=fr. If to the former part of this first equation ei-rk be added, and fr to the latter, then go+hq+ei=ao+bs+cd+fr; that is, the sum of the northings is equal to that of the southings.

H h

The eastings cs+qa=ob+de+if+rg+oh, the westings. For aq+yo (az) = de+if+rg+oh, and bo=cs-yo. If to the former part of this first equation, cs-yo be added, and bo to the latter, then cs+aq=ob+de+if+rg+oh; that is, the sum of the eastings is equal to that of the westings. 2. E. D.

## SCHOLIUM.

This theorem is of use to prove whether the field-work be truly taken, or not; for if the sum of the northings be equal to that of the southings, and the sum of the eastings to that of the westings, the field-work is right, otherwise not.

Since the proof and certainty of a survey depend on this truth, it will be necessary to shew how the difference of latitude and departure for any stationary line, whose course and distance are given, may be obtained by the table, usually called the Traverse Table.

To find the difference of Latitude and departure, by the Traverse Table.

This table is so contrived, that by finding therein the given course, and a distance not exceeding
120 miles, chains, perches, or feet, the difference of
latitude and departure is had by inspection: the
course is to be found at the top of the table when
under 45 degrees; but at the bottom of the table
when above 45 degrees. Each column signed with
a course consists of two parts, one for the difference

of latitude, marked Lat. the other for the departure, marked Dep. which names are both at the top and bottom of these columns. The distance is to be found in the column marked Dist. next the left hand margin of the page.

#### EXAMPLE:

In the use of this table, a few observations only are necessary.

- 1. If a station consist of any number of even chains or perches (which are almost the only measures used in surveying) the latitude and departure are found at sight under the bearing or course, if less than 45 degrees; or over it if more, and in a line with the distance.
- 2. If a station consist of any number of chains and perches, and decimals of a chain or perch, under the distance 10, the lat. and dep. will be found as above, either over or under the bearing; the decimal point or separatrix being removed one figure to the left, which leaves a figure to the right to spare.

If the distance be any number of chains or perches, and the decimals of a chain or perch, the lat. and dep. must be taken out at two or more operations, by taking out the lat. and dep. for the chains or perches in the first place; and then for the decimal parts.

To save the repeated trouble of additions, a judicious surveyor will always limit his stations to whole chains, or perches and lengths, which can commonly be done at every station, save the last.

1. In order to illustrate the foregoing observations, let us suppose a course or bearing, to be S. 35°. 15'E. and the distance 79 four-pole chains. Under 35°. 15', or 35! degrees; and opposite 79, we find 64. 52 for the latitude, and 45. 59 the departure, which signify that the end of that station differ in latitude from the beginning 64. 52 chains, and in departure 45. 59 chains.

Note. We are to understand the same things if the distance is given in perches or any other measures, the method of proceeding being exactly the same in every case.

Again, let the bearing be 54½ degrees and distance as before; then over said degrees we find the same numbers, only with this difference, that the lat. before found, will now be the dep. and the dep. the lat. because 54½ is the complement of 35½ degrees to 90, viz. lat. 45. 59. dep. 64. 52.

2. Suppose the same course, but the distance 7 chains 90 links, or as many perches. Here we find the same numbers, but the decimal point must be removed one figure to the left.

Thus, under 35th and in a line with 79 or 7.9, are

Lat. 6, 45 Dep. 4, 56

the 5 in the dep. being increased by 1, because the 9 is rejected; but over 54% we get

Lat. 4. 56 Dep. 6. 45 3. Let the course be as before, but the distance 7.79, then opposite

•	7. 70 9	Lat. 6. 29.	Dep. 4. 43
	-		
	<b>7</b> . 79	<b>6</b> . <b>36</b>	4. 49

# Or opposite

7. 00 . 79	Lat. 5. 72 . 64	Dep. 4. 03 . 46
7. 79	<b>6. 36</b>	4. 49

## THEO. II.

# When the first meridian passes through the map.

If the east meridian distances in the middle of each line be multiplied into the particular southing, and the west meridian distances into the particular northing, the sum of these products will be the area of the map.

#### PL. 10. fig. 1.

Let the figure abkm be a map, the lines, ab bk to the southward, and km ma to the northward, NS the first meridian line passing through the first station a.

The meridian 
$$\begin{cases} zd \times ao \\ \text{Distances east} \end{cases}$$
  $\begin{cases} zd \times ao \\ tu \times ex(by) \end{cases}$  is Area  $\begin{cases} am \\ ow \end{cases}$ 
The meridian  $\begin{cases} ef \times gx \\ hh \times ga(my) \end{cases}$  = Area  $\begin{cases} xp \\ sl \end{cases}$ 

These four areas am+ow+xp+gl will be the area of the whole figure cmswiprle, which is equal to the area of the map abkm. Complete the

figure.

The parallelograms am and ow, are made of the east meridian distances dz and tu, multiplied into the southings ao and ox. The parallelograms xp and gl are composed of the west meridian distances ef and hh, multiplied into the northings xg and ga (my) but these four par llelograms are equal to the area of the map; for if from them be taken the four triangles marked Z, and in the place of those be substituted the four triangles marked O, which are equal to the former; then it is plain the area of the map will be equal to the four parallelograms. 2. E. D.

## THEO, III.

If the meridian distance when east, be multiplied into the southings, and the meridian distance when west be multiplied into the northings, the sum of these less by the meridian distance when west, multiplied into the southings, is the area of the survey.

PL. 10. fig. 2.

# Let abc be the map.

The figure being completed, the rectangle of is made of the meridian distance cq when east, multiplied into the southing an; the rectangle yk is made of the meridian distance xw, multiplied into the northings cz or ya. These two rectangles, or parallelograms, af +yk, make the area of the figure dfnyikd, from which taking the rectangle oy, made of the meridian distance tu when west, into the southings oh or bm, the remainder is the area of the figure dfohikd, which is equal to the area of the map.

Let bou=Y, urih=L, ric=O, wrc=Z=, akw=K, and efb=B, ade=A. I say, that Y+Z+B=K+L+A.

Y=L+O, add Z to both, then Y+Z=L+O+Z; but Z+O=K, put K instead of Z+O; then Y+Z=L+K, add to both sides the equal triangles B and A, then Y+Z+B=L+K+A. If therefore B+Y+Z be taken from abc, and in lieu thereof we put L+K+A, we shall have the figure dfohikd=abc, but that figure is made up of the meridian distance when east, multiplied into the southing, and the meridian distance, when west, multiplied into the northing less by the meridian distance, when west, multiplied into the southing. Q. E. D.

#### COROLLARY.

Since the meridian distance (when west) multiplied into the southing, is to be subtracted, by the same reasoning the meridian distance when east, multiplied into the northing, must be also subtracted.

#### SCHOLIUM.

From the two preceding theorems we learn how to find the area of the map, when the first meridian passes through it; that is, when one part of the map lies on the east and the other on the west side of that meridian. Thus,

#### RULE.

The merid. \ east \ \ multiplied \ \ southings \ \ Dist. when \ west \ \ into the \ \ northings \ \ their sum is the area of the map.

## But,

The merid { east } multiplied { northings }
Dist when { west } into the { southings }
the sum of these products taken from the former
gives the area of the map.

These theorems are true, when the surveyor keeps the land he surveys, on his right hand, which we suppose through the whole to be done; but if he goes the contrary way, call the southings northings, and the northings southings; and the same rule will hold good.

# General Rule for finding the Meridian distances.

- 1. The meridian distance and departure, both east, or both west, their sum is the meridian distance of the same name.
- The meridian distance and departure of different names; that is, one east and the other west, their difference is the meridian distance of the same name with the greater.

Thus in the first method of finding the area, as in the following field-book.

The first departure is put opposite the northing or southing of the first station, and is the first meridian distance of the same name. Thus if the first departure be east, the first meridian distance will be the same as the departure, and east also; and if west, it will be the same way.

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UT	А	Mr.	A5.

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The first meridian distance The next departure	6.61 E. 6.61 E.	
The second meridian distance The next departure	13.92 E. 1.80 E.	
The third meridian distance	15.02 E.	
At station 5, the meridian distance The next departure	5.78 E. 7.76 W.	
The next meridian distance	1.98 W.	
At station 11, the meridian distance 0.12 W. The next departure 5.84 E.		
The next meridian distance	5.72 E.	

#### PL. 10. fig. 3.

In the 5th and 11th stations, the meridian distance being less than the departures, and of a contrary name, the map will cross the first meridian, and will pass as in the 5th line, from the east to the west line of the meridian; and in the 11th line it will again cross from the east to the west side, which will evidently appear, if the field-work be protracted, and the meridian line passing through the first station, be drawn through the map.

The field-book cast up by the first method, will be evident from the two foregoing theorems, and therefore requires no further explanation; but to find the area, by the second method, take this

#### RULE.

When the meridian distances are east, put the products of north and south areas in their proper columns; but when west, in their contrary columns; that is, in the column of south area, when the difference of latitude is north; and in north when south: the reason of which is plain, from the two last theorems. The difference of these two columns will be the area of the map.

No. St. Bearings. C. L. Lat.and Merid. Area. Dedu halfDep Dist.  1 NE 75 13.70 E 6.61 E 23.394  N 9.67 15.02 E	
1 NE 75 13.70 E 6.61 13.22 E 23.399	14
N 0 57 15 09 V	觚
2 NE 204 10.30 E 1.80 15.82 E	30
3 East 16.20 E 8.10 33.02 E	
6 SW 33 3 35.30 S29.4423.28 E 685.3632	
5 SW 76 16.00 S 3.87 5.78 E 22.3686 W7.76 1.98 W	
6 North 9.00 N 9.00 1.98 W 17.8200	
7 SW 84 11.60 S 1.21 7.75 W 9.37	75
8 NW 53 <sup>1</sup> / <sub>4</sub> 11.60 N 6.94 18.16 W 126.0304	
9 NE 363 19.20 N 15.68 17.06 W 262.3828	1
10 NE 221 14.00 N12.93 8.64 W 111.7152	1
11 SE 761 12.00 S 2.75 0.12 W E 5.84 5.72 E 0.330	00
12 SW 15 10.85 S 10.48 4.32 E 45.2736 W 1.40 2.92 E	
13 SW 162 10.12 S 9.69 1.46 E 14.1474	
1285,1012 178,0499	19
Content in chains, 1107.0513	

# 4 The foregoing Field-Book, Method II.

is needless here to insert the columns of bearing or distances in chains, they being the same as before.

-					217	15.30
No St			Dep.	Merid. Dist.	N. Area.	S. Area
1		NE	3.54	6.61 E 13.22 E	23.3994	4.33
-	2	NE	9.65	15.02 E 16.82 E	THE STATE OF STREET	
2	3	E	0.00	24.92 E 33.02 E		3717
Te	1	s W	29.44	23.28 E 13.54 E		685.3632
-		SW	3.87	5.78 E 1.98 W		22.3686
T	5	N	9.00	1.98 W		17.8200
	7	S	1.21	7.75 W 13.52 W	13 2775	1000
	8	NW	6.94	18.16 W 22.80 W	W. S. S. S.	126.0303
-	9	NE	15.38	17.06 W	20.31	262.3828
1	0	NE	12.93	8.64 W 5.96 W		111,7152
1	1	SE	2.75	0.12 W 5.72 E	0.3300	
1	3	SW	10.48	4.32 E 2.92 E	STEEL STEEL	45.2736
1	3	SW	9.69	1.46 E	THE REAL PROPERTY.	14.1674
-		144		0.00	178.0499	1284.1012 178.0499
1	Λ	rea	in chai	ns, as be	fore,	1107.0513
-						

Construction of the Man from either the 1st or the 2d Table.

## PL. 10. fig. 3.

Draw the line NS for a north and south line, which call the first meridian; in this line assume any point, as I, for the first station. Set the northing of that stationary line, which is 3.54, from I to 2, on the said meridian line. Upon the point 2 raise a perpendicular to the eastward, the meridian distance being easterly, and upon it set 13.22, the second number in the column of meridian distance from 2 to 2, and draw the line 1 2, for the first distance line : from 2 upon the first meridian, set the northing of the second stationary line, that is, 9.65 to 3, and on the point 3 erect a perpendicular eastward, upon which let the meridian distance of the second station 16.82, from 3 to 3, and draw the line 23, for the distance line of the second station. And since the third station has neither northing nor southing, set the meridian distance of it 33.02, from 3 to 4, for the distance line of the third station. To the fourth station there is 29.44, southing, which set from 3 to 5; upon the point 5, erect the perpendicular 55; on which lay 13.54, and draw the line 4 to 5.

In the like manner proceed to set the northings and southings on the first meridian, and the meridian distances upon the perpendiculars raised to the east or west; the extremities of which connected by right lines, will complete the map. A Specimen of the Pennsylvania Method of CALCULATION; which, for its Simplicity and Ease, in finding the Meridian Distances, is supposed to be preferable in Practice to any Thing heretofore published on the Subject.

IND in the first place, by the Traverse Table, the lat. and dep. for the several courses and distances, as already taught; and if the survey be truly taken, the sums of the northings and southings will be equal, and also those of the eastings and westings. Then in the next place, find the meridian distances, by choosing such a place in the column of eastings or westings, as will admit of a continual addition of one, and subtraction of the other; by which means we avoid the inconvenience of changing the denomination of either of the departures.

The learner must not expect that in real practice the columns of lat. and those of dep. will exactly balance when they are at first added up, for little inaccuracies will arise, both from the observations taken in the field, and in chaining; which to adjust, previous to finding the meridian distances, we may observe, That if, in small surveys, the difference amount to two tenths of a perch for every station, there must have been some error committed in the field; and the best way in this case, will be to rectify it on the ground by a re-survey, or at least as much as will discover the error. But when the differences are within those limits, the work may be balanced in the following manner: on a slate, or separate piece of paper, find the lat. and dep. to each course and distance,

as in the following example, observing to add an half of the differences to the numbers in the lesser column, and to subtract it from those of the greater, in such manner, as that the numbers may be altered nearly in proportion to their corresponding distances.

	į.	-						Bee!	201	Sec.	Z	4	1
	1	20			6	5		8	00		No.	-	
	1	20,7	?	M	S. 8	00	z	Z	N.	8.	Co	Seld	ž
	1	50	77	West.	W B	S. 81 E	orth.	. 36 E	S M	40 W	Courses	No	ā
		92,69	P	1 1		8			뚭		٥	65	y
-	U	69 1	Y	130	187	186	2	25	68	0.2	Per.		ï
lip &	Diff	9	218.0		i,		54.0	101	62,9		Z	ľ	ı
14		W.	=	4			10	-	9			P	W
10	4	218.0	218.4	V	135.7	29,1	u		b	53.6	gs	From the Tables	EXAMPLE
	-	100	1 91	5		-			1	100			100
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		I	257,0	113				1	10	4	1	*	1
		ı		130.0	9.4		8	1	62.9	45.0			ı
		U	218.2		1	1	5	101.2	16	1	Z		l
		R			1	1	54.0	20	63.0		1		ı
		3	218.2 257.1		135,0	29.		1	1	5.36	on	B	
		1	80	-	18	10	1	1	10	18	100	Jane	
		K	257			9.881		13.5		1	10	ed.	l
					-	16	1	16	1	1	1	1	1
			257.1	130.0	1 2	1	1	1	62.9	45.0	15	-	-
			E	jö	2.61	1	1	1	lie	0	3		ı

The latitudes and departures being thus balanced. proceed to insert the meridian distances by the above method, where we still make use of the same field notes, only changing chains and links into perches and tenths of a perch. Then by looking along the column of departure, it is easy to observe, that in the columns of easting, opposite station 9, all the eastings may be added, and the westings subtracted without altering the denomination of either. Therefore by placing 46.0, the east departure belonging to this station in the column of meridian distances, and proceeding to add the eastings and subtract the westings, according to the rule aiready mentioned, we shall find that at station 8, these distances will end in 0, 0, or a cypher, if the additions and subtractions be rightly made. Then multiplying the upper meridian distance of each station by its respective northing or southing, the product will give the north or south area, as in the examples already insisted on, and which is fully exemplified in the annexed specimen. When these products are all made out, and placed in their respective columns, their difference will give double the area of the plot, or twice the number of acres contained in the survey. Divide this remainder by 2, and the quotient thence arising by 160 (the number of perches in an acre) then will this last quotient exhibit the number of acres and perches contained in the whole survey; which in this example may be called 110 acres, 103 perches, or 110 acres, 2 quarters, 23 perches.

FIELD-NOTES, of the two foregoing Methods, as Practised in Pennsylvania.

# Cast up by perches and tenths of a perch.

į.		_	_						
1	Courses.	Dist.	/ N.	S	E.	11.	MD	N. Area.	3. Areas
Fe.	N 75.00 E	54.8	14.2		52.9		2553 288.2	3341.26	
	N 20.30 E	41.3	38.6		14.4		302.6	11680.36	
,	East.	64.8			64.8		381.8 446.6		
4	3 33.30 W	14.12		117.7		77.9	;68.7 2.jo.8		43395-99
5	9 76.00 W	114.0		15.5		62.1	228 7 166 6		3544.85
12.6	No th.	36.0	36.0				166.6	5977.60	
57	\$ 84.00 W	46.4		4.9		46.1	74.4		590.45
3,	N 53.15 W	46.4	27 8			37.2	37.2	1034.16	
9	N 36.45 E	76.8	61.5		46.0		46.0 92.0	2829.00	
10	N 22.30 E	56.0	51.7		21.4		113.4 134 X	5862.78	
11	S 76.45 E	48.0		11.0	46.7		181.5		1996.50
12	9 15.00 W	+3•4		41.6		11.2	217.0 201.8		9092 30
23	S 16.45 W	40.5		38.8		11.7	197.1		7531.08
			229.8	229.8	246.2	246.2		30745.16	30745.16
								2	15406 21
							Area in	perches.	17703005
								•	

SECTION. IV.

### OF OFF-SETS.

IN taking surveys it is unnecessary and unusual to make a station at every angular point, because the field-work can be taken with much greater expedition, by using off-sets and intersections, and with equal certainty; especially where creeks, &c. bound the survey.

Off-sets are perpendicular lines drawn or measured from the angular points of the land, that lie on the right or left hand to the stationary distance, thus,

## Pt. 11. fig. 2.

Let the black lines represent the boundaries of a farm or township: and let 1 be the first station; then if you have a good view to 2, omit the angular points between 1 and 2, and take the bearing and length of the stationary line 1, 2, and insert them in your field-book: but in chaining from 1 to 2, stop at d opposite the angular point a, and in your field-book insert the distance from 1 to d, which admit to be 4C. 25L. as well as the measure of the off-set ad, which admit to be 1C. 12L. thus: by the side of your field-book in a line with the first station, say at 4C. 25L. L. 1C. 12L. that is, at 4C. 25L. there is an off-set to the left hand of 1C. 12L.

This done, proceed on your distance line to e opposite to the angle b, and measure eb, supposing then 1 e to be 7C. 40L. and eb 3C. 40L. say (still in a line with the first station in your field-book) "at 7C. 40L. L. 3C. 40L." that is, at 7C. 40L. there is an off-set to the left of 3C. 40L. proceed then with your distance line to f opposite to the angle c, and measure fc; suppose then 1 f to be 13C. and fc 1C. 25L. say in the same line as before, at 13C. L. 1C. 25L. Then proceed from f to 2, and you will have the measure of the entire stationary line 1, 2, which insert in its proper column by the bearing.

In taking off-sets, it is necessary to have a perch chain, or a staff of half a perch, divided into links for measuring them; for by these means the chain in the stationary line is undisturbed, and the number of chains and links in that line from whence, or to which, the off-sets are taken, may be readily

known.

Having arrived at the second station, if you find your view will carry you to 3, take the bearing from 2 to 3, and in measuring the distance line, stop at l'opposite g; admit 2l to be 4C. 10L. and the off-set lg 1C. 20L. then in a line with the second station in your field-book, say at 4C, 10L. R. 1C. 20L. that is, the off-set is a right hand one of IC. 20L. Again at m, which suppose to be 10C. 25L, from 2; take the off-set mh of 1C. 15L. and in a line with the second station, say at 10C. 25L. R. 1C. 15L. In the same line when you come to the boundary at i, insert the distance 2i, 13C. 10L. thus, at 13C. 10L. 0; that is, at 13C. 10L. there is no off-set. At n, which is 15C. from 2, take the offset nk 45L, and still opposite to the second station say at 15C L. 45. L.

Let the line, 3, 6, represent the boundary, which by means of water, briers, or any other impediment cannot be measured. In this case make one or more stations within or without the land, where the distances may be measured, and draw a line from the beginning of the first to the end of the last distance, thus; make stations at 3, 4, and 5, taking the bearings, and measuring the distances as usual, which insert in your field-book, and draw a mark like one side of a parenthesis, from the third to the fifth station, to shew that a line drawn from the third station to the farthest end of the fifth stationary line will express the boundary. Thus,

No. Sta.	Deg.	Ch. L.
(3	1721	5.45
14	200	13.25
(4	250	3.36

Suppose the point p of the boundary to be inaccessible, by means of the lines 6p or p7, being overflowed, or that of a quarry, furze, &c. might prevent your taking their lengths; in this case take the bearing of the line 6, 7, which insert opposite to the sixth station in your field-book with the other bearing; then direct the index to the point p, and insert its bearings on the left side of the field-book, opposite to the sixth station, annexing thereto the words, Int. for boundary; and having measured and inserted the distance 6, 7, set the index in the direction of the line 7p, and insert its bearing on the left of the seventh station of the field-book, annexing thereto the words Int. for boundary: the crossing or intersection of these two bearings will determine the point p, and of course the boundary 6p7 is also determined.

If your view will then reach in the first station,

take its bearing, stationary line, and off-sets, as before, and you have the field-book completed. Thus,

The Field-Book.

Remarks and intersect.	N.1 St.	Deg.	C. L.	OFF-SETS.
318 Int. to a tower	1	35 <b>8</b>	22.12	At 4 C. 2 L. L. 1C. 12L at 7C 40L. L. 3C. 40L. at 13C. L. 1C. 25L.
231 1 Int. to ditto	2	297 <b></b>	22.12	At 4C. 10L. R. 1C. 20L. at 10C. 25L. R. 1C. 51L. at 1SC. 10L. 0. at 15C. L. 45L.
155¼ Int. for bound. 274 Int. for ditto.		200° 250 125	5.45 13.25 3.36 15.15	At 1C. 20L. L. 2C

Close at the first station.

If you would lay down a tower, house, or any other remarkable object in its proper place; from any two stations take bearings to the object, and their intersection will determine the place where you are to insert it, in the manner that the tower is set out in the figure, from the intersection taken at the first and second stations of the above field-book.

A protraction of this will render all plain, on which lay off all your off-sets and intersections, and proceed to find the content by any of the methods in section the 4th.

The foregoing field-book may be otherwise kept, thus,

Remarks and intersection.	1	Deg.	L.han Offset Ch.L.	Dist. Ch.L.	R.han. Off-si Ch.L.
318 Int. to a tower	1	358	1.12 3.40 1.25	4.25 7.40 13.00 22.12	
2321 Int. for ditto.	2	297 <del>3</del>	0.45	4.10 10.25 13.10 15.00 21.21	1.20
155 $\frac{1}{2}$ Int. for bound.	3 4 5 6	172; 200 250 125		5.45 13.25 3.36 15.15	
274 In. for boundary.	7	105	2.20 2.32	1.20 7.45 11.25 12.25 15.10	0.36

How to cast up off-sets by the pen.

$$1, 2-1f=2f-1e=fe, 1e-1d=ed.$$

Then  $1d \times \frac{1}{2}da = 1da$ , by prob 6, page 183, and  $\frac{1}{2}ed \times da + fc = befc$ , and  $2f \times \frac{1}{2}fc = cf9$ ; the sum

of all which will be labc21; the area contained between the stationary line 1, 2, and the boundary, 1 abc 2.

In the same manner you may find the area of 2ihg2 of ik3i, as well as what is without and withinside of the stationary line 7, 1.

If therefore the left hand off-sets exceed the right hand ones, it is plain, the excess must be added to the area within the stationary lines, but if the right hand off-sets exceed the left hand ones, the difference must be deducted from the said area; if the ground be kept on the right hand as we have all along supposed; or in words thus;

# To find the contents of off-sets.

- 1. From the distance line, take the distance to the preceding off-set, and from that the distance of the one preceding it, &c. in four-pole chains; so will you have the respective distances from off-set to off-set, but in a retrogade order.
- 2. Multiply the last of these remainders by ½ the first off-set, the next by ¼ the sum of the first and second, the next by half the sum of the second and third, the next by half the sum of the third and fourth, &c. The sum of these will be the area produced by the off-sets.

Thus, in the foregoing field-book, the first stationary line is 22C. 12L. or 11C. 12L. of four pole-chains. See the figure.

From	Ch. L.	Ch. L.	Ch. L.
	11.12=1,2	6.50=1f	3.90=1e
	6.50=1f	3.90=1e	2.25=1d
	4.62 <u>-</u> 2f	2.60=ef	1.65=ed

Ch. L.

 $1d=2.25\times32$ L. half the first off-set= .7200  $ed=1.65\times1$ C. 26L. $\frac{1}{2}$  the sum of the 1st and 2d 2.0790  $ef=2.60\times1$ C. 32L. $\frac{1}{2}$  the sum of 2d and 3d=3.4320  $2f=4.62\times37$ L. half the last off-set= 1.7094 Content of left off-sets on the first dist. in square four-pole chains 7.9404

In like manner the rest are performed.

The sum of the left hand off-sets will be
And the sum of the right hand ones

14.0856 3.6825

Excess of left hand off-sets in squ. 4 pole C. 10.4031 Acres 1.04031

.16124

Perches

6.4496

Excess of left hand off-sets above the right hand ones, 1A. OR. 6P. to be added to the area within the stationary lines.

#### SECTION V.

To find the area of a piece of Ground by intersections only, when all the angles of the field can be seen from any two Stations on the outside of the ground.

#### PL. 12. fig. 1.

LET ABCDEFG be a field, H and I two places on the outside of it, from whence an object at every angle of the field may be seen.

Take the bearing and distance between H and I, set that at the head of your field-book, as in the annexed one. Fix your instrument at H, from whence take the bearings of the several angular points A, B, C, D, &c. as they are here represented by the lines HA, HB, HC, HD, &c. Again fix your instrument at I, and take bearings to the same angular points, represented by the lines IA, IB, IC, ID, &c. and let the first bearings be entered in the second column, and the second bearings in the third column, of your field-book; then it is plain that the points of intersection, made from the bearings in the second and third columns of every line, will be the angular points of the field, or the points A, B, C, D, &c. which points being joined by right lines, will give the plan ABCDEFGHA required.

Bear. 180	Dis.	28C. of	the S	ta. H and I.
	No.	Bear.	Bear.	
	A	261 t	3311	
	В	265≩		
	C	248	3071	
	D	238		
	E	$215^{1}_{2}$	262‡	
	F	<b>3</b> 08‡	286±	
	G	220	300	

The same may be done from any two stations within-side of the land, from whence all the angles of the field can be seen.

This method will be found useful in case the stationary distances from any cause prove inaccessible, or should it be required to be done by one party, when the other in whose possession it is, refuses to admit you to go on the land.

To find the content of a field by calculation, which was taken by intersection.

In the triangle AIH, the angles AHI, AIH, and the base HI being known, the perpendicular Aa, and the segments of the base Ha, AI may be obtained by trigonometry: and in the same manner all the other perpendiculars Bb, Cc, Dd, Ee, If, Gg, and theseveral segments at b, c,d, e, f, and g: if therefore the several perpendiculars be supposed to be drawn into the scheme (which are here omitted to prevent confusion arising from a multiplicity of lines) it is plain that if from bBCDEeb, there be taken bBAGFeb, the remainder will be the map ABCDEFG.1.

As before half the sum of Bb, and Cc multiplied by bc, will be the area of the trapezium bBCc; after the same manner, half the sum of Cc, and Dd, multiplied by cd, will give the area of the trapezium cCDd; and again, half the sum of Dd, and Ee multiplied by de, gives the area of the trapezium dDEe; and the sum of these three trapezia will be the area of the figure bBCDeb.

Again, in the same manner, half the sum of Bb and Aa multiplied by ah, will give the area of the trapezium BbAa; and half the sum of aA, and gG, by ag, gives the trapezium aAGg; to these add the trapezia gGFf, and fFEe, which are found in the like manner, and you will have the figure bBAGFEeb, and this taken from bBCDeb, will leave the map ABCDEFGA. 2. E. F.

It will be sufficient to protract this kind of work, and from the map to determine the area as well as in plate 10. fig. 3. to find the areas of the pieces, 3, 4, 5, 6, 3, and 6, 7, 7, 6, from geometrical constructions.

How to determine the station where a fault has been committed in a field book, without the trouble of going round the whole ground a second time.

From every fourth or fifth station, if they be not very long ones, or oftener if they are, let an intersection be taken to any object, as to any particular part of a castle, house, or cock of hay, &c. or if all these be wanting, to a long staff with a white sheet or napkin set thereon, to render the object more conspicuous, and let this be placed on the summit of the land, and let the respective intersections so

taken be inserted on the left hand side of the fieldbook, opposite to the stations from whence they were respectively taken.

In your protraction as you proceed, let every intersection be laid off from the respective stations from whence they were taken, and let these lines be continued; if they all converge or meet in one point, we thence conclude all is right, or so far as they do converge; but if we find a line of intersection to diverge or fly off from the rest; we may be sure that either a mistake has happened between the station the foregoing intersection was taken at, and the station from whence the intersection line diverges, or there must be an error in the intersection; but to be assured in which of these the fault is, protract on to the next intersection, and having set it off, if it converges with the rest, though the foregoing one did not, we may conclude the fault was committed in taking the last intersection but one, and none in any station, and that so far is true as is protracted; but if this as well as the foregoing intersection diverge or fly from the point of concourse or converging point of the rest, the error must have its rise from some station or stations, at or after that, from whence the last converging intersection line was taken: so that by going to that station on the ground, and proceeding on to that where the next, or from whence the following diverging intersection was taken, we can readily and with little trouble set all to rights.

But in most tracts of land, one object cannot be seen from every station, or from perhaps one fourth of them; in this case we are under the necessity to move the pole after we begin to lose sight of it, to some other part of the land, where

it may be seen from as many more stations as possible; which is easily done by viewing the boundary before it be surveyed: the pole then being fixed in an advantageous place, the first intersection to it is best to be made from the same station from whence the last one was taken, and then as often as may be thought convenient, as before; in like manner the whole may be done by the removal of the pole.

When we here speak of stations, we do not mean such at are usually taken at every particular angle of the field: for it is to be apprehended, that every skilful surveyor, particularly such who use calculation, vill take the longest distances possible, not only tolessen the number of stations, for the ease of either protraction or calculation, but with greater certainty to account for the land passed by, on the right hand or on the left, which is taken by off-ses: and surely it will be allowed that any measure aken on the ground, and the content thence arithmetically computed, will be much more accurate than that which is obtained from any geometrical projection.

From what has been said it is plain, that from this method any fault committed in a survey can be readly determined, and therefore must be much preferble to the present method of taking diagonals, c the bearings and lengths of lines across land, b accomplish that end; which last method is too requently used by surveyors to approximate or arrie near the content, which will ever remain uncertin, let these diagonals be ever so many, till the station or stations wherein the error or errors were committed, be found; and the fault or fault be corrected.

Where one diagonal is taken, it may perhaps close or meet with one part of the survey and not with the other; in this case, if the surveyor would discover his error, he must survey that part of the land which did not close, and this may be half or more, of the whole. And should the diagonal close with neither part, but be too long, or too short, or should it fall on either side of the assigned point it was to close with, he ought to go over the whole, and make a new survey of it in order to discover his error.

A number of diagonals are frequently taken, the sum of the lengths of which very often exceeds the circuit of the ground, and after all they are but approximations; and the content remains uncertain as before; therefore he who returns a map, nade up by the assistance of diagonals, where there remains a misclosure in any one part, runs the risque of being detected in an error, and must suffer measiness in his mind, as he cannot be certain of the return he makes.

The frequent misclosures which are botcled up by diagonals, occasion the many and frequen scandalous broils and animosities between sureyors, which tend to the loss of character of the oncor the other, and indeed often to the disrepute o both, as well as to that of the science they profess

But these may be easily remedied by intersections, and the bearing or line to be adjusted where the fault was committed, and till this be foundnothing can be certain.

#### SECTION VI.

#### TO ENLARGE OR DIMINISH MAPS.

To enlarge or diminish a map, or to reduce a map from one scale to another; also the manner of uniting separate maps of lands which join each other, into one Map of any assigned size.

AY the map you would enlarge, over the paper on which you would enlarge it, and with a fine protracting pin, prick through every angular point of your map, join these points on your paper (laying the map you copy before you) by pencilled or popped lines, and you have the copy of the map you are to enlarge: in this manner any protraction may be copied on paper, vellum, or parchment, for a fair map.

If you would enlarge a map to a scale which is double, or treble, or quadruple to that of the map to be enlarged, the paper you must provide for its enlargement must be two, or three, or four times as long and broad as the map; for which purpose in large things you will findit necessary to join several sheets of paper, and to cement them with white wafer or paste, but the former is best.

Then pitch upon any point in your copied map for a centre; from whence if distances be taken to its extreme points, and thence if those distances be set in a right line with (but from) the centre, and these last points fall within your paper, the map may be increased on it to a scale as large again as its own; and if the like distances be again set outwards in right lines from the centre, and if these last points fall within your paper, it will contain a map increased to a scale three times as large as its own, &c.

## PL. 12. fig. 2.

Let the pricked or popped lines represent the copy of a down or old survey, laid down by a scale of 80 perches to an inch, and let it be required to enlarge it to one laid down by 40 to an inch.

Pitch upon your centre as O, from whence thro' a lay the fiducial edge of a thin ruler, with a fine pointed pair of compasses, take the distance from a to the centre O, and lay it by the ruler's edge from a to A: in the like manner take the distance from the next station b to the centre O, and lay it over in a right line from b to B, and join the points A and B by the right line AB; in the like manner set over the distance from every station to the centre, from that station outwards, and you will have every point to enlarge to; the joining of these constantly as you go on by right lines, will give you the enlarged map required.

In taking the distance from every station to the centre, set one foot of the compasses in the station, and the other very lightly over the centre-point, so lightly as scarcely to touch it, otherwise the centre-point will become so wide, that it may occasion several errors in the enlarged map: for

if you err from the exact centre but a little, that error will become double, or treble, or quadruple, as you enlarge to a scale that is double, or treble, or quadruple of the given one; therefore great accuracy is required in enlarging a map.

When you have done with a station, give a dash with a pen or pencil to it, such as at the station a and b; by this means you cannot be disappointed in missing a station, or in laying your ruler over one station twice.

From what has been said it is plain, that if a map is to be enlarged to one whose scale is double the given one, that the distances from the respective stations to the centre, being set over by the ruler's edge, will give the points for the enlarged one. And thus may a map be enlarged from a scale of 160 to one of 80, from one of 80 to one of 40, from one of 20 to one of 10 perches to an inch. &c. For to enlarge to a scale that is double, the number of perches to an inch for the enlarged map. must be half of those to an inch for that to be enlarged: to enlarge to a scale that is treble the given one, the number of perches to an inch for the enlarged map, will be one third of those for the other; if to a scale that is quadruple the given one, the number of perches to an inch for the enlarged map, will be one fourth of those for the other, &c. therefore if you would enlarge a map which is laid down by a scale of 120 perches to an inch, to one of 40 perches to an inch, the distance from the several stations to the centre, being set twice beyond the said stations, will mark out the several points required, for these points will be three times further from the centre than the stationary points of the map are.

In the same manner, if you would enlarge a map from a scale of 160, to one of 40 perches to an inch, the distance from the several stations to the centre, being set three times beyond said stations, will lay out the points for your enlarged map, for these points will be four times further from the centre than are the stations of the map.

When a map is enlarged to another, whose scale is double, or treble, or quadruple, &c. of the given one, every line, as well as the length and breadth of the enlarged map, will be double, or treble, or quadruple, &c. those of the given one, for it must be easy to conceive that those maps are like: but the area, if the scale be double, will be four times; if treble, nine times: if quadruple, sixteen times that of the given figure; that is, it will contain four, nine, or sixteen times as many square inches as the given one (for it has been shewn that like polygons are in a daplicate proportion with the homologous sides). Yet these figures being cast up by their respective scales, will produce the same content.

Thus much is sufficient for enlarging maps, and from hence, diminishing of them will be obvious; for one fourth, one third, or half the distances from the several stations to the centre, will mark out points, which if joined, will compose a map similar to the given one, whose scale will be four times, three times, or twice as small as the given one.

Thus, if we would reduce a map from 40 to 80, from 20 to 40, from 10 to 20 perches to an inch, &c. half the distance of the stations from the centre will give the points requisite for drawing the

map; if we would reduce from 40 to 120, from 20 to 60, from 10 to 30 perches to an inch, &c. one third of the distances to the centre, will give the points for the map: and if we would reduce from 40 to 160, from 20 to 80, from 10 to 40 perches to an inch, &c. one fourth of the distances to the centre, will give the points for the map.

By the methods here laid down I have reduced a map from a scale of 40 to one of 20 perches to an inch, which contained upwards of 1200 acres, and consisted of 224 separate divisions, without the least confusion from the lines; for none can arise if the methods here laid down be strictly observed.

I have also from the same methods reduced a large book of maps, each of which was an entire skin of parchment, and the whole contained upwards of 46000 acres, to a pocket volume; and afterwards connected all these maps into one map, which was contained in one skin of parchment: therefore upon the whole I do recommend these methods for reducing maps to be much more accurate than any of the methods commonly used, such as squaring of paper, using a parallelogram, proportionable compasses, or any other method I ever met with, though the figures to be reduced were ever so numerous, irregular, or complicated.

To unite separate maps of lands which join each other, into one map of any assigned size.

If there be several large maps contained in a book, each of which suppose to take up a skir

of parchment, or a sheet of the largest paper; which maps of lands join each other; and it be required to reduce them to so small a scale, that all of them when joined together may be contained in one skin, half a skin, or any assigned sized piece of parchment, or paper.

Having pricked off and copied the several maps on any kind of paper, unite them by cutting with scissors along the edge of one boundary which is adjoining the other, but not cutting by the edge of both, and throw aside the parts cut off; then lay these together on a large table, or on the floor, and where the boundaries agree, they will fit in with each other as indentures do; and after this manner they are easily connected: measure then the length and breadth of the entire connected maps, and the length and breadth of the parchment or paper you are confined to; if the former be three, four, or five times greater (that is, longer and broader) than the latter, reduce each copied map severally to a scale that is three, or four, or five times less, as before; and the same parts of the boundaries you cut by in the large maps, by the same you must also cut in small ones, and unite the small as the large ones were united; cementing them together with white wafer: thus will your map be reduced to the assigned size, which copy over fair, on the parchment, or paper you were confined to.

But it is not always that a person is confined to a given area of parchment, or paper; in such cases, if there are many large maps to be united into one, reduce each of them severally to a scale of 160 perches to an inch, and unite those by the contiguity or boundaries, as before: or if you have a few, it will be sufficient to reduce them to a scale of 120, &c. But having the maps given, and the scale by which they are laid down, your reason will be sufficient to direct you to know what scale they should be reduced to.

### Directions concerning surveys in general.

If you have a large quantity of ground to survey, which consists of many fields or holdings, and that it be required to map and give the respective contents of the same, it is best to make a survey of the whole first, and to be satisfied that it is truly taken, as well as to find its content; and as you go round the land, to make a note on the side of your field-book at every station where the boundary of any particular field or holding intersects or meets the surround; then proceed from any one of those stations, and in your field-book say, " proceed from such a station," and when you have gone round that field or division, insert the station you close at, and so through the whole: a little practice can only render this sufficiently familiar, and the method of protraction must be evident from the field-notes. When the whole is protracted, and you are satisfied of the closes of the particular divisions, cast up each severally, and if the sum of their contents be equal to the content of the whole first found, you may safely conclude that all is right.

The protraction being thus finished and cast up, transfer it on clean paper, vellum, or parchment, as before; be careful to draw your lines with a fine pen, write on it the names of the circumjacent lands, and set No. 1, 2, 3, 4, &c. in every parti-

cular field or division; let every tenant's particular holding be distinguished by a different coloured paint being run finely along the boundaries; let all the roads, rivulets, rivers, bridges, bogs, ponds, houses, castles, churches, beacons (or whatever else may be remarkable on the ground) be distinguished on the map. Write the title of the map in a neat compartment either drawn, or done from a good copper-plate graving, with the gentleman's arms. Prick off one of your parallels with the map, and on it make a mariner's compass. and draw a flower-de-luce to the north, and this will represent the magnetical north; after which set off the variation, which express in figures, and through the centre of the compass, let a true meridian line be drawn of about 3 inches long, by which write True Meridian. Let a scale be drawn, or it is sufficient to express the number of perches to an inch, the map was laid down by. Draw a reference table of three, or, if occasion be, of four or more columns; in the first insert the number of the field or holding: in the next its name, and by whom occupied: in the third the quantity of acres, roods, and perches it contains: if you have unprofitable land, as bog or mountain, let the quantity be inserted in the fourth column; and, if it be required, you may make another column for statute measure, and then the map is completed.

#### SECTION VII.

THE METHOD OF DIVIDING LAND, OR OF TAKING OFF OR IN-CLOSING ANY GIVEN QUANTITY.

#### Example 1.

#### PL. 12. fig. 1.

Let ABCD, &c. be a map of ground, containing 11 acres, it is required to cut off a piece as DEFGID, that shall contain 5 acres.

Join any two opposite stations as D and G, with the line DG, (which you may nearly judge to be the partition line) and find the area of the part DEFG, which suppose may want 3R. 20P. of the quantity you would cut off: measure the line DG, which suppose to be 70 perches. Divide 3R. 20P. or 140P. by 25, the  $\frac{1}{2}$  of DG, and the quotient 4 will be a perpendicular for a triangle whose base is 70, and the area 140P. Let HI be drawn parallel to DG, at the distance of the perpendicular 4, and from I, where it cuts the boundary, draw a line to D, and that line DI, will be the division line; or a line from G to H will have the same effect; all which must be evident from what has been already said.

But if hills, trees. &c. obstruct the view of the points D and I from each other, it will be necessary in order to run a partition line, to know its bearing; and it may be proper on some occasions, to have its length; both these may be easily calculated from the common field-notes only, as in the following example, without the trouble of any other measurement on the ground, or any dependance on the map and scale.

### EXAMPLE II.

PL. 12. fig. 3.

Let ABCDEFGHIA be a tract of land, to be divided into two equal parts, by a right line from the corner I to the opposite boundary CD; required the bearing and length of the partition line IN, by calculation, from the following field-notes, viz.

Fi	eld-	Notice	nel A	· ·
Boun.	II.	Bea	illing.	reich.
AB	N.	190	O'E	108.
BC.	S.	77.	OE	. 91.
CD	S.	27.	OE	. 115.
DE	S.	52.	ow	. 58.
March and Street		15.		76.
FG			st	70.9
100000000000000000000000000000000000000		36.		. 47.
HI			rth.	
IA	IN.	62.	15W	59.
100	152	A.	IR.	25.9P.

# Operation.

THE RESERVE AND ADDRESS OF THE PARTY OF THE	<b>DESCRIPTION</b>	N.	The second second	E. 1	W.	12
IA N. 62° 4 W. AB N. 19 E.		27.5 102.1	_		52,2	crid
	91		20.5	35.2 88.7	71.7	dist.
Area, 8722.3 per	ches	129.6	129.6	123.91	123.9	% C.

152A. 1R. 25.9P.=24385.9 perch. half, to be divided off, = 12192.9 the part IABCI = 8722.3 subt.

Triangle ICNI =3470.6 perches.

The second second	Per.	A STATE OF THE STA	S.	E.	W.   Z
	115	109.1		71.7	CIN
CD S. 27, E.	-	-	102.5	52.2	1000
Di	-	THE	6.6		143.9
Area, 6522.1	per.	109.1	109.1	122.0	123.9

Then, { ICDI: CD:: ICNI: CN } Th. 18
as { 6522.1:115:: 8470 6:61.19 } Sec. 1
which determines the point N in CD.

ICNI.	Per N	1.   5	E.	W.
IC as before CN S 27 E.		9.1 54.6	17.7 27.8	
NI	=	54.6	-	99.5

As dif. lat. 54.6 | As S. Bear. 61°15's : Radius S. 90 deg | : Depart. 99.5 : Depart. 99.5 | :: Radius S. 90 deg : Tang. Bear. 61°15's : Distance 113.49

Answer, { IN runs N. 61° 15′ E. } 113.5 per.

In the part IABCI, the difference between the northings and the southings of the three lines, IA, AB and BC (109.1) is the difference of latitude, and that of their eastings and westings (71.7) the departure of the line CI, which is placed thereto, so as to balance the columns; see theo. I. sect. 5. hence the content is obtained, as already taught, without the bearing or length of the line CI.

For the triangle *ICDI*, the diff. lat. and dep. of *IC* are taken from the preceding table, which is going from *I* to *C* will be northing and easting: those of *CD* are found by the bearing and distance, and of *DI* by balancing the columns, as before for *CI*.

The difference of latitude (54.6) and departure (99.5) of the line NI, in the third table are found by balancing those of IC and CN; and as they are the base and perpendicular of a right angled triangle, of which the line NI is the hypothenuse, and the angle opposite to the departure, the bearing, we have the answer by two trigonometrical statings, as above; and thus may any tract be accurately divided, or any proposed quantity readily cut off or inclosed.

Now the student or practitioner may calculate the content of the part ABCNIA (the bearing and distance, or the diff. lat. and dep. of CN and of NI being known) and if it be found equal to the intended quantity, it proves the truth of the operation

EXAMPLE III.

PL. 12. fig. 3.

It is proposed to cut off 38A. 16P<sub>2</sub>. to the south end of this tract, by a line running from E due West 40 perches to a well at O, and from thence a right line to a point M in the boundary HI; the place of M, and the bearing and length of the line OM are required; the field-notes being as in example 2d.

Answer, { M from H, north, 43.23 } perches.

### In this example we find,

The area of	OEFGHO =	5270.5
Consequently of	HOMH =	826.0
Dif. lat. of the line	HO=HV=	35.2
Departure of ditto	<b>_2</b> V =	38.2

As HI happens to be a meridian, the area of HOMH divided by half OV (19.1) quotes HM (43.23) without finding the area of HOIH, as we did of ICDI in example 2d. and HM—HV=VM=8.03 = dif. lat. of OM, which with its dep. VO=38.2 gives the bearing and distance as before.

#### EXAMPLE IV.

### Pl. 12. fig. 4.

A trapezoidal field ABCD, bounded as under specified, is to be divided into two equal parts by a right line EF parallel to AB or CD; required AF or BF?

Bou.	Bearing.	Per.	
	South.	30.	
BC	N. 80 W.	60.	
CD	N. 39‡ W. S. 60 E.	45.5	
DA	S. 80 E.	89.4	•
1	3A. 3R. 7P		١.
1		]	

In the triangle CBG are given BC and all the angles (known by the bearings) to find BG, and thence the area by prob. 9. sect. 4. which + half the area of ABCD=area of EFG; then as the area of CBG to that of EFG, so is the square of BG to the square of FG, and FG—BG=BF.

# Operation at large.

Angle G 39° 30', log. S. Co Ar. Side BC 60 per. log. Angle C 40° 30', sine	0.19649 1.77815 9.81254
Side BG 61.26 per, Side BC 60 per, Angle B 100° 0', sine	1.78718 1.77815 9.99335 add
2)3619.8, log.	3,55868
As $CBG = 1809.9$ Co. Ar. 1103.5 = BCEF	6.74235
To $EFG = 2913.4$ , log. So sqr. $BG$ 61.26, log.	3.46440 1.78718 1.78718
To sqr. FG 77.72	2)3.78111
Ansr. $BF = 16.46$ per.	1.89055

By the application of this method a tract of land may be divided accurately, in any proportion, by a line running in any assigned direction.

Note. When the practitioner would wish to be very accurate, it will be much better to work by four-pole chains and links than by perches and tenths; one tenth of a perch square being equal to 6½ square links.

#### EXAMPLE V.

The following Field-Notes (from A. Burns) are of a piece of land, which is proposed, as an example, to be divided into three equal parts by two right-lines running from the sixth and seventh stations; and proved, by calculating the content of the middle part.

St.	Bear	ng.	4P.C.
1	N.E.	56°‡	21.60
2	N.E.	26 <u>‡</u>	13.44
· 3	S.E.	711	18.96
4	S.E.	26}	13.44
5	8.W.	714	14.96
6	S.E.	45	9.47
7	S.E.	63 <u>k</u>	13.44
8	N.E.	45	8.47
9	S.E.	26½	13.44
10	s.w.	45	8.47
11	s.w.	631	13.44
12	N.W.	76	24.73
13	N.W.	363	30.00
A	A rea 167		P. 24.

## EXAMPLE VI.

PL. 8. fig. 5.

The plot ABCDEFGHA is proposed to be divided, geometrically, in the proportion of 2 to 3, by a right line from a given point in any boundary or angle thereof, suppose the point D.

Reduce the plot to the triangle cDe, as already taught; divide the base ce in the point N, so that eN be to Nc in the ratio of two or three, by prob. 14. page 53; draw DN, and it is done.

## EXAMPLE VII.

PL. 12. fig. 3

Example 2d may likewise be performed geometrically.

Produce CD both ways for a base, and reduce the whole to a triangle, making I the vertical point; then bisect the base in N, and draw IV. But,

Notwithstanding this geometrical method is demonstrably true in theory, it is not as safe, on practical occasions requiring accuracy, as the calculation, even when performed with the greatest care; for which reason we will not enlarge on it here.

#### EXAMPLE VIII.

Suppose 864 acres to be laid out in form of a right-angled parallelogram, of which the sides shall be in proportion as 5 to 3; required their dimensions?

For the greater side, multiply the area by the greater number of the given proportion, and divide

by the less, or, for the less side, multiply by the less number, and divide by the greater; the square root of the quotient will be the side required: thus,

864A.=138240P 5	1.38240 3
3)691200	5)411720
Answ. ✓ 230400=480.	<b>√</b> 8 <del>2944</del> =288.

## EXAMPLE IX

If it be required to lay out any quantity of ground, suppose 47A. 2R. 16P. in form of parallelogrem, of which the length is to exceed the breadth by a given difference, for instance 80 perches, then add the square of half this difference to the area, and take the square-root of the sum; to which add half the difference for the greater side, and subtract it therefrom for the less; thus,

2)80	47A.	2R.	16P.	=7616 perches.
40				
40			٧	9216=96
1600 hal	f diff.	add	and	subt.—40
	Anow	<b>S</b> tl	he len	$gth = \overline{136}$ $eadth = 56$
	ищям.	( tl	he bre	adth = 56

Any proposed quantity of ground may be laid out or inclosed in the form

of a Square - by prob. 2d. Parallelogram, 1 side giv. by pro. 4th. Triangle of a given base, by pro. 7th. Circle - by prob. 13th.

It is sometimes most convenient, when land is to be laid out adjacent to a creek, river, or other crooked boundary, to measure off-sets to the angles or bending thereof, from a right line or lines taken near such boundary, and to deduct the area of these off-sets from the given quantity, and then to lay off the remainder from the right-line or lines, in the desired form.

In laying out new lands, attention must be paid to the allowance for roads, as exemplified in prob. 14th.

# EXAMPLE X.

It is required to divide off 30 acres, to the south east end of the tract, of which the field-notes are given in example 4th, by a right-line to run N. 20° E. See example 4th.

#### BECTION VILL

#### of Surveying Harbours, Shoals, Sands, &c.

#### PL. 13. fig. 1.

HERE are three methods whereby this may be performed; for the observations may be made either on the water or on the land. Those made on the water are of two kinds, one by the log-line and compass (as in plane sailing measuring) the course and distance round the sand; and then to be plotted as a large wood, or any inclosure taken by the circumferentor.

This method I omit for two reasons; first, because it is to be deduced from the writers of navigation: and, secondly, because the distances thus measured are liable to the errors of currents, which generally attend shoals or sands near the shore.

The second method, where there are no distances to be measured on the water, though still there is one inconvenience, common also to the former, because the bearings or observations are to be taken on that unstable element (an error scarce mentioned by practical artists) I shall briefly hint at; and so rather choose a third, which is liable to neither of these imperfections.

Oο

Let a boat be manned out with a signal flag, a log and line, lead and line, and to observe the bearings of any land-mark, a compass with sights.

Take two or more objects or places, as A, B, C, on the shore, from whence the boat may be seen on the several parts of this shoal, and determine their relative position by bearing and distances either before or after the other necessary observations are made.

One of the boat's crew is to sound till he finds himself on the edge of the sand, by the depth of water, and then to come to an anchor; which he is to signify to two persons on the shore, at B and C, by his signal. And then from those known land-marks, B and C, the observers are to take the bearings of the boat, and to register their observations; which, when done, they are to signify to the crew by waving a flag, or by some other signal.

And in the mean time, to prevent mistakes, let the crew take the bearings of each of these landmarks: Then weigh anchor, which suppose at D.

Then by sounding, proceed to E, and make like observations. And so at E, F, G, &c. till you have surrounded your sand.

And if in this process, you are about to loose the sight of one of your land-marks suppose C, let your assistant at C, or B, who at that time will also be about to loose the sight of the boat, by signals (before agreed on) remove to some other object before-hand agreed on, suppose to H, or K; and then to proceed as before.

Lastly, if the sand runs so far out at sea, that the object cannot be seen by the boat, nor the boat by the observer on shore; there may be rockets fired by the boat's crew, and also by the observers on the shore in the night, whereby those bearings may be taken almost at as great a distance as the light can be seen. For supposing they rise but a quarter of a mile above the apparent horizon, its stay will be about 9 seconds, and its distance for this quarter of a mile will be visible about 44 miles.

But rockets rise much higher, and then the distances are much greater, whereby they are visible.

Or two boats may lay at anchor instead of the land marks, and then you may work as before.

Now, since the land-marks B and C are fixed, their position may be laid down in the draught, as in common surveying, by plotting the distance between B and C. And then, by plotting the line BD, and the line DC, according to their position, their common intersection will give the point D. And in like manner E, F, G, &c. may be plotted; and so the shoals completed. And this from the bearings taken at B and C.

If this be a standing lake, environed by bogs, or other impediments, the observations at D, E, F, &c. by taking their opposites, may suffice to plot the same from the land-mark, A, B, C, &c. as well as those taken on the land: or, indeed, by the course and distance, as in navigation, if the water be smooth and without a current.

In sea shoals, it is convenient to note at each observation the depth of the water found by the lead, and the drift and setting of the current by the log and compass, while the boat is at anchor, which may be done with ease and expedition enough. For while the boat rides at an anchor, her stern points out the setting of the current, and the log and glass will measure its drift.

And these ought to be noted on the draught, which may be thus:

The currents may be shewn, by drawing a dart pointing out its setting, and its drift by the Roman capital letters, the depth of the water by the small figures, and rocks by little crosses, &c.

SECTION IX.

## LEVELLING.

PL. 13. fig. 2.

EVELLING is the art of ascertaining the perpendicular ascent or descent of one place (or more) above or below the horizontal level of another, for various intentions; and of marking out courses for conveyance of water, &c.

The true level is a curve conforming to the surface of the earth; as ABG.

The apparent level is a tangent to that curve; as ADE.

The correction, or allowance for the earth's curvature, is the difference between the apparent level and the true, as BD. The quantity of this correction may be known by having, in the right-angled triangle CAB, the two legs, AC=the semidiameter of the earth (=1267500 perches) and AD=the distance of the object, to find the hypothenuse CD, from which taking CB: (=CA) the remainder will be the correction BD; but it may be obtained more practically thus;

Square the distance in

four-pole chains and divide by 800,
or in perches and divide by 12800,
or in miles and multiply by
for the correction in inches.

#### EXAMPLE.

Required the correction for 20 four-pole chains =80 perches= \(\frac{1}{2}\) mile.

 $800)90 \times 20 = 400(.5)$   $12800)80 \times 80 = 6400(.5)$   $\frac{1}{2} = .25$ , and  $.25 \times 25 \times 8 = .5$ that is .5, or  $\frac{1}{2}$  inch, the correction required.

But, to save the trouble of calculation, we insert the following table of corrections.

A Table of Corrections.

The distances in four-pole Chains.

Distan.	Correc.	Distan.	Correc.
Chains	Inches	Chains.	Inches.
OF STREET	0,00125	27	0,91
2	0,005	28	0,98
3	0,01125	29	1,05
4	0,02	30	1,12
5	0,03	31	1,19
6	0,04	32	1,27
DO THE	0,06	33	1,35
8	0,08	34	1,44
9	0,10	35	1,53
10	0,12	36	1,62
11	0,15	37	1,71
12	0,18	38	1,80
13	0,21	39	1,91
14	0,24	40	2,00
15	0,28	45	2,28
16	0,32	50	3,12
17	0,36	55	3,78
18	0,40	60	4,50
19	0,45	65	5,31
20	0,50	70	6,12
21	0,55	75 _	7,03
22	0,60	80	8,00
23	0,67	85	9,03
24	0,72	90	10,12
25	0,78	95	11,28
26	0,84	100	12,50

The first thing necessary in levelling, is the adjusting of the level, which may be performed several ways: The following is very easy and practical.

Choose some ground which is not above 4 or 5 feet out of the level, for the distance of 8 or 10 chains length, and suppose it be AB (fig. 3.) and find the middle between A and B, which suppose to be C; plant the instrument at C: direct the tube to a station-staff, held up at A, and elevate or

depress the tube, till the bubble is exactly in the middle of the divisions; then by signals direct your assistant at A, to rise or depress the vane, sliding on the station-staff, till the horizontal hair in the glass, cuts the middle of that vane: then see how many feet, inches, and parts, are cut by the upper part of the vane, which suppose to be 3 feet 4 inches and 6 tenths.

In like manner direct to the other staff at B, and suppose the upper edge of that vane to cut at the height of 6 feet, 5 inches and two tenths, then will these two vanes be on a level.

From 6 feet 5.2 inches subtract 3 feet 4.6 inches, and reserve the remainder 3 feet 0.6 inches.

Now, remove the instrument as close to the higher station-staff as you can; so that the middle of the telescope may almost touch it. Then bring the telescope as near to a level as the judgment of the eye will direct.

Measure from the ground, the height of the top of the telescope; and also of the bottom, in feet, inches, and parts; suppose them to be 4 feet, 10.5 inches, and 5 feet 0.3 inches; then half the sum of the heights 4 feet 11.4 inches is the height of the centre of the glass; and to this add half the breadth of the vane, which suppose to be 1 inch and 5 tenths, and to the sum 5 feet 0.9 inches, add the preceding remainder 3 feet 0.6 inches; then let the person at B move his vane, till the upperedge cut 8 feet 1.5 inches, the sum of the preceding numbers.

SCHOOL OF REAL PROPERTY AND ADDRESS OF THE PARTY OF THE P

Now, so elevate or depress the hair or the bubble, till the hair cut the middle of the vane at B, and at the same time the bubble stands at the middle of the divisions; and then will the instrument be duly adjusted.

If you have a mind to be more accurate, repeat the operation; but when you place the instrument at C, turn the tube at right angles to the line AB, and there set it level; then proceed with a repetition of the work. Only observe to cross-level it in this adjustment, and in all future uses whatsoever.

Or the level may be adjusted thus: As before, first plant the instrument in the middle between A and B (fig. 4.) and observe the heights on the station-staves, which suppose to be as above; and consequently their difference, as before, is 3 feet 0.6 inches. Now measure from C towards the highest ground A, some distance that comes almost to A; suppose 4 chains to D, and DB will be 9 chains, and DA one chain: Then plant the instrument at D, direct the telescope to A, and, setting the bubble to the middle of the division, direct your assistant to move the vane, till the hair cuts the middle of it; and note down the feet, inches, and parts cut by the upper edge of the vane; which suppose to be 3 feet 8.4 inches: To this add the difference 3 feet 0.6 inches, and the sum 6 feet 9 inches reserve.

Now direct the telescope to the staff at B, level it, and direct your assistant to move the vane, till the hair cuts the middle thereof; and then, if the upper edge of the vane cuts the foregoing sum 6 feet 9 inches, the hair and bubble are truly adjusted. But if not, say, As BD less AD, is to the difference between the numbers cut by the upper edge of the vane, and the number 6 feet 9 inches; so is the distance AD to a number, which added to that cut by the vane, when less than 6 feet 9, and subtracted from the number cut by the vane, when it is greater than 6 feet 9, will give a number to which let the assistant fix the vane; then so elevate or depress the hair or the bubble, till the hair cuts the middle of the vane at B, and the bubble stands in the middle of the divisions; for then the level, will be adjusted. The operation may be again repeated, and at every station cross-levelled, which will confirm the former adjustment.

Or it will be still better to set the station staves equally distant from the instrument (suppose about 16 or 20 perches each) at an angle of about 60° or soas to form nearly an equilateral triangle therewith, and level the 2 vanes (A and B fig. 5.) as before, which will be then both in the same horizontal level. whether the instrument be right adjusted or not, because one will be as much above or below the true level of the instrument, as the other, being in the same distance from it; then remove the instrument as near as may be to one of them, suppose A, and raise or lower the vane A to the exact level of the visual ray in the instrument, noting precisely how much it is moved, and have the other vane B move just as much, in order to bring them again to a level, allowing for the correction of the apparent level if it be a sensible quantity; then adjust the instrument to the level of the vane at B.

To adjust the rafter level (plate 13 fig. 6.) which may be 10, 12, or 14 feet in the span AB; set it on a plank or hard ground nearly level, and mark

where the plumb line cuts the beam mn, suppose at c, then invert the position by setting the foot A in the place of B, and B in that of A, marking where the line now cuts, as at e; the middle point between c and e will be the true levelling mark.

To continue a level course with this instrument, set the foot A to the starting place, and move B upward or downward toward D or E, till the point B be determined and marked for a level with A, then carry the instrument forward in the direction of C till the foot A rests at B, whence the point C is levelled as before, &c. Sights may be placed at r and s, and the instrumentadjusted to them, as before, by reversing them in the direction of some distant object.

After the instrument is duly adjusted, you may proceed to use it. Let the example be this annexed (fig. 7.) where A every where represents the level, and B the station staves; and suppose the route be made from a to e; first plant the instrument between the staves a and b: at A direct the level to a B, bring the bubble to the middle of the divisions, and instruct your assistant so to place the vane, that the hair in the telescope cuts the middle of the vane, then in a book divide into two columns, the one entitled Back sights, the other Fore sights, enter the feet, inches, and parts cut by the upper edge of the vane at a B, in the column intitled Back sights.

Then look toward the other staff b B, bring the bubble to the middle of the divisions, and direct your assistant to place the vane so, that the hair cuts the middle of the vane; then enter the feet, inches, and parts cut by the upper edge of the vane. in the column of Fore sights.

Now, plant the instrument at  $A^3$ , still keeping the staff Bb exactly in the same place, and carry the staff aB forwards to the place cB; now look back to the staff bB, and enter the numbers cut by the vane there under the title Back sights; then look forwards to cB, and enter the observation under the title Fore sights. Do the like when the instrument is planted at  $A^3$ ,  $A^4$ , &c. always taking care to keep the staff in the same place when you looked at it for a Fore sight, till you have also taken with it a Back sight.

Having finished your level, add up the column of Back sights into one sum, and the column of Fore sights also into one sum; and the difference between these sums is the ascent or descent required. And if the sum of the Fore sights be greater than the sum of the Back sights then e is lower than a; but if the sum of the Fore sights be less than the sum of the Back sights, e is higher than a. For example let the numbers be as in the following table.

	Ba	ck eigh	te.	,	: :	F	ore sigh	te.	
Feet.		Inch.		Tenths.	Feet.		Inch.	•	Tenths.
3	•	7	3	5 j	6	•	4	7	. 5
4		6	,	8 ]	. 8		3	,	. 2
<b>6</b> ·	٠.	0	,	2 ''	5		4	,	.7
9		5	,	0	. 8	٠. •	7	,	8 ·
1		0	,	7	9		4	,	8
24	•	8	-,	2 .	38	•	ì	,	0
		•		į	24		8	,	2
				. 1	13		4	_	8
Henc	e ti	ne desc	ent	is	13	•	4	,	8

## Observations.

- 1. And if the distances thus taken are short, the curvature of the earth may be rejected. For, if the distance from the instrument be every where about 100 yards, all the curvatures in a mile's work will be less than half an inch.
- 2. If the distance from the instrument to the hindermost staff, be every where equal to the distance from the instrument to the corresponding staff; the curvature of the earth, and the minute errors of the instrument will both be destroyed. Hence it will be much best to set the instrument as equally distant from both staves as may be.
- 3. If the distances of the instrument from the staves, be very unequal and very long, the curvatures must be accounted for, and the distances in order thereto, must be measured.
- 4. Therefore it appears, that the best method to take a level is to measure the several distances from the instrument to the back and forward station staves; and enter them in the field-book, according to the titles of their several columns, as in the following example; and correct the heights from the table of allowances, which may be done at home when you are about to sum up the heights.

	Backwa	rds.	Forwards.					
Distan. Height Corne		Cornected	Distan.	Height	Corrected.			
Links.	Inches.	Inches.	Links.	Inches.	Inches.			
370	3,25	3,24	418	4,36	4,34			
430	6,10	6,08	328	7,18	7,17			
760	5,38	5,31	289	6,75	6,67			
. 584	7,25	<i>7</i> ,21	520	9,53	9,50			
326	8,15	8,14	485	11,25	11,22			
658	10,25	. 10,20	376	8,65	8,63			
530	6,32	6,29	720	10,34	10,28			
3658	i [	45,47	31,46		57,81			
3146	ľ †	-		1	46,47			
68,04	1			l [	11,34			

So that the fall in 68 chains is about 11 inches and 1 of an inch.

Lastly, Though hitherto we have considered the level with one telescope only, the same observations may be applied to a level with a double telescope; and I would advise those who use the double telescope, at every station to turn that end of the telescope forward, which before was the contrary way.

A more general method of levelling adopted to the surveying of roads and hilly ground is exhibited in the following exdutile, in which the measures are given in links.

# Examples.

#### Pl. 13. Ag. 8.

Required the bearing and distance of the place B from A, and its perpendicular ascent or descent, above or below the horizontal level of A.

Course or Bearing			Dist.		Lut.	
N E 79°15 N E 75 00		738 684	705 635	NAME OF TAXABLE PARTY.	131	692
3 N E 50 30 A S E 85 15	E 14 00	976 930	947	236.1	602	730
5 S E 70 00	E 19 15	620	585	204.0	200	549
SULTS 13	100	3948	3783	Control of the last of the las		3492 E.

As Dif. Lat. 622

Is to radius S. 20°,
So is Dep. 3492

To T. Bear. 79° 54'

As S. Bear. 79° 45' Is to Dep. 3492, So is radius S. 90° To Dist. 3547.

As 100 links: 66 feet:: 217.6 links: 143.6 feet, the descent B below the level of A.

Hence, B bears N. 79° 54'E. from A
Nearest horiz. dist. 3547 links.
Sum of obl. dist. 3948 links.
Sum of horiz. dist. 3783 links.
Perp. desc. 217.6 L,=143.6 F.

With the angular elevation or depression in the third column, and the oblique distance in the fourth (as course and distance) are found the horizontal distance in the fifth, and the perpendicular ascent or descent on the sixth, for each station (as difference of latitude and departure:) then, with the bearing and horizontal distance we get the difference of latitude and departure in the two last columns.

The ascents and descents in the sixthcolumn are distinguished by the letters E and D in the third, signifying elevation or depression; and being added separately, the difference of their sums is set at the

bottom of the column with the name of the greater, and shews the perpendicular descent of B below the horizontal level of A.

In like manner the northings and southings in the seventh column are distinguished by the letters N and S in the second, &c.

## PROMISCUOUS QUESTIONS.

The perambulator, or surveying wheel, is so contrived as to turn just twice in the length of a pole or 16½ feet; what then is the diameter?

2.626 feet.

2. Two sides of a triangle are respectively 20 and 40 perches; required the third so that the content may be just an acre?

Answ. either 23. 099 or 58.876 perches.

3. I want the length of a line by which my gardener may strike out a round orangery that shall contain just half an acre of ground.

Answ. 273 yards.

4. What proportion does the arpent of France, which contains 100 square poles of 18 feet each, bear to the American acre, containing 160 square poles of 16.5 feet each, considering that the length of the French foot is to the American as 16 to 15?

Answ. as 512 to 605

5. The ellipse in Grovesner square measures 840 links the longest way, and 612 the shortest, within the rails: now the wall being 14 inches thick, it is required to find what quantity of ground it incloses, and how much it stands upon.

Answ. it incloses 4A. 6P. and stands on 17601

square feet.

6. Required the dimensions of an elliptical acre with the greatest and least diameters in the proportion of 3 to 2?

Answ. 17.479 by 11.653 perches.

- 7. The paving of a triangular court at 18d. per foot, came to 100l. The longest of the three sides was 88 feet: what then was the sum of the other two equal sides?

  Answ. 106.85 feet.
- 8. In 110 acres of statute measure, in which the pole is 10½ teet, how many Cheshire acres, where the customary pole is 6 yards, and how many of Ireland, where the pole in use is 7 yards?

Answ. 92A. 1R. 28P. Cheshire; 67A. 3R. 25P.

Irish.

9. The three sides of a triangle containing 6A.
1R. 12P, are in the ratio of the three numbers, 9, 8, 6, respectively; required the sides?

Answ. 59.029, 52.47, and 39.353.

10. In a pentangular field, beginning with the south side, and measuring round towards the east, the first or south side is 2735 links, the second 3115, the third 2370, the fourth 2925, and the fifth 2320; also the diagonal from the first angle to the third is 3800 links, and that from the third to the fifth 4010; required the area of the field?

Answ. 117A. 2R. 28P.

11. Required the dimensions of an oblong garden containing three acres, and bounded by 104 perches of pale fence?

Answ. 40 perches by 12.

12. How many acres are contained in a square meadow, the diagonal of which is 20 perches more than either of its sides.

Answ. 4A. 2R. 11P.

13. If a man six feet high travel round the earth, how much greater will be the circumference described by the top of his head than by his feet?

Answ. 37.69 feet.

- N. B. The required difference is equal to the circumference of a circle 6 feet radius, let the magnitude of the earth be what it may.
- 14. Required the dimensions of a parallelogram containing 200 acres, which is 40 perches longer than wide?

Answ. 200 perches by 160.

15. What difference is there between a lot 28 perches long by 20 broad, and two others, each of half the dimensions?

Answ. 1A. 3R.

# PART III

AND THE PERSON NAMED AND PERSON OF THE PERSO

Containing the Astronomical methods of finding the Latitude, Variation of the compass, &c. with a description of the instruments, used in these operations.

## SECTION I.

INTRODUCTORY PRINCIPLES.

DAY and night arise from the circumrotation of the Earth. That imaginary line about which the rotation is performed, is called the Axis, and its extremities are called Poles. That towards the most remote parts of Europe is called the North Pole, and its opposite the South Pole. The Earth's Axis being produced will point out the Celestial Poles.

The Equator is a great circle on the Earth, every point of which is equally distant from the Poles; it divides the Earth into two equal parts, called Hemispheres: that having the North Pole in its centre is called the Northern Hemisphere—and the other, the Southern Hemisphere. The plane of this circle being produced to the fixed stars, will point out the celestial Equator or Equinoctial. The Equator, as well as all other great circles of the sphere, is divided into 360 equal parts, called degrees; each degree is divided into 60 equal parts, called minutes; and the sexagesimal division is continued.

Note. The ancients having no instruments by which they could make observations with any tolerable degree of accuracy, supposed the length of the year, or annual motion of the earth, to be completed in 360 days: and hence arose the division of the circumference of a circle into the same number of equal parts, which they called degrees.

The Meridian of any place, is a semi-circle passing through that place, and terminating at the Poles of the Equator. The other half of this circle is called the opposite Meridian.

The Latitude of any place, is that portion of the Meridian of that place, which is contained between the Equator and the given place; and is either North or South, according as the given place is in Northern or Southern Hemisphere, and therefore cannot exceed 90°.

The Parallel of Latitude of any place, is a circle passing through that place, parallel to the Equator.

The Difference of Latitude between any two places, is an arch of a meridian intercepted between the corresponding parallels of latitude of those places. Hence, if the places lie between the Equator and the same Pole, their difference of latitude is found by subtracting the less latitude from the greater: but if they are on opposite sides of the Equator, the Difference of latitude is equal to the sum of the latitudes of both places.

The First Meridian is an imaginary semicircle, passing through any remarkable place, and is therefore arbitrary. Thus, the British esteem that to be

the First Meridian, which passes through the Royal Observatory at Greenwich; and the French reckon for their First Meridian, that which passes through the Royal Observatory at Paris .- Formerly many French geographers reckoned the meridian of the island of Ferro to be their First Meridian; and others, that which was exactly 20 degrees to the west of the Paris Observatory. The Germans, again, considered the metidian of the Peak of Tenerifie to be the First Meridian. By this mode of reckoning, Europe, Asia, and Africa, are in east longitude; and North and South America, in west longitude. At present, the first meridian of any country is generally esteemed to be that which passes through the principal Observatory, or chief city of that country. Equator and the given place i system of the country.

The Longitude of any place is that portion of the Equator which is contained between the first meridian, and the meridian of that place: and is usually reckoned either east or west, according as the given place is on the east or west side of the first meridian; and, therefore, cannot exceed 180°.

The Difference of Longitude between any two places is the intercepted arch of the Equator between the meridians of those places, and cannot exceed 180°.

There are three different Horizons, the apparent, the sensible, and the true. The apparent or visible Horizon is the utmost apparent view of the sea or land. The sensible is a plane passing through the eye of an observer, perpendicular to a plumb line hanging freely; And the true or rational Horizon is a plane passing through the centre of the Earth, parallel to the sensible Horizon.

Altitudes observed at sea, are measured from the visible Horizon. At land, when an astronomical quadrant is used, or when observations are taken with a Hadley's quadrant by the method of reflection, the altitude is measured from the sensible Horizon; and in either case, the altitude must be reduced to the true Horizon.

The Zenith of any given place is the point immediately above that place, and is, therefore, the elevated pole of the Horizon: The Nadir is the other pole, or point diametrically opposite.

A Vertical is a great circle passing through the Zenith and Nadir; and, therefore, intersecting the Horizon at right angles.

The Altitude of any celestial body is that portion of a Vertical, which is contained between its centre and the true Horizon. The Meridian Altitude is the distance of the object from the true Horizon, when on the Meridian of the place of observation. When the observed Altitude is corrected for the depression of the Horizon, and the errors arising from the instrument, it is called the apparent Altitude; and when reduced to the true Horizon, by applying the parallax in Altitude, it is called the true Altitude. Altitudes are expressed in degrees, and parts of a degree:

The Zenith Distance of any object is its distance from the Zenith, or the complement of its Altitude.

The Declination of any object is that portion of its meridian which is contained between the equinoctial and the centre of the object; and is either north or south, according as the star is between the equinoctial and the north or south pole.

The Ecliptic is that great circle, in which the annual revolution of the Earth round the Sun is performed. It is so named, because Eclipses cannot happen but when the moon is in or near that circle. The inclination of the Ecliptic and Equinoctial is at present about 23° 28'; and by comparing ancient with modern observations, the obliquity of the Ecliptic is found to be diminishing—which diminution, in the present century, is about half a second yearly.

The Ecliptic, like all other great circles of the sphere, is divided into 360°; and is further divided into twelve equal parts, called Signs: each Sign, therefore, contains 30°. The names and characters of these Signs are as follows:

Aries, r Cancer, Libra, Capricornus, F Taurus, & Leo, & Scorpio, m Aquarius, = Gemini, I Virgo, M Sagittarius, & Pisces,

Since the Ecliptic and Equinoctial are great circles, they, therefore, bisect each other in two points, which are called the Equinoctial Points. The Sun is in one of these points in March, and in the other in September; hence, the first is called the Vernal, and the other the Autumnal Equinox-and that sign which begins at the Vernal Equinox is called Aries. Those points of the Ecliptic, which are equidistant from the equinoctial points, are called the Solstitial Points; the first the summer, and the second the winter solstice. That great circle which passes through the equinoctial points and the poles of the earth, is called the Equinoctial Colure: and the great circle which passes through the solstitial points and the poles of the earth, is called the Solstitial Colure.

When the Sun enters Aries, it is in the Equinoctial; and, therefore, has no declination. From thence it moves forward in the Ecliptic, according to the order of the signs, and advances towards the north pole, by a kind of retarded motion, till it enters Cancer, and is then most distant from the Equinoctial; and moving forward in the Ecliptic, the Sun apparently recedes from the north pole with an accelerated motion till it enters Libra, and being again in the Equinoctial, has no declination; the Sun moving through the signs Libra, Scorpio, and Sagittarius, enters Capricorn; and then its south declination is greatest, and is, therefore, most distant from the north pole; and moving forward through the signs Capricorn, Aquarius, and Pisces, again enters Aries: Hence, a period of the seasons is completed, and this period is called a Solar Year.

The signs Aries, Taurus, Gemini, Cancer, Leo, and Virgo, are called Northern Signs, because they are contained in that part of the Ecliptic which is between the Equinoctial and North Pole; and, therefore, while the Sun is in these signs, its declination is north: the other six signs are called Sonthern Signs. The signs in the first and fourth quarters of the Ecliptic are called Ascending Signs: because, while the Sun is in these signs, it approaches the north pole—and, therefore, in the northern, temperate, and frigid zones, the Sun's meridian altitude daily increases; or, which is the same, the Sun ascends to a greater height above the horizon every day. The signs in the second and third quarters of the Ecliptic are called Descending Signs.

The Tropics are circles parallel to the Equinoctial, whose distance therefrom, is equal to the obli-

quity of the Ecliptic. The Northern Tropic touches the Ecliptic at the beginning of Cancer, and is, therefore, called the Iropic of Cancer; and the Southern Tropic touches the Ecliptic at the beginning of Capricorn, and is hence called the Iropic of Capricorn.

Circles about the poles of the Equinoctial, and passing through the poles of the Ecliptic, are called Polar Circles; the distance, therefore, of each Polar Circle from its respective Pole, is equal to the inclination of the Ecliptic and Equinoctial. That Circle which circumscribes the North Pole is called the Artic, or North Polar Circle; and that towards the South Pole, the Antartic, or South Polar Circle.

That semicircle which passes through a star, or any given point of the heavens, and the Poles of the Ecliptic, is called a Circle of Latitude.

The Reduced Place of a Star is that point of the Ecliptic, which is intersected by the circle of latitude passing through that star.

The Latitude of a Star is that portion of the circle of latitude contained between the Star and its reduced place—and is either north or south, according as the Star is between the Ecliptic and the north or south pole thereof.

The Longitude of a Star is that portion of the Ecliptic, contained between the Vernal Equinox and the reduced place of the Star.

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#### SECTION II.

Description of the Instruments, requisite in Astronomical.

Observations.

# THE QUADRANT.

T is generally allowed that we are indebted to John Hadley, Esq. for the invention, or at least for the first public account of that admirable instrument, commonly called Hadley's Quadrant, who in the year 1731, first communicated its principles to the Royal Society, which were by them published soon after in their Philosophical Transactions; before this period, the Cross Staff and Davis's Quadrant were the only instruments used for measuring altitudes at sea, both very imperfect and liable to considerable error in rough weather; the superior excellence however of Hadley's Quadrant, soon obtained its general use among seamen, and the many improvements this instrument has received from ingenious men at various times, has rendered it so correct, that it is now applied, with the greatest success, to the important purposes of ascertaining both the latitude and longitude at sea, or land.

The Octant or Frame, is generally made of ebony, or other hard wood, and consists of an arch firmly attached to two radii, or bars, which are strengthened and bound by the two braces, in order to prevent it from warping.

The Arch, or Limb, although only the eighth part of a circle, is on account of the double reflection, divided into 90 degrees, numbered 0, 10, 20, 30, &c. from the right towards the left; these are subdivided into 3 parts, containing each 20 minutes, which are again subdivided into single minutes, by means of a scale at the end of the Index. The arch extending from 0 towards the right hand is called the arch of excess.

The Index is a flat brass bar, that turns on the centre of the instrument; at the lower end of the Index there is an oblong opening: to one side of this opening a Nonius scale is fixed to subdivide the divisions of the arch; at the bottom, or end of the index, there is a piece of brass which bends under the arch, carrying a spring to make the Nonius scale lie close to the divisions; it is also furnished with a screw to fix the Index in any desired position.

Some instruments have an adjusting or tangentscrew, fitted to the Index, that it may be moved more slowly, and with greater regularity and accuracy than by the hand; it is proper, however, to observe, that the Index must be previously fixed near its right position by the above mentioned screw, before the adjusting screw is put in motion.

The Nonius is a scale fixed to the end of the Index for the purpose, as before observed, of dividing the subdivisions on the Arch into Minutes; it sometimes contains a space of 7 degrees, or 21 subdivisions of the limb, and is divided into 20 equal parts; hence each division on the Nonius will be one-twentieth part greater, that is, one minute longer than the divisions on the Arch; consequent-

ly, if the first division of the Nonius, marked 0, be set precisely opposite to any degree, the relative position of the Nonius and the Arch must be altered one minute before the next division on the Nonius will coincide with the next division on the Arch, the second division will require a change of 2 minutes, the third of 3 minutes, and so on, till the 20th stroke on the Nonius arrives at the next 20 minutes on the Arch; the 0 on the Nonius will then have moved exactly 20 minutes from the division whence it set out, and the intermediate divisions of each minute, have been regularly pointed out by the divisions of the Nonius.

The divisions of the Nonius scale are in the above case reckoned from the middle towards the right, and from the left towards the middle; therefore the first 10 minutes are contained on the right of the 0, and the other 10 on the left. But this method of reckoning the divisions being found inconvenient, they are more generally counted, beginning from the right-hand towards the left; and then 20 divisions on the Nonius are equal to 19 on the limb, consequently one division on the Arch will exceed one on the Nonius by one-twentieth part, that is, one minute.

The 0 on the Nonius, points out the entire degrees and odd twenty minutes subtended by the objects observed; and if it coincides with a division on the Arch, points out the required angle: thus, suppose the 0 on the Nonius stands at 25 degrees, then 25 degrees will be the measure of the angles observed; if it coincides with the next division on the left hand, 25 degrees 20 minutes is the angle; if with the second division beyond 25 degrees,

then the angle will be 25 degrees 40 minutes; and so on in every instance where the O on the Nonius co reides with a division on the Arch; but if it does not coincide, then look for a division on the Nonius that stands directly opposite to one on the Arch, and that division on the Nonius gives the odd minutes to beadded to that on the Arch nearest the right-hand of the 0 on the Nonius; for example, suppose the Index division does not coincide with 25 degrees, but that the next division to it on the Nonius is the first coincident division, then is the required Angle 25 degrees I minute; if it had been the second division, the Angle would have been 25 degrees 2 minutes, and so on to 20 minutes, when the 0 on the Nonius would coincide with the first 20 minutes on the Arch from 25 degrees. Again, let us suppose the 0 on the Nonius to stand between 50 degrees and 50 degrees 20 minutes, and that the 15th division on the Nonius coincides with a division on the Arch, then is the angle 50 degrees 15 minutes. Further, let the 0 on the Nonius stand between 45 degrees 20 m nutes and 45 degrees 40 minutes, and at the same time the 14th division on the Nonius stands directly opposite to a division on the Arch, then will the Angle be 45 degrees 34 minutes.

The Index Glass is a plane speculum, or mirror of glass quicksilvered, set in a brass frame, and so placed that the face of it is perpendicular to the plane of the instrument, and immediately over the centre of motion of the Index. This mirror being fixed to the Index moves along with it, and has its direction changed by the motion thereof.

This glass is designed to reflect the image of the Sun, or any other object, upon either of the two horizon glasses, from whence it is reflected to the eye of the observer. The brass frame, with the glass, is fixed to the Index by the screw; the other screw serves to place it in a perpendicular position, if by any accident it has been put out of order.

The Horizon Glasses are two small speculums on the radius of the Octant; the surface of the upper one is parallel to the Index glass when the O on the Nonius is at 0 on the Arch; these mirrors receive the rays of the object reflected from the Index glass, and transmit them to the observer. The fore Horizon glass is only silvered on its lower half, the upper half being transparent, in order that the direct object may be seen through it. The back Horizon glass is silvered at both ends; in the middle there is a transparent slit, through which the Horizon may be seen. Each of these glasses is set in a brass frame, to which there is an axis; this axis passes through the wood work, and is fitted to a lever on the under side of the quadrant, by which the glass may be turned a few degrees on its axis, in order to set it parallel to the Index glass.

To set the glasses perpendicular to the plane of the quadrant, there are two sunk screws, one before and one behind each glass: these screws pass through the plate on which the frame is fixed into another plate, so that by loosening one and tightening the other of these screws, the direction of the frame, with its mirror, may be altered, and thus be set perpendicular to the plane of the instrument.

The Dark Glasses, or Shades, are used to prevent the bright rays of the Sun, or the glare of the Moon, from hurting the eye at the time of observation; there are generally three of them, two red, and one green. They are each set in a brass frame

which turn on a centre, so that they may be used separately or together, as the brightness of the object may require. The green glass may be used also alone, if the Sun be very faint; it is likewise used in taking observations of the Moon; when these glasses are used for the fore observation, they are set immediately before the fore Horizon glass, but in front of the other Horizon glass, when a back observation is made.

The Sight Vanes are pieces of brass, standing perpendicular to the plane of the instrument: that one which is opposite the fore horizon, is called the fore Sight Vane, the other the back Sight Vane. There are two holes in the fore Sight Vane, the lower of which, and the upper edge of the silvered part of the fore Horizon glass, are equidistant from the plane of the instrument, and the other is opposite to the middle of the transparent part of that glass; the back Sight Vane has only one hole, which is exactly opposite to the middle of the transparent slit in the Horizon glass to which it belongs: but as the back observations are liable to many inconveniences and errors, we shall not give any directions for their practice.

## ADJUSTMENTS.

The several parts of the Quadrant being liable to be out of order from a variety of accidental circumstances, it is necessary to examine and adjust them, so that the instrument may be put into a propers tate, previous to taking observations.

An instrument properly adjusted, must have the Index glass and Horizon glasses perpendicular to the plane of the Quadrant; the plane of the fore Horizon glass parallel, and that of the back Horizon

glass perpendicular to the plane of the Index glass, when the 0 on the Nonius is at 0 on the Arch; hence the Quadrant requires five adjustments, the first three of which being once made, are not so liable as the last two to be out of order; however they should all be occasionally examined in case of an accident.

I. To set the Plane of the Index Glass perpendicular to that
of the Instrument.

Place the Index near to the middle of the Arch, and holding the Quadrant in a horizontal position, with the Index glass close to the eye, look obliquely down the glass, in such a manner that you may see the Arch of the Quadrant by direct view, and by reflection at the same time; if they join in one direct line, and the Arch seen by reflection forms an exact plane, or strait line, with the Arch seen by direct view, the glass is perpendicular to the plane of the Quadrant; if not, it must be restored to its right position by loosening the screw, or tightening it, or vice versa, by a contrary operation.

II. To set the Fore Horizon Glass parallel to the Index Glass the Index being at 0.

Set the 0 on the Nonius exactly against 0 on the Arch, and fix it there by the screw at the under side. Then, holding the Quadrant vertically, with the Arch lowermost, look through the Sight Vane, at the edge of the sea, or any other well defined and distant object. Now, if the Horizon in the silvered part exactly meets, and forms one continued line with that seen through the unsilvered part, the Horizon glass is parallel to the Index glass. But if the Horizons do not coincide, then loosen the

the button-screw in the middle of the lever, on the under side of the Quadrant, and move the Horizon glass on its axis, by turning the nut at the end of the adjusting lever, till you have made them perfectly coincide; then fix the lever firmly in this situation by tightening the button-screw. This adjustment ought to be repeated before and after every observation. Some observers adopt the following method, which is called finding the Index error. Let the Horizon glass remain fixed, and move the Index till the image and object coincide; then observe whether 0 on the Nonius agrees with 0 on the Arch, if it does not, the number of minutes by which they differ is to be added to the observed altitude or angle, if the 0 on the Nonius be to the right of the 0 on the Arch, but if to the left of the O on the limb, it is to be subtracted.

It has already been observed, that that part of the Arch beyond 0, towards the right hand, is called the Arch of excess: the Nonius, when the 0 on it is at that part, must be read the contrary way, or which is the same thing, you may read off the minutes in the usual way, and then their complement to 20 minutes will be the real number, to be added to the degrees and minutes pointed out by the 0 on the Nonius.

III. To set the Fore Horizon Glass perpendicular to the Plane of the Quadrant.

Having previously made the above adjustment, incline the Quadrant on one side as much as possible, provided the Horizon continues to be seen in both parts of the glass; if when the instrument is thus inclined, the edge of the sea seen through the lower hole of the Sight Vane continues to form

one unbroken line, the Horizon glass is perfectly adjusted; but if the reflected Horizon be separated from that seen by direct vision, the speculum is not perpendicular to the plane of the Quadrant: then if the limb of the Quadrant is inclined towards the Horizon, with the face of the instrument upwards, and the reflected sea appears higher than the real sea, you must slacken the screw before the Horizon glass, and tighten that which is behind it; but if the reflected sea appears lower, the contrary must be performed. Care must be always taken in this adjustment to loosen one screw before the other is screwed up, and to leave the adjusting screws tight, or so as to draw with a moderate force against each other.

This adjustment may be also made by the Sun, Moon, or a Star; in this case the Quadrant is to be held in a vertical position; if the image seen by reflection appears to the right or left of the object seen directly, then the glass must be adjusted as before by the two screws.

It will be necessary, after having made this adjustment, to examine if the Horizon glass still continues to be parallel to the Index glass, as sometimes by turning the sunk screws the plane of the Horizon glass will have its position altered.

## USE OF HADLEY'S QUADRANT.

The use of the Quadrant is to ascertain the Angle subtended by two distant objects at the eye of the observer; but principally to observe the altitude of a celestial object above the Horizon: this is pointed out by the Index when one of the ob-

jects seen by reflection is made to coincide with the other, seen through the transparent part of the Horizon glass.

To take an Altitude of the Sun, Moon, or a Star, by a Fore Observation.

Having previously adjusted the instrument, place the 0 on the Nonius opposite to 0 on the Arch, and turn down one or more of the screens, according to the brightness of the Sun; then apply the eye to the upper hole in the fore Sight Vane, if the Sun's image be very bright, otherwise to the lower, and holding the Quadrant vertically, look directly towards the Sun so as to let it be behind the silvered part of the Horizon glass, then the coloured Sun's image will appear on the speculum: move the Index forward till the Sun's image, which will appear to descend, just touches the Horizon with its lower or upper limb; if the upper hole be looked through, the Sun's image must be made to appear in the middle of the transparent part of the Horizon, but if it be the lower hole, hold the Quadrant so that the Sun's image may be bisected by the line joining the silvered and transparent parts of the Horizon glass.

The Sun's limb ought to touch that part of the Horizon immediately under the Sun, but as this point cannot be exactly ascertained, it will be therefore necessary for the observer to give the Quadrant a slow motion from side to side, turning at the same time upon his heel, by which motion the Sun will appear to sweep the Horizon, and must be made just to touch it at the lowest part of the Arch; the degrees and minutes then pointed out by the Index on the Limb of the Quadrant will be the observed altitude of that limb which is brought in contact with the Horizon.

When the meridian or greatest altitude is required, the observation should be commenced a short time before the object comes to the meridian; being brought down to the Horizon, it will appear for a few minutes to rise slowly; when it is again to be made to coincide with the Horizon by moving the Index forward; this must be repeated until the object begins to descend, when the Index is to be secured, and the observation to be read off.

From this description of the Quadrant and its use, the manner of adjusting and using the Sextant will be readily apprehended. Our limits will not allow a particular description of this excellent instrument.

# The Artificial Horizon.

In many cases it happens that altitudes are to be taken on land by the Quadrant or Sextant; which, for want of a natural horizon, can only be obtained by an artificial one. There have been a variety of these sorts of instruments made, but the kind now described is allowed to be the only one that can be depended upon. It consists of a wood or metal framed roof, containing two true parallel glasses of about 5 by 2½ inches, fixed not too tight in the frames of the roof. This serves to shelter from the air a wooden trough filled with quicksilver. In making an observation by it with the Quadrant, or Sextant, the reflected image of the sun, moon, or other object, is brought to coincide with the same object reflected from the glasses of the Quadrant or Sextant: half the angle shown upon the limb is the altitude above the horizon or level required. cessary in a set of observations that the roof be always placed the same way. When done with, the roof folds up flat-ways, and, with the quicksilver in a bottle, &c. is packed into a portable flat case.

#### SECTION III.

To find the Latitude by the Meridian Altitude of the Sun-

The Latitude of a place is its distance from the equator, either North or South; and is measured by an arch of a Meridian contained between the Zenith and the equinoctial. Hence, if the distance of any heavenly body from the Zenith, when on the Meridian, and its declination, or the number of degrees and minutes it is to the Northward, or Southward of the equinoctial, be given, the Latitude may thence be found

The Altitude of the Sun, observed by a Quadrant, or Sextant, requires four corrections in order to obtain the true altitude; these are

the Semidiameter, Dip, Refraction, and Parallax.

By the Semidiameter of the Sun is meant the angle subtended by the distance from its centre to its apparent circumference. The quantity of this angle is given for every sixth day in the year in table 10.

The Dip of the Horizon is a vertical angle contained between a Horizontal plane passing through the eye of an observer, and a line drawn from his eye to the visible Horizon. This Dip is found in Table 8, when the visible horizon is formed by the apparent junction of the water and sky; but in Table 9, when land intervenes. In this case, the line that separates the land and water is used as the Horizon, and its distance from the observer must be duly estimated.

The Refraction of any celestial body is the difference between its apparent place, and that wherein it would be seen, if the space between the observer and object, was either a void, or of a uniform

desity. Table 6 contains this Refraction.

That part of the heavens, in which an object appears, when viewed from the surface of the earth, is called its apparent place; and the point, wherein it would be seen, at the same instant, if viewed from the centre of the earth, is called its true place; the difference between the true and apparent places, is called the Parallax. The Sun's Parallax in Altitude is found in Table 7.

#### RULE

For finding the Latitude from the Sun's Meridian Altitude.

Having observed with the Quadrant, or Sextant, the altitude of the Sun's lower limb above the visible horizon,—or the line of separation of the land from the water, when that horizon is obstructed by land—add thereto the semidiameter, taken from table 10 at the given day of the month, or the one nearest to it, and from this sum subtract the

Dip, from table 8 or 9, corresponding to the height of the observer's eye above the surface of the water; and this result will be the apparent altitude of the Sun's centre. Then take the refraction from table 6, and the parallax from table 7, corresponding to this altitude, and the difference of these quantities, called the correction, being subtracted from the apparent altitude, the remainder will be the Sun's true altitude; the complement of which will be its zenith distance, north or south, according as the Sun bears south or north, at the time of observation.

When the observation has been made by bringing the Sun's image in the Quadrant, or Sextant, to a just coincidence with its image in an artificial horizon, half the angle shown on the instrument is the Sun's apparent altitude, which must be corrected by the corresponding refraction and parallax only, in order to obtain the true altitude.

Take the Sun's declination from table 13, answering to the given year, month and day, observing whether it be north or south, and reduce it, as there directed, by the help of table 14, to the longitude of the place of observation. Then the sum, or difference of the zenith distance and declination, according as they are of the same, or of a contrary denomination, will be the latitude of the place of observation, of the same name with the greater of those two quantities.

Latitude.

#### EXAMPLES.

1st. March 10th, 1811, in longitude 70° W. the Mer. Alt of C. L. W. at noon, the angular distance L. was observed to be 49° 50' between the O bearing south, and bearing south—height of the obits reflected image in the artificial server's eye 12 feet, required the horizon was found with a sextant to be 98° 30' 40" required the latilatitude in

Mer. Alt O L. L. = 49° 50′ 00° S. tude.

- +16 08 98° 30′ 40° ÷ 2=49° 15′ 20°

- +16 08 98° 30′ 40° ÷ 2=49° 15′ 20° O Ap. Alt. 19 Dip-table 8 -03 =49° 15' 20" S. Correction 43 **= 50** 02 49 Ap. Alt. True Alt. =49 Correction -42 14 90 True Alt. 50. 03 07 =40Zenith Dist. 90 Reduced Dec. =17 = 39 57 53 N. Zenith Dist. = 4 15 29 S. Latitude. Reduced Dec. =58

= 35 42 24N

3d. July 24th, 1811, in long 62° 4th. October 11th, 1812, in long 30' W. the Mer. Alt. of ① L. L. 91° W. the Meridian Altitude of above the border of a lake was O L. L. above the visible horizon observed, by a person on the op- was observed to be 47° 13' bearposite shore, to be 56° 32' bear- ing S. the height of the eye being ing S -the distance of that bor- 25 feet; required the latitude. der of the lake beneath the sun Mer Alt. O L. L = 47° 134 00" S. and the height of his eye above Dip from table 8 = +16 06 being 5 miles from the observer, Semidiameter the surface of the water, 8 feet; Ap. Alt. =4724 19 required the latitude. Correction -46 Me.: Alt. ⊙ L. L. = 56° 32/ 00" S. =47 Semidiameter True Alt. 23 33 = +1548\_2 36 Dip from table 9 = 90 = 45 = 56 45 13 Zenith Dist. 27 N. Ap. Alt. = 6 58 16 S. Correction -33 Reduced Dec. -56 = 3538 11 N. True Ait. Latitude N. B For the various other me-90 21 X thods of finding the latitude by description, the surveyor must apply to books professedly on prac-= 33 Zenith Dist. Reduced Dec. \_\_ 19 = 53 15 07 N. tical astronomy. He will, however, find a method of observing the latitude by the altitude of the north star, in the explanation of table 12, annexed to this treatise.

#### SECTION IV.

### VARIATION OF THE COMPASS.

The variation of the compass is the deviation of the points of the mariner's compass from the corresponding points of the horizon, and is termed east or west variation, according as the magnetic needle, or north point of the compass, is inclined to the eastward or westward of the true north point of the horizon.

The true amplitude of any celestial object is an arch of the horizon contained between the true east or west points thereof, and the centre of the object at the time of its rising or setting; or it is the degrees and minutes, the object rises or sets to the northward or southward of the true east or west points of the horizon.

The magnetic amplitude, is an arch contained between the east or west points of the compass and the centre of the object at rising or setting; or it is the bearing of the object, by compass, when in the horizon.

The true azimuth of an object is an arch of the horizon contained between the true meridian and the azimuth circle passing through the centre of the object.

The magnetic azimuth, is an arch contained between the magnetic meridian and the azimuth circle passing through the centre of the object; or it is the bearing of the object, by compass, at any time when it is above the horizon,

The true amplitude, or azimuth, is found by calculation, and the magnetic amplitude, or azimuth, by an azimuth compass.

#### THE AZIMUTH COMPASS.

From the accounts of the compasses, heretofore given in the description of surveying instruments, it is presumed that the nature and properties of the azimuth compass will be readily conceived by a contemplative inspection; the directions for its uses are as follow:

#### To observe the Sun's amplitude.

Turn the compass-box until the vane containing the magnifying glass is directed towards the sun: and when the bright speck, or rays of the sun collected by the magnifying glass, falls upon the slit in the other vane, stop the card by means of the nonius, and read off the amplitude.

Without using the magnifying glass, the sight may be directed through the dark glass towards the sun; and in this case, the card is to be stopped when the sun is bisected by the thread in the other vane.

The observation should be made when the sun's lower limb appears somewhat more than his semiliameter above the horizon, because his centre is really then in the horizon, although it is ap-

parently elevated on account of the refraction of the atmosphere; this is particularly to be noticed in high latitudes.

To observe the Sun's Azimuth.

Raise the magnifying glass to the upper part of the vane, and move the box, as before directed, until the bright speck fall on the other vane, or on the line in the horizontal bar; the card is then to he stopped, and the divisions being read off, will be the sun's magnetic azimuth.

If the card vibrate considerably at the time of observation, it will be better to observe the extreme vibrations, and take their mean as the magnetic azimuth. When the magnetic azimuth is observed, the altitude of the object must be taken, in order to obtain the true

azimuth.

It will conduce much to accuracy if several azimuths be observed, with the corresponding altitudes, and the mean of the whole taken for the observation.

# To find the variation of the Compass by an amplitude.

RULE—1 To the log. secant of the latitude, rejecting the index, add the log. sine of the sun's declination, corrected for the time and place of observation; their sum will be the log sine of the true amplitude, to be reckoned from the east in the morning, or the west in the afternoon, towards the north or south, according to the declination.

2. Then if the true and magnetic amplitudes, be both north or both south, their difference is the variation; but if one be north and the other south, their sum is the variation; and to know whether it be easterly or westerly, suppose the observer looking towards that point of the compass representing the magnetic amplitude; then if the true amplitude be to the right hand of the magnetic amplitude, the variation is east, but if to the left hand, it is west.

#### **EXAMPLE L**

July 3, 1812, in latitude 9° 36' 8, the Sun was observed to rise E. 12º 42' N : required the variation of the compass.

9" 36' S. Latitude 22 59 N. Declination

Secant 0.00613 Sine 9 59158

Sine 9.59771

True amplitude E. 23 20 N. Mag amplitude E. 12 42 N.

10 38 west, because the true amplitude is to the left of the magnetic.

#### EXAMPLE IL

September 24, 1812, in latitude 26° 32′ N. and longitude 78° W. the Sun's centre was observed to set W. 6° 15′ S. about 6h. P. M. required the variation of the compass.

0° 30' S. Sun's declination Corr for long. 78° W. 6 Corr. for time 6h P. M.

Reduced declination 41 8.07650 Sine Latitude 26 32 Secant 0.04834

W. 0 46 S. W. 6 15 S. Sine 81,2484 True amplitude Mag. amplitude

5 29 east, because the Variation true amplitude is to the right hand of the magnetic.

To find the Variation of the Compass by an Azimuth.

RULE. 1.— Reduce the Sun's declination to the time and place of observation, and compute the true altitude of the Sun's centre.

- 2. Subtract the Sun's declination from 90°. when the latitude and declination are of the same name, or add it to 90°, when they are of contrary names; and the sum, or remainder, will be the Sun's polar distance.
- 3. Add together the Sun's polar distance, the latitude of the place, and the altitude of the Sun; take the difference between half their sum and the polar distance, and note the remainder.
  - 4. Then add together

the log. secant of the altitude \rejecting their the log. secant of the latitude (

the log. co. sine of the half sum. and thelog. co. sine of the remainder. 5. Half the sum of these four logarithms will be the sine of an arch, which doubled, will be the Sun's true azimuth; to be reckoned from the south in north latitude, and from the north in south latitude: towards the east in the morning, and towards the west in the afternoon.

6. Then if the true and observed azimuths be both on the east, or both on the west side of the meridian, their difference is the variation: but if one be on the east and the other on the west side of the meridian, their sum is the variation; and to know if it be east or west, suppose the observer looking towards that point of the compass representing the magnetic azimuth; then if the true azimuth be to the right of the magnetic, the variation is east, but if the true be to the left of the magnetic, the variation is west.

### EXAMPLE.

November 2, 1812, in latitude 259 32' N. and longitude 75° W. the altitude of the Sun's lower limb was observed to be 15° 36', about 4h. 10m. P. M. his magnetic azimuth at that time being S. 58° 32' W. and the height of the eye 18 feet; required the variation of the compass.

Sun's de. Nov. 2, at n. 14° 48'S. Corr. for long. 75° W. + 4 Co. for ti. 4h. 10m. af n. + 3	Obs. alt. Sun's lower limb 15° 66' Semidiameter 16' } + 12
Reduced declination 14 55 90 00	Refraction - 3
Polar distance 104 65	True altitude - 15 45
Latitude - 25 32	- Secant 0.01562 - Secant 0.04463
Sum 146 12 Half 73 6	- Co. sine 9 46345
Remainder - 31 49	- Co. sine 9.92929
True azimuth 8, 64 28 W	Sinc 9.72699
20 W.	

Variation - 5 36 east, because the true azimuth is to the right of the magnetic.

To draw a true meridian line to a man, having the variation and magnetical meridian given.

On any magnetical meridian or parallel, upon which the map is protracted, set off an angle from the north towards the east, equal to the degrees or quantity of variation, if it be westerly, or from the north towards the west if it be easterly, and the line which constitutes such an angle with the magnetical meridian, will be a true meridian line.

For if the variation be westerly, the magnetical meridian will be the quantity of variation of the west side of the true meridian, but if easterly on the cast side, therefore the true meridian must be a like quantity on the east side of the magnetical one, when the variation is westerly, and on the west side when it is easterly.

To lay out a true meridian line by the circumferentor.

If the variation be westerly, turn the lox about till the north of the needle points as many degrees from the flower-de-luce towards the cast of the box, or till the south of the needle points the like number of degrees from the south towards the west, as are the number of degrees contained in the variation, and the index will be then due north and south: therefore if a line be struck out in the direction thereof, it will be a true meridian line.

If the variation was easterly, let the north of the needle point as many degrees from the flower-de-luce towards the west of the box, or let the south of the needle point as many degrees towards the cast, as are the number of degrees contained in the variation, and then the north and south of the box will coincide with the north and south points of the horizon, and consequently a line being laid out by the direction of the index, will be a true meridian line.

This will be found to be very useful in setting an horizontal dial, for if you lay the edge of the index by the base of the stile of the dial, and keep the angular point of the stile toward the south of the box, and allow the variation as before, the dial will then be due north and south, and in its proper situation, provided the plane upon which it is fixed be duly horizontal, and the sun be south at noon; but in places where it is north at noon, the angular point of the index must be turned to the north.

How maps may be traced by the help of a true meridian line.

If all maps had a true meridian line laid out upon them, it would be easy by producing it, and drawing parallels, to make out field-notes; and by knowing the variation, and allowing it upon every bearing, and having the distances, you would have notes sufficient for a trace. But a true meridian line is seldom to be met with, therefore we are obliged to have recourse to the foregoing method. It is therefore advisced to lay out a true meridian line upon every map.

To find the difference between the present variation, and that at a time when a tract was formerly surveyed, in order to trace or run out the original lines.

If the old variation be specified in the map or writings, and the present be known, by calculation or otherwise, then the difference is im-

...

# VARIATION, &c.

by inspection; but as it more frequently happens, that ainly known, and as the variation of different instru-ways alike at the same time, the following practical

found to answer every purpose.

et of the premises where any two adjacent corners are of one can be seen from the other, take their bearing; ed with that of the same line in the former survey, erence. But if trees, hills, &c. obstruct the view of the line according to the given bearing, and observe the nearest distance between the line so run and the corner, then,

As the length of the whole line

Is to 57.3 degrees, \*
So is the said distance
To the difference of variation required.

#### EXAMPLE.

Suppose it be required to run a line which some years ago bore NE. 45°, distance 80 perches, and in running this line by the given bearing, the corner is found 20 links to the left hand; what allowance must be made on each bearing to trace the old lines, and what is the present bearing of this particular line by the compass?

> 20 21000 1146,0(0°, 34

# 2**168176**0.0

Answer, 34 minutes, or a little better than half a decree to the left hand, is the allowance required, and the line in question bears N. 44° 26′.E.

Note. The different variations do not affect the area in the calculation. as they are similar in every part of the survey.

• 57.3 Is the radius of a circle (nearly) in such parts as the circumference contains 360.

FINIS.

#### TABLE I.

#### L'OGARITHMS OF NUMBERS.

#### EXPLANATION.

OGARITHMS are a series of numbers so contrived, that the sum of the Logarithms of any two numbers, is the logarithm of the produc of these numbers. Hence it is inferred, that if a rank, or series o numbers in arithmetical progression, be adapted to a series of number in geometrical progression, any term in the arithmetical progression will be the logarithm of the corresponding term in the geometrica progression.

This table contains the common logarithms of all the natural numbers from 0 to 10000, calculated to six decimal places; such, on account of their superior accuracy, being preferable to those, that are

computed only to five places of decimals.

In this form, the logarithm of 1 is 0, of 10, 1; of 100, 2; of 1000, 3. &c. Whence the logarithm of any term between 1 and 10, being greater than 0, but less than 1, is a proper fraction, and is expressed decimally. The logarithm of each term between 10 and 100, is 1, with a decimal fraction annexed; the logarithm of each term between 100 and 1000 is 2, with a decimal annexed, and so on. The integral part of the logarithm is called the Index, and the other the decimal part.—Except in the first hundred logarithms of this Table, the Indexes are not printed, being so readily supplied by the operator from this general rule; the Index of a Logarithm is always one less than the number of figures contained in its corresponding natural number—exclusive of fractions, when there are any in that number.

The Index of the logarithm of a number, consisting in whole, or it parts, of integers, is affirmative; but when the value of a number is less than unity, or 1, the index is negative, and is usually marked by the sign, —, placed either before, or above the index. If the first significant figure of the decimal fraction be adjacent to the decimal point the index is 1,— or its arithmetical complement 9; if there is one cipher between the decimal point and the first significant figure in the decimal, the index is — 2, or its arithmetical complements, the index is — 3, or 7, and so on; but the arithmetical complements, 9, 8 Y &c. are rather more conveniently used in trigonometrical calculations

The decimal parts of the logarithms of numbers, consisting of the same figures, are the same, whether the number be integral, fractional, or mixed: thus,

N. B. The arithmetical complement of the logarithm of any number, is found by subtracting the given logarithm from that of the radius, or by subtracting each of its figures from 9, except the last, or right-hand figure, which is to be taken from 10. The arithmetical complement of an index is found by subtracting it from 10.

## PROBLEM I.

To find the logarithm of any given number.

#### RULES.

1. If the number is under 100, its logarithm is found in the first page of the table, immediately opposite thereto.

Thus the Log. of 53, is 1.724276.

2. If the number consists of three figures, find it in the first column of the following part of the table, opposite to which, and under o, is its locarithm.

Thus the Log, of 384 is 2.584331-prefixing the index 2, because

the natural number contains 3 figures.

Again the log, of 65.7 is 1.817565—prefixing the index 1, because there are two figures only in the integral part of the given number.

3. If the given number contains four figures, the three first are to be found, as before, in the side column, and under the fourth at the top of

the table is the logarithm required.

Thus the log of 8735 is 3.941263—for against 873, the three first figures found in the left side column, and under 5, the fourth figure found at the top, stands the decimal part of the logarithm, viz .941263, to which prefixing the index, 3, because there are four figures in the natural number, the proper logarithm is obtained.

Again the logarithm of 37.68 is 1.576111—Here the decimal part of the logarithm is found, as before, for the four figures; but the index is 1, because there are two integral places only in the natural number.

4. If the given number exceeds four figures, find the difference between the logarithms answering to the first four figures of the given number, and the next following logarithm; multiply this difference by the remaining figures in the given number, point off as many figures to the right-hand as there are in the multiplier, and the remainder, add-

ed to the logarithm, answering to the first four figures, will be the fequired logarithm, nearly.

Thus; to find the logarithm of 738582; the log. of the first four figures, viz. 7385 .368350 the next greater logarithm = 868469

Dif. 59 = 82

118 472

then to .868350 add 48

the sum 5.868398, with the proper index prefixed, is the required logarithm.

5. The logarithm of a vulgar-fraction is found by subtracting the logarithm of the denominator from that of the numerator; and that of a mixed quantity is found by reducing it to an improper fraction, and proceeding as before.

Thus to find the Logarithm of  $\frac{7}{8}$ ; from the log. of 7 = 0.845098 subtract the log. of 8 = 0.903090

Remainder = 9.942008 = the required log.

#### PROBLEM II.

To find the number answering to any given logarithm.

#### RULES.

1. Find the next less logarithm to that given in the column marked at the top, and continue the sight along that horizontal line, and a logarithm the same as that given, or very near it, will be found; then the three first figures of the corresponding natural number will be found opposite thereto in the side column, and the fourth figure immediately above it, at the top of the page. If the index of the given logarithm is 3, the four figures thus found are integers; if the index is 2, the three first figures are integers, and the fourth is a decimal, and so on.

Thus the log. 3.152580 gives the Nat. Numb. 1357
2.132580 gives 13.57
1.132580 gives 13.57
0.132580 gives 1.357
9.132580 gives 1.357 &c.

2. If the given logarithm cannot be exactly found in the table, and if more than four figures be wanted in the corresponding natural number; then find the difference between the given and the next less loga-

rithms, to which annex as many ciphers as there are figures require above four in the natural number; which divide by the difference is tween the next less, and next greater logarithms, and the quotient se next to the four figures formerly found, will give the required nature number.

Thus to find the natural number of the log. 4.828991; the next less log. is .828982 which gives 6735; the next greater log. is 829046

Dif. = 64 next less log. = 828982 given log. = 828991

Dif. with one o annexed = 96 then 64) 90 (1.4

260 256

therefore 1.4 being annexed to 6735, the required natural number 67351.4, is now obtained.

#### TABLE I.

[No.]	Log.	No.	Log.	No.	Log.	No.	Log.	No.	Log
1	0.000000	21	1.322219	41	1,612784	61	1.785310	21	E-SDE415
2	0.301030	22	1.342423	42	1.623249	62	1.792391	82	1.013514
3	D.477121	23	1.361728	43	1.633468	63	1.799341	83	1,919078
4	0.602060	24	1,380211	44	1.643453	64	1,806180	84	1.016275
5	0.698970	25	1.397940	45	1.653213	65	1.811913	84	1.920479
6	0.778151	26	1.414973	46	1.662758	66	1.810544	86	1-93445
7	0.845098	27	1.431364	47	1.672098	67	1.826075	57	1-939519
8	0.903090	28	1.447158	48	1.681241	68	1.832500	28	1.944451
9	0.954243	29	1.462398	49	1.690196	69	1.838849	Sq.	1.949597
10	1.000000	39	1/477121	50	1.698970	70	1.845098	90	1,954741
1 11	1.041393	31	1.491362	51	1.707570	71	1.851258	91	2.950041
12	1.079181	32	14505150	52	1.716003	72	1.857332	112	1-953735
13	1.113943	33	1,518514	53	1.724276	73	1.863333	91	1.958451
14	1.145126	34	4531479	54	1-732394	74	1.869232	94	1.973128
15	1,176091	35	1-544068	55	1.740363	75	1.875061	95	3.97775
16	1.204120	36	1.556302	56	1.748188	76	1.880814	96	1,982271
1 37	1.230449	37	1.568202	57	1.755875	77	1.386491	97	1.980772
28	1.255273	38	1.579784	58	1.763418	78	1.892095	98	1.991 230
19	1.278754	39	1.591065	59	1.770852	79	1,897627	99	1.995835
20	1030	40	1.602060	60	3.778151	80	1.903090	100	1.000000

0		2	3	4	5	6	7	8	9
342423	342520	342817	343014	348212	\$48400	343506	343802	341999	14440
	344589				345374	345570	245756	345962	14514
346353	346549	346744	346939	347115	147330	847525	147720	302915	345 (4)
	348500								10005
	350449							351790	19198
	354375							353724	
354108	354304	354493	354685	354876	355068	355200	355652	355043	35583
\$46026	356217	256408	326400	350000	356681	357172	357503	257.854	36774
357936	258125	348316	358506	158646	3 (8886	359076	350266	354450 301350	35904
359855	300025	\$50±15	360404	360593	360383	360972	361161	301340	30853
								163236	
								105113	
								180081	
	367542								30000
204324	397542	201180	390915	Shores	anotas	270228	270545	SANENE	17086
109210	369401	200200	200105	309930	370743	3/9340	374313	SAME A	37272
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573	75815	758230	758306	758382	758458	758533	758600	75868	758761	258830
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	84	766413						766859			
	85	767156		767304			767527	767601	767675	767749	767823
	86			768046				768342			
	88			769525		769673		769820			770042
	89	770115		770263	770336	770410	770484	779557	770631		770778
	90	770852		770999		771145	771220	Married Street,	771367	774440	771514
	91	771587		771734	771808	771881	771955	772028	772102	772175	772248
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	02	779596		779741			779957		750101	780173	
	03	780317	780389	780461	780533	780605	780677	780749	780821	780893	380965
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	620	792392	792462	792532	792602	792672	792742	792812	792882	792952	793022
	621	793091		793331	793301	793374	793441				793721
	622	793799		793930				794109			
	624	794481	79535	795324	794697	795461	795522	794906	795671	795741	
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1	803	904715	904770	904824	904878	004031	904986	9044499	904553	9051480	005201
п	804	905256	905310	905364	905418	905472	905526	905580	90 (634	904688	005742
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	892	950369	950413	950462	950511	1950500	950508	950657	950705	950754	9666
	893	950851	950900	950949	950997	951046	951095	951143	951192	951240	95126
	894	951337	951386	951435	951483	951532	951580	951629	951677	954726	95117
	845	1951823	951872	951920	951969	952017	952000	952114	952103	952211	0745
	896	952308	952356	952405	952453	952502	952550	952599	952047	952090	95===
	897	052702	1 052841	0.02880	952938	952986	953034	1953083	953131	953180	0.03333
	898	953270	953325	953373	953421	1953470	953518	953566	953615	953663	953718
	899	953760	953808	953856	953909	953953	954001	954049	954098	954146	954198
	900		954291								-
	924	05477	954773	054834	DEASE	0 54918	054066	055014	055062	055110	
	902	05530	955255	055002	05575	055700	954900	055405	DESERT	DEEED	04/540
	903	195520	955736	955303	95737	333395	95544	055076	05600	056050	general
		195500	8 056216	955704	95503	1955000	955920	955910	950020	006000	orthon.
	904		956216								
	905	95004	9 956697	1950745	95079	950040	95000	950930	95090	957030	9575
	906		8 957176								
	907	95700	7 957655	1957703	95775	957/9	95704	7 957094	95794	95799	950030
	908	95808	6 958134	958181	95022	9 95027	95032	5 950373	950424	95040	95051
	909	95050	4 958612	958059	95870	95075	95000	3 950050	95009	95094	119 70 304
	910	95904	1 959089	959137	95918	4 95933	2 95928	0 959328	95937	95942	1959474
	911	95951	8 959566	959614	95966	1 95970	95975	7 959804	95985	95990	959941
	912	95999	5 960042	960090	96013	8 96018	5 96023	3 960281	96032	96037	6 96041)
	913	96047	8 959566 5 960042 1 960518	960566	96061	3 96066	1 96070	9 960756	96080	4 96085	£ 96034
	914	96094	5 90099	001041	190108	9 96113	6 90118	4 961231	901270	96432	0 00157
	915	196142	1 961469	1961516	96156	3 96161	1 96165	8 961706	96175	96180	1 96184
	916	96189	5 961469	961990	96203	8 96208	5 96213	2 962180	96222	96117	5 96533
	917	96236	9 962417	962464	196251	1 96255	9 96260	6 962653	96270	1 96274	8 95279
	918	96284	3 962890	962937	96298	5 96303	2 96307	9 963126	96317	4 96322	1 96335
	919	06331	5 96336	963410	96345	7 96350	4 96355	2 963599	196364	6 96369	5 96174
	920		8 96383								-
	921		0 96430								
	922		1 96477		06480	2 06404	90449	5 964543	90459	065	3 9040
	923		2 96524	06:206	96524	2 06:20	0 00490	2 06 448	06-43	1 0655	8 9651
	924	96:67	2 965719	0 06 5 766	10658	2 06 - 96	2 06400	7 905404	06500	1 96604	8 460
	925	96614	2 966 18	066236	06629	2 06622	0/0664	6 966	95500	064	- 064
	926	96661	1 96665	8 06620	19665	2 0667	8 0668	5 0669	96647	0660	6 9610
	927	06708	0 06712	7 06717	06773	0 06776	7 96004	1 06-26	96093	8 0654	1 1050
	928	96754	8 96759	06764	06769	8 06750	5 96731	7 90730	90740	90745	4 9675
	929	96801	6 96806	06810	0681-	6 06822	7 90778	0 0682	96787	06939	250
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	931	90895	0 968996	969043	96909	0 96913	0 96918	3 969229	9 96927	6 96932	3 9693
	932	90941	0 909462	2 969 500	96955	6 96960	2 96964	9 96969	06074	2 00078	8 9660
	933	190900	21909921	909974	197902	1 97006	8 07011	4 07016	1 97020	7 97020	4 9703
	934	97034	7 97939	31970440	97048	6 97053	2 07057	0 07002	regree	1 97071	9 9707
	935	97001	2 970058	970904	97005	1 97099	7 97104	4 07 1000	OTELL	7 97 1 13	310711
	936	97127	0 07131	1 971300	97141	5 07 140	1 07150	8 07 155	107160	0 07104	T 00 10
	937	97174	0 971781	11971832	107187	0 07 102	5 07107	1 07201	07206	1 07211	COPE
	938	19/ HAW	2 32-44	21972291	197234	2107278	0 07242	4 073460	07252	7 07447	
	939	97266	6 97271	972758	97280	4 97285	1 97289	7 97294	97298	9 97301	5 0720
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							THE RESERVE AND ADDRESS OF THE PERSON NAMED IN COLUMN TWO				

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940	973128	973174	973220	973266	973313	973359	973405	973451	9-349-	4-3543
941	973590	973636	973682	973728	973774	973820	973866	973915	4-3954	174005
942	974051	974097	974143	974184	974235	974281	974327	9: +373	9. 1420	974400
943	974512	974558	974004	1974050	974090	974742 975202	974700	974034	974000	97.4920
944	974972	975018	075524	975110	0-1616	975661	076727	075753	075700	476845
946	07:841	075037	UT 508 2	076020	476075	976121	976166	076212	076258	4"6704
947	976350	976396	976442	976487	976533	976579	976625	976671	976717	9:6762
948	976808	976854	976900	976946	976991	977037	977083	977129	977175	977420
949						977495				
950	977724	977769	977815	977861	977906	977952	977998	9-8013	978589	978135
951	478180	978226	978272	978317	978363	978409	978454	9:8500	9.85.16	9-8591
952	978637	978683	978728	978774	978819	978865	978911	978956	979002	979047
953	979993	979138	979104	979230	979275	971321	979300	0:0867	9/945	9.9503
954 955	080003	080010	080201	080140	08018	980231	080276	9,000	9.9912	080412
956	982458	080502	080:40	9" 504	980640	980685	980-30	4807-6	480821	166 17
957	983912	980957	981201	81048	981093	981139	981184	981226	981275	081325
958	981365	981411	981450	981501	981547	981597	91163-	981643	481- 28	981,23 981,73
959	481819	981864	981929	981954	982000	9:2045	982090	982135	982181	982226
₩ 960	982271	982516	982362	982407	982452	982497	982543	082588	49:633	982678
961	982733	981-09	982814	982859	983904	982947	982994	083040	983085	983130
962	983175	943220	983265	1983310	983356	983.5011	973446	340	983536	983130 983581 , 4032
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964	100 4 1224	20000	081617	108166	108 1707	6×47=2.	084-07	001842	XAYXO	0545221
966	084077	985022	985067	985112	98515	985202 985651	98;24-	985292	.8:337	485382
967	985426	985471	985516	985561	985606	985651	98,6,6	985741	95576	985830
968	1085875	085020	985905	086010	936055	980100	980144	031060	480234	4502.91
969	986324	986369	986413	986455	986503	986548	986593	98663-	986682	986727
970	086772	086816	986861	086006	986951	986995	987040	487385	987132	95:174
971	987219	98: 164	987309	98-353	98-398	987443	987487	987532	987577	95-622
972	987666	987711	987756	987800	987845	987890	987931	98-979	988024	489008
973	988113	988157	988202	988247	985291	988336	088816	988425	088016	488063
974 975	980005	980003	080001	080128	080182	988782	980272	980316	680161	989405
976	080450	080101	989534	989583	989628	989672	989717	489761	439806	989850
977	0808nc	ahanza	480087	000028	000072	000117	000161	000206	000250	0602021
F. 978	990339	990383	990428	990472	990516	990561	990605	990650	469066	990738
27.9	990783	990827	990071	990910	940900	991004	991049	991393	991137	491102
980	991226	991270	991315	991359	991403	991448	491494	4,91530	991580	991625
981	991659	991713	1991757	991802	941846	991890	991034	9919"9	992023	992007
982	992111	992156	992200	992244	992288	992333	992377	992421	99:405	99:5:39
983	992553	992598	992042	992030	992730	992774	002260	0022201	992907	993392
985	002426	993039	993524	993:68	993613	993657	941701	993745	993789	
986	007877	007021	997965	004000	004053	994097	0011411	991185	994320	9942731
987	004317	004361	994405	994449	994493	994537	994581	994025	994009	9947131
988	1994757	994801	994845	994889	994933	994977:	995021	995204	945100	99515-1
989	995196	995240	995284	995328	995372	995416	995460	995:04	995547	995591
990	995635	995679	995723	995767	995811	995854	995848	995942	995986	996030
991	996074	996117	996161	996205	996249	996293	996336	996380	996424	990408
992	996512	996555	996599	996643	996687	996730	990774	990818	990802	990935
993	996949	996993	997037	997080	997124	997168	007648	997255	007776	99,343
994	997380	997430	99 4/4	1997517	997501	998041	948386	998118	998172	998216
995	008250	008202	995746	998390	998434	998477.	998521	993504	998608	995057
997	99866:	998730	998782	1998820	998869	998913	998950	999000	999043	99900
998	1000123	00017.1	000218	1000201	205000	999348	999392	900435	499170	9995221
929	999565	999609	999652	949696	999:39	999783	999826	9698-0	999913	40995
	0	1	2	3	4	5	6	7	3	9 1
		-	_	-	-	-	-	-	-	-



Logarithmic Since, Tangente, and Secanta.

This table contains the logarithmic, or, as they are sometimes called, the artificial sines, tangents, and secants, to each degree and minute of the quadrant, with their complements of the quadrant, with their complements of the quadrant, and co-secants, to six places of figures besides us index.

To find the Logarithmic Sine, Co-Sine, Us. of any Number of Degrees and Minutes.

If the given degrees be under the they are to be taken from the top, and the minutes from the left the minutes, opposite to which in that column with the name of the logarithm at the top, will be found the required logarithm. But if the degrees be more than 45, they will be found at the bottom of the page, and the minutes in the right side column; likewise the name of the logarithm is to be taken from the bottom of the page.

When the given degrees exceed 90, they are to be subtracted from 180 degrees, and the logarithm of the remainder taken out as before Or the logarithmic sine, tangent, &c. of degrees more than 90, is the logarithmic co-sine, co-tangent, &c. of their excess above 90 degrees.

#### EXAMPLES.

			۵	•		logarithm
Requ	ired th	e log. sine of	36	32	•	9.774729
-	-	co-sine of	61	18	-	9.681445
-	-	tangent of	54	17	-	10 143263
-	-	co-tang. of	42	50	-	100:2877
-	-	secant of	19	27	_	10.025519
-	-	co-secant of	70	33	-	10.025519
-	-	sine of	108	36)		
-	C	r sine of	71	24		9.976702
• '	•	or co-sine of	18	36		

Ro find the Degrees and Minutes nearest corresponding to a given Logsrithmic Sine, Co-sine, &c.

Look in the column marked at the top or bottom with the name of the given logarithm, and when the nearest to it is found, the corresponding degrees and minutes will be those required, observing that when the name is at the top of the column, the degrees are to be taken from the top and the minutes from the left side column, but if the name is at the bottom, the corresponding degrees will be there like wise, and the minutes in the right side column.

#### RYAMPLES.

#### The degrees and minutes corresponding to the

log. sine	9.265390	are	100	37'
	9 - 28461		70	
tangent	9 70156		26	42
secant	10.25413		56	9

The logarithmic sines, &c. taken out to degrees and minutes only are in general sufficiently accurate but in some of the more rigid astronomical calculations, it is frequently necessary to take them out to the nearest second; when this is the case they are to be found in the following manner:

To find the sine, tangent, Ws. of an arch expressed in degrees, minutes and seconds.

#### RULE.

Find the sine, tangent, &c. answering to the given degree and minute, and also that answering to the next greater minute; multiply the difference between them by the given number of seconds, and divide the product by 60; then, the quotient added to the sine, tangent, &c. of the given degree and minute, or subtracted from the co-sine, co-tangent, &c. will give the quantity required, nearly.

If the arch be less than three degrees, it will be necessary to use the following rule:—

To the arithmetical complement of the given degrees and minutes reduced to seconds, add the logarithm of the given degrees, minutes, and seconds, reduced to seconds, and the logarithm, tangent, &c. of the given degrees and minutes, the sum, rejecting 10 from the index, will be the logarithm, tangent, &c. of the proposed number of degrees,

minutes, and seconds.

To find the degrees, minutes, and seconds, answering to a given logarithmic sine, tangent, &c.

#### Ruls.

Find the degrees minutes and seconds answering to the next less logarithmic sine, tangent, &c. which subtract from that given; multiply the remainder by 60, and divide the product by the difference between the next less and next greater logarithms, and the quotient will be the seconds to be annexed to the degrees and minutes before found.

If the given logarithm is that of the sine or tangent of a small archen, to the arithmetical complement of the next less logarithm in the tables, add the given logarithm, and the logarithm of the degrees and minutes, in seconds, answering to the next less logarithm, the sum, rejecting radius, will be the logarithm of the number of seconds in the required arch.

M	Sine 0 Degree-										
1 6.459296 6.930673 6.930673 2 6.740736 6.7916 6.930673 3 6.940847 6.064328 6.986605 7.007794 7.027907 7.047303 56 4 7.06786 7.745376 7.700548 7.116938 7.13733 7.147973 56 6 7.41877 7.735376 7.726535 7.276639 7.287034 7.229047 7.339145 7.401578 7.409850 7.41998 7.445937 7.445375 7.441449 7.4449002 7.456426 07 10 7.465715 7.470904 7.477966 7.484915 7.491754 7.49850 07 11 7.505118 7.11649 7.518083 7.544423 7.350042 7.530824 47 12 7.543106 7.483907 7.538064 7.590053 7.56035 7.56035 7.570083 7.614993 7.020072 7.632003 7.632005 7.604954 47 13 7.57668 7.483907 7.524806 7.550055 7.560587 7.572066 47 14 7.6094173 7.698410 7.702606 7.705762 7.705784 7.604934 47 17 7.694173 7.698410 7.702606 7.705762 7.710879 7.714957 12 7.74897 7.7299 7.772606 7.705762 7.710879 7.714957 12 7.78994 7.78376 7.79397 7.	M	1 0"	10"	20"	30"	40"	50"				
1 6.469;26 6.350673 6.38565; 6.038617 6.085575 6.726507 3 2 6.764756 6.79475 6.769;18 6.83173 3.686666 6.886695; 7.027994 7.027997 7.02997 7.0	0		5.685575	5.986605	6.162696	6.287635	6,184545	50			
3 6.940847 6.964328 6.986605 7.007794 7.027997 7.047303 56 4 7.05786 7.853515 7.00548 7.11933 7.12733 7.417973 56 5 7.16366 7.176936 7.19043 7.19043 7.200869 7.217054 7.220605 54 7 7.308824 7.319043 7.329027 7.338787 7.45795 7.236767 57 7.308824 7.319043 7.329027 7.338787 7.447903 7.459376 7.355757 7.384544 7.393145 7.401578 7.404803 51 9 7.41968 7.435937 7.437375 7.444449 7.44902 7.459436 53 100 7.463735 7.4470904 7.477966 7.484915 7.401578 7.404803 51 11 7.504118 7.51649 7.518083 7.444449 7.44902 7.459436 53 12 7.54306 7.58307 7.554806 7.560635 7.560637 7.550638 7.572065 7.572065 7.57306 7.58301 7.59306 7.59307 7.554806 7.59307 7.554806 7.560637 7.560637 7.56043 7.572065 7.57206 7.58301 7.50494 7.572345 7.50799 7.581208 7.56370 7.65297 4.7694173 7.694173 7.694173 7.702606 7.70279 7.704777 7.746270 7.750031 7.753758 7.757454 7.761119 40 7.744477 7.746270 7.750031 7.753758 7.757454 7.761119 40 7.764754 7.78376 7.81302 7.78494 7.78383 17.78383 17.78383 17.82229 17.78457 7.81311 7.82229 17.78367 7.81302 7.81311 7.82229 17.78457 7.81311 7.82229 17.783668 7.88360 7.99360	1	6.463726	6.530673				6:726967	58			
4 7.06c786 7.083315 7.100348 7.110938 7.131233 7.142933 55 7.16066 1.7004 7.20642 54 7.2					The state of the s			57			
5 7 163646 7 217034 7.17035 2.17034 7.20605 2.17034 7.20605 2.17034 7.308824 7.319043 7.329027 7.318787 7.307872 7.407882 7.325707 2.32707 7.384524 7.393145 7.401578 7.404883 2.70187 7.401578 7.404883 2.70187 7.401578 7.404883 2.70187 7.401578 7.404883 2.70187 7.401578 7.404883 2.70187 7.401578 7.404883 2.70187 7.40187 7.401578 7.404883 2.70187 7.4				A CONTRACTOR OF THE PARTY OF TH	All land to the same						
6 7 241877 7.308844 7.319043 7.329027 7.36839 7.287935 7.298328 33 7 7.308844 7.319043 7.329027 7.318787 7.348332 7.357672 32 8 7.36816 7.375770 7.384544 7.393145 7.401578 7.468830 31 10 7.463735 7.47904 7.47966 7.484915 7.441490 7.449680 32 11 7.50518 7.511649 7.518083 7.5444149 7.449680 32 11 7.50518 7.511649 7.518083 7.524423 7.520672 7.530832 41 12 7.543966 7.548897 7.554806 7.506035 7.566387 7.530832 41 12 7.509833 7.614993 7.620072 7.625035 7.656387 7.570662 47 14 7.609853 7.614993 7.620072 7.625035 7.658081 7.652929 47 15 7.607844 7.673345 7.676799 7.681208 7.685573 7.66239 47 17 7.694173 7.68410 7.072606 7.07662 7.70879 7.744971 7.722099 7.725065 7.730896 7.734791 7.732691 7.722099 7.725065 7.730896 7.734791 7.734791 7.742477 7.746270 7.720006 7.70562 7.778994 7.73894 19 7.744477 7.746270 7.72001 7.753758 7.757494 7.751495 41 7.783943 7.783943 7.783946 7.783946 7.783946 7.783946 7.783946 7.783946 7.783946 7.783946 7.783946 7.783946 7.784947 7.84994 7.784947 7.784947 7.784947 7.784947 7.784947 7.784941 7.784941 7.84994 7.784943 7.84994 7.784943 7.84994 7.784943 7.84994 7.784944 7.84994 7.784944 7.84994 7.785948 7.789948 7.789948 7.789978 7.784994 7.784948 7.78994 7											
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34         7.995198         7.997322         7.999435         8.001538         8.003631         8.002914         15           36         8.020021         8.022027         8.024023         8.026011         8.027989         12           37         8.031919         8.035871         8.035814         8.037749         8.039057         8.041592         21           38         8.043501         8.045401         8.047294         8.049178         8.051054         8.052921         21           39         8.056776         8.056633         8.058477         8.060314         8.062142         8.063063         20           40         8.066776         8.067582         8.069380         8.071171         8.072955         8.074731         29           41         8.076500         8.078261         8.080016         8.081764         8.083304         8.081328         18           42         8.086965         8.088684         8.090398         8.09104         8.095497         17           43         8.107167         8.108809         8.110444         8.112074         8.113697         8.115315         18           45         8.116926         8.118532         8.120131         8.121315         8.123313					THE REAL PROPERTY.			15			
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51         8.171280         8.172697         8.174109         8.175517         8.176920         8.178319         2           52         8.179713         8.181102         8.182488         8.183868         8.185245         8.1866t7           53         8.18985         8.189348         8.190707         8.192062         8.193413         8.194760         6           54         8.196102         8.197440         8.198774         8.200104         8.201430         8.202752         5           55         8.204070         8.205334         8.206694         8.208000         8.20302         8.201430         8.202752         5           56         8.211895         8.213185         8.214472         8.215755         8.217034         8.18300         3           57         8.219581         8.220849         8.222113         8.223374         8.224631         8.225884         2           58         8.227133         8.228380         8.239622         8.230861         8.232096         8.233128         1           59         8.234557         8.235782         8.237003         8.238221         8.239436         8.240647         0           6011         501         401         301         201				Name and Address of the Owner, where the Owner, which is the Own				=			
52     8.179713     8.181102     8.182488     8.183868     8.185245     8.186617     7       53     8.187985     8.189348     8.190707     8.192062     8.193413     8.194760     6       54     8.196102     8.197440     8.198774     8.201430     8.202752     5       55     8.204070     8.205384     8.206694     8.208000     8.20302     8.210601     4       56     8.211895     8.213185     8.214472     8.215755     8.217934     8.18309     3       57     8.219581     8.220849     8.22113     8.223374     8.224631     8.225884     2       58     8.227133     8.228380     8.229622     8.230861     8.232996     8.233128     1       59     8.234557     8.235782     8.237003     8.238221     8.239436     8.240647     0       6011     501     4011     3011     2011     4011     1011							5.109859	1 2			
53 8.187985 8.189348 8.190707 8.192062 8.193413 8.194760 6 54 8.196102 8.197440 8.1987440 8.200104 8.201430 8.201752 5 55 8.204070 8.205384 8.206694 8.208000 8.209302 8.210601 4 56 8.211895 8.213185 8.214472 8.215755 8.217034 8.218300 3 57 8.219581 8.220849 8.222113 8.223374 8.224631 8.225884 2 58 8.227133 8.228380 8.229622 8.230861 8.232996 8.233128 1 59 8.234557 8.235782 8.237003 8.238221 8.239436 8.240647 0 50" 50" 40" 30" 20"					8.182868	8.185245		1 0			
54     8.196102     8.197440     8.198774     8.200104     8.201430     8.201430     8.201752     5       55     8.204070     8.205384     8.206694     8.208000     8.209302     8.210601     4       56     8.211895     8.213185     8.214472     8.215755     8.217034     8.18300     3       57     8.22938     8.222113     8.223374     8.224631     8.225884     2       58     8.227133     8.238380     8.229622     8.230861     8.232096     8.233128     1       59     8.234557     8.235782     8.237003     8.238221     8.239436     8.240647     0       601     501     4011     3011     2011     4011					The second secon	8.193413	THE RESERVE OF THE PARTY OF THE	6			
55 8.204070 8.205384 8.206694 8.208000 8.20302 8.210601 4.205384 8.213185 8.214472 8.215755 8.217034 8.218309 3.219581 8.220849 8.22213 8.223374 8.224631 8.225884 2.25884 2.25884 8.234557 8.235782 8.239622 8.233261 8.232096 8.233228 1.2324557 8.235782 8.237003 8.238221 8.239436 8.240647 0.2016 001 501 4011 3011 2011 2011						8.201430					
56 8.211895 8.213185 8.214472 8.215755 8.217034 8.18309 3 57 8.219581 8.220849 8.222113 8.223374 8.224631 8.225884 2 58 8.227133 8.228380 8.229622 8.230861 8.232096 8.233128 1 59 8.234557 8.235782 8.237003 8.238221 8.239436 8.240647 0 6011 5011 4011 3011 2011 4011	55	8.204070	8.205384	8,206694	8.208000	8.209302		- 4			
58 8.227133 8.228380 8.239622 8.230861 8.232996 8.233128 9.234557 8.235782 8.237003 8.238221 8.239436 8.240647 0.2011								3			
59 8.234557 8.235782 8.237003 8.238221 8.239436 8.240647 0	57										
60" 50" 40" 30" 20" 10" 20				A COLUMN TO A COLU							
				THE RESERVE AND ADDRESS.				_			
		6011	50		A STATE OF THE PARTY OF	50	( fd.,	DE			

Co-sinc 89 Degrees.

			Tangent (	Degree,	The state of the s	1	
M	0"	10"	20"	50."	40"	50"	
0		5.685575	5.986605	6.162696	6.287635	6.384545	59
1	6.463726	6.530673	6.588665	6.639817	6.685575	6.726968	58
3	6.764756	6.799518	6,831705	6.861666	6.889695	6.916024	57
3	6.940847	6.964129	6.986605	7.007794	7.027998	7.047303	56
4	7.065786	7.083515	7.100548	7.116939	7-132733	7.147.973	55
5	7.162696	7-176937	7.190715	7.204089	7-217054	7-229643	54
6	7.241878	7-253777	7.265359	7.276640	7.287635	7.298359	53
7 8	7-308825	7-319044	7.329028	7-338788	7-348333	7.357673	52
	7.366817	7-375772	7.384546	7-393146	7-401579	7.409852	51
9	7.417970	7.425939	7.433764	7-441451	7-449004	7.456428	50
10	7.463727	7.470906	7-477968	7.484917	7.491756	7-498490	49
2.1	7.505120	7.511651	7.518085	7.524426	7.539675	7.536835	48
12	7.542909	7.548900	7.554808	7.560638	7.566390	7.572068	47
13	7.577671	7.583204	7-588667	7.594062	7.599391	7.604655	46
14	7.609857 7.639820	7.614996	7.649366	7.625097	7.630060	7.634968	45
16	7.667849	7.672350	7.676804	7.681213	7.685578	7.689900	44
17	7.694179	7.698416	7.702612	7.706768	7.710885	7.714961	42
18	7.719003	7.723005	7.726972	7.730902	7-734797	7.738648	41
19	7-742484	7-746277	7.750037	7-753765	7-757462	7-761127	40
20	7.764761	7.768365	7.771940	7-775485	7.779002	7-782490	39
21	7.785951	7.789384	7.792790	7.796170	7-799524	7.802852	38
22	7.806155	7.809432	7.812686	7.815915	7.819120	7.821302	37
23	7.825460	7.828596	7.831710	7.834801	7.837870	7.840918	36
24	7.843944	7.846950	7.849935	7.852900	7.855844	7.858769	35
25	7.861674	7.864560	7.867426	7.870274	7.873104	7.875915	34
26	7.878708	7.881483	7.884240	7.886981	7.889704	7.892410	33
27	7.895099	7.897771	7.900428	7.903068	7.905692	7.908301	32
28	7.910894	7.913471	7.916034	7.918581	7.921113	7-923631	31
29	7.926134	7.928623	7.931098	7.933559	7.936006	7.938439	30
30	7.940858	7.943265	7-945657	7.948037	7-950404	7.952758	29
31	7.955100	7.957428	7 959745	7.962049	7.964341	7.966621	28
32	7.968889	7-971145	7.973389	7.975622	7.977844	7.980054	27
33	7.982253	7.984441	7.986618	7.988785	7.990940	7.993085	26
34	7.995219 8.007809	7-997343	7.999456 8.011926	8.001560	8.003653	8.005736	25
35	8.020044	8.022051	8.024047	8.026035	8.028014	8.029984	24
37	8.031945	8.033897	8.035840	8.037775	8.039701	8.041618	22
38	8.043527	8.045428	8.047321	8.049205	8.051081	8.052949	21
39	8.054809	8.056661	8.058506	8.060342	8.062171	8.063992	20
40	8.065806	8.067612	8.069410	8.071201	8.072985	8.074761	19
41	8.076531	8.078293	8.080047	8.081795	8.083536	8.085270	18
42	8.086997	8.088717	8.090430	8.092137	8.093837	8.095530	37
43	8.097217	8.098897	8.100571	8.102239	8.103899	8.105554	16
44	8.107202	8.108845	8.110481	8.112110	8.113734	8.115352	15
45	8.116963	8.118569	8.120169	8.121763	8.123351	8.124933	14
46	8.126510	8.128081	8.129646	8.131206	8,132760	8.134308	13
47	8.135851	8.137389	8.138921	8.140447	8.141969	8.143485	12
48	8.144996	8.146501	8.148001	8.149497	8.150987	8.152472	XX
49	8.153952	8.155426	8.156896	8.158361	8 159821	8.161276	10
50	8.162727	8.164172	8.165613	8.167049	8.168480	8.169906	9 8
51	8.171328	8.172745	8.174158	8.175566	8.176969	8.178368	
52	8.179763	8.181152	8.182538	8.183919	8.185296	8.186868	7 6
53	8.188036	8.189400	8.190760	8.192115	8.193466	8.194813	
54	8.196156	8.197494	8.206750	8.208057	8.201485	8.210658	5
55	8.211953	8.205440	8.214530	8 215814	8.209359	8.218369	4
57	8.219641	8.220909	8.232174	8.223434	8.224692	8.225945	3 2
1 3/4	The Person named in column 2 is not to the Person named i		1			0	
C.8	8-227105	8.228442	8.220685	8,270024	5-222100	0.277703	
57 58 59	8-227195	8.235846	8.229685	8.230924	8.232160	8.233392	0
59	8-227195 8-234621	8.228442 8.235846 50''	8.229685 8.237068 4()"/	8.230924 8.238286	8.239501	8.240713	0 1

	Sine 0 Degree.									
i	M	0"	10"	20"	30"	40"	50"			
	0		5.685575	5.986605	6.162646	6.287635	6,384545	59		
ı	1	6.463726	6.530673	6 588865	6.639817	6.685575	6.726967	59		
ı	2	6.764756	6.799518	6.831703	6.861666	6.889695	6.916024	57		
ı	3	7.065786	7.083515	7.100548	7.007794	7.027497	7.047303	56		
P	4	7.162696	7.176936	7.190725	7.204089	7.217054	7.229643	55		
ı	5	7-241877	7.253776	7.265358	7.276639	7.287635	7.298358	53		
R	7 8	7.308824	7.319043	7.329027	7.338787	7-348332	7.357672	50		
ı	No.	7.366816	7.375770	7.384544	7-393145	7.401578	7.409850	51		
B	9	7-417968	7:435937	7.433762	7.441449	7,449002	7-450416	50		
ı	10	7.463725	7.470904	7.477966	7.484915	7.491754	7-49 487 7-516832	440		
K	12	7.542906	7-548897	7.554806	7.560635	7.566387	7.572065	47		
ı	13	7.577668	7-583201	7.588664	7 594059	7.599388	7.604052	46		
N	14	7.609853	7.614993	7.620072	7 625093	7.630056	7 634963	45		
N	16	7.639816	7.644615	7.649361	7.654056	7.658701	7.663297	35		
ı	15	7.697844	7.672345	7.676799	7.706762	7.685573	7.689894	43		
ı	17	7.718997	7.722999	7-726965	7.730896	7-734791	7-738651	41		
ı	19	7.742477	7.746270	7-750031	7.753758	7-757454	7.761119	40		
ı	20	7-764754	7-768358	7-771932	7-775477	7.778994	7-782482	39		
۱	2.1	7.785943	7.789376	7.792782	7-796162	7.799515	7.801843	38		
ı	22	7.806146	7.809423	7.811677	7.815905	7.819111	7.822292	37		
ı	23	7.825451	7 828586	7.849924	7.834791	7.837860	7.840907	36		
ı	25	7.86:662	7 864548	7.867414	7.870262	7.873092	7.875902	34		
ı	26	7.878695	7.881470	7.884228	7.886968	7.889690	7.892396	31		
ı	27	7.895085	7.897758	7.900414	7.903054	7.905678	6.908187	32		
ı	28	7.910879	7-913457	7.916019	7.918566	7.921098	7-923616	프		
ı				7.931082	7-933543	7.935989	7.938422	30		
ı	30	7.940842	7.943248	7-945641	7.962031	7.950387	7.952741 7.966601	20		
ı	32	7.968870	7.971126	7-973370	7.975603	7.977824	7.980034	37		
ı	33	7.982233	7.984421	7.986598	7.988764	7.990919	7-993064	26		
ı	34	7.995198	7.997322	7-999435	8.001538	8.003631	8.005714	25		
ı	35	8.007787	8.009850	8.011903	8.013947	8.015981	8.018005	#		
ı	37	8.031919	8.033871	8.024023	8.037749	8.039675	8.029959	3		
ı	38	8 043501	8.045401	8.047294	8.049178	8.051054	8 052922	21		
1	39	8,054781	8.056633	8.058477	8 060314	8.062142	8.063963	10		
ı	40	8.065776	8.067582	8.069380	8.071171	8.072955	8.074731	19		
ı	41	8.076500	8.078261	8,080016	8.081764	8.083504	8.085238	18		
ł	43	8.086965	8.088684	8.090398	8.102204	8.093804	8,095497	17		
I	44	8.107167	8 108800	8.110444	8.112074	8,103864	8.105519	15		
ı	45	8.116926	8.118532	8.120131	8.121725	8.123313	8.124895	14		
ı	46	8.126471	8.128042	8.129606	8.131166	8.132720	8.134168	15		
ı	47	8.135810	8.137348	8.138879	8.140406	8.141927	8.143443	時		
ı	48	8.144953 8.153907	8.146458	8.147959 8.156852	8.149453	8.150943	8.152428	10		
ŀ		8.162681	THE RESERVE THE PERSON NAMED IN	Married World Co., or other Printers of the Party of the	_		8.161231	_		
ı	50	8.171280	8.164136	8.165566	8.175517	8.161433	8.169859	8		
ı	52	8.179713	8.181102	8.182488	8.183868	8,185245	8,186617	1		
	53	8.187985	8.189348	8,190707	8.192062	8.193413	8.194760	6		
1	54	8.196102	8.197440	8,198774	8 200104	8.201430	8.202752	9		
1	55	8.204070	8.213185	8.206694	8.208000	8 209302	8.210601	1		
1	57	8.219581	8.220849	8,214472	8.215755	8.224631	8.218309	N 100		
	58	8.227133	8.228380	8.229622	8.230861	8.232096	8.233338	1)		
	59	8.234557	8.235782	8.237003	8.238221	8.239436	8.240647	0		
		60"	50"	40"	30"	2011	10%	M		
			The Real Property lies	Co-sine 89	Degrees.	-		-		
				Co desper		1				

Tangent O Degree, 40" 0" 10" 20 30. 50" M 6.384545 6.287635 5.685575 5.986605 6.162696 0 59 1 6.463726 6.530673 6.588665 6.639817 6.685575 6.726968 6.831703 6.861666 6.889695 6.916024 6.764756 6.799518 2 57 6.940847 6.964329 6.086605 7.007794 7.02-908 7.047303 3 7.116939 7.083515 7-132733 7.065786 7.100548 7.147973 4 55 7.217054 7.229643 7.162696 7.176937 7.190745 7.204089 5 54 7.298359 7.241878 7.265359 7.287635 7.276640 7.253777 53 7.329028 78 7.308825 7.319044 7-338788 7-348333 7.357673 52 7.366817 7-375772 7.393146 7.401579 7.409852 7.384546 51 7-456428 50 9 7.417970 7.425939 7.433764 7-441451 7-449004 10 7-470006 7 484917 7-477968 7.463727 7.491756 7.498490 49 7.524426 7.560638 7.518085 7.536835 11 7.505120 7.511651 7-530675 7-554808 7.566390 7.548900 7.572068 12 7.542909 47 7.577671 7.604655 7.583204 7.588667 13 7.594062 7-594391 46 7.634968 7.614996 7.6200-6 7.609857 7.625097 45 14 7.630060 7.6;8:06 15 7.654061 7.639820 7.644619 7.649366 7.663301 44 7.684900 7.667849 7.676804 7.681213 7.672350 7.685578 16 43 7.698416 7-702612 7.706768 7-710885 17 7.694179 7.714962 42 18 7.719003 7.723005 7.726972 7.730902 7-734797 7.738658 41 19 7.742484 7-746277 7.750037 7-753765 7.757462 7.761127 40 20 7.764761 7.768365 7.771940 7-775485 7.779002 7-782490 39 7.792790 7.796170 7.789384 7.802852 38 21 7.785951 7-799524 7.806155 22 7.819120 7.822302 37 7.840918 36 23 7.825460 7.828596 7.831710 7.834801 7.837870 7.858769 7.843944 7.846950 7.849935 7.852900 7.855844 24 35 25 7.861674 7.864;60 7.867426 7.870274 7.873104 7.875915 34 7.878708 7.884240 7.881483 7.886981 7.892410 26 7.889704 33 7.895099 7.897771 7.903068 7.008201 27 7.900428 7.905692 32 28 7.910894 7 916034 7.918581 7.913471 7.921113 7.423631 31 7.928623 7.931098 7.936006 29 7.926134 7-938439 30 7-933559 7.940858 7-943265 30 7 945657 7.948037 7-952758 7.950404 29 7.955100 7-957428 31 7.962049 7-966621 7 959745 28 7.964341 7.968889 -.980054 32 7-971145 7-973359 7.975622 7.977844 27 7.984441 7.986618 7.982253 7.988785 33 7.990940 7.993085 26 7.999456 8.001560 8 00 3653 8.005736 7.995219 7.997343 34 25 8.009872 8.016004 8,007800 8.011026 8.01 .029 24 35 8.013970 8.026035 8.029984 36 4.020044 8.022051 8.024047 8.028014 23 8 031945 8.033897 8.035840 8.037775 8.039701 37 8.041618 22 8.045428 38 8.043527 8.047321 8.049205 8.051081 8.052949 21 8.060342 8.062171 39 8.054809 8.058506 8.063992 20 40 8.065806 8.067612 8.069410 8.071201 8.072985 8 074761 19 8.080047 8.078293 8.083536 41 8.076531 8.081795 8.085270 42 8.088717 8 093837 8.095530 8.086997 8.090430 8.092137 17 8.098897 8.097217 8.100571 8.102230 8.103899 8.105554 16 43 8.107202 8.108845 8. 110481 8.112110 8.113734 8.115352 44 15 8.118569 8.116963 8.120169 8.121763 8.123351 8.124933 14 46 8.128081 8.134308 8.126510 8.129646 8.131206 8.132760 13 8.138921 8.135854 8.137389 8.140447 8.141969 8.143485 47 12 8.148001 48 8.144996 8.146501 8.149497 8.150987 8.152472 .. 8.156896 8.158361 49 8.153952 8.155426 8 159821 8.161276 10 8.162727 8.165613 8.167040 8.168480 8,169906 8.164172 50 9 8.172745 8.171328 8.174158 8.175566 8.176969 8.178368 51 8.181152 8.182538 8.183919 8.185296 8.179763 8.186663 52 76 8.188036 8 180100 8.190760 8.192115 8.193466 53 8.194813 8,200159 8.196156 8.198829 8.197494 8,202808 8.201485 54 5 8.208057 8.210658 8.204126 8.206750 8.209359 55 8.205440 4 8.211953 8.213243 8.214530 8 215814 8.218360 8.217093 3 8.222174 8.223434 57 8.219641 8.220909 8.224692 8.225945 2 8.228442 8.227195 8.229685 8.230924 8.232160 8.233392 1 59 8 234621 8.235846 8.237068 8.238286 8.239501 8.240713 0 59" 20" 10" 30% 6011 40" M

Co-tangent 89 Degrees.

			The state of the s	Sine 1		S. A. Landon		100
H	M	0"	10"	20"	30"	40"	50"	1-1
ı	0	8.241855	8.243060	8.244261	3.245459	8,246054	8.247845	59
		8.249033	8.250218	8.251400	8.252578	8.253753	8.254925	1 58
п	2	8.250094	8,257260	8.258423	8.259582	8.160739	8.261892	57
п	3	8.263042	8.264190	8.265334	8.266475	8.267613	8.268749	56
п	4	8.209881	8 271010	8.272137	8.273260	8.274381	8.275499	55
и	5	8.176614	8.277726	8.278835 8.285431	8.279941	8.287608	8.288692	60 11
ı		8.283243	8.290852	8 291928	8.293002	8.294073	8.295141	1 41
1	7 8	8.296207	8.297270	8.298330	8.299388	8.300443	8.301496	CI
ı	9	8.302546	8.303594	8.304639	8,305581	8.306711	8.307759	10
ı	10	8.108794	8-309827	8.310857	8.311885	8 312910	8.311933	44
1	11	8.314954	8.315972	8.316987	8.318001	8.314012	8.320020	49
ı	12	8.321027	8.322031	8.323033	8.324032	8.325029	8,326024	47
ı	13	8.327016	8.328007	8.328995	8.329980	8.330964	8 331945	45
ı	14	8,332924	8.333901	8,334876	8.335848	8.336819	8.337787	45
п	15	8.338753	8.339717	8 340678	8.341638	8.342596	8.343551	***
1	16	8.344504	8.345455	8.346405	8.347352	8.348297	8.349340	43
1	17	8.355783	8.356710	8,357035	8.358558	8.359479	8.360398	11
u	19	8.361315	8.362230	8.363143	8.364054	8.364964	8.365871	40
1	20	8,366777	8.367681	8.368582	8,369482	8.370380	8.371477	
1	21	8.372171	8.373063	8.373954	8 874843	8.375730	8.376015	30 32
и	22	8.377499	8.378380	8.379260	8.380138	8.381015	\$ 381889	37
п	23	8.382762	8.383633	8.384502	8.385370	8.386236	8.387100	16
и	24	8.387962	8.388813	8.389682	8.390539	8.391395	8 392249	35
и	25	8.393101	8.393951	2.394800	8.395647	8.396493	8.397337	34
ı	26	8.398179	8.399020	8.399859	8.400696	8.401532	8.402366	35
ı	27	8.403199	8.404030	8.404859	8.405687	8.411438	8.407338	31
ı	29	8.413068	8.413880	8.414691	8.415500	8.416308	8.417114	30
ı	30	8.417919	8.418722	8.419524	-			24
Н	31	8.422717	8.423511	8.424304	8.420324	8.425886	8.426675	28
н	32	8,427462	8.428248	8.429032	8.429815	8-430597	8.431377	27
1	33	8.432156	8.432933	8:433709	8.434484	8.435257	8.436029	36
1	34	8.436800	8.437569	8.438337	8.439103	8.439868	8.440632	25
1	35	8.441394	8.442155	8.442915	8.443674	8.444431	8.445186	24
1	36	8.445941	8.446694	8.447446	8.448196	8.448946	8.449694	23
1	37	8.450440	8.451186	8.451930	8.452672	8,453414	8.454154	22
4	39	8.454593	8.455631	8.460761	8,457103	8.457837	8.458570	10
1		8.463665	-		-		-	-
4	40	8.467985	8.464388 8.468701	8.465110	8.465830	8.466550	8.467268	19
1	43	8 47 1263	8.472971	8,473679	8.474386	8.475091	8.475795	17
ı	43	8.476498	8.477200	8.477901	8.478601	8.479299	8 479997	16
1	44	8.490693	8.481388	8.482082	8.482775	8,483467	8.484158	15
1	45	8.484848	8.485536	8.486224	8.486910	8.487596	8.488z80	14
1	46	8.488963	8.489645	8.490326	8.491006	8,491685	8-492363	15
1	47	8.493040	8.493715	8.494390	8.495064	8,495736	8.496408	12
1	49	8.497078	8.497748	8.502405	8.499084	8.499750	8,504386	10
1	$\overline{}$		-			8.503727	-	-
1	50	8.505045	8.505702	8,506358	8.507014	8.507668	8.512221	9,00
1	52	8.512867	8.513513	8.514157	8.514801	8.515444	8.516086	
1	53	8.516726	8.517366	8.518005	8.518643	8.519280	8.519916	7 6
1	54	8.520551	8,521186	8.521819	8.522451	8,523083	8.523713	5
1	55	8.524343	8.524972	8.525599	8,526226	8.526852	8 527477	4
1	56	8,528102	8.528725	8.529347	8.529969	8,530589	8.511209	H 16 18
1	57 58	8.531828	8.532446	8.533063	8.533079	8.534295	8.514909	3
1	59	8,535523	8.539794	8.536747	8.537358	8.537969	8.538578	10
1-	39	6011	-		8.541007	8.541612	8.541216	=
L		0011	50".	40"	30"	20"	10"	34

Co-sine 88 Degrees.

Tangent 1 Degree.

1 0" 10" 20" 30" 40"	5()#
0 8.241921 8.243126:8.244328.8.245526 5.246721 8.2	
1 8.249101 8.250287[8.251409]8.252048[5.253823]8.2	247913. 56
	254996 55
2 8.256165 8.25733118.258494-8.259654-8.230 11 8.2	261,03 5-
3 8.263115 8.204263 8.265408 8.20054 18.267688 8.2	208524 56
4 8.269950 8.271006 8.272213 5.273357 8.274458 8.2	275570 5.
5 8.276691 8.277604 3.27691318.280022 5.281124 5.20 8.233323 8.284414 8.285522 8.286002 8.287684 8.2	202225 54
0 \$.233323 \$.28441., \$.28551218.256002 \$.287684 \$.2	
7   8,289556   8,29393 (18,292312   8,29356) 6, 294457 6, 3 8   8,298202   8,297355(5,298416,3,294474) 8,30353 8,	
	101,83 51
3.35263, 8 1.3692 1.354727 0.355 10 8.356411 8.	<u> </u>
\$ 10 1 8.00360 at the continue tions 5 2110 0 8 21 color 8 .	314325 4.
11   8.3150.0   \$1.1160.50 317561 8.318695 8.31910008. 12   8.3214   31.3221778.523149 8.324128 8.325120 8.3	32311; 44
12   8.3211 3.,7221 - 7. 5.,231 - 9. 8.324128 8.324120 8.3	320121 4-
13   1.32*112   8   22112   1.329393   8.3330.50   8.331.004   8.3	332045 46
1 14 1 8 2.2 to 1 8 2.5 C.2 7 . 2 p. 77 - 2 . 2 y 5 9 8 2 2 0 y 2 1 8 3	33-17-12 45
# 15   Sigg8: 56   N 2 (19: 2)   1:34 778   141743 8 142701 8 3	3+34,7 4;
16   Sagabao   8.345 har refabra 22,1 34 12018 34 4 518.3	3+4348 ,
# #7   8 350 . Ya   E. 75 (229 in 352 (65) in 353 (4) (1) (1) (1)	234465 :-
■ 48 4 8 mm m S <sub>1</sub> = 1.8 mm 68mm (s <sub>1</sub> = 1.00 mm s <sub>2</sub> = 2.00 mm (s <sub>2</sub> = 1.00 mm s <sub>2</sub> = 1.00	0.612
19 8.361447 8.397345 8.3942 4 19.171 10.405. 1 / 14	325955
20 8.360 .94 8.36 99 8.365 - 01 .36 21 8.5 . 3.2	.71
21 8.372291 8 373184,8 374076 3.3740.18 37	5 7 7 8 38
■ 22   8.377622   8.578304 S.37938 (F.38039 T. N. S. 1445 N.	2.16 2"
24 8.38809 8.388953 8.3848.2 3.0000 8.341.26	; 3 . (y-3 1 - 3 )
25 8.393234 8 394085 8.39493395 8215 39564	19-1/2 3.1
24 8.38809* 8.3889538 384812 3 30670 8 301.26 5 25 8.393234 8 3940858839493 3 395782 5 39622 5 26 8.398315 8.399150 8.399090 5.400654 8 4 5 6 5 8	1 4 5 33
27 8 403338 8.404170 8.405000 8.405628.6 4 15-10	12 1 32
28 8 408204 8, 109126 8 4799461 41076 1 8.411 1 13 18.4	
30 8.418068 8.418872 8.419674 8.420475 6.421274 8.4	121572 29
31 8 422869 8.423664 8 42445 8 8 425250 8.420040 8.3	(2003) 25
32 8.427618 8.428464 8.424139 8.4299 3. 6.430, 55 8	171530 27
33 8.432315 8.433093 8 4338 0 4.434645 8 435419 8.4	
34 8.436,46 8.437,72 8.437,72 8.43,750 8.43,767 8.4445,31 8.447,30 8.444,30	11 -0-1 25
# #5   0-441500 0.142525;0-44504(0-44504)[0-44509[0-4	1453551 24
36	119806 23
37   8 450613   8.451359  5.452104  6.45284 - 19.453589  5.4	15 13 3 2 2 3
38 8.455070 8.455868 8.4654518.4572818.458016 8.4 39 8.454481 8.462212 8.48.401218.461670 8.482398 8.4	158-49 21
39 8.459481 8.46 1212 8.46.19 12 8.46 16 2 8.462398 8.4	1031-1
40 8.463749 8 40+57218.4652.15 8.406216 6.460736 8.4	14-455 10
41 8.468172 8.465829 8.4699 (4.8.470318 5.471031 8.4	471743; 18
42 8.4724.4 8.473163 8.47387 8 474579 8.475285 8.4 43 8.476603 8.47396 4700 7 8 478798 8.47528 8.4 43 8.476603 8.47396 4700 7 8 478798 8.476497 8.4	1,5990 17
43   8.476693   8.477396   478297   8.478798   8.479497   8.4	180194 16
44   nideo de luitardo de la continua del continua de la continua de la continua del continua de la continua del continua de la continua de la continua de la continua de la continua del continua de la continua del	1847 15
45   8.4850 (0   8 485) (0   3.4864 0   5.487 (15) (3.48789)   8.4	14, 126, 14
1 40 4 \$ 4501.5   \$150025   5040   5040   5050   4000   5060   6000   604	49 '37 a   13 i
47 8.493250 .49392" ".4040-228.205270 8.40592)	10-00-2 12
47 8.493250 (493927) (3.41502) 8.195270 8.44592) (3.47502) 8.49720 8.45730 8.499300 8.49936 (3.57196) 8.501208 (3.57196) 8.501228 (3.57196) 8.50128	5-2033 11
49 8.501298 5.55196: 3.532 125 1.33387 3.533945 4.5	(0.00%) 10
51 8:508302 8:308833[8:,10563] 8:311153 7:311832 8:3	\$ 12451
52 8.51309 8.713714 514380 518880 51567 8.5 53 8.516.61 8.71702 8.51804 18.7180 518880 51551 8.5 54 8.520700 8.7142 8.7223 8.7223 8.7220 5.7233 8.7230 6.723	7 (61501
53 8.516.61 8 117000 8.518241 3 51888018 51951-18 5	20154 6
54 8.520-90 8.511423 8 502250 5226 22 2.52 324 5.5	\$230,50 5
55 8.524586 N., 2, 215 5.525-42 N.5264 2 N.52-69 N.5	4 4
# &Q   1   8,8267.10   A.23407.21 % SAGNY 19 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	
1 57   8.622080   8.622606  5.623310.8.633933  6.63354.15 6	4331"H 2
1 58   8.535770   8.536392   1.537005   8.537616   6.5322   6.5	\$386.71 L
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d-i-l	10" M
60" 50" 40" 50" 20" 1	

O Degree. Co-tang. Co-sec Co-sine Tang. 0.000000 Infinite 6.463716 6.463726 13-536274 10.000000 12.516274 10.000000 6.764756 13.135244 10.000000 13.235244 10,000000 6.940847 13.059153 10.000000 13.059153 10.000000 7.065786 12.934214 10.000000 12.934214 10.000000 7.162696 12.837304 10.000000 12.837304 9.999990 7.241878 12.758122 10.000001 12.758123 12.934214 7.065786 7 24 1877 9.999999 7.36885 12.691175 10.000001 12.691176 9.999999 7.368817 12.633183 10.000001 12.633184 9.999999 7.417970 12.582030 10.000001 12.6833184 9.999998 7.463727 12.536273 10.000002 12.536274 2-308824 7 366816 7-417968 7-463726 9-99998 7-505120 12-494880 10-000002 12.494882 7-505118 9.999997 7.542909 [2.457091 [0.000003 [3.457094 9.999997 7.577672 [2.422]28 [0.000003 [2.422]3 7.541406 12 7.577663 13 9.999997 7.577672 12.422328 10.000003 12.3333 9.999996 7.699857 12.390143 10.000004 12.390147 9.999996 7.69820 12.360180 10.000004 12.360184 9.999995 7.69849 12.332151 10.000005 12.323155 9.999997 7.694179 12.305821 10.000005 12.323155 9.999994 7.719003 12.280997 10.000006 12.28103 7.609853 14 7.639816 15 2.667845 16 7.694173 17 18 7.718997 9.999993 7.742484 12.257516 10.000007 9.999993 7.764761 12.235239 10.000007 7-742478 12.257522 7-764754 9.999992 7.785951 12.214049 10.000008 12.214952 9.999991 7.806155 12.193845 10.000009 12.193854 9.999990 7.825460 12.174540 10.000010 12.174549 9.999989 7.845944 12.156056 10.000011 12.156066 7.785943 21 7.806146 22 7.825451 23 7.843934 9.999989 7-861674 12.138326 10.000011 12.150306 9.999988 7-861674 12.138326 10.000011 12.158338 9.999988 7-875708 12.121292 10.000012 12.1213105 9.999987 7-895099 12.104901 10.000013 12.104915 9.999986 7-910894 12.089106 10.000014 12.089121 9.999985 7-926134 12.073866 10.000015 12.073881 9.999983 7-940858 12.059142 10.000017 12.059158 7.861662 7.878695 7.895085 28 7-910879 7.926119 29 7.940842 9.999982 7.955100 12.044900 10.000018 12.044918 9.999981 7.958389 12.031111 10.000019 12.03130 9.999980 7.983253 12.017747 10.000020 12.017767 9.999977 7.995819 12.004781 10.000021 12.004801 9.999977 8.007809 11.992191 10.000023 13.99213 31 7.955082 7-968870 3= 7.982233 7.995198 8.007787 8 020021 9-999976 8.020045 11.979955 10.000024 11.97997 36 9.999975 8.031945 11.968055 10.0000025 11.968011 9.999973 8.043527 11.956473 10.000027 11.956499 9.999972 8.034809 11.945191 10.000028 11.945219 8.031919 18 8.043501 8.054781 39 9.99971 8.065806 11.934194 10.000029 11.93424 8.065776 8.076500 9.999969 8.076531 11.923469 10.000031 11.923500 9-999968 8.086997 11.913003 10.000031 11.91303 9-999968 8.097217 11.902783 10.000034 11.903817 9-999964 8.107202 11.892798 10.000036 11.892833 9-999963 8.116963 11.883037 10.000037 11.883074 8.086965 42 8.097183 8.107167 8.116926 8.126471 9-999961 8-126510 11.873490 10,000039 11.873529 9 999959 8.135851 11.864140 10.000041 11.864190 9 999958 8.144996 11.855004 10.000042 11.85647 9.999958 8.153952 11.846048 10.000044 11.84609 3 9.999954 8.162747 11.837273 10.000046 11.83731.6 8.135810 8.144953 8.153907 49 8.162681 8.171280 9 999952 8.171328 11 828672 10.000048 11.82872 9-999950 8-179763 11.820237 10.000050 11.820287 9-999948 8-188016 11.811964 10.000052 11.812015 8.179713 8.187984 53 9-999946 8.196156 11.803844 10.000054 11.803898 9-999944 8.204126 11.795874 10.000056 11.78805 9-999942 8.214641 11.788047 10.000058 11.78805 9-999940 8.214641 11.780359 10.000066 11.78041 8.146102 8.204070 8.211895 8.119581 8.227134 9.999938 8.227195 11.772805 10.000062 11.772866 58 8.234557 8.141855 9.999936 8 234621 11.765379 10.000064 11.765443 50 9.999934 8.241922 11.758578 10.000066 11.758145

Co tong Tang.

i Co-sine

Sine

				. 1	Degree.	5	A 10	
E	361	Sine	Co-sine.	Tang.	Co-tang	Secant	Co-sec.	I K
r	-	8.241855	-	8.241921	11 708070	10,000000	_	60
	1	8.249033	9,999934		11.758079	10.000068	11.758145	1000
ı	2	8.255004	9.999932		11,743835	10,000001	1 Tv743906	59
п	3	8.263042	9.999929	8.263115	11,736885	10.000071	17.736948	38
п	4	8.269881	THE REAL PROPERTY.		11,730044	10.000075	27.730110	55
п	5	8.276614	9.999925		11.723300	10.000078	11.7211E6	
ı	6	8.283243	9.999922		11.710077	10.000080	11.716747	55
ı		8.289773	September 1		11.710144	10.000082	11-710227	50
и	7	8.296207	9.999918		11,703708	10,000085	11.703793	53
н	9	8.302546	9.999915		11.697366	10,000087	11.697454	82
4	10	8.308794	9-991913	8.308884	The second second		11,691250	91
В			9.999910		11.691116	10,0000090	-	50
н	2.2	8.114954	9-999907	8.315046	11.684954	10,000093	11.685046	99
ı	12	8.321027	9.999905		11.678378	10,0000095	11.678973	48
ı	13	8.327016			11,672886	10,0000098	11.671984	47
ı		8.332924			11.666975	10 000101	11.667076	40
ı		8.338753			11.661144	10 000103	11.001247	45
1	16	8.344504	9.999894	8.344610	11.653390	10.000106	11.655496	44
1		8 350181		8.350289	11.649711	10.000109	11,649819	43
ı		8.355783		8.455895	11.644105	10,000112	11.644217	42
1		8.361315			11.638570	10.000115	11.638685	45
1	20	8.366777	9.999882	8 366895	11 633105	10,000118	11.633223	40
ı	21	8.372174	9.999879	8.272202	11.627708	10.000121	11.627820	39
ı	22	8.377499			11.622378	10.000124	11.622501	38
	23	8.382762			11.617111	10.000127	11.617238	37
п	24	8.387962	2000	The second second	11.611908	10.000130	11:612038	36
н	25	8.393101	9.999867		EI 606766	10.000133	11.606899	35
ı	26	8.198179	9 999864		11.601685	10,000136	12,601821	34
п	27	8.403199		8.403338	T4.596662	10:000130	11,546801	
ı	28	8 408161		8.408304	11.591696	10 000142	11,591839	33
ı	29	8.413068		8.413213	11.586787	10.000146	11.586932	
ı	-	8.417910		8.418068	11.581932	10.000149	11-582081	31
н				A PROPERTY.			-	30
п		8.412717	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	8.422869	11.577131	10.000152	17-577283	29
н	-	8.427462		8.427618	11,572382	10.000156	11.572538	28
н		8 432156		8.433315	11.567685	10,000159	11,507844	27
н		8,436800		8.436962	11.563038	10.000102	11.503500	26
и	35	8.441394	9.999834	8.441560	11 558440	10.000166	11 558606	25
п	36	8.445941	9 999831	8 446110	11.553890	10.000169	11.554059	24
п	37	8,450440	9.9998=7	8.450613	11.549387	10,000173	11.549560	23
п	38	8.454893	9 999824	8.455070	11-544930	10 000176	11.545107	22
ı	39	8.459301	9.999820	8,459481	11.540519	10.000180	11.540699	21
1	40	8 463665	9.999816	8 463849	11.536151	10.000184	11-536335	20
I	41	8.467985	9.999813	8.468172	11.531828	10.000187	11,532015	19
		8.472263	9.999809	8.472454	1 t. 527 546	10/000191	11-527737	18
1		8.476498	9.999805	8,476693	11.523307	10,000195	11.523502	17
ı		8.480693		8.480892	11.519108	10.000199	11,519307	16
		8 484848		8.485050	11.514050	10.000103	111515152	15
		8 488963		8.489170	11.510830	10.000208	11.511037	14
ı	47	8.493040	CONTRACTOR DE LA CONTRA	8.493250	11.506750	10 000210	11.506960	13
1	48	8.497078		8.497293	11,502707	10.000214	11.502922	12
1	49	8. (01080		8,501298	11.498702	10.000218	11.498920	111
ı	50	8.505045		8.505267	11.494733	10.000222	11.494955	10
ŀ	_			-		-		
ı		8.508974		8.509200	11,490800	10.000226	11.491026	9
			9-999769		11.486902	10.000231	11-487133	1
ı			9.999765				11.483274	6
					11 479210		11.479449	
		8,524343	9-999757	8.524586			11-475057	5
ı	56	8.528102	9-999753	8.528349	11.47 1651	10.000247	11.471898	(4)
1			a manufacture of	8,532080	11.467920		11.468172	3
1		8,535513		8.535779	11.464221	10.000256	11.454477	19
	59			8.539447	11.460553	10.000260	11.400814	(2)
1	60	K. 542819	9-999735	8,543084	11.456916	10.000265	11-457181	D
1	34	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant.	31
1				- 6	-	-		

2 Degrees

	U 0.00 2 10 10 10			Brook			-
8- M	1 Sine.	Co-sine.	Tang	Co-tang.	Secult .	Co-sec	. M .
	1	-		-	-		
0	8.542819	9-9997.35	E-543084	11.456916	10 000265	11/457181	60
1.0	8.545433	9.999731	8.546691	11.453309	10.000269	11,453578	59
12	8.540005	0.999726	W.550268	11.449731	10.000174	11 450005	58
3	8.551530	9.999722	8.553817	11.445183	10.000278	11.446461	57
	8.557054	9.999717	8,557336	11.443564	10 000283	11.441946	46
1 5			8.555828		10.000189	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	
1 5	8 560540	9.999713		11.439172	THE RESERVE OF THE PARTY OF THE	The second second	55
6	8,563999	9.999708	8.564291		10.000292	11.435001	54
7	8 507431	9.999704	8.567727	11.432273	10.000296	11.432569	93
3	8.570836	9.999699	8.571137	11.428863	10.000301	11.429164	52
9	8.574214	9.999694	8.574520	11-425480	10.000 106	FI 485786	51.
10	8.577 566		8.577877	11-422123	10.000311	F1.482434	50
		-		-	The second second	_	200
111	8.580892	9.999685	8.581208	11.415792	10.000315	11.419108	49
12	8.584193	9.999680	R 584514	11.415486	BD.000320	11.415807	48
113	8.587469	9-999675	8.587795	11.412205		11.412531	47
172	8.590721	9.999670	8.591051	11.408949	10.000330	11.409279	46
	0.590721		8.594283		10.000335	11.405052	
15	8.593948	9.999665	0.594203	11.405717			45
10	8.597152	9.999660	8.597492	11.402508		11.402848	44
17	8 600333	9.999555	8 600677	11.399323	10.000349	11.399668	45
18	8,603489	9 999550	8.603839	11.396161	10.000350	11.396514	42
19	8.606623		8.606978	11.393022	AND THE OWNER, WHEN THE	11.393377	100
20	8,009734	9.999640	8.610094	11.389906		11.390266	30
		-	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED I			NAME OF TAXABLE PARTY.	
21	8,612823	9.999635	8.613169	11.386811	10.000365	11,387177	39
22	8.615891	9.999629	8.616262	11.383738	10.000371	11.384109	38
23	8.618937	9.999624	8.619313	11.380687	10.000376	11.381063	37
24	8.621952		8.622343	11.377657	10.000181	11.378018	40
					10.000 186		20
75	8.624965	9.999614	8.625352	11.374648	the state of the state of	11.375055	35
26	8.627948		8.628340	11.371660	10.000392	11.372055	34
27	8.630911	9.999603	8.631308	11.368692	10.000397	11,369039	133
28	8.633854	9-999597	8.634256	11.365744	10.000403	11.300146	32
39	8 636776	9.999592	8 637184	11 362816	10.000408	11.363224	121
35	8,639680	9.999586	8.640093	11.359907	10.050414	FR. THO TED	1000
			THE RESERVE AND ADDRESS OF THE PERSON NAMED IN			-	30
31	8.642563	9.999381	8.642982	11.357018	10.000419	11.357437	20
33	8.645428	9.999575	8.645853	11.354147	10.000305	11.354572	28
33	2.648274	9.999570	8.648704	11.351796	10.000430	11.351726	27 6
34	8 651102	9.999564	8.651537	11.348463	10.000,136	11.348868	20.4
			86-13-57				_
35	8,653911	9-999558	8.654352	11.345648	10.000442	11.146089	.25
36	8,650702	9-999553	8.657149	11.342851	10.000447	11 343168	24
37	8.659475	9.999547	8.659928	11.340072	10.000453	11.340525	21
38	8.662230	9.999541	8.662689	11.337311	10.000459	11.337770	22
39	8.554958		8.665433	11.334567	10.000464	11.335032	200
27			8.668160		10.000471		25
40			-	11.33 (840	The second secon	11.332311	
41	8.670393		8.670870	11.329130	10 000476	11.329507	10
42		9 999518	8.673563	11.326437	10.000481	11.52beaD	15
43			8.676239	11.323761	10.000488	11.354244	17.
44	8.678405	9 999506	8 678900	11.321100	10 000494		10
	8.68:043		8 681				-
45		9.999500	8,681544	11.318456	10.000500	11.318957	站
46			8 684172	11.315828	10 000507	11.310335	218
47			8.686784	11.313216	10.000513	11.312728	13
48	8.688863	9.999481	8.689381	11.310619	10 200519	11.311137	12
10	White Street Street			11.308037	10.000515	11.308562	24
50				11.305471	10.000531	11-100/002	12
3-	manufacture and	The same of the last	-	-		-	-
54	8,696543	9.999463	6 697081	11.302919	10.000537	11/303457	9
52	8.699078	9.999456	8.599617	11.300383	10.000544	11.300917	8
53				11.297861		11.298411	191
	A STREET, SQUARE, SQUARE,					CONTRACTOR OF THE PARTY OF THE	6
54	200					11.295910	Sec.
55						11.193423	5
56			OR OTHER DESIGNATION OF THE PERSON OF THE PE			11.295951	4
57					10.000576	11.288493	3
58		9.999418			10.000582	11.286048	2
59				CONTRACTOR OF THE PARTY OF THE		11.283617	100
60	No. of Street,	ALCOHOLD DO NOT THE REAL PROPERTY.	CONTRACTOR OF STREET			11.281300	0
-					390		
M	Co-smg.	Sine.	Co-tang.	Tang '	Counce !	Secant	24
		-			-		

S Degrees.

M	Sine.	Co-sinc.	Ting	Co-tang	S		
					Secant.	Co-sec.	M
	9 2 2 2 2		<u>_</u>	<b>.</b>	10.60-591.		<del></del> -,
ĭ	9 713600	199404	8 - 24866	11.2.50054	10.000594	11.751203	6
					10.000602		54
-	0. 23545	9.999391	0.724204	11,275,90	12.035404	11 5.0. 505	)
					10.000616		57
					10.00623		ih
					10 000629		• -
6	8-727027	9-999304	3.73 300 3	11.2003;	13.600036	11 21 64-31	· ·
3	735354	9.99035?	× 73,4490	11 -64934	1.35 44	11.26 (11.5)	; .
	8.737067	9.996350	5 735317	11 3010,3	17,050640	11.3023.3	57
				11.259374		11.205.021	5:
10	8.7422,0	0.969736	1202	11.257075	and the	11.25 41	40
	3.714520	0.000 (23	8.743.07	11.254.93		11.25 (41.3	
	3 16802	0.000:22	8.717373	11 2:2:20	10 0 .01.	11.2	:
12	8.710055	0.000212	8.710710	11.27. 250	10.00% 3	27.22	
14	8.7512:,7				in theny		14
					. 7 3. (6,9		
							*
					and the second of		11
4/1	77955	9.997	6	11.2.13,1	13.000	: 1.24° ~~ ~ .	•
	0.700151	9-9972-19	175.06.5	11.036.53	10.00 /101	11.239 41	
9	0 7 2 3 6 7 6	9.1, 19272	3 .6	11 23191	10.000115		.; 1
			· · -	11.231-4		11 7354" 1	- ;
2 1	5.760675	9.99935	3. :67417	. 11.2325 -2	10.000-43	11.233;25	• 4
					10.0007;		,3
23	4.435425	9.999242	8.771727	11.218273	10.000155	1:.2297331	3 -
					10.000765		36
3;	8.775223	9.9.922	8.775995	11 224527	10,000,000	11.2241	33
20	8.777333	9.9.9220	8.7-8114	11.3218.0	10.000710	11.22206-	34
27	8 9434	9.999212	880222	11.21)8	10.000488	11.233,06	33
28	8.781524	4.999205	882320	11.217510	10.000795	11 215476.	32
					10.000805		31
					117000.0		30
				**	10.000019		
					10.555 26		24
, , .	2	9.9991		11.20 9	10.000\$34	11.210213	18
2.5	8 767850	0.0001.3		11.7	10.0001,4	11.2301.2	27.
34	0.793059	9.799155	5 - 0/ - 21	11.22,2299	10.000842	11.200151	
					10.00015		25
							24
					15.505% 0		23
					10.000%*4		22
					10.0005572		31
					10.000190	11.10:1.	27
41	8.557810	9.999124	\$ (1.6517)	وكنريين	10.05559	11.1921 1:	19
+2	P. 509777	9 4990 ).	** \$.106°(j)	1111/9317	10.000906		18
					10.000914		1 ~
					as shoyay		15
					15.000931		15
					10.000939		14
					10.000947		13
					16,000936		12
					15,500,64		iı
					15.000913		14
				• • •	13,000,01		<del></del> ,-
3.	8 82538	4.999019	5.32.5.4	11.1.23.0	10.500000	71 171111	ż
٠,	Q Q 200 400	0.000	3 8212.5	11.162222	10 000098	11.16.32	
5?	8 822600	0.004.0	A 2 - 26 -	11.166-5-	10.0000	11:67:20	i,
					10.731016		••
2).	9 B 26 20-1	9.890904	5 8 27 12 -	11.194525	19 2, 1034	11.16.22	•
50.	4 8 2 4 4 4 7	9.9949 0	9 (19 14 A	11.11.55	1034		.4
					13.551033.		;
ς:"					10.001042		
77	0.0 H24	7.94,505	S 42 . 45	11.157175	10 001030	1 S	4
e. ·	0.041.35.	9 99, 641;	* * * 17 jel	11 155356	15,291959	14.1	_ '
	C1-5111"		Cont. a.	Tang.	Caree	Secure,	· ::

			4	Degrees.			
M	Sine.	Co-sine	Tang.	Co-tang.	Secant.	Co-sec.	26
	-		_	-	10.00101		60
2	8.843585	9.998941	8.844644	11.155956	10.001059	10156415	THE REAL PROPERTY.
12	8.845387	9.998931	8 846455	11.153545	10.001068	11.154613	59
12	8.847183	9.998923	8,848160	11.151740	10.001077	11.152817	58
3	8,848971	9.998914	8.850057	11.149943	10.001086	11.151029	57
3	8.850751	9.998904	8.851846	11.148154	10.001095	11.149249	56
5	8.852525	9.998896	8.853628	11.146372	10.001104	11.147475	55
0	8.854291	9.998887	8,855403	FF. 144597	10.001113	11,145709	54
7	8.856049	9.998878	8 857171	11.142820	10.001122	11.143951	53
8	8.857801	9.998869	8.858932	11,141068	10.001131	11-142199	52
9	8.859546	9.998860	8.860686	11.139314	10.001140	11 140454	51
10	8.861283	9.998851	8.862433	11.137507	10.001149	11.138717	50
11	8.863014	9.998841	8.864173	11.135827	10,001159	11,136986	49
12	8.864738	9.998832	8.865906	11.134094	10.001168	11.135161	48
13	8.866455	9.998823	8.867632	11.132368	10.001177	21.133545	47
14	8.868165	9.998813	8.869351	11.130649	10.001187	11.111835	46
15	8.869868	9.998804	8 871064	11.128936	10.001196	11.130155	45
16	8.871565	9 998795	8.872775	11 127230	10.001205	FF 128415	44
17	8.873255	9.998785	8 874469	11.125531	10 001215	FE-126745	43
28	8.874938	9.998776	8.876162	11.123838	10.001224	11.125063	42
19	8.876615	9.998766	8.877849	11.122151	10.001234	11.113385	41
20	8.878285	9.998757	8.879529	11.120471	10.001243	11.121715	40
21	8.879949	9.998747	8.881202	11.118798	10,001253	11,100051	
22	8 881607	9.998738	B.882869	11-117131	10.001262	FE. T 1 S 2 0 3	38
23	3.883258	9.998728	8.884530	11-115470	10.001272	T1.116741	37
24	8 884903	9.998718	8 886185	11.111815	10 001282	11.615097	16
25	8.886542	9.998708	8.887833	11.112167	10.001202	MARKET STATE OF THE PARK OF TH	
26	8.888174	9.998699	8.889476	11.110524	10.001301	11.711826	35
27	8.889801	9.998689	8.891112	11.108888	10.001311	11.110190	34
28	8.891421	9.998670	8.891742	11.107258	10,001321	11.108579	33
20	8.893035	9.998669	8.894366	11.105634	10.001331	11.105965	32
30	8.894643	9.998659	8.805984	11.104016	10.001341	THE RESERVE OF THE PARTY OF THE	31
	A 40 4 5 TO	-		Tolerand.	-	11.105357	30
31	8.896246	9.998649	8.897596	11-102404	10.001351	11.101754	29
32	8.897842	9 498639	8.899203	11.100797	10.001361	11,102158	28
33	8.899432	9.998629	8.900803	11.099197	10.001371	11,100568	27
34	8.901017	9-998019	8,902398	11.097602	10.001381	11 008083	16
35	8,902596	9.998609	8.903987	11.096013	10 001391	11.097404	25
36	8.904169	9.998599	8.905570	11.094430	10.001401	11 095831	24
37	8.905736	9.998589	8,907147	11.092853	10.001411	11 094254	23
38	8.907297	9.998578	8.908719	11.091281	TO.001422	11.092703	22
39	8.908853	9.998568	8.910285	11.089715	10.001432	11.091147	2.0
40	8.910404	9.998558	8.911846	11.088154	10.001442	11.089596	225
41	8.911949	9-998548	8 913401	11.086599	10.001452	11,0880;1	19
42	8.913488	9 998537	8,914951	11.085049	10.001463	11,086412	18
43	8.915022	9.998527	8,916495	11.083505	10.001473	11.084978	17
44	8.916550	9.998516	8.918034	11.081966	10 001484	11.083450	10
45	8.918073	9.998506	8.919568	11.080432	10.001404	11.081927	15
46	8.919591		8.921006	11.078904	10.001505	11.080404	14
47	8.921103		8.922019	11.077381	10.001515	11.078897	11
48	8.922610		8.924136	11.075864	10.001526	11.077390	112
49	8.924112	9.998464	8 925649	11.074351	10.001536	11.074888	41
50	8.915609	9.998453	8.927156	11.072844	10.001547	11.074391	10
	0.000		-	-	No.	-	-
51	8.927100	9-998442	8.928658	11.071342	10,001558	11.072900	3
52				11.069845		11.071413	2
					10.001579		1
54	0.931544	9.998410	8.933134	11-066866	10.001590	11.068450	6
55	0-933015	9.998399	0 934616	11.065384	10 00 (601		5 4 3
	8.93448t	9-9983 8	8.436093	11.063407	10,001512	11.065519	(4)
57	3-935942	9-99-377		11.062435		11.064058	3
58		9.995300		11.060968	10 001634	11,062602	2
59	8 9333350	9-990355	940494	11.059506	10.001645	11.061150	1
_				11.058048	10.001656	11.059704	0
E	Comme.	Sine.	Co-tungs	Tang.	0-500	Secant	34
	-			Deserve		_	

_			5 1	Degrees.	100	700	100
100	Sine	Co-sine	Tang-	Co-tang.	Secant.	Co-sec.	M
	8.940196	9.998344	8 941952	11.058048	10,001656	11.059704	60
13	8.941738	9.998333	8.943404	11.056596	10.001667	11.058262	59
3	8.943174 8.944606	9.998322	8.944892	11.053705	10.0016%	11.056826	57
14	8.946024	9.998300	8 9477 14	11.052266	10.001700	11.053966	56
5	8.947456	9.998289	8.949168	11.050832	10.001711	11.052544	55
	8.948874	9.998277	8,950597	11,049403	10 001723	11.051126	54
7 8	8.950287	9.998255	8.953441	11.047979	10.001734	11.049713	52
9	8,953100	0.008243	8.954856	11,045144	10.001757	11.046900	51
10	8.954499	9.998232	8.956267	11.043713	10.001768	11,045501	50
11	8.955894	9.998210	8.957674	11.042320	10.001780	11.044106	49
12	8.957284		8,954075	11.040925	10.001791	11:042716	48
73	8.958670	9.998197	8.960473	11.039517	10.001803	11,041330	42
14	8.961429		8.961866 8.963255	11.035745	10.001814	11.039948	45
16	8.962801		8 964639	11,035361	10.001837	11.037199	44
17	8.964170	9.998151	8.966019	11.033981	10.001849	11.035830	43
18	8.965534		8.967304	11.031606	10.001861	11.034466	42 -
19	8.968893		8.968766	11,031234	10.001872	11.033107	41
31				Annual Control		11.031751	40
22	8.969600	9.998104	8 971496	11.018504	10.001896	11,020003	39
23	8.972289	DOMESTIC: US	8.974200	11.025791	10.001930	11.027711	37
24	8.973628	9.998068	8.975560	11.024440	10.001932	11.026375	36
25	8.974962		8.976906	11.013094	10.001944	11.025038	35
26	8 977619		8.978248	11.021752	10.001956	11.023707	34
28	8.978941		8,980921	11.019079	10.001980	11.021059	32
29	8.980259		8.982251	11.017749	10.001991	11.019741	31
30	8 981573	9.997996	8 983577	11.016423	10.001004	11.018427	30
31	8 982883	9-997984	8-984899	11.015101	10.001016	11.017117	29
32	8.984189		8.986217	11.013783	10.002028	11.015811	28
33	8.985491	MINISTER STATE OF	8.987532 8.988842	11.012468	10.002041	11.014509	27
34	8.988083		8.990149	11.009851	10.002065	11.011917	25
36	8.989374		8.991451	11.008549	10.002078	11.010626	24
37	8.990660	9.997910	8.992750	11.007250	10.002090	11.009340	23
38	8.991943		8,994045	11.005955	10.002103	11.008057	22
40	8 993222		8.995337 8.996624	11.004663	10.003115	11.005778	20
41	8.995768	-	-		10.002140	11,004232	19
42	8.997036		8.997908	11.0000912	10.002153	11.002964	18
43	8.998299	9.997835	9.000465	10.999535	10.002165	11.001701	17
44			9.001738	10.998252	10.002178	11.000440	16
45	9.600816		9.003007	10 996993	10.002191	10.999184	15
47	9.002069	Self-residence of the contract	9.004272	10.995728	10.002203	10.997931	13
48	9.004463	The second second	9.000792	10.993208	10.002229	10.995437	12
49	9.005805	9.997758	9.008047	10.991953	10.002141	10.994195	11
50	9.007044	9-997745	9.009298	10.990702	10.002255	10.992956	10
51	9.008278	9.997732		10.989454	10.002268	10.991722	9 8
52	9.009510	9.997719	9.011790	10.988210	CO. O. STATES OF	10.990490	
53	0.011061	9.997706	9.014368	10.985732	10.002307	10.988038	7 5
54 55 56 57 58		9.997680			10-002320	10,486818	5
56	9.014400	9.997667	9.016732	10.983268	10.002333	10.98 5600	4
57		9.997654		10.983041		10,984387	2
50	0.018031	9.997648	0.020403	10.980817	10.002359	10.983176	1
60	9 019234	9.997614		10.978380	10.002386	10.980765	0
N	Co-sinc.	Sine		Tung.	Co-sec.	Beeunt.	34
1	Car Calling		H. KHARAGA		-	-	-

3		-		- 61	Degrees.			
ľ	20	5me	Co-sine.	Tang	Co-tang.	Secunt .	Co-sec.	88
•	0	Q.GINETS.	9-997014	9.021620	10.978380	10.001386	10.980765	60
8	ĭ	9.020415	9.997601	9.022834	10 977 166	10,003344	10.979465	50
	2		9.997388	9.024044	10.975956	15,002412	10.978368	58
,	3	9.012815	9-997574	9.025251	10.974749	10.001426	10.977175	57
	4	9.024016	9-997561	9.036455	10.973545	10.002439	10.975984	56
	5	9.035303	9-997547	4.037644	10.972345	10.001453	10-974797	\$5
۰	6	9.026386	9/997534	9.028852	10.971148	10.002466	10.973614	54
ı	7	9.027567	9-997520	9 010046	10 969954	10.002480	10-072433	55
п	8	9.038744	9.997597	9.031237	10.968763	10.002493	10.971256	52
ı	9	9-029918	College College College	9-033435	10.967575	10.002507	10.970082	51
в	10	9.031089	9.997480	9.033009	10.966391	10.002520	10.068931	50
в	123	9.012257	9.997466	9.034791	10.955309	10.001514	10.967743	49
n	12	9.033411	9-997452	9.035949	10-964031	10.001548	10 966 179	48
в	13	9.014582	9-997439	9 037144	10.002856	10.002561	10.965415	47
ĸ	15	9-935741	9-9974=5	9.038316	10.961684	10.003575	10.964259	40
и	15	9.036896	and the second	9.039485	10.960515	10.001589	10,963104	45
1	16		9-997397	9.040051	10.959349	10.002603	10 001052	99
2	12	9.039197	9.997388	9.041813	10.958187	10.002617	10.960803	43
2	18	9-040342	INCOME.	9.042973	10.957017	10.002631	10.950658	#
	10	0.041485	9-997355	9.044130	10.955870	10,002645	10.058515	41
	_	9.041015	9.997341	9.045284	10.954710	10,002659	10.957375	40.
	21		9-997327	9.046434	10/953566	10.001673	10.956238	34
	2.0	9.044895	9-997513	9 047 588	10.952418	10.002687	10.955105	32
	23		9-997399	9-048727	10.951273	10.001701	10 953974	37
×	24	9-947154	MEDICALISATION	9-049869	10.950131	10.002715	10.952840	36
	2	9.048279	The second second	0.031008	10.948992	10.001719	10.961723	35 34
	2.7	0.050510	I THE PARTY OF THE	9.052144	10.947856	10.002743	10.949481	33
	28		9.997728	9.054407	10 945593	10.001772	10.448364	31
	24	0.052749		9,055535	10.044465	10 002786	100047858	11
н	30		9-997199	0.016650	10 943341	10.002801	10.046141	39
۰	31	9.054966	-		-	-		29
•	32	9.050071	THE REAL PROPERTY.		10,941100	10.002815	10,945034	28
۰	33		9-997170	9.060016	10,939984	10.002844	10.941939	27
2	34	9.058271		9.061110	10.958870	10.002850	10.941729	133
	35	0.050367	9.997147		10,957760	10.002873	10.940633	25
3	36	9.060460		9/063348	10.036652	10.001888	10.919540	
	37	9.061551		9.064453	10.035547	10.002902	10.938449	23
	38	9.002619	THE RESIDENCE OF	9.063536		10.002917	10.937201	21
	19	9.063724		9.000055	10.933349	10 002932	10.950076	21
8	40	9.064806	9 997053	9.067752	10.932248	10,002947	10.935194	20
в	43	9.065885	9.991039	9.068846	10.951154	10.002961	10-934415	10
	42	9.066961	9.997024	9.069938	10.930062	10,002976	10 933018	18
1	43	9.068036		9.071027	10.928973	10,002001	10.931954	17
	44	9.069107	9.996994	9.072113	10.917887	10.003006	10.930893	16
1	45	9.070176	9.996979	9.073197	10.926803	10.003021	10.929824	15
	46	9.071242	9.996964	9:074378	10.925722	10.003036	10,938752	14
	47	9.072306	9-996949		10.924644	10.003051	10-927044	13
1	48		Charles Tales &	S. C. Line	10.923568	10.003066	10.926634	12
1	49	9.074424	9.996919		10.922495	10.003081	10.925576	1.8
1	20	9.075480	9.996904	9 078576	10.921434	10.003096	10.924500	10
1	51	9.076533	9 996889	9.079644	10.920350	10.003111	10.913467	0.
1	52	9.077583	9.996874	9 0807 10	10,919390	10.003126	10.923417	8
1	53	9.078631	0.996858	9.081773	10.918227	10,003144	10-921309	3
	54				10.917167	10,003157	10,920324	
	55		9.996818		10.916109	10.003118	10,919281	5
J	50	9.081759	9.990812		10.915053	10.003188	10 918241	10
1	57	9.082797		9.086000	10.914000	10.003203	10,917203	3-
	59	9.083832	9.996782		10.012950	10.003218	10-916168	8
1	00	9:085894	9.996766	9.089144	10.011902	10.003234	10.915136	0
	M		9.996751	The second second	10.9 10856	10.003249	10.914106	_
7		Co-sine.	Sine.	Co-tang.	Tang/	Cu-sec-	Social.	21
		THE RESERVE TO SERVE THE PERSON NAMED IN	_	4000	STREET, SQUARE, SQUARE,			

7 Degrees.

	200.0		Mark Marks and Parks			
x Sine.	Co-sine.	Tang.	Co-Ling.	. Secant	Co-sec.	1-21-
0.0000804	a antice	o okozaa		10.003349	JOALALON	60
1 9 086922	0.000725	9.000187	10 000812	10.002265	10.912100	00
219.087947	0.006730	0.001228	10.008772	10.001380	10.913075	
210.088070	0.005774	0.002366	10.001714	10.002206	10.01.000	58
319.088970 419.089990	a water 8	0.002202	10 006608	10.002212	10.917030	57
	0.990077	0.004716	10.001664	10.003327	10:913010	
6 9.092024	0.000073	p.Da: 161	10 004622	100001111	10.900992	55
7 0 00101	9.995641	0.006106	10.902602	10.003359	10.907970	54
8 9.094047	9.990041	9.007425	10.003578	10.003339	10.900983	53
0.0000000	0.006610	0.008446	10.0031544	10.003390	10.903953	
9 9.095050	a policos	0-700458	10/00/21	10.003406	10.902933	51
						50
11 9.097065	9.996578	9-100487	10.899513	10.00 1422	10.002035	149
12 9.098066	9.995502	9-101504	10.598490	10.003438	10.901934	48
13 9.099065	9 990540	9.102519	10 897481	10.005454	10.400033	42
14 9.100002	9.000230	9-103532	10.890408	10 003470	ED.399938	46
15 9-101050	9 996514	9 124542	10/895458	10.003486	10.898944	45 1
	9-996498	9-105550	10.894450	10.003502	10.897952	44
17 9.103037	9-995482	9-100550	101893444	10.003518	10.896963	43
18 9.104015	9.996465	9-107559	10.892441	10.003535	10 895975	42
19 9.105010	9.496449	9-108500	10.801440	10 003551	10.893990	41
20 9.105992	9.996433	9 109559	10-800441	10.001567	10 804008	40
21 9.106973	9 996417	9-110556	10.889444	10.003583	10.801017	39
22 9.107951	0.006400	9-111551	10.888440	10.003600	10.803040	38
23 9 108927	0.006:84	9-112547	10.887457	10.003616	10 801072	37
24 9.100901	9.996168	9-113533	10.886467	10.003632	10 800000	26
25 9.110873	g.apotet	Q.TIACRE	10.83 (470	10.003640	10.880155	
				10.003665		35
27 9.112809	0.006218	0.116401	10.882100	10.003682	TO SECTION	35
28 9-113774	0.006200	9-117473	10.882528	10.003698	10 886 ++6	155
				10.003715		35
THE PERSON NAMED IN	0.005260	5.110020	10.880521	10.003731	10.88,203	31
						30
31 9-116056	9.996252	9-120404	10.879590	10.003748	10.888344	29
32 9.117613	9.996235	9-121377	10.878623	10.003764	10.882387	28
33 9.128567	9.996219	4.122348	10.877652	10.003781	10.881433	27
34 9.119519	9.996202	9-123317	10.876683	10.0037.98	10.180481	20
35 9-120409	9.996185	9-124284	10.875716	10 003815	FD.879524	25
36 9-121417	9.996168	9-125249	10.874751	10.003832	10 878583	24
37 9.122362	0.006151	126211	10.873789	10.003849	10.877638	23
38 9 223306	9-996184	1.127172	10.872828	10.003866	10.876694	22
39 9.124248	9.996117 9	128130	15.871870	10.003883	10.875752	21
40 9.129187	9 996100	9.129087	10.870913	10 003900	10.874813	20
	9.90558:	2-130041	10.869959	10.003917	10.872826	19
				10.003934		18
43 9-127993	0.000048	1-131044	10.868046	10.003054	10.872007	17
44 9.128925						16
45 9.129854	0.006012	1.23820	10.866161	10.003985	10.8701-6	
46 9 130781	ADSTOR !	1.124784	10.864216	10.004003	ID 860210	28
47 9 131706	0.00 (0.50	1175716	10.864274	10.004030	10.86820	_
48 9.132630	0.000	4.45667	10 867777	10.004047	10.807.77	13
49 9 133551 9	7939-313	127600	10.863345	10.004024	10.266	12
colo 124450	005075	1.128547	10.861.44	10.004071	10.865530	
GD 9-1 34470 5	332344	3,34	700	12.00	7 04	10
50 9.155687 9	1.993921 5	1-139470	10.000534	10.004089	10.884613	- 9
50 9.136303 9	995894 9	+140409	10,859591	10.001106	IC. 863647	8
53 9-157216 5	995876 9	141340	10,858000	10.004124	10.862784	7
54 9.158128	9.995859 9	1.143204	10.857731	10.004141	10.861872	6.3
CE QUITADET S	1.995841	1143140	10 850804	10.004159	10.860g63	15
56 9-139944 5	995823 9	1.144121	50.855874	10.004176	10.8600 46	100
57 9 1408 50 9	995806 9	1.145044	10.854956	10.004194	10.869160	4
e8 0.141724 C	0.005788	1-145966	10.8 (4014)	10.004212	10.848946	19
CO 9. 641544 0	0.005771	1-146885	10.853115	10.004220	10.857345	100
60 9.143555	1.945753	9-147803	10.852197	10/004247	10.840.245	33
a Co-sine		Cotang.	Tang	Co-sec.	SCEANE	16
	The Late of the La	100000			The state of the s	-

-		0.1	D	Degrees.			
1005	bine.	Co-sine.	Tang-	1 Co-tang	. Scennt.	Co-sec.	1 35
100	9-143555	9.995753	9.14780	10.85210	7 10.004247	10.856445	60
113			9.14871	10.85128			59
1 2	S SHIP SHAPE	O RESIDENCE PROPERTY OF	9.14963	THE PARTY NAMED IN			58
1 3	The second secon	I MANUAL TO STATE OF	9-15054	THE RESERVE OF THE PERSON NAMED IN			57
11.4	Mary Contract	A PROPERTY AND A SECOND	9.15145		10.004314		
5	The Contract		9.15236	10.84763	10.004336	10.851974	55
6		9.995646	9.153260	10.84673	10.004354		54
7	9 149802	9.995628	9.15417	10.845826	10.00437	10.850198	53
8			9-15507	10.84492	10.004390		52
1 9	9 151569	9.995591	9.155971				51
10	9-152451	9-995573	9.156877	10.84312	10.004427	10.847549	50
11	9.153339	9.995555	9-15777	10.84222	10.00444	10.846670	49
12	A COLUMN TO SERVICE A		9-15867		10.004463		15
12.3	1		9.15956	10.84043	10.004481	10.844917	47
14	A CONTRACTOR OF THE PARTY OF TH		9.16045	10.83954	10.004499		45
15	9.156830	9.995482	9.161347	10.838653	10-004518	10.843170	48
16	9.157700	9.995464	9.162236			10.842300	44
127					A STREET, SQUARE, SQUARE,		43
18	I Downson Annual				A DESCRIPTION OF THE PARTY OF T	THE WATER STATE OF	44
19		9.995409	9.164892				41
20	9 161164	9-995390	9.165774		-	Section 1981	40
21	9-161015	9.995372	9.166654	10.833346	10.004628	10.837975	39
22	9.161885	9.995353	9.167532			10.837115	18
23	9 163743	9.995334	9.168409	10.831591	10.001666		32
24	9.164600	9.995316	9.169284	10.830716	10.004684	10.835400	36
25	9,165454	9.995297	9-170157			10.834546	35
20	9 166307	9.995278	9.171029			10.833693	34
27	9.167159	9.995260	9-171899		THE RESIDENCE OF THE PARTY OF T	10.852841	33
28	9 168008	ALC: UNKNOWN				10.831991	31
29	9.168856	9.995222	9.173634			10.831144	31
30	9-109701	9-995203	9-174499	10.825501	10.004797	10.830298	39
31	9-170547	9.995184	9 175362	10 824638	10.004816	10.829453	29
32	9.171389	9.995165			10.004835	10.828611	28
33	9.172230	9.995146			10.004854	10 827770	27
34	9.173070	9.995127	9.177942	10.822058	10.004873	10.826930	26
35	9.173908	9.995108		10.821201		10.826092	25
36	9-174744	9.995089		10.820345		10.825256	24
37	9.175578	9.995070				10.824421	23
38	9.176411	9.995051				10.823589	23
39	9.177242	9.995032		10.817789	DESCRIPTION OF THE PARTY OF THE	10 822758	21
40	9.178072	9-995013	9.183059	10.816941	10,004987	10.821928	20
41	9.178900	9-994993	9.183907	10.816093	10.005007	10.821100	19
42	9.179726	9-994974		10.815248	10 005026	10.820274	18
43	9.180551	9-994955	9.185597	10.814403	10,005045	10.819449	17
		9-994935		10.813561	10,005065	10.818016	16
		9.994916		10.812720	10.005084	10.817804	13
		9.994896		10.811880	10.005104	10.816984	14
		9.994877		10.811042	10.005123	10.816166	13
		9.994857		10.810206	10,005143	10.815349	12
1000000		9.994838		10.809371	10.005162	10.814534	3.0
	and the second	9.99481819	-	10.808538	10.005182	10.813720	10
		9.994798 9		10.807706	10.005202	10.812908	9
52	9.187903	9 994779 9	-193124	10.806876	10.005221		8
53	9.188712	9-9947 9 9	193953	10.800047	10.005241	10.811258	7
54	189519	9-9947 19 9	194780	10.805220	10.005261	10.810481	6
55 5	0.190325	9.994710 9	195606	10.804394	10.00 (281	10.809675	
50 5	191130	9-994700 9	.190430	10 803570	10.005300	10.808870	10 mm
57 5	191933	9.994680 9	197253	10.802747	10.005320	10.808067	31
50 5	102-34	9.994000 9	198074	10.801926	10.005340		
60 0	193334	0.004670	190894	10.801106	10.005360	10.805455	1
				10.800187	The second second	10.805668	0
M 1	o sine.	Sine (	o-tagg	Tang	Co sec.	ecant.	M"
	-	Value of the last	811	Degrees.			-

9 Degrees.

•			9_	Degrees.			
IN	Sine.	Co-sine	l'ang.	Co-tang	Secant.	Co-sec.	М
0	0.101222	0.00162	2 9.19971	3 10.50028	7 10.005 280	10.85068	03
li	0.105120	u.u.,1460	0 9.200 52	10.7994	10 00 1400	10.804871	59
1 2	0.145425	9.99458	019.20134	5,10.74865	10.005420	10.804574	53
3	0.196714	4.944.6	019.202150	10 -9-84	10.005440	10.803281	; ;-
14	19.197511		0   9, 20297	1,10.797024	10.00546	10.852489	50
5	9.198302	9.44451	y y 20378:	2 <sup>i</sup> 10.79 <b>62</b> 18	10.005481	10.801648	. 55
6	100001	4.994499	9 9. 20459	t! 10.795408	10.005501	10.800909	5.4
1 7	9.199879	9-994479	9.20,450	0 10.794600	10.005521	10.800121	1 53
8	9.200666	9-994459	9,9.206237	10.793793	10.005541	10.799534	1 52
9	9.201451	9.994438	9.207013	10.792987	10.005562	10.798549	51
10	9.202234	9.994418	9.207817	10.792183	10.005582	10.797760	50
11	9.203017	9.994398	9.208619	10.791381	10.005602	10.796983	49
112	9.203797	9.994377	19.209420	10.790580	10 005623	10.796203	48
13	9.204577	9-994357	7 9.210220	10 789780	,,10.33,643	10.795423	
114	9.205354.	9.994336	9.211018	10.788983	10.005664	10.794640	46
15				10.788185			45
16				:10.787389			44
17	9.207679;	9-994274	9.213405	:10.786595	10.005726	10.792321	43
18				10 78 5802			
19	9.209222	9.994233	19 214989	10.785011	13.005767		41
25				10.784220		10.790008	42
21	9.216760	9.994191	19.216568	10.783432	13.035839	10.789240	39
22	9.211526	9.994171	9.217356	10.782644	10.005829	10.788474	38
23	9.212291	9-994150	9.218142	10 781858	10 00 58 50	10.787709	
24				10.781074			36
25				10.780290			35
26 27	9.214579	y 99400. n nn 1066	0.220492	10.779508	10.005913	10.781667	34
28	9.216097			10.777948	10.005934	10.784002	33
20				10.777170			32 31
30				10.7-6393			30
	,						
-				10.775618			29
I-				10.774071		10.780132	2S 27
				10.773330		10.779382	26
35				10.772529		10.778633	25
				10.771761		10.777885	24
37	9.222861				10 006146	10 777139	23
38	9.223606 9	1.993832	9.229773	10.770227	10.006168	10.776394	22
39	9.224349	9.993811	9.230539	13.769461	10.006189	10.775651	21
40	9.225092	).993789	.9.231302	10.708698	10.006211	10.774408	20
41				10.767935		10.774167	19
<b>42</b>	9.226573	.993746	9.232826	19.767174	10.006251	10.773427	18
	9.227311	1.993725	9.233586	10.766414	10.006275	10.77.2689	17
44	9.228048	993703	9-234345	10.765655	10.006297	10.771952	16
45	9.228784 9	9.99 :68 1	9.235103	10.764897	10.006319	10.771216	15
46	9.229518	J.yy3660	9.235859	10.764141	10.006340	10 770482	14
47	9.230252	.993638	9.236614	10.763386	10.006362	10.769748	13
48	9.230984 9	.993616	9-237368	10.762632	10.006384	10.769016	12
49	9.231715	993594	9.238120	10.761880	10.006406	10 768285	11
50				10.761128		10.767556	10
51				10.760378		10.766828	9
52	9.233899.9	.993528	9.240371	10.759629	10.006472	10.766101	8
53	9.234625 9	.993526	9.241118	10.758882	10,006494	10.765375	7
				10.758135			6
55 !	9.236073 9	.993462	9.212010	10.757390	10.006538	10.703927	5
55	9.230795 9	.993440	9-243354	10.756646	10.000 500	10.703205	+
				10.755903		10.762475	3 2
, o				10.755101		10.761047	î
	9.239670 g	.uo2261	0.216210	10.753681	10.0066	10.760330	6
							<u>~</u> (
И.	Co sine.	Sine.	· -tang	Tang.	Co-sec.	secint	

10 Degrees.

8	_				or Breeze		_	-
П	34	Sine.	Co-sine.	Tang.	Co-tang-	Secunt.	Co-sec.	M
ı	0	0.270670	9.993351	0.246310	10.753681	10.006640	10,760330	00
ı	1				10.752943			59
ı								58
ı	4	9.241101	9.993397	9-447794	10.752206	10.000093	10.758099	
ı	3	9.241014	9.993205	9.440530	10.751470	10,000715	10.750100	57
ı	4				10.730736			36
ı	5	9.243237			101750002			55
ı	6	9.243947			10 749270			54
ı	70	9.244656	9.993195	9.251461	10.748539	10 006805	10.755344	53
ı	3	9.245363	9.993173	9.252191	10.747809	10.006818	10.754637	52
ı	9				10-747080	10.006851	10.753931	51
	10		9.993127				10.753125	10
ı				-	-		-	
ı	II	9.247478	9.993104	9-254374	10.745626		10.752522	49
۱	12	9-248181	19.993081	9.255100	10.744900		10.751819	48
ı	13	9.248883	9.993059	9.255824	10-744170	10.005941	10.751117	47
٨	14	9.249583	9.993036	9.256547	10 743453	10.006964	10.750417	45
	251	9.240182	9.993013	9-257269	10-742731		10.749718	45
ı	100				10.742010			44
ı	LY.	9.251677	9.992967		10.741290		10.748313	41
	:8:	9.252373	9-992944				10.747627	41
	19	9.151067					10.745933	41
	19	0.75556	9.992898			10.007079	10.746220	
1		9-253761		THE REAL PROPERTY.	-		-	40
1	21	9.254453	9 992875	9.261578	10.738422	10,007129	10.745547	39
ı	42	9.355144	0.992852	9.263292	10:737708	10.007148	10.744856	32
B	43	9 255834	9.992829	9.263005	10.736995	10.007171		37
n	=4	19.356523	9.992806	9.263717	10.736283			30
R		9.247211		9.254428			10.742780	35
	36	9-257898	0.003750	9.265138			The second second second	30
u	37	9-257090	9 99=739					27
6		9.258583	9,992730	9.265847		10.007264	10.741419	33
ı	28	9.259268		9.266555		10.007387	The second second second	32
ı	20	9.259951	9.992090			10.007311		91
ĸ	10	9.260633	9.992866	9 267967	10:732633	10 007334	10.739367	30
R	31	9-261314	9 992643	9.268671		10.007357	10.738686	29
,	32	9.201994						28
8	13	9.202673		9.270077				27
ı						10.007404		26
ı	3+	9.263351			10.729221			
В	35	9.264027			10.728521			25
2	36	9.264703	A CONTRACTOR OF THE PARTY OF TH					24
N	37	9.265377	9.992501	9-27 2876	10.727124	10.007499	10.734613	73
N	38	9.266051	9.992478	9.273573	10.726427	10.007522	10.733949	22
ĸ	39	9.265723	9.992454	9.274269	10-725731	10,007546	10.733277	2.0
ø	40	9 267395				10.007570	10.732605	20
1	41	9.268065	9-992406	The state of the state of		-		1000
		9.268734		Section 2 Section 2			10.731935	19
	13		9.992382	Comment of the Comment	10-723649			38
	43	9.269402			10.722957			17
	44		9.992335		10.722266			1.6
	49	9.270735			10.721576	10,007689	10,729265	15
1	46	9.271400		9-279113	10.720887		10,728600	14
1	47	9.272064	9.992263		10.720199		10.737936	13
1	48		9.992239		10/719512			12
	49		9.992214	9.281174	10.718826	10,000984	10.716612	14
1	50	9-274049		9.281853	10.718142		10.725951	to
							-	-
	50	9-274708		Carlot and the same			10.725292	9
	52		9.992142	9.283225	10.716775	10 007858	10.724633	18
	53		9.992118		10.716093	10.007881	10.723975	7
	54	9.276681	9.992093	9.284588	10.715412	10,007907	10.721110	7 6
	55	9.277337	9.992069	9.285268	10.714732	10,007021	10.72166	- 5
	56		9.992044		10,714050			4
	57				10.713376			100
1	53		9.991996			10.008004		3
1					THE RESERVE OF THE PARTY OF THE			
1	59		9.991971	0 -996		10.008029		2
	70		9-991947	9.288652		10.008053	10.719401	0
1	DE.	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant	M
n	-	_	of the Parcel of the Parcel of	_		-	-	

11 Degrees.

			11	Degrees.			
M	Sine.	Co-sine.	Tang.	Co-tang	Secant	Co-sec.	N
-	9.282599	0.001 17	0.288652	10.711348	13.008053	10.719401	60
		0.991922	9.289326	10.710674	10.008078		59
2	0.281847	9 991897	9.289999	10.710001	10.008103		
21	0.282544	9.091873	9.290671	10.709324	10.008137		57
4	9.283193	9.991848	9.291342	10.708658	10.008152		
5	9.283836	9.991823	9.292013	10.707987	10.008177	10.716164	55
6	9.284480	9.991799	9.292682	10.707318	10.008201	10.715520	54
7	9.285124	9.991774	9.293350	10.736650	10.008216		53
ક		. 9-99 1749.			10.008251		52
9	9-580408	9.991724	9.294684	10.705316	10.008276	10.713592	51
_10	9.287048	9.991099	9.245349	10.704651	10.009 ;01:		50
		9.991674			10.005326	10.712312	49
		9.991649			10.008351		
		9.991624.			10.008376		
					10.008401		46
		9.991574			10.008426.		
		9.991549.			10.008451:		
17	0.202127	2.33.3-4	a 100628	10.50020	10.008502:	10.707860	43 42
					10.008527		41
20	9.293399	9.991418	9.301951	10.698049	10.008552	10.706601	40
					13.058578		_
22	9.2916 (8	(4.991707	9.301261	10.606730	10.008603	10.70:242	39
					10.008628		
	9.295913	9.991346	9.304567	. 10.695433	10.008654	10.704087	36
25	9.296539	9.991321	9.305218	10.694782	10.008679	10.703461	35
	9.297164	9.991295	9.305869	10.694131	10.0087051	10.702836	34
					10.008730.		33
28	9.298412	9.991244.	9.307168	10.692832	10.008756	10.701588	32
29	9.299034	9.491218	9.307815	10.092185	10 008782, 10.008807	10.700966	31
							_30_
					10.008833		29
32	9.300895	9.991141	9.309754	10.093246	10 008859	10.699105	28
					10.008885		27
34	9.302132	9.991090	9.311042	10.000950	10.00%936 10.00%910.	10.697868	25
32	0.202264	0.0012:3	0.312.37	10 687672	10.008962!	10.09, 252	25 24
27	0.707070	0.001012	0.212067	10.687322	10.008988	10.606031	23
38	0.101101	9.940486	0. 31 3608	10.686392	10.009014	10.60 (10-	22
39	9.305207	9 999960	9.314247	10.685753	10.009040	10.694793	21
					10.009066:		20
					10.009392		19
					10.009118		18
					10.009145		17
44	9.308259	9.990829	9.317430	10.682570	10.0091711	10.691741	16
45	9.308867	9.995853.	9.318064	10.621936	10.000107	10.691133	15
46	9.309474	9-99C777	9.318697	10.681303	10.009223	10.690526	14
47	9.310085	9.990750	9.319329	10.680671	10.009150	10.689920	13
48	9.310085	9.990724	9.319901	10.030033	10.009176	10.089315	13
49	9.311289	9.990097	9 320592	10.079403	10.009305,	12 688 12-	11
					10.309329		
51	9.312495	9.9906.15	9.321851	10.678149	10.009355	10 687505	9
52	9.3:3097	9.993018	9.322479	10.077521	10.009382	10.0869031	8
53	y. 513098	9.990591	9.323100	10.0,0094	10.009409	10.68	6
24	0.21480~	0.000c22:	0 22422	10.67:642	10.009435	10.68 - 10.2	5
2)	7.3.40%/	2.3300411	0.324082	10.674017	10.009489	10.681602	4
57	9.316002	0.000185	0.324607	10.674302	10.000212,	10.687008	3
58	9.316680	9.990458	9.326271	10.67 1760	10.009542	10 683311	2
59	9.317284	9.990431	9.326853	10.673147	10.0095691	10.682716	
60	9.317879	9.990404	9.327475	10.672525	10.009 596	10.682121	0
٠.	Co-sine.	Sine.	Co-tang.	Lare.	CO-SEC. I	Secunt.	, ",

-			12	Degrees.	1		
, M	Sine	Co-sine	Tang.	Co-tang.	Secant-	Co-sec.	16
10	9.317879	9-990404	9.327474	10.672526	10,009396	10.682121	fo
1					10.009622		59
3					10.009649		58
4					10.009703		56
5	9.520840	9.990270	9.330570	10.669430	10,009730	10.679160	55
7	9.321430				10.009757		54
8	9.322607	9.990188			10.000812		53
9	9-323194	9.990161	9.333033		10.009839		.51
10	233	-	-	10.666354			30
11	200	13 3 3		10.665741		10,675634	49
13	Manager Street			10.665129		10.674466	48
14	A CONTRACTOR OF THE PARTY OF	9.990025		10-663907		10.673883	45
15		The second second		10.663298		10.673300	45
10	17 18 11 10 10	9.989970		10.662689		A CONTRACTOR OF THE PARTY OF TH	44
18	1000			10.661473		10.671558	1
19	A SACRAGO AND AND AND ASSESSMENT	The second second		10.660867		10.670979	ar.
20	-	-		10,660261	-	10.670401	40
21	No. of Contract of	1		10.659656	The second secon	10.669814	30
23	I be be be distributed to			10.658448		10.663671	18
24	TO THE RESERVE	CORPORATION AND ADDRESS OF THE PARTY NAMED IN COLUMN ASSESSMENT AND ADDRESS OF THE PARTY NAMED ASSESSMENT ASSESSMENT AND ADDRESS OF THE PARTY NAMED ASSESSMENT ASSESSMENT ASSE		10.657845		10.068097	10
25	Control of the last	The state of the s		10.657243	10.010279	10.667521	35
20	100000	I Indiana Salata and		10.656643		10.666376	34
28	AND THE REAL PROPERTY.	The state of the state of	C C SCACA	10.655441	The contract of the contract o	10 665805	32
29		9.989610	SAME OF THE PARTY OF	10.654843	23	10.665133	31
30		9 989582	9.345755	10.654245	10.010418	10.664663	30
31	PERSONAL PROPERTY.	I SHOW THEFT	9-346353	10.053647	10.010447	10.661094	25
32	9.337045		The second second	10.653051	10.010475	10.662957	27
34	9.337610	9.989469	9-348141	10.651859	10.010531	10.662390	10
35	A COUNTY OF THE PARTY OF THE PA	Technology of the latest to	SOMEON STATE OF THE PARTY OF TH	10.651265		10.661834	35
36	THE RESIDENCE OF THE PARTY OF T	9.989413	9-349319	10.650671	10.010587	10.660601	24
38		9.989356	9 350514	10.649486	10.010644	10.000119	1
39		9.989328	9.351106		10 010672	10.659566	21
40	The second second	-	9.351697	10.648303	10.010700	10.659004	20
41	9.341558	9.989271	9.352287	10.647713	10.010729	10.658442	18
43	9.342679	9-989214	9.353465	10.646535	10.010786	10.657321	17
44	9.343239	9.989186	9.354053	10.645947	10.013814	10.656761	10
45	9.343797	9.989157		10.645360	10.010843	10.656203	15
46	9.344355			10.644773	10.010872	10.655645	14
48	9.345469	9.989071	9.356398	10.643602	10.010929	10.654531	12
				10.643018		10.653976	11
50	Section 201	- 00 0	-	10.642434		10.653411	10
51	9-147134	9.988985	9.358140	10 641851	10.011015	10.651866	9
53	9-346240	9.988927	9.359313	10.640687	10,011073	10.651760	7
54	9:348792	9.988898	9.359893	10.640197	10.011102	10.0 (1208	6
55	9-349343	9.988869	9.360474	10.039526	10.011131	10.050657	5
57	9.349093	9.988811	9.361632	10.678+68	10.011160	10.64nce=	4
58	9.350992	9.988782	9.362210	10.637100	10.011218	10.6400081	3 2
59	9-351540	9.988753	9.362787	10.637213	10.0:1247	10.648460	1
	Co-sine		Co-tang.	Tang.	Co-sec.	Secant.	D M

13 Degrees.

Sine   Co-sine   Tang   Co-tang   Secant   Co-sine   1   9.352038   9.8521   3.65364   10.63665   10.011270   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   10.647501   0   0   10.647501   0   0   10.647501   0   0   10.647501   0   0   10.647501   0   0   10.647501   0   0   10.647501   0   0   0   0   0   0   0   0   0				TO	Derres.			
0 9352088	М	Sine.	Co-sine.	Tang.	Co-tang.	, Secant.	Co-sec.	. 1
1 9.353513	<u> </u>	0.2.2388	0.685-21	- <del></del>	10 0:60:6	10 011276	10 017012	D:-
2 9.353151 9.3805036529 10.634910 10.011361 10.646274 57 3 9.35327 9.3805036529 10.634910 10.011361 10.646274 57 3 9.35327 9.3805036529 10.63261 10.011361 10.046727, 57 5 9.35451 9.3856736627 11.633190 10.011451 10.043757 57 6 9.35591 9.38584 9.36361 10.632618 10.011461 10.04359 57 6 9.35694 9.38540 9.36834 10.632618 10.011461 10.04359 57 7 9.35592 9.38540 9.36834 10.632618 10.011461 10.04359 57 10 9.357524 9.38540 9.36834 10.632618 10.011540 10.04359 57 11 9.357524 9.38540 9.36963 10.63263 10.0111540 10.04359 57 12 9.35803 9.38541 9.36963 10.623768 10.011540 10.04359 57 13 9.35044 9.38542 9.371367 10.624633 10.621638 10.011649 10.04439 57 13 9.35914 9.38532 9.371367 10.624633 10.6011649 10.04439 57 14 9.35603 9.3852 9.371367 10.624633 10.011649 10.04439 57 15 9.360215 9.38522 9.371367 10.624633 10.011649 10.04439 57 16 9.360215 9.38522 9.371367 10.624633 10.01177 10.643978 54 16 9.360215 9.38532 9.371367 10.624633 10.01177 10.639785 47 18 9.36184 9.98513 9.37369 10.62267 10.011718 10.639785 47 18 9.36184 9.98513 9.37369 10.62267 10.011718 10.63978 42 19 9.36184 9.98513 9.37369 10.62267 10.01177 10.63578 42 19 9.36184 9.98513 9.37369 10.62267 10.01187 10.63578 42 19 9.36184 9.98513 9.37369 10.62267 10.01187 10.63578 42 19 9.36184 9.98513 9.37369 10.62267 10.01187 10.635764 41 10 9.36234 9.98513 9.3739 10.62267 10.01187 10.63576 41 11 9.36242 9.98513 9.37519 10.62267 10.01197 10.63551 3 10 9.36184 9.98513 9.37519 10.62267 10.01197 10.63551 3 10 9.36184 9.98513 9.37519 10.62267 10.01197 10.63551 3 10 9.36184 9.98513 9.37519 10.62267 10.01197 10.63326 3 10 9.36184 9.98513 9.37519 10.62231 10.01228 10.63280 3 10 9.36184 9.98513 9.37519 10.62231 10.01228 10.63280 3 10 9.36184 9.98513 9.37519 10.62231 10.01228 10.63230 3 10 9.36184 9.98513 9.38513 10.62279 10.01229 10.01229 10.03231 10.62261 10.01228 10.63230 3 10 9.36184 9.98513 9.38513 10.62266 10.01229 10.62271 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267 10.62267	•							•
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17    9,361287   9,98822;   9,373624   10,628936   10,011777   10,638713   43   43   9,361821   9,88163   9,374195   10,621857   10,011857   10,637644   41   10,361821   9,98863   9,88133   9,374195   10,621821   10,011867   10,646778   39   9,361942   9,988033   9,37432   10,62244   10,011867   10,646778   39   361943   9,988033   9,37442   10,62397   10,01195   10,63696   38   23   9,36445   9,488623   9,37442   10,62397   10,01195   10,634634   36   37   37   37   37   37   37   37								
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19 9,362350 9,988103,9,57419 12.62284 12.01867 1637111 42. 20 9,36342 9,988103,9,37437 11.62244 10.011867 1637111 42. 21 9,36342 9,988103,9,37531 1624481 10.011937 12.636046 38 23 9,364485 9.88243 9.376442 12.652358 10.011937 12.636046 38 24 9.365216 9.98733 9.37531 12.622437 10.011937 12.636046 38 24 9.365216 9.98793 9.378122 12.622437 10.012047 12.634344 36 22 9.366576 9.98793 9.378122 12.622437 10.012047 12.634343 36 22 9.366576 9.98793 9.378322 12.622437 10.012047 12.634343 36 22 9.366076 9.98793 9.378322 12.622437 12.02047 12.632869 32 9.366076 9.98793 9.379797 12.622437 12.0212047 12.632869 32 9.366076 9.98793 9.379797 12.622076 12.021208 12.632396 33 30 9.368185 9.98732 9.379797 12.622076 12.021208 12.632396 32 32 9.36556 9.98732 9.382920 12.622076 12.021238 12.632396 32 32 32.6428 12.998732 9.382920 12.622076 12.021238 12.632396 32 32 32.6428 12.998732 9.382920 12.64909 12.021238 12.63239 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2326 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 12.6326 12.2329 12.6226 1	17	9 361287	9.98822;	9.3-3004	10.626936	10.011777		
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23	22	9 36 3954	9.958073	9.3-5881	10.624119	10.011927		
24	23	9.364485	9.088043	4.3-6442	10.523,58	10.01195-	10.635515	37
26    9.36665   9.98   9.37   9.37   8122   10.621878   10.012078   10.633396   32    9.36666   9.98   9.37   8081   10.62203   10.01218   10.633396   32    9.367659   9.88   802   9.37   97797   10.620203   10.01218   10.632341   31    9.368185   9.98   802   9.37   9.354   10.61266   10.01218   10.632341   31    9.368185   9.98   71   9.38   9.354   10.61266   10.01219   10.031289   29    39.39236   9.36826   9.98   71   9.38   9.36920   10.61276   10.01229   10.6323764   32    9.369276   9.98   77   9.38   9.38   9.37   10.617980   10.012290   10.629715   26    27	24	9.365016	9.983013	9.323	13.622997	13.01198-	10.634984	
26    9.36665   9.98   9.37   9.37   8122   10.621878   10.012078   10.633396   32    9.36666   9.98   9.37   8081   10.62203   10.01218   10.633396   32    9.367659   9.88   802   9.37   97797   10.620203   10.01218   10.632341   31    9.368185   9.98   802   9.37   9.354   10.61266   10.01218   10.632341   31    9.368185   9.98   71   9.38   9.354   10.61266   10.01219   10.031289   29    39.39236   9.36826   9.98   71   9.38   9.36920   10.61276   10.01229   10.6323764   32    9.369276   9.98   77   9.38   9.38   9.37   10.617980   10.012290   10.629715   26    27	25	9.305546	9 98-983	9 37-503	12.622437	10.012017	10.634454	35
28    9.56-121   9.93-302   9.3-9230   10.620761   10.012108   10.632869   32   9.367659   9.98-802   9.3-9797   10.62023   10.012138   10.632381   30   9.368185   9.98-802   9.38-921   10.619646   10.012168   10.632381   30   9.368185   9.98-802   9.38-920   10.61990   10.012190   10.031285   29   38-266   9.98-710   9.38-202   10.61990   10.012290   10.630239   27   38-285   9.98-710   9.38-202   10.617980   10.012290   10.630239   27   37   38-285   9.98-710   9.38-3120   10.617980   10.012290   10.639-15   28   29   37   380   9.98-710   9.38-3120   10.616318   10.012290   10.629-75   24   38   9.3-1330   9.98-718   9.38-3120   10.616318   10.012290   10.629-75   24   38   9.3-1330   9.98-718   9.38-318   9.38-313   10.615214   10.012412   10.62265   22   23   23   23   23   23   23   2	26	9.360075	9.95-9;3	9-178122	10.621878	10.012047	13.633925	34
29   9.367659   9.987802   0.37479   10.62223   10.012138   10.612341   31   32   368185   19.48732   9.58344   10.614646   10.012168   10.031815   30   368185   19.48732   9.58344   10.614646   10.012168   10.031815   30   31   9.58871   9.383420   10.618534   10.012229   10.032764   29   33   9.369276   19.987710   9.383620   10.617980   10.012220   10.62376   27   37   10.617980   10.012220   10.62371   27   28   28   28   28   28   28   28	27	9.366604	9.95 .22	9.378681	10.62 - 319	10.012078	10.633396	33
30	28	9.56-131	9.93 392	9.3-9239	13.620761	10.012108	10.632869	32
31 9. 368711 9.9° 821 9.382920 10.619090 10.012199 10.031289 28 32 9.369236 9.98171 9.381466 10.618534 10.012229 10.030764 28 33 9.369761 9.98171 9.382020 10.617980 10.012260 10.630239 27 34 9.37285 9.987710 9.582575 10.6117425 10.012290 10.629715 26 35 9.370808 9.987649 9.383129 10.616871 10.012220 10.629715 26 36 9.371330 9.987649 9.383129 10.616318 10.012321 10.628670 24 37 9.3718521 9.987611 9.384234 10.615318 10.012321 10.628670 24 38 9.37233 9.987588 9.384786 10.615214 10.012412 10.627627 22 49 9.372414 9.987557 9.38538 10.614665 10.012412 10.627627 22 40 9.373414 9.987526 9.38538 10.614665 10.012412 10.626676 20 41 9.373933 9.987440 9.386438 10.61356 10.012474 10.62667 10 42 9.374452 9.987465 9.38598 10.61356 10.012535 10.625548 18 43 9.34970 9.987444 9.387536 10.61361 10.012550 10.625548 18 45 9.376003 9.987445 9.388084 10.611366 10.012566 10.625030 16.9376003 9.98734 9.388084 10.611366 10.012567 10.625481 14 47 9.377035 9.987310 9.388084 10.611366 10.012658 10.625930 15.625948 18 48 9.375487 9.987310 9.38088 10.610322 10.012659 10.625481 14 49 9.375487 9.987310 9.38088 10.610325 10.012659 10.625481 14 49 9.378567 9.987310 9.38088 10.610325 10.012659 10.623965 13 48 9.378567 9.987310 9.390270 10.605040 10.01278 10.62396 13 50 9.378577 9.987317 9.390270 10.605640 10.012783 10.62396 13 51 9.379089 9.987186 9.39193 10.605640 10.012783 10.62399 15 52 9.380614 9.987619, 39193 10.605640 10.012783 10.611423 10 53 9.380624 9.987692 9.393531 10.605546 10.012390 10.611476 6 9.381633 9.987020 9.39133 10.605927 10.012930 10.611476 6 9.381643 9.987020 9.39594 10.605386 10.012930 10.611876 6 9.381643 9.987020 9.39594 10.605386 10.012930 10.611876 6 9.381643 9.987020 9.39594 10.605386 10.012930 10.611876 10.610876 6 9.381643 9.987020 9.39593 10.605927 10.012930 10.611876 10.610876 6 9.382667 9.98698 9.39593 10.605927 10.012930 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.6	29	9 357659	9.98-802	9-3-4797	10 620203	10.012138	10.6323 11	31
31 9. 368711 9.9° 821 9.382920 10.619090 10.012199 10.031289 28 32 9.369236 9.98171 9.381466 10.618534 10.012229 10.030764 28 33 9.369761 9.98171 9.382020 10.617980 10.012260 10.630239 27 34 9.37285 9.987710 9.582575 10.6117425 10.012290 10.629715 26 35 9.370808 9.987649 9.383129 10.616871 10.012220 10.629715 26 36 9.371330 9.987649 9.383129 10.616318 10.012321 10.628670 24 37 9.3718521 9.987611 9.384234 10.615318 10.012321 10.628670 24 38 9.37233 9.987588 9.384786 10.615214 10.012412 10.627627 22 49 9.372414 9.987557 9.38538 10.614665 10.012412 10.627627 22 40 9.373414 9.987526 9.38538 10.614665 10.012412 10.626676 20 41 9.373933 9.987440 9.386438 10.61356 10.012474 10.62667 10 42 9.374452 9.987465 9.38598 10.61356 10.012535 10.625548 18 43 9.34970 9.987444 9.387536 10.61361 10.012550 10.625548 18 45 9.376003 9.987445 9.388084 10.611366 10.012566 10.625030 16.9376003 9.98734 9.388084 10.611366 10.012567 10.625481 14 47 9.377035 9.987310 9.388084 10.611366 10.012658 10.625930 15.625948 18 48 9.375487 9.987310 9.38088 10.610322 10.012659 10.625481 14 49 9.375487 9.987310 9.38088 10.610325 10.012659 10.625481 14 49 9.378567 9.987310 9.38088 10.610325 10.012659 10.623965 13 48 9.378567 9.987310 9.390270 10.605040 10.01278 10.62396 13 50 9.378577 9.987317 9.390270 10.605640 10.012783 10.62396 13 51 9.379089 9.987186 9.39193 10.605640 10.012783 10.62399 15 52 9.380614 9.987619, 39193 10.605640 10.012783 10.611423 10 53 9.380624 9.987692 9.393531 10.605546 10.012390 10.611476 6 9.381633 9.987020 9.39133 10.605927 10.012930 10.611476 6 9.381643 9.987020 9.39594 10.605386 10.012930 10.611876 6 9.381643 9.987020 9.39594 10.605386 10.012930 10.611876 6 9.381643 9.987020 9.39594 10.605386 10.012930 10.611876 10.610876 6 9.381643 9.987020 9.39593 10.605927 10.012930 10.611876 10.610876 6 9.382667 9.98698 9.39593 10.605927 10.012930 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.611876 10.6	30	9.368185	9.45-332	9 28-354	10.614646	10.012168	10.031815	30
32 9.369236 9.98737 9.381466 10.618534 10.012229 10.030764 28 33 9.369761 9.987710 9.382022 10.617980 10.012260 10.630339 27 34 9.37288 9.987710 9.582575 10.617425 10.012290 10.629715 26 35 9.370808 9.987649 9.383129 10.616871 10.012220 10.629715 26 36 9.371330 9.987649 9.383129 10.616318 10.012321 10.628677 24 37 9.371852 7.98761 9.384234 10.616318 10.012321 10.628677 24 38 9.37233 9.987588 9.384786 10.615214 10.012412 10.627627 22 49 9.372494 9.987557 9.38538 10.615214 10.012412 10.627627 22 40 9.373414 9.987526 9.38588 10.614665 10.012412 10.626676 20 41 9.373933 9.987440 9.386438 10.613563 10.012594 10.626676 20 42 9.374452 9.987465 9.38698 10.613563 10.012535 10.625548 18 43 9.34970 9.987445 9.38698 10.61366 10.012597 10.625548 18 45 9.376003 9.987347 9.388084 10.611366 10.012567 10.625633 16 47 9.375487 9.98749 9.388084 10.611366 10.012567 10.625481 14 49 9.377540 9.987370 9.38631 10.611366 10.012659 10.625481 14 49 9.377540 9.987310 9.38028 10.61026 10.012659 10.625481 14 49 9.378567 9.987310 9.380270 10.605640 10.012557 10.621481 14 50 9.378577 9.987317 9.390270 10.605640 10.012783 10.621423 10.9378503 19.987124 9.390270 10.605640 10.012783 10.621423 10.938064 19.38064 19.39089 10.607011 10.012878 10.62399 11 50 9.380644 9.987024 9.393531 10.605640 10.012783 10.611436 10.61987 6 9.381134 9.987024 9.393531 10.605646 10.012908 10.611476 6 9.381643 9.987024 9.393531 10.605646 10.012909 10.611876 6 9.381643 9.987024 9.393531 10.605646 10.012909 10.611876 10.	_						13 021280	70
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36    9.371330    9.987649   9.883682   10.616318   10.012351   10.625677   24   3718521 19.87611   9.384234   10.615766   10.012412   10.627627   23   9.372594   9.987588   9.384786   10.615214   10.012412   10.627627   24   9.3734314   9.987587   9.38588   10.614665   10.012474   10.626686   20   9.3734314   9.987465   9.386438   10.614612   10.012474   10.626686   20   41   9.373933   9.987465   9.386438   10.613561   10.012594   10.625648   18   9.374452   9.987465   9.38698   10.613561   10.012597   10.625548   18   9.374470   9.374445   9.38688   10.61366   10.012597   10.625548   18   9.376033   9.87372   9.388084   10.611366   10.012597   10.625033   16   9.376519   9.987310   9.38631   10.611366   10.012697   10.625481   14   9.377035   9.987310   9.38678   10.610276   10.12692   10.623481   14   9.377549   9.987310   9.38678   10.610276   10.12692   10.623451   14   19.378035   9.987310   9.380815   10.6025640   10.012783   10.623451   12   12   10.623451   12   12   12   12   12   12   12								
37 9 3-1852 9.98-61 9.384234 10.615766 10.012382 10.628145 23 38 9.3-2733, 9.95758 9.384756 10.615214 10.012412 10.62762- 22 40 9.372894 9.98-557 9.385381 10.614063 10.012413 10.627062- 22 41 9.373933 9.987405 9.38588 10.614812 10.012413 10.625666 20 41 9.373933 9.987405 9.386438 10.613562 10.012504 10.626667 10 42 9.374452 9.987465 9.386987 10.613013 10.012535 10.62548 18 43 9.34470 9.98-403 9.388084 10.611916 10.012597 10.625030 17 44 9.375487 9.98-403 9.388084 10.611916 10.012597 10.624513 16 45 9.376519 9.987310 9.388084 10.611969 10.012597 10.624513 16 47 9.377035 9.987310 9.387851 10.610822 10.012659 10.623481 14 47 9.377549 9.98-341 9.38918 10.610226 10.012690 10.623481 14 49 19.37549 9.987219 9.390270 10.610276 10.012690 10.623481 14 50 378577 9.987310 9.380815 10.605840 10.012783 10.623491 12 50 9.378577 9.987317 9.391360 10.605640 10.012783 10.621423 10 51 9.379089 9.987186 9.39193 10.605640 10.012783 10.621423 10 52 9.380614 9.987020 9.393531 10.605640 10.012845 10.62399 8 53 9.380113 9.987124 9.39289 10.607011 10.012876 10.619876 10.61987 15 59 9.381134 9.987020 9.393531 10.605640 10.012900 10.61857 16 59 9.381643 9.987020 9.393531 10.605640 10.012900 10.61876 10.61987 10.938064 9.39500 10.012900 10.61876 10.61876 10.61885 10.61885 10.61885 10.012900 10.61876 10.61885 10.61885 10.012900 10.61876 10.61885 10.618								
38   9.3 - 27; 3.9.9 5 5 8   9.3 8.47 6   10.61 5 214   10.01 2412   10.62 7 6 2 -   22   23 24   9.9 8 5 7   9.3 8 5 3 7   10.61 406 5   10.01 2443   10.62 7 10.6   24   24   24   24   24   24   24   2								
39 9.3-2894 9.98-557 9.38-538 10.614663 10.012443 10.627106 21 40 9.37341419.98-520 9.38-588 10.614812 10.012474 10.616566 20 41 9.373933 9.98-7465 9.38-648 10.613013 10.012504 10.62667-10 42 9.374452 9.98-7465 9.38-688 10.613013 10.012535 10.625548 18 43 9.34-70 9.98-7414 9.38-536 10.612464 10.012505 10.625030 17 44 9.37548-19.98-403 9.38-8084 10.611916 10.012597 10.642593 16 45 9.37603-9.98-737-9.38-8034 10.611916 10.012597 10.625930 17 46 9.376519-9.98-741 9.38-9178 10.612369 10.012628 10.623997 15 47 9.37-035, 9.98-7310 9.38-9178 10.61282 10.012659 10.622965 13 48 19.37-5349 9.98-7310 9.38-9178 10.61282 10.012659 10.622965 13 48 19.37-5349 9.98-7310 9.38-9178 10.60282 10.012752 10.623937 15 49 19.378507, 9.98-7310 9.360270 10.60282 10.012752 10.621937 11 50 9.378577, 9.98-7317 9.360270 10.605640 10.012783 10.621423 10 51 9.379089 9.98-186 9.39-193 10.605640 10.012783 10.621423 10 52 9.380113.9.98-7124.9.39298 10.607011 10.012856 10.61988 53 9.380113.9.98-7124.9.39298 10.607011 10.012856 10.61988 54 9.380644 9.98-7020 9.393531 10.605646 10.012908 10.61876 55 9.381134 9.98-7050 9.39594 10.605358 10.012970 10.61857 56 9.381643 9.98-7050 9.39594 10.605358 10.012970 10.61857 57 9.382661 9.39698 9.395154 10.603366 10.012970 10.61857 58 9.382661 9.38098 9.395154 10.603366 10.013033 10.61852 59 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852 9 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852 9 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852 9 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852 9 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852 9 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852 9 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852 9 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852 9 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852 9 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852 9 9.38368 9.86936 9.395233 10.603767 10.013064 10.616852								
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42   9.374452   9.987465   9.386987   10.613013   10.012535   10.62548   18   43   44   75   75   75   75   75   75   75	_							
43 9 374470 9 987414 9 387536 10.6 12464 10.0 12566 10.0 25030 17 44 9 375487 19.98 10.9 388084 10.6 11369 10.0 12597 10.6 124513 16 45 9.376619 9.98 137 9.388084 10.6 11369 10.0 12597 10.6 124513 16 46 9.376619 9.98 131 9.389178 10.6 10822 10.0 12658 10.6 23997 15 47 9.377035, 9.98 131 0.389178 10.6 10276 10.0 12659 10.6 23965 13 48 19.378549 9.98 1248 9.390815 10.6 10.0 12752 10.6 12935 12 49 19.378503 9.98 1248 9.390815 10.6 10.0 12752 10.6 10.0 12745 11 50 .9.378577, 9.98 117 9.39136 10.6 10.0 12783 10.6 121937 11 51 19.379089 9.98 1186 9.391903 10.6 10.0 12783 10.6 12091 1 92 19.379089 9.98 1186 9.391903 10.6 10.0 12844 10.0 12091 1 93 10.380624 9.98 10.98 10.6 10.0 12086 10.6 1988 10.98 10.98 10.6 10.0 12086 10.6 1988 10.98 10.6 10.0 12086 10.6 1988 10.98 10.6 10.0 12086 10.6 1988 10.6 10.0 1208 10.6 10.0 1209 10.6 1988 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.0 1209 10.6 1885 10.6 10.6 10.0 10.0 10.0 10.0 10.0 10.0								
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45   9.37603; 9.987372   9.388631   10.61369   10.012628   10.623997   15   46   9.376619; 9.987310   9.389178   10.610322   10.012659   10.622481   14   19.377035   9.987310   9.389178   10.610325   10.012690   10.622965   13   48   19.377036   9.987219   9.390270   10.602973   10.602721   10.622451   12   10.62363   10.012752   10.621937   11   10.625640   10.012783   10.621937   11   10.379089   9.987186   9.391903   10.605640   10.012783   10.621423   10   10.012878   10.621423   10   10.012878   10.623911   9.379089   9.987186   9.391903   10.605640   10.012884   10.602911   9.380113   9.987154   9.392447   10.60753   10.012845   10.602911   9.380624   9.987020   9.39351   10.002646   10.01286   10.610887   54   9.381134   9.987020   9.39531   10.605927   10.012908   10.61876   6.9381643   9.987020   9.39514   10.6055386   10.012970   10.61876   4.938064   9.986998   9.395154   10.603368   10.012970   10.61876   4.938661   9.986998   9.395154   10.603368   10.012970   10.61876   4.938667   9.886998   9.395994   10.603368   10.012970   10.61876   4.938667   9.886998   9.395994   10.603368   10.012970   10.61876   4.938667   9.886998   9.395994   10.603368   10.012970   10.61876   4.938667   9.886998   9.395934   10.603368   10.012970   10.61876   4.938667   9.886998   9.395934   10.603368   10.012970   10.61876   4.938667   9.886908   9.395934   10.603368   10.012970   10.616872   10.288667   9.886908   9.395934   10.603368   10.012970   10.616872   10.288667   9.886908   9.395934   10.603368   10.012970   10.616872   10.288667   9.886908   9.395934   10.603368   10.012970   10.616872   10.288667   10.01208   10.616872   10.288667   10.01208   10.616872   10.288667   10.01208   10.616872   10.288667   10.01208   10.616872   10.288667   10.01208   10.616872   10.288667   10.01208   10.616872   10.288667   10.01208   10.616872   10.288667   10.01208   10.616872   10.288667   10.01208   10.616872   10.288667   10.01208   10.616872   10.288667   10.88868   10.88868   10.28868   10.28868   10.28868   10.28868	•				12.012464	10.012566		
45   9.376519   9.987310   9.389178   10.610822   10.012659   10.623481   14   14   19.377035   9.987310   9.380727   10.610276   10.012690   10.622455   12   13   13   13   13   13   13   13								
47   9.377035   9.987310   9.38724   10.610276   10.012695   10.622965   13   148   9.377549   9.987248   9.390270   10.609730   10.6012721   10.622451   12   12   12   12   12   12   12								
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49 19.378563 9.987.248 9.39.0815 10.609.185 10.0127.52 10.621937 115   50 .9.378577 9.987.247 9.39.360 10.605640 10.012783 10.623911 9.39.39089 9.987.186 9.39.1903 10.605640 10.012783 10.623911 9.52 19.379601 19.987.155 9.39.2447 10.607.53 10.012845 10.6223919 9.38.0113.9.98712419.392989 10.607011 10.012876 10.619887 7.53 9.380123.9.98712419.392989 10.607011 10.012876 10.619887 7.54 9.380624 9.987092 9.39353 10.605536 10.012908 10.61876 6.59.381134 9.987050 9.39.1914 10.605536 10.012900 10.61876 7.59.381134 9.987050 9.39.1914 10.605536 10.012970 10.61876 7.59.382661 9.986998 9.395154 10.604846 10.013023 10.617840 3.59 9.382152 9.986998 9.395154 10.604366 10.013023 10.617840 3.59 9.382661 9.98098 9.395233 10.603767 10.013064 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 9.88694 9.39594 10.603229 10.013096 10.616832 10.283675 10.012959 10.616832 10.283675 10.012959 10.012959 10.616832 10.283675 10.012959 10.616832 10.283675 10.012959 10.012959 10.616832 10.283675 10.012959 10.616832 10.283675 10.283675 10.012959 10.616832 10.283675 10.012959 10.012959 10.283675 10.012959 10.012959 10.616832 10.283675 10.012959 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10.283675 10								
50 .9.378577 9.487217 9.391360 10.605640 10.012783 10.621423 10.51   9.379089 9.987186 9.391903 10.608097 10.012814 10.020911   9.379081 9.987154 9.392447 10.607553 10.012845 10.603897   7.381134 9.987124 9.39289 10.607011 10.012876 10.619887   7.380624 9.987022 9.393531 10.805469 10.012908 10.610376   6.59381134 9.987022 9.393531 10.805469 10.012908 10.610376   6.59381643 9.987020 9.39114 10.605386 10.012909 10.618547   4.381624 9.986989 10.98911 10.603386 10.012900 10.618547   4.381624 9.986989 10.395994 10.604866 10.013003 10.617848   6.59386 10.012909 10.618547   4.38162 9.986989 10.395994 10.604366 10.013003 10.617848   6.59386 10.012909 10.618547   6.59386 10.012909 10.618547   6.59386 10.012909 10.618547   6.59386 10.61854   6.59386   6.593								
51   9.379089   9.987186   9.391903   10.60809   10.012814   10.020911   9   9.379081   9.987155   9.392447   10.607553   10.012845   10.620399   8   53   9.380113, 9.9871449, 392989   10.607011   10.012876   10.619887   54   9.380624   9.987030   9.393531   10.806469   10.012908   10.610376   6   6.381643   9.987030   9.39404   10.6055927   10.012909   10.618857   6   9.381643   9.987030   9.39414   10.605586   10.012909   10.618857   4   6.532661   9.989389, 395154   10.603366   10.013033   10.617540   3   9.382661   9.893695   9.39594   10.603366   10.013033   10.617530   10.63686   10.616872   10.63866   10.63866   10.616872   10.63866   10.63866   10.616872   10.63866								
52   9 3 9 601 9 98 7 15 5 9 3 9 2 4 4 7 10.60 7 5 5 3 10.0 128 4 5 10.62 0 3 9 9 8 9 3 8 0 113 9 9 8 7 124 19 3 9 2 9 8 9 10.62 7 0 11 10.0 128 7 6 10.6 1 9 8 7 1 2 4 19 9 9 7 0 7 10.0 128 7 6 10.6 1 9 8 7 10.6 1 9 7 10.0 129 8 10.6 1 9 7 10.6 1 9 10.	50	,9.378577	9.49.31.	4.391360	12.002640	10.012783	10.021423	15
52   9 3 9 601 9 98 7 15 5 9 3 9 2 4 4 7 10.60 7 5 5 3 10.0 128 4 5 10.62 0 3 9 9 8 9 3 8 0 113 9 9 8 7 124 19 3 9 2 9 8 9 10.62 7 0 11 10.0 128 7 6 10.6 1 9 8 7 1 2 4 19 9 9 7 0 7 10.0 128 7 6 10.6 1 9 8 7 10.6 1 9 7 10.0 129 8 10.6 1 9 7 10.6 1 9 10.	51	19.379084	9 987186	9.391903	15.608097	10.512814	10.020911	9
53   9.380113.9.987124;9.392989   10.607011   10.012876   10.619887   7.9.380624   9.9870929.393531   10.006469   10.012908   10.610376   6.56   9.381643   9.9870929   10.6055386   10.012939   10.61876   7.56   9.381643   9.987030   9.397154   10.605386   10.012970   10.61876   4.57   9.382162   9.886998   9.395154   10.604846   10.013003   10.61876   4.58   9.382661   9.98096   9.395094   10.604306   10.013003   10.617339   2.59   9.383168   9.886904   9.395233   10.603767   10.013064   10.616872   1.56   10.3865   10.56   10.5	52	10 3"9601	9.987155	9.392447	10.607553	10.012845	15.625300	
54 [9.383624] 9.987092 9.393531 10.056469 10.012908 10.610376 6 55 [9.381134] 9.987050 9.39407 1 10.655327 10.012939 10.618567 9.381643 9.987050 9.39154 10.655386 10.012970 10.618557 9.382152 9.986998 9.395154 10.064846 10.013033 10.617540 3 58 [9.382661] 9.86998 9.395194 10.604360 10.013033 10.617540 3 59 [9.38368] 9.86936 9.395294 10.603767 10.013064 10.616872 1 60 [9.38367] 9.986904 ) 790771 10.603229 10.013096 10.616325 0 4 Cosine. Sine. (Costing. Faig. Coses. Secure v.	53	9.380113	9.987124	9.392989	10.657011	10.012876	10.61988-	-
55 9.381134 9.987061-9.394073 [10.605927 [10.012939] [10.618640] 56 9.381643 9.987030 [0.304014] [10.6055386 [10.012970] [10.618757] 57 9.382152 9.986998-9.395994 [10.604846 [10.013033] [10.617840] 58 9.382661 9.98096 9.395994 [10.604306] [10.013033] [10.617540] 59 9.383168 9.986936 9.395233 [10.603767 [10.013064] [10.616872] [10.2833675 9.986934] ) [19.771 [10.603229] [10.013096] [10.616325] [10.833675] [10.616872] [10.833675] [10.83	154	.9. 180621	4.487542	0.303531	10.506469	10.012008	10.619376	6
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57 9.382152 9.986998:9.395154 10.064846 10.013002 10.017844 3 58 9.382661 9.98096 9.395094 10.064306 10.013033 10.017539 2 59 9.38368 9.986959 9.395233 10.063767 10.013064 10.016872 1 60 9.383675 9.986994 9.796777 [10.053229 10.013096 10.016325 0  4 Co-sine. Sine. (Co-ting. Fang. Co-ec. Security v.		9.381643	9.487030	9.391914	110.605586	10.01 29°0	10.617; 57	
58 9.382661 9.38096 9.395094 10.604306 10.013033 10.617334 2 59 9 183168 9.386936 9.395233 10.603767 10.013064 10.616832 1 60 9.383675 9.386904 ) 796771 10.603229 10.013096 10.616325 0  4 Co-sine. Sine. (Co-ting. Fing. Co-ec. Security 9.		9.382152	9.986998	9.395154	10.564846	10.013002	10.617546	
59 9 383168 9 986936 9 396233 10.603767 10.013064 10.616832 1 60 9.3836-5 9 986904 ) 396771 10.603229 10.013096 10.616325 0  4 Co-sine. Sine. (Co-ting. Fing. Co-ec. Secure v.		9.382661	ე ეგიერ -	9.395094	10.604366	10.013033	10 617 ; ; 4	
65 9.3836-5 9.986904 ) 795771 10.603220 10.013096 10.616325 0  9 Co-sine. Sine. (Costang. Fang. Cosec. Secure of		9 383168	ე ყზრყვნ	9 395233	10.603767	10.013064	10.616532	
M Co-sine. Sine. (Co-tang. Fang. Co-ec. Secunt. ) N		9. 38 36 " 5	9 48690;	) 795771	10.603229	10.013096	10.616;25	റ
	7				Finder			(
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14 Degree

	-	-	-	4 Degree.	A CHARLES	-	
3 3	Sine.	Co-sine	Tang	Co-tang	Secunt.	Co-sec.	1. 24
10	9.383675	9.986904	9.39677	10/60312	9 10.013096	10.61612	60
1 1		9.986873		the second state of the second	The second second	A DESIGNATION OF THE PERSON NAMED IN	
1 2		9.986841	9.39784		and the second second second	District Control of the Control	
	THE RESERVE OF THE PARTY OF THE	9.986809	9.39838			a compression on	-
1 3		9.986778	9.39891		OF THE OWNER, AND ADDRESS.	THE RESERVE OF THE PARTY OF THE	
1 4	9.386201	9.986746	9.39945	of the latest terminal to the latest terminal te		The second second	-
1 6	9.386704	9.986714	9.39999	A STREET STREET, SA	21		1864
	19.387207	9.986683	9.40052	C 100 100 100 100 100 100 100 100 100 10	A STATE OF THE PARTY OF THE PAR	The second second	100
7 8		9.986651	9.40105				
	1 000	9.986619	9.40159			-	
1 9	200	9.986587	9.40212			10.611280	enen
10					-	-	
100	9.389211	9.986555	9.40265	22/33		10.610789	
12	THE RESIDENCE OF THE PERSON NAMED IN	9.986523	9.40318		of the second second	10.610289	
13		9.986491	9.40371	N. Street, Square, and Square,	O STATE OF THE OWNER, WHEN	The second second	
14	9-390708	9.986459	9.40424	10.59575	1 10.013541	10:609191	46
15	9.391206	9.986417	9.40477	10.59522	10.013573	10.608794	45
16	9.391703	9.986395	9.405301	10.59469		10.608597	44
17	9.392199	9.986363	9.405830		10.013637	10.607801	43
18	9.392695	9-986331	9.406364			10.607305	41
19	9.393191	9.986299	9.40689	10.59310	10.013701	10 606810	41
20	9.393685	9-986266	9.407419	10.59258	10,013734	10,606315	40
11	9.394179	9-986234	9.40794	10.59205	10.013766	10.606811	39
22	9.394673	9-986202	9.40847		of Discounting Control of	10.605317	18
13	9.395166	9.986169	9.408997	The second second		10.654834	37
124	9.395658	9.986137	9.400521	The second second	A STATE OF THE PARTY OF THE PAR	10.604341	36
25	9.395150	COLUMN ASSESSMENT OF THE PARTY	9-41004	1 2 2 1 1 1 2		10.601310	35
26	9.396641	9.986072	9.410560			10.601340	34
27	9.397132	ACCURATION AND ADDRESS OF THE PARTY OF THE P	9.41.1092	ALCOHOL: NAME OF TAXABLE PARTY.		10.602868	35
28	9.397621	9.986007	9.411619			10.602379	35
29	9.398111	The second	9.412137	A STATE OF THE PARTY OF THE PAR		10.601889	23
30	9.398600	9.985942	9.412658	Charles of the Control of the Contro	a management of the last	10.601400	80
			27	200		-	
31	9-399088	9.985909	9-413179			10.600912	24
32			9 413699			10.600425	85
33	THE RESERVE OF THE PERSON NAMED IN	m - m - m	9-414219	The second second		10.599938	57
34		0 01	9.414738			10.599451	26
35			9.415257	Date of the latest the		10.598965	25
36			9.415775			10.598480	24
37		Company of the Compan	9.416293	The second second	100 1 100 C	10.597995	23
38		Marie Committee of the	9.416810			10.597511	23
39	AND DESCRIPTION OF THE PARTY OF		9-417326			10.597018	21
40	9 403455	9.985613	9 417842	10 582158	10.014387	10.596545	10
41	9.403938	9.985580	9.418358	10.581642	10.014420	10.596062	10
42			9-418873	10 581127	CONTRACTOR STORY	10-595580	110
43			9.419387	10.580613		10.595099	12
44			9.419901	10.580099	THE RESERVE OF THE PERSON NAMED IN	10.594618	16
45			410415	10.579585	CONTRACTOR OF STREET	10.594138	15
46	1 2 2 2	CONTRACTOR OF THE PARTY OF THE	0.420927	10.579073		10.593659	14
47	The state of the s	THE RESERVE OF THE PARTY OF THE	421440	10.578560	AND DESIGNATION OF	10.593180	15
48		COLUMN TO SERVICE SERV	421952	10.578048	AMERICAN STREET, STREE	10-592701	13
49		Chicago Contract of	422463	10.577537	The second secon	10-502223	Ti
50		- A - A-	422974	10.577026	The second second	D. (01746)	10
				-		The second second	
51		CONTRACTOR OF THE PARTY OF THE	423484	10.576516		0.591269	9
52	9.409207 9	0-0-		10.570007	D	0.590793	8
53	9.409681 9	905100 9	4=4503	10.575497	10.014820 1	0.593318	1
54	9.415157 9	086140 9	425011	10.574989	10.014854	0.509043	6
55	9.410032 9	08 5070	425519	10.574401	10.014887	0.509308	5 4
50	9.41110619	084019 9	420027	10.573973	10.014921	0 500894	1
3/					10.014955		3
30	9.412052 9				10.014989		8
57 58 59 60	9.412524 9					0.587475	1
-			-	10.571948		0.587004	0
M	Co-sine-	Sine. C	o-tang.	Tang.	Co-sec.	Secant.	M
			75.1	дедтесь.		-	_

			-10	Degrees.	-			
la 30	Sine.	Co-sine-	Tang.	Co-tang.	Semant.	Co-sec.	34	ı
1	4.412996	9.984944	9. 528051	10.471948	10.015056	10.587004	60	П
1 ,	9-413467	9.984910	9-428557	20.571943	10.01 (0)0	10.586533	59	ı
1	9-413938		9 149062	10.570938	IDATETAL	10,586061	58	1
3	9.414408		9.429506	(0.579434	1D.DESESS	10.585592	57	ı
4	9-414878		0-470010	10.569950	10,015192	10.585122	36	ı
. 5		9.954774	1430573	10.560427	10-015246	10.584655	35	ı
6	9.415815		9-431075	rm. şêliya ş	10,015160	13.58a185	94	ı
7	9-416185		0 431577	10.508403	10.019294	10.583747	53	ı
8	9.416731		9-411079	10.567911	10.015338	10.583310	52	ı
9		9.984638	9-45E580	10.567410	10.015361	10.582783	51	ı
10		0.084603	9-433080	10.966920	10.015307	10.582516	50	ı
162			The second second	10.566420	10.015931	ro 581850		ı
12	9.412616	9.984559	9-433510	10.505920	10 01 5465	10.581385	48	ı
13	9.419074	9.984500	9-434010	10 565421	10.015500	10.580921	42	ı
14	9 419544	9.984466	9-434379	10.564922	10.015534	10.580456	46	ı
/15	9.420007	9.984432	9-435978	10.564424	10.01556K	10.579993	45	ı
16	9 410470	9-984397	9-436075	10.563927	10.015603	10.579530	94	ı
17	9 410933	9.984363	9-436570	10.563430	10.015637	10.579007	43	ı
18	9-421395	9.984328	9-437067	10.562971	10.015672	10.578603	42	
19	9-421857	0.984194	9-437563	10 562437	10.015706	10.578143	41	
/30	9-422318	9.984259	9.418019	10.561941	10.015741	10.577682	40	
=			-					ı
37	9.423778	9.984224	9-438554	10.561446	10.019776	10.577222	39	ı
22	9.413238	9.984190	9-439048	10.560457	10,015845	10.576762	38	ı
33	9.423697		9-439543	ID 559964	10.015880	AND PARTY AND PA	37	ı
25	9.424615	9.984085	9-440529	10.559471	10 015915	10.575844	35	ı
	9.425073	9.984050	9:441022	10.558978	10,015950	10.574937	34	ı
27	0.435430	9.484015	9-441514	10.558486	10 01 5989	10.574470	31	ı
	4.425987	9.983981	9:442006	10.557994	10.016019	10.574013	31	ı
	0.410443	9.983946	9 442497	10.557503	10.016044	10.573557	31	ı
	9.436899	9.983911	9-442988	10.557012	10.016089	10.573101	10	ı
	-		Name and Address of the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner, which i	-	THE RESERVE OF		=	ı
	9-437354	9.983875	9-443479	10.556521	20.016125	10:57 2540	29	ı
	91427809		9-443908	10.550032	10,016160	PO-572191	28	ı
	9.418163		9-444458	10.555542	10.010195	10 371737	27	ı
1000	9-428717		9-444947	10.595053	10.016250	10.571235	26	
35	9.419170		9-445435	10.554565	10.016265	10.970830	25	ı
30		9.983700	9-445923	10.554077	10,016330	10.570377	23	ı
37	9.430075		9-446898		Market Street, Square,	10,569935	22	ı
10000	9 430517		91447384	10 533 10%	10,010371	10.500022	21	ı
39	9.430978	SECURIOR SE	9 447870	10.532016	10.016442	10.568571	10	ı
1	0.435429				The Parket		_	
45	9.431879	Contract of the Contract of th	9-448350	10.551644	10 016477	10.698131	1.0	
	9.432329		9:448841	10:551150	10.016513	101567671	43	
43	9-431778		9-449326	101550674	10.018545	10.567222	15	
	9.433020		9.449810	10.550100	10.016564	10.466774	10	
45	9 433675		9.450294	BOOK ALMONDO	10.016619	10 566535	7.5	
46	9-454122		9.450777		10.016555	10.565878		
47	9.474569		9.451260	101548740	10.016591	10.595431	Lg.	
48	9.435916		9.451743	10/547775		10.504584	11	
49	9 43 (462)	0.03230	9.452225			101101111111111111111111111111111111111	10	
10			9-452706	State Francisco	The second second		_	
15.1			9-453187	101546813		10(503047)	9	
52	CARL CO.	9.983130	LOSS SALES		10 015810		-	
5.3	9.437242			101545851				
54	9.4 5, 080	9.983058	9-454028	10.545372	10 010941	10.461314		
55					10.010978		5	
50		9.952986				10,561418		
	9-139-14	9.982950	9.450004		10.017050		15.00	
58	9 939450	9.982914	3-45-547	10 (43458	10.017122	10 560544	-	
59	9 419197	9.981878	9-457919	10.242401	10.017158	10 scoffs	0	
					_		=	1
24	Co-sine.	Sime	Co-lang.	Tang-	Co-sec.	Secun	1 38	1
-		-	- 74	Degrees.				

				161	legrees.			100
31	100	me.	Co-aime	Tanga	Co-tang.	Secant	Contec	36
-	9.4	40358	9 982842	9.457496	10.542504	10.017158	10.559562	60
HD.	9.4	40778	9-98+805	9-457973	10-542027	10-017195	10.559333	59
1 2			9.981759	9-45-419	10.501551	10.017231	10.558782	58
1 3	4 3 000		9-982733	9-458935	10.541075	10.017304	10.557904	57
113			9.982596	9-459875	10.540135	10/017340	10.557485	55
i			9.982624	9.460149	10.539651	10.017376	10.557027	54
100			9.981587	9-460823	10.539177	10.017413	10 556 590	51
1/3			9.982551	9.461297	10.538703	10,017449	10-556153	line.
1 9			9.983514	9.461770	10.538230	10.017486	10,995716	53
10			9.982477	9 462242	10.5377.58	10.017423	10-111280	50
100	9.4	45155	9 982441	9-462714	10.537286	10.017559	10.554845	-89
18	9-4	45590	9.982404	9.463186	10.536341	10.017596	10.554410	185
13			9.982331	9.464128	10.53537#	10.017669	10,553975	40
18			9.982294	9-464599	10.535401	10.017706	10.555107	45
16			9.982257	9-465069	10-534931	10.017741	10-552074	44
17	9.4	47759	9 982220	9-465539	10.534461	10.017780	ID-SERBER	41
18			9.982183	9-466008	10.533992	10.012817	10.551809	1
(20)			9.982146	9-466476	10,533524	10.017854	AG-552327	1
20		-	9.982109	9-466945	10-533055		10,550940	40
23			9.982072	9.467413	10.532587	10.017955	10.550515	10
23			9.981998	9.468347	10.532120	10.017903	10.550005	35
24			9.981961	9.468814	10.531186	10.018030	10.544111	10
25	9-4	51204	9 981924	9.469280	10.530720	10.018076	10.54K746	35
26	9.4	51632	9.981886		10.530254	10.018144	10.548368	24
22			9.981849	9.470211	THE REAL PROPERTY.	10.018151	10-547940	31
28			9.981812	9.470676	10.529324	10.018188	10 547515	33
30			9.981737	9-471141	10.528859	10.018263	10-5470%5	2
				-				르
31			9.981700	9-472668	10.527468	10.018100	10.545806	20
33			9.981625	9 47 2995	10,527005	Market Comments	10-545381	21
34			9.981587	9-475407	10.526543	10.018413	10.544956	25
35					10.526081	10.018461	10.544531	20
36			9.981512		10.525019	10.018488	10-544107	26
				9-474842	10.525158	10.018526	10.543664	23
			9.981399		10.524697	DOMESTIC OF STREET	10.543201	at
40				9-47/223		10.018549	10.642410	80
141					10.523317	10.018677		Ziji.
42	9.45	8427	9.981285	9-477142	10.422848	10,018715		11
43	9.45	8848	9-981247	9-477601	10.522200	10.0+8755		12.
441	9-45	9268	9.981209	9 478050	10.52/041	10.018791	10-540732	15
45	9.45	9088	9.981171	9-478517	10.521483	10.018529	10,540312	18
46	9.40	0(27	0.081205	9-470975	10.521025			34
-48	9 45	OBAB	9.981043	9-479-53-	10.520508	10.018905	10:539473	13
49	9.46	1364	9.981019	9.480346	10.519655	10.018081	10.518616	22
50	9.46	17821	9.980981	9 480801		10.019019		10
					10.518743	ED.019058		-
52	940	12010	9.980904	9-481712	10. (18288)	10.019096	10.032184	5
53	9.45	3032	9.980866	9-482167	10.517833	10.019154	10.536968	7
154	9.40	34450	9,980827	9-482621	10.517270	10,010172	10,026,002	10.7
35	9.40	5004	0.900789	403075	10 516925	10.019311	10.530136	5 47
5.7	gusto	4994	g.q%0712 (	1-45498±	10.410018	28401001	ID ETERNE	- 1
CK.	0.40	£108 0	1.000007 \$ 10	0.48A415	10 21246F	IO OLODAN	10-12-1202	3
391	9:40	SSMAIS	agavass c	404887	10.014112	10.019166	10.534478	100
60	9.44	2437	1.980590 9	405339	10.514661	10.019404	10,534065	0
м		sine	Sine (	to tange	Tang.	Co-sec.	Secant.	24
-	800	NAME OF TAXABLE PARTY.	-		egrees.			-

-	-		17	Degrees.			
1 24	Sine.	Co-sine	Tang.	Co-tang.	Secunt	Go-sec.	26
0	9.45 4935	9.980596	9.485339	10.514661	10.019404	10.534065	60
1	9.466348	0.980558	9.485791	10.514109	10,019442	10 533652	59
2	9.466761	9.980519	9 486242	10.513758	10.019481	10.533239	58
3	9.467173		9.486693		10.019520	10,532827	57
4	9 467 58 5		9.487143		10,019558	10:932415	36
6	9.4674996		9.487593	10.511407	10.019697	10.531004	55
2	9.468847		9.488492	-	10.019675	10:531183	54
8	9.469227			10:511059	10.019714	10 630713	32
9	9 469637	91980247	9.489390	10.510610	10:019753	10.530363	51
10	9.470046	9.980208	9.489838	10:510163	10.019793	10.529954	50
22	9 470455	9.980169	9-490286	10.509714	10,019831	10.539545	49
12				10 509167	10,019870	20.529137.	48
13				10 508820	10.019909	10 1287.09	43
54			TANK DATE OF THE PARTY OF THE P	10 508375	10.019948	10.518321	46
16	9.473492	0.979973	9.492073	10.507481	10.019988	10.527914	45 44
17	DOMESTIC OF THE PARTY OF THE PA	0.979934		10 507035	10-020066	10.527101	43
18		9.979895		10.500500	10.020105	20.526696	43
19	9 47 37 10	9.979855		10-506146	10.020145	20,526290	41
25	9.474105	9.979816	9.494299	10/505701	10.020154	20.525885	40
20	9 474519	9.979776	9 494743	10:505257	10 010114	10.525481	39
29	9 4749#3	9.979737	9.495186	10.504814	10.020263	10 5#5077	38
23	9-475327	9.979697	9.495830	10.504370	10.020303	10.514678	37
24	9.475730	9.979648 9.979618	9.496573	10.503927	10.030342	10 514170	35
26	9 476536	9 979579	9.496957	10.501043	10-010411	10.513807	54
27	9 476938	0.079539	9-497399	10.502601	10 020461	10 (11061	31
28	9.477340	9 979499	9.497841	10.502159	10.020501	10.522660	32
29	9-477741	9 979459	9.498282	10 501718	10.010541	10.522259	31
30	9.478142	9.979420	9 498722	10.501278	10,010580	10.524858	30
31		9.979380	9-499163	10.500837	10.020620	10.527458;	29
32	The second second second		9 499603	10.500397	10,020660	10.521058	28
33			9 500041	10 49995%	10.020700	10.520658	27
35	9 479741		9.500481	10.499519		10.520259	20
36	9.480339		9.501359	10:498641	10.020780	10.519860	24
37 N	9.480937		9.501797	10.498203	DOCUMENT OF THE PARTY OF THE PA	10.519063	23
38	9.481334		9 502235	10,497765	10.020900	MERCEAN UNIVERSITY	21
39	9-481731	CONTRACTOR OF THE PARTY OF THE	9.502672	10.497328	10.020941	COLUMN TO SERVICE A	31
40		919979019	9.503109	10.496801	10.050981	10.517274	30
31		9 978979	9.501546	10.496454	10.021021	10.517475	19
82		9 978919	9.503981	10.495018	10.021061	10.517079	18
43 44		9.978898 9.978848	9.504418	10.495582	10.021102	10.516684	16
45	9.484107	9.978817	Control of the Contro	10.494721	CONTRACTOR AND	10.515893	15
46		9-978777	9 505724	10.494276	10.021223	CONTRACTOR OF THE PARTY OF THE	14
47		9.978737	9.500159	10.493841	10.021003	Marie Company of the	13
48		9.978696	9.506593	10.493407	10.021304	MARKET MARKET AND	12
49	9.485682		9.507027	10 492973	10.021345	CONTRACTOR AND ADDRESS OF	11
50		9.978615		10.492540		10.513925	10
51	9 486467	9.978574	9.507893	10.402107	10.021426	10.513533	2
20	9 480360	9.976533	9.508326	10.491674	10.021467	10.513140	3
53 54	9.487641			10.490809	10.021548		7
58	9.488034		9.509622	10.490578	10,021589		5
56	9 438424		9.510054	10.489946	10.021630		4
57	9 488814	9.978329	B. \$10485	10.489515	10.011671	10.511186	3
48	Dalla Processor 1	9.978288	9.510910	10.414084	10.001713		1
59		978247			10.021753		1
60		9.928206		10 488224	10/021791	10.510018	0
36	Co-sine	Hine.	Co-tang.	Tang	Conte	SEEDIN	×
			40.5-34				

18 Degrees

			100	red force			-
SEL	Sine	Ch-sine.	Tang	Co-tang.	Secant.	Co-sec	26
0	9.489983	9-978100	9-511776	10.488224	10.021794	10.510018	60
1	9.490371	9.978165	9:513206	10,487794		10 (00620	59
2	9-499759	9.978154	9.512635	10.487165	10.021876	10-500231	38
3	9-491547	u.978085	9-513064	10.486936	10.021917	10-508853	57
4	9-491535	9:978042	9-513493	10486507	820150.01	10-507-05	56
15	9.491912		STEEL SOLE	10.486079	10,011999	10,508073	93
6	9:492308		WS14349	10.485651	10.022041	10.507692	54
7	9-492695		9/5/4777	10.485223	10.012081	10.507305	88
8	9 493081		9.515204	10.484796	10.022123	10.506919	52
9	9-493455		9.515634	10.484369	CONTRACTOR OF THE PARTY OF THE	10.500534	5.8
10	9-498841	9-977794	9/516057	10.483943	10.022206	10,506 (49	50
11.	9-494236	9-977752	9-510484	10 483510	10.011148	10 505764	149
12	9-494021	9-977711	9.516910	100000000000000000000000000000000000000		10.505379	48
13	9.495005	9/977009				10,504995	47
24	9 495388					10.504610	49
35	5 495772		0.00			10.504918	45
110	0.495154				COURSE CONTRACTOR OF THE PARTY	10.503846	44
12	0.400537	The second second	Maria San Park			10 (0 (46)	43
138	9.495919		9.519458			10,5000%1	42
19	9.407301		The second second	The second second	The second second second	10-502599	41
	-		91520305		Control of the	10.501318	165
21	9.498064	I MANUAL PROPERTY.	9.520728	10.479171		10.501935	39
22	9-498444			10.478849	CONTROL OF COMMENT	10:501556	36
23	9-198825	The second second				PARTICION	1-27
24	9-449304	The second second	The second	10.478009	The second second	10.500798	30
25	9-409584	No. of Concession, Name of Street, or other party of the Concession, Name of Street, or other pa	7 4 4	10.477583		10.500410	35
27	9-500342	The second second	the second second	The second second	NORTH CONTRACTOR OF THE PARTY O	10.300037	
23	9.500721	The second second	1000	10.476330	and the second second	10.499278	佳
20	9.501099	I Marie Sales Company		I DESCRIPTION OF STREET		10.40 8001	6
30	0.501476	100000000000000000000000000000000000000	9.524520	10.475480		10.498514	333
		100000000000000000000000000000000000000	-				_
34	9.501850	9.976914	The second	10.475061		10.498146	23
	9-502131	0.976872	A CONTRACTOR OF THE PARTY OF TH	10.474641	District Section 2	10.497769	125
33	9.502984		9:525778	10.473803	10 023213	10.497392	27
25		9.976745	9.526615	10 473385	10.033866	10.496640	20
36	9 503735	9.976701	9-527933	10.472967	10.013208	10.496365	21
37	9.504810	The second	9.537451	10.472549	10-021340	10.495860	24
38	9.504485		9 517868	10.472132	10.023383	10.495515	
30	9.504860		9.528285	10.471715	10.011026	10.495140	21
40	9.505234	9.976532	9.528702	10.471298	10.021468	10.494766	20
411	9 505608	9.976489	9 529119	10.470881	10.023511	10 494192	79
42	9.505981	9.976446	9.539535	10-470465	THE RESERVE THE PERSON NAMED IN	10-494010	12
43	9.506354	CONTRACTOR OF THE PARTY OF THE	9.539950	10/470050	PROPERTY AND ADDRESS OF THE PARTY AND ADDRESS	10 445646	121
44	9.506727	9 976362	9.530366	10.469634	COUNTY STATE OF THE PARTY.	10.495575	16
45	9.507099	9.976318	9.530781	10.409219	WANTED TAXABLE IN	10.492951	15
46	9.507471	9.976275	9.531196	10.468804	10,023725	10.402519	14
47	9.507843	9 976232	9.531611	10 468 189	Committee of the Commit	10.492157	13
48	9.808214	9.976189	9.532025	10.487975		10.491786	10
49	9,508585	9.976146	9-537-959	10.467561	COLUMN TWO IS NOT THE OWNER.	10.491415	11
50	9.508856	9-976103	9.532853	101467147	10,023897	10.491044	10
5.0	9.509396	9-976060	9 535266	10.456734	10.023940	10.490674	197
52		9.976017	9.533679	40.466321	10.023983	10.490304	8
53	9-610005	9.975974	9.534092		10.024026		7
54	9.510484	0.97.5910	9:534504		10.024070		6.4
55	9.510803	9.975887	9.554916	10.465084	10.034413		3
56	9-5-11-72	9-975844	9,535328	10:464672	10.024156	0.488818	
	9 511540			10.464161		0.488460	4 15
	9-511907					0.488093	8
59 60 -			9:53656:	10 463439		0-487725	2
				10.463028		0.487398	0
35	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secant	26
			23.3	heureen			

M   Sine   Co-sine,   Tang.   Co-tang.   Secant   Co-sec.   1				19.1	bigrees.			
1	1 ×	Sine	Co-sine.	Tang:	Co-tang.	Secant	Co-sec.	A.
1	0	0.513642	9.07.5670	9.536971	10.463025	10,024330	10.457348	60
0.514741 0.975479 9:538002 10454748 10.024468 10.285629 57	I				10:462618			59
0   0   0   0   0   0   0   0   0   0	_							
0		Real Property and the Control of the					THE RESERVE AND ADDRESS OF THE PERSON NAMED IN COLUMN 1	
0		Market Control			Marie Control	The second second	STATE OF THE PARTY	
9		Contract of the Contract of th		THE RESERVE TO STATE OF THE PARTY OF THE PAR	MEDICAL PROPERTY.			
0	17	9.515202	9-975365	0-539837	10 469163	10.024935	10.484791	
1			Management of the Parket of th	CORPORATION CO.	BETTER E-COLE.C.			
### 9-516667 9-971439 9-541408 10-46571 10-02181 10-48534] ### 12 9-517020 9-9714419 514876 10-48512 10-02180 10-48260 ab 17 17 517020 9-971419 9-517020 10-48713 10-02180 10-482618 47 14 9-517745 0-971470 9-517020 10-48713 10-48713 40-47027 10-517020 10-48713 10-48713 40-47027 10-517020 10-48713 10-48713 40 10-45690 10-001407 10-48713 40 17 9-51868 9-974480 9-514320 10-45690 10-001407 10-48713 40 17 9-518010 9-514320 10-45690 10-001407 10-48713 40 18 9-51917 9-974780 9-544320 10-45690 10-001407 10-48713 40 18 9-51917 9-574720 9-545130 10-45640 10-001407 10-48713 40 18 9-51917 9-574720 9-545130 10-45640 10-001407 10-48713 40 18 9-51917 9-574720 9-545130 10-45640 10-001407 10-48713 40 18 9-51917 9-574720 9-545130 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-001407 10-48713 10-45640 10-47910 37 10-45640 10-47910 9-546713 10-45650 10-001540 10-47910 37 10-45640 10-47910 9-546713 10-45650 10-001540 10-47910 37 10-45640 10-47910 9-546713 10-45650 10-001540 10-47910 37 10-45640 10-47910 9-546713 10-45650 10-001540 10-47910 37 10-45640 10-47910 9-546713 10-45650 10-001540 10-47910 37 10-47910 37 10-47910 9-546713 10-45650 10-001540 10-47910 37 10-47910 37 10-47910 9-546713 10-45650 10-001540 10-47910 37		The second second	Maria Divisions			THE REAL PROPERTY.	CONTRACTOR AND ADDRESS OF THE PARTY OF THE P	
12 9-51720 9-07514-0-9-51751 10457719 10.021879 10.482818 47 14 9-517745 9-973057 9-512081 10457719 10.021879 10.482818 47 15 9-51807 9-973057 9-512081 10457719 10.021873 10.482818 45 15 9-51807 9-97407 9-512081 10-45690 10.02187 10-481593 45 16 9-51809 9-97487 9-512081 10-45690 10.02187 10-481593 45 17 9-51889 9-97487 9-514091 10-45690 10-02187 10-481593 45 18 9-51919 9-97487 9-514519 10-45690 10-021812 10-481610 42 19 9-51951 9-97487 9-514519 10-45691 10-021812 10-481610 42 10 9-51051 9-97487 9-514519 10-45691 10-02182 10-481610 42 11 9-51051 9-97487 9-514519 10-45487 10-02182 10-481610 42 12 9-51051 9-97487 9-514519 10-45487 10-02182 10-48081 40-487910 39 12 9-510991 9-97487 9-514518 10-45487 10-02182 10-479119 39 13 9-510991 9-97487 9-514518 10-45487 10-02182 10-479119 38 14 9-510990 9-97487 9-514518 10-45487 10-02182 10-479119 38 15 9-510990 9-97487 9-514713 10-45488 10-02182 10-479119 38 15 9-510990 9-97487 9-514713 10-45186 10-02182 10-479119 38 15 9-510990 9-97487 9-514713 10-45186 10-02182 10-479119 38 16 9-510990 9-97487 9-514713 10-45186 10-02187 10-479119 36 17 9-51009 9-97487 9-514713 10-45186 10-02187 10-479119 36 18 9-51099 9-74487 9-514713 10-45186 10-02187 10-479119 36 19 9-51098 9-97448 9-514943 10-45185 10-02187 10-477919 35 19 9-51108 9-97448 9-514949 10-45085 10-02187 10-477919 35 10 9-51108 9-97448 9-514949 10-45085 10-02187 10-477919 32 11 9-51108 9-97448 9-514949 10-45085 10-02187 10-477919 32 11 9-51108 9-97448 9-514949 10-45085 10-02187 10-477919 32 11 9-51108 9-97448 9-514918 10-45085 10-02187 10-477919 32 11 9-51108 9-97448 9-514918 10-45085 10-02187 10-477919 32 11 9-51108 9-97448 9-514918 10-45085 10-02187 10-477919 32 12 9-51108 9-97448 9-514918 10-45085 10-02187 10-47789 32 14 9-51108 9-97448 9-514918 10-45085 10-02187 10-47789 32 15 9-5185 9-97447 9-51978 10-45084 10-02187 10-47789 32 15 9-5185 9-97447 9-51978 10-44784 10-02187 10-47789 32 17 9-5185 9-97487 9-51878 10-44784 10-02187 10-47789 32 18 9-5185 9-97789 9-51879 10-4488 10-02187 10-47789 32 19 9-51879 9-9788 9-55073 10-4			THE RESERVE AND THE		-		The second	
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15		9.530990	9.97,4859			DECEMBER AND APPLICATION OF STREET	10.479010	37
16 9.521066 9.974525 9.547540 10.452637 10.025541 10.477954 34 18 9.52151 9.0477451 9.547451 10.452637 10.025564 10.477552 32 18 9.523751 9.047436 9.545345 10.451651 10.025564 10.477650 32 19.523153 9.074374 9.540740 10.450551 10.025569 10.476505 32 19.523153 9.074374 9.540740 10.450551 10.025569 10.476505 32 19.523495 9.074374 9.540740 10.450551 10.025569 10.476505 32 19.523405 9.074374 9.540740 10.450551 10.025653 10.476505 32 19.524504 9.974177 9.549951 10.450049 10.025653 10.476505 32 19.524504 9.974177 9.550753 10.445245 10.0255743 10.477540 25 15 9.52573 9.974172 9.550753 10.445245 10.0255743 10.477540 25 15 9.52573 9.974172 9.550753 10.445245 10.025574 10.4774570 24 15 9.52573 9.974172 9.550553 10.445245 10.025673 10.4774570 24 15 9.52573 9.974072 9.555553 10.445245 10.025673 10.4774570 24 15 9.52573 9.971679 9.55573 10.445245 10.02593 10.4774570 24 15 9.52573 9.971679 9.55573 10.445245 10.02593 10.4774570 24 15 9.52573 9.971679 9.555553 10.445245 10.02593 10.4774570 24 15 9.52573 9.971679 9.55573 10.447240 10.025053 10.4774570 24 15 9.52573 9.971679 9.55573 10.447240 10.025053 10.477360 12 12 12 12 12 12 12 12 12 12 12 12 12		The second second		CONTRACTOR OF THE PARTY OF THE				
17 9.522424 9.974481 9.547443 10.452037 10.025504 10.477576 31 28 9.523781 9.974391 9.548347 10.451851 10.025504 10.477576 31 29 9.523495 9.974347 9.549440 10.450351 10.025503 10.477505 32 31 9.523832 9.974301 9.549501 10.450450 10.025633 10.477505 32 32 9.524208 9.974377 9.549951 10.450450 10.025633 10.4756248 29 32 9.524208 9.97437 9.550353 10.449648 10.025733 10.475792 28 33 9.524504 9.974677 9.550353 10.449648 10.025833 10.475638 29 34 9.524920 9.974677 9.550353 10.449648 10.025833 10.475830 25 35 9.525259 9.974677 9.555531 10.448348 10.025833 10.475820 25 36 9.525259 9.974679 9.555531 10.448348 10.025833 10.475820 25 37 9.525259 9.974679 9.555531 10.448348 10.025833 10.475800 25 38 9.30339 9.971687 9.55531 10.447840 10.025033 10.473601 21 39 9.52659 9.973879 9.552351 10.447840 10.025053 10.473601 21 40 9.52525 9.973807 9.553348 10.447840 10.025053 10.473661 21 40 9.52525 9.973807 9.553348 10.447840 10.025053 10.473641 21 42 9.528458 9.973761 9.554344 10.445651 10.025633 10.472600 19 42 9.52850 9.973807 9.553348 10.448641 10.025633 10.471247 18 43 9.52850 9.973807 9.553348 10.446451 10.025633 10.471247 18 44 9.528458 9.973761 9.555530 10.447840 10.025633 10.471247 18 45 9.52850 9.973807 9.555530 10.444861 10.025633 10.471247 18 46 9.528458 9.973764 9.555530 10.444861 10.025633 10.471247 18 47 9.528510 9.973807 9.555530 10.444861 10.025633 10.471247 18 48 9.52850 9.973844 9.555530 10.444861 10.025633 10.471247 18 49 9.52850 9.973844 9.555530 10.444861 10.025633 10.471247 18 49 9.52850 9.973844 9.555530 10.444861 10.025633 10.471247 18 49 9.52850 9.973844 9.555530 10.444861 10.025633 10.471247 18 49 9.52850 9.973849 9.555533 10.444867 10.025646 10.470487 13 40 9.52850 9.973344 9.555530 10.444807 10.025646 10.470487 13 40 9.530849 9.973849 9.55073 10.442879 10.025646 10.470487 13 40 9.530849 9.973849 9.55073 10.442879 10.025648 10.468735 8 4 9.53086 9.973344 9.550707 10.442879 10.025646 10.46873 8 5 9.53086 9.973344 9.550000 10.442879 10.025648 10.46873 8 5 9.53080 9.973144 9.55900 10.442897 10.025648 10.46873								
18							Company of the Compan	
29		Difference of the last of the		Delivery of the last of the la				120
1	24	The second second	TATION AND ADDRESS OF THE PARTY			CONTRACTOR OF THE PARTY OF THE	10.476862	31
2	30	9-523495	9-974347	9-549140	10-450851	10,025653	10.476505	3>
3	31	9-523852	9.974301	9-549 550	10:450450	10.025698	10.476148	20
14   9.524920   9.974674   9.550752   10.445248   10.025873   10.475080   25   10.925873   10.475080   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475702   25   10.925873   10.475861   22   10.925873   10.475861   22   10.925873   10.475861   22   10.925873   10.475862   20   10.925873   10.475862   20   10.925873   10.475862   20   10.925873   10.475862   20   10.925873   10.475862   20   10.925873   10.475862   20   10.925873   10.475862   20   10.925873   10.475862   20   10.925873   10.475862   10.925873   10.475862   10.925873   10.475862   10.925873   10.475862   10.925873   10.475		NAME AND ADDRESS OF	ESSECTION SERVICE			NOT THE REAL PROPERTY.	CONTRACTOR AND ADDRESS OF THE PARTY OF THE P	
			THE RESERVE TO SHARE THE PARTY OF THE PARTY					
16			CONTRACTOR OF THE PERSON NAMED IN			THE RESIDENCE OF THE PARTY OF T		
1		Marie Company of the						
39 9-\$36593 9-97387 9-\$51749 10.44730 10.026058 10.471307 21 40 9-\$27050 9-97387 9-\$51749 10.447891 10.026103 10.472600 19 41 9-\$27753 9-973807 9-\$53348 10.448481 10.026193 10.472600 19 42 9-\$28505 9-973761 9-\$554344 10.44861 10.026193 10.472600 19 43 9-\$28505 9-973710 9-\$554344 10.445850 10.026193 10.472600 19 44 9-\$28505 9-973710 9-\$554344 10.445801 10.026284 10.471391 10.447869 10.026284 10.471391 10.457210 10.026284 10.471391 10.457210 10.026284 10.471391 10.471391 10.026284 10.471391 10.471391 10.026284 10.471391 10.470839 14 47 9-\$29513 9-97380 9-\$55535 10.444861 10.026375 10.470839 14 48 9-\$29504 9-97380 9-\$55535 10.444861 10.026375 10.470839 14 49 9-\$30015 9-97380 9-\$55753 10.444861 10.026420 10.470487 13 49 9-\$30015 9-97380 9-\$55753 10.444867 10.026420 10.470487 13 49 9-\$30015 9-973380 9-\$55753 10.444879 10.026520 10.469785 11 51 9-\$30015 9-\$7338 9-\$55753 10.442879 10.026556 10.459435 10 51 9-\$30015 9-\$7338 9-\$55753 10.442879 10.026556 10.459435 10 51 9-\$30015 9-\$7338 9-\$55753 10.442879 10.026648 10.465785 11 51 9-\$30015 9-\$7338 9-\$55763 10.442879 10.026648 10.465785 10 51 9-\$30015 9-\$7338 9-\$55763 10.442879 10.026648 10.465985 9 52 9-\$33009 9-\$73189 9-\$55907 10.44287 10.026648 10.465735 8 52 9-\$33509 9-\$73189 9-\$5907 10.44289 10.026681 10.465805 6 53 9-\$33509 9-\$73189 9-\$5907 10.44090 10.026681 10.46788 5 53 9-\$33509 9-\$73189 9-\$5907 10.44090 10.026881 10.46788 5 53 9-\$33509 9-\$73189 9-\$5907 10.44090 10.026881 10.46788 5 54 9-\$3369 9-\$73189 9-\$5907 10.44090 10.026881 10.46788 5 55 9-\$33700 9-\$73189 9-\$5907 10.44090 10.026881 10.46788 5 56 9-\$33700 9-\$73189 9-\$50079 10.44090 10.026881 10.46788 12 59 9-\$33700 9-\$73189 9-\$50079 10.44090 10.026881 10.46788 12 59 9-\$33700 9-\$73189 9-\$50079 10.44090 10.026881 10.46788 12 59 9-\$33700 9-\$73189 9-\$50079 10.44090 10.026881 10.46788 12 59 9-\$33700 9-\$73189 9-\$50079 10.44090 10.026881 10.46788 12 59 9-\$33700 9-\$73189 9-\$50079 10.44090 10.026881 10.46788 12 59 9-\$33700 9-\$73189 9-\$50079 10.44090 10.40090 10.46600 10.46600 10.46600 10.46600 10.46600 10.46600 10.466	100			LOSS CONTRACTORS			THE RESERVE OF THE PERSON NAMED IN	
40			9-971987	9-552351		The second second		
## 9.527.400 0.973852 0.53348 10.446452 10.026193 10.472600 19 9.52753 0.973807 9.533946 10.446452 10.026193 10.472600 19 9.528505 9.973761 9.554741 10.44550 10.026193 10.472693 17 4 9.528505 9.973761 9.554741 10.44550 10.02623 10.471543 17 4 9.528510 9.973671 9.55573 10.444861 10.02623 10.471543 17 4 9.529513 9.97363 9.55530 10.444861 10.02637 10.470839 14 17 9.529513 9.97383 9.55531 10.444861 10.02637 10.470839 14 17 9.529513 9.97383 9.55531 10.444861 10.02637 10.47083 14 17 9.529513 9.97383 9.55531 10.44387 10.02642 10.470487 13 10.930815 9.973489 9.555725 10.443871 10.02642 10.470487 13 10.930815 9.973444 4.557121 10.44287 10.02645 10.45047 17 18 11 19 9.530815 9.973444 4.557121 10.44287 10.02656 10.45043 11 10.46591 10.46573 11 10.4508	39					The second secon		
41 9.528505 9.973760 9.5533940 10.44850 10.026193 10.471247 18 41 9.528505 9.973760 9.554741 10.44550 10.026284 10.471247 17 42 9.528505 9.973760 9.554741 10.44550 10.026284 10.471592 17 43 9.528510 9.973671 9.555530 10.444850 10.026284 10.471592 15 46 9.529161 9.973623 9.555530 10.444850 10.026375 10.470839 14 47 9.529512 9.973889 9.555531 10.444850 10.026375 10.470839 14 48 9.529864 9.973523 9.555913 10.444851 10.026375 10.470839 14 49 9.530845 9.973489 9.555725 10.443267 10.026465 10.470487 13 49 9.530865 9.973444 4.557121 10.442879 10.026566 10.459425 10 41 9.530865 9.973444 4.557121 10.442879 10.026566 10.459425 10 41 9.530865 9.973444 9.557121 10.442879 10.026566 10.459425 10 41 9.531265 9.973369 9.557597 10.442879 10.026648 10.465943 10 41 9.531646 9.97307 9.558708 10.441892 10.026648 10.468735 8 41 9.53164 9.97307 9.558708 10.441892 10.026683 10.468735 8 41 9.53166 9.97316 9.558708 10.441892 10.026683 10.46873 8 42 9.53266 9.97316 9.558708 10.44199 10.026851 10.46788 5 43 9.53266 9.97316 9.55949 10.44090 10.026851 10.46788 5 44 9.53164 9.97307 9.55969 10.44090 10.026851 10.46783 4 45 9.53266 9.97316 9.55949 10.44090 10.026851 10.46788 5 45 9.533009 9.973144 9.55900 10.44090 10.026851 10.46788 5 45 9.533009 9.973144 9.55900 10.44090 10.026851 10.46788 5 45 9.533009 9.973144 9.55900 10.44090 10.026851 10.46788 5 45 9.533009 9.973144 9.55900 10.44090 10.026851 10.46788 5 45 9.533009 9.973144 9.55900 10.44090 10.46091 10.46004 10.460		-		-		-		=
41 9.528458 9.973710 9.554344 50.445650 10.026239 10.471892 17 44 9.528458 9.973710 9.554741 10.45239 10.026286 10.071542 16 45 9.52850 9.973671 9.555730 10.444861 10.026375 10.471190 15 46 9.52961 9.97362 9.555530 16.444466 10.026375 10.470839 14 47 9.52951 9.973580 9.55530 16.444466 10.026375 10.470839 14 48 9.53951 9.973489 9.556725 10.443671 10.026420 10.470487 13 9.53021 9.973489 9.556725 10.443871 10.02645 10.470487 11 50 9.53021 9.973484 9.55711 10.443871 10.02651 10.465785 11 1 9.53021 9.97388 9.557517 10.442483 10.026628 10.469785 11 2 9.531265 9.973444 9.55711 10.442483 10.026628 10.469785 10 1 9.53031 9.97389 9.55793 10.44283 10.026648 10.468735 8 1 9.53164 9.97397 9.558308 10.44189 10.026698 10.468735 8 2 9.53164 9.97381 9.55997 10.44090 10.026569 10.46837 6 2 9.53266 9.97316 9.55849 10.44090 10.02655 10.46837 6 3 9.53266 9.97316 9.55949 10.44090 10.02655 10.46768 5 57 9.53300 9.97318 9.55997 10.44090 10.02655 10.46768 5 58 9.53370 9.97308 9.50073 10.44097 10.02685 10.46768 12 58 9.53370 9.97308 9.50073 10.44393 10.02685 10.46768 12 59 9.53370 9.97308 9.50079 10.43971 10.02698 10.46094 12 59 9.53370 9.97308 9.50073 10.43932 10.02688 10.46094 12 59 9.53370 9.97308 9.50073 10.43932 10.02688 10.46094 12 59 9.53370 9.97308 9.50073 10.43932 10.02688 10.46094 12 59 9.53370 9.97308 9.50073 10.43932 10.02688 10.46094 12 59 9.53370 9.97308 9.50073 10.43932 10.02688 10.46094 12 59 9.53370 9.97308 9.50073 10.43932 10.02688 10.46094 12 59 9.53370 9.97308 9.50073 10.43932 10.02688 10.46094 12 50 9.53408 9.97308 9.50073 10.43932 10.02688 10.46094 12 50 9.53408 9.97308 9.50073 10.43932 10.02688 10.46094 12 50 9.53408 9.97308 9.50073 10.43932 10.02688 10.46094 12 50 9.53408 9.97308 9.50073 10.43932 10.02688 10.46094 12 50 9.53408 9.97308 9.50073 10.43932 10.02688 10.46094 12 50 9.53408 9.97308 9.50073 10.43932 10.02688 10.46094 12 50 9.53408 9.97308 9.50073 10.43893 10.02688 10.46094 12 50 9.53408 9.97308 9.50074 10.46094 12 50 9.53408 9.9008 9.5008 9.5008 9.5008 9.5008 9.5008 9.5008 9.5008 9.5008 9.5008 9.5008 9.5			SHIP COMPANY TO SHIP	SUBSECULAR STATE OF THE PARTY O		DESCRIPTION OF THE PERSON AND PER	STREET, SAME PARKET	I TOTAL STREET
44 9.528458 9.973716 9.554741 10.445239 10.426284 10.471592 15 46 9.528310 9.973671 9.555539 10.444861 10.028332 10.471592 15 46 9.529361 9.97362 9.555538 10.444861 10.028373 10.471592 14 47 9.529513 9.97380 9.555933 10.444861 10.028373 10.470839 14 48 9.53026 9.973489 9.556725 10.443671 10.026420 10.47083 13 49 9.53026 9.973489 9.556725 10.443671 10.026421 10.466785 12 50 9.53026 9.973484 9.55721 10.442879 10.02655 10.469785 12 51 9.53026 9.97338 9.557571 10.442879 10.02663 10.469785 12 51 9.53026 9.97338 9.557571 10.442879 10.02663 10.469785 12 51 9.53026 9.97336 9.55898 10.44189 10.02663 10.46873 8 51 9.531614 9.97390 9.55898 10.44189 10.02663 10.46873 8 51 9.531614 9.97397 9.558997 10.44287 10.02663 10.46873 8 52 9.53266 9.97316 9.559997 10.44090 10.02663 10.467688 5 53 9.53266 9.97318 9.559097 10.44090 10.02683 10.467688 5 54 9.53369 9.97318 9.559097 10.44090 10.02683 10.467688 5 55 9.53369 9.97318 9.559097 10.44090 10.02683 10.467688 5 57 9.53369 9.97318 9.559097 10.44090 10.02683 10.467688 5 58 9.53370 9.97318 9.50007 10.44037 10.02698 10.46768 12 59 9.53370 9.97318 9.50007 10.44037 10.02698 10.46769 1 59 9.53370 9.97308 9.00007 10.44037 10.02698 10.46769 1 50 9.53403 9.97308 9.50007 10.44037 10.02698 10.46769 1								
65 9.523810 9.973671 9.555839 10.444861 10.028329 10.471190 15 47 9.529311 9.973625 9.555330 10.444861 10.028373 10.470839 14 17 9.529513 9.97368 9.555330 10.444067 10.026420 10.470839 14 18 18 9.530215 9.973535 9.55032 10.443671 10.026420 10.47083 13 19 9.530265 9.973444 9.557821 10.443671 10.02655 10.46978 11 10.45878 11 10.45738 11 10.45			THE REAL PROPERTY.					100.00
47			9.971671				10.471190	15
88   9.839864   9.973835   9.565735   10.443871   10.026465   10.470136   12     10   9.830345   9.973444   9.557731   10.443879   10.026556   10.469785   11     11   9.830345   9.973344   9.557737   10.443879   10.026655   10.456435   10     12   9.831365   9.973383   9.557537   10.443879   10.026643   10.468735   10     13   9.831364   9.97397   9.558308   10.441893   10.026643   10.468735   10     14   9.831364   9.97397   9.558308   10.441893   10.026643   10.468735   10.468735   10     15   9.83256   9.973315   9.559097   10.46909   10.26585   10.467688   5     16   9.83266   9.973169   9.55949   10.44090   10.02663   10.467839   4     17   9.833009   9.973144   9.559097   10.440309   10.026578   10.467688   5     18   9.83266   9.973078   9.56073   10.44015   10.02698   10.460901	16	9.529161	THE RESERVE OF THE PERSON NAMED IN COLUMN 1	Manager Street, Square, Square				
9 9-530545 9-973444 9-557121 10.441879 10.026556 10.459425 10 1  9 9-530545 9-973444 9-557121 10.441879 10.026556 10.459425 10 1  11 9-530545 9-973352 9-557517 10.441879 10.026648 10.459425 10 1  12 9-531265 9-973352 9-557973 10.441893 10.026648 10.468735 9  13 9-531264 9-973079 9-558308 10.441893 10.026648 10.468735 9  14 9-531264 9-973079 9-558308 10.441893 10.026648 10.468337 6  15 9-531264 9-973159 9-559097 10.440903 10.026785 10.467888 5  16 9-532667 9-973149 9-559097 10.440903 10.026785 10.467888 5  17 9-533009 9-973144 9-559097 10.440903 10.026531 10.467339 4  18 9-533704 9-973078 9-500279 10.44015 10.02693 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.926878 10.460903 10.460903 10.926878 10.460903 10.4	147	DESCRIPTION OF STREET	THE RESIDENCE OF THE PERSON NAMED IN	SCOT WAY SHOWING				100000
\$\begin{array}{c} 9.530\cdot \\ 9.673\cdot 44 \\ \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		The second second		NAME AND POST OFFICE ADDRESS OF				
\$\\ \\ 9.\\$309\\$\\ 9.\\$733\\\ 8\\ 9.\\$733\\\\ 9.\\$733\\\\ 8\\ 9.\\$733\\\\ 9.\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	100	9.530664	10064000000000			MILLS OF BUILDING		100001
\$\\ \begin{array}{cccccccccccccccccccccccccccccccccccc	1	0.620034	-		-		Witness Street	0
\$6 9.53266 9.973214 9.559997 10.440903 10.02678; 10.467688 5 9.532666 9.973169 9.55949 10.440909 10.026831 10.467339 4 9.533009 9.973124 9.55988 10.44015 10.026831 10.465991 1 8 9.53374 9.973078 9.500279 10.439721 10.026988 10.46643 2 9 9.53374 9.973032 9.360673 10.439327 10.026988 10.466496 1 9 9.534032 9.973986 9.501066 10.418934 10.037014 10.465496 0	6	9.511264	9.973342	9.557913	10.447087	10.026648	10.468715	8
\$6 9.53266 9.973214 9.559997 10.440903 10.02678; 10.467688 5 9.532666 9.973169 9.55949 10.440909 10.026831 10.467339 4 9.533009 9.973124 9.55988 10.44015 10.026831 10.465991 1 8 9.53374 9.973078 9.500279 10.439721 10.026988 10.46643 2 9 9.53374 9.973032 9.360673 10.439327 10.026988 10.466496 1 9 9.534032 9.973986 9.501066 10.418934 10.037014 10.465496 0	155	9.531614	9-973309			10.016693		71
	154	9-531963	9.973481	9.558701	10.441198			_
	55				10.540903			
	150				10-110-109			
	58		9.973078					
	159			9.560673	10.439327		10.456196	21
	60				10,418934	10.017014		0
		Co-sine	Sine.	Co-taug.	Tang.	Co-sec	Becaut.	1 11

20 Degrees.

	Sine:	Co-sine.	Tang.	Co-tang	Secant	Co-sec	100
-							M
0	9.534052	9:972986	9.561066	10.438934	10.027014	10 405945	60
	9-534399	9-97=940	9.561459	10.438541	10.027060	1046;601	59
3.3	9-534745	9.971894	9.562244	10.438149	10.027100	10.484144	58
3	9-535092	9.971502	0.562636	10.437364	10-017198	10.464903	57
2	9.535438	9-972755	9 563028	10.436972	10/027245	10/464317	150
5	9.535129	9.972709	0.503419	10.436681	10.027291	10.46 1871	55
2	9.539474	9,922663	0.563811	10.436189	10.027337	10.46 7516	24
É	9.536818	9.972617	9.564202	10.435798	40,027383	10.463 : 82	17
0	9.537163	9.972570	9.564592	10435408	20.027430	10.462837	51
10	9:437507	0.072524	9.564983	10.435017	10.017476	10.460493	50
12	9.537851	9 972478	9.565373	10.434627	10:027522	10.452140	
12	9.538194	9.972431	9.565763	10.434237	10/027560	10.461806	48
13	9.538438	9.972385	9.566153	10.433847	10.027615	10.451462	47
16	9.538880	9.97±338	9.500541	10.433458	ED.017661	10.451110	器
15	9.539223	9.971201	9.566932	10.433068	10.027709	10.460777	28
16	9.539565	9.972245	9.567320	10.431680	10.027755	10,460435	26
17	0.539907	9.972198	9.567709	10.432291	10.027802	20.860003	43
18	9.540149	9.972151	9.568098	10 431902	10.017840	10.459751	42
19	9.540590	9.972105	4.568486	10.431514	10.017895	10419410	41
20	9-540931	9.972058	9.568873	10.431127	10.027942	10.459069	40
21	9.541271	91971011	9-569261	10.430719	10.017080	10.4(8728	
22	0.441613	9.971964	9.569648	10 430352	10.018016	10.448187	39
23	9.54/953	9.971917	9.570035	10.429965	10:018081	10.458047	
24	9:542293	9.971870	9.570432	10:429578	10.025110	10457707	#
25	9.541652	9.971823	9.970809	10.429191	10.018171	10.457368	67
26	9.542971	9.971776	9.571195	10.4 18805	101028222	10.417019	(1)
27	9.543310	9.971729	9.571581	10.428419	10.028271	10.4(5690	33
18	9.543649	9.971682	9.571967	10.428011	10.028318	10415341	32
29	9-543987	9 97 1635	9.572352	10.427648	10.018365	10.456013	21
30	9.544325	9-971588	9.572738	10.427262	10.018412	10.455673	10
31	9.544663	9.971540	9.573123	10.426877	10.018450	10.455337	20
32	9.545000	9/971493	9.573507	10.426493	10.018407	10.455000	100
33	9-545338	9.971446	9.573892	10 426108	10.038554	10.454662	27
34	9.545674	9.971198	9.574276	10.425724	10.018602	10.454116	20
35	9.546011	9.971351	9.574660	10.425340	10,018649	10.453980	25
36	9.546347	9.971303	9.575044	10.424956	10.018697	10.453653	24
37	9.546683	9.971256	9.575427	10.424573	10.018744	10-453117	10
38	9.547019	9-971208	9.575810	10.424190	10.038791	10.453981	22
39	9-547354	9.971161	9.575193	10.423807	10.028839	10.452646	21
40	9.547689	9.971113	9.576576	10.423424	10.028837	10.457516	20
41	9.548024	9.971066	9.576958	10.421042	10.028934	10.451076	70
123	The second secon	9.971018	9-577341	10.422650	10.018982		
43	CONTRACTOR OF THE PARTY OF THE	9.970970	9.577723	10.422277	10.029030		100
44		CONTRACTOR OF THE PARTY OF THE	9.578104	10.421896		10.450073	Brill.
43			9.578486	10.421514	10.039136	10.450640	21
46	9.549693	9.970827	9.578867	10.421133	10.019173	10.450707	mes.
47	9.550026	9.970779	9.579248	10.420752	10.029111	10.449974	
48			9.579629	10.420371	10.029269	10-449541	162
49		9.970683	9.580009	10.419991		10-449308	41
50	9.551024	9.970635	9.580389	10.419611	10.029365	10.448976	10
158	9.551356	9.970586	9.580769	10.419231	10.029414	10.448644	9
52			9.581149	10,418851	10.029462		- 8
53	9.552018	9.470490	9.581528	10.418472	10.029510	10 447982	71
54	9 552349	9.970442	9.581907	10.418093	10.029 958	10 447651	6
55	9.552680	9-970394	9.582286	10.4177 4	10.024505	10.14" 120	- 5
56	9.553010	9.970345	9.582665		10.029655		4
57	9.553341	9.970297	9.583043	19 4169571	10,029703	10-146-59	3
58	9.553070	9.970249			10,029751		E
		9.970200			10.034800		1
_		9.970152	-	10/21/253	10.029848	-	P
25 4	Co-sine.	Sing.	Co-tang	Tank -	60-16-	Sechit	BC L
			- 60 0	exters.	Section 1		-

				ruckaces.			
1-15	Sine-	Co-sine	Tang-	Co-tang.	Secant	Co-sec.	26.1
100	_	_		-		1	-
9	9 554379	9.970152	9.584177	10.415823	10.009848	10.445671	60
1 3	9.554658	9.970101	9-584555	10.415445	10.029897	10.445347	59
2	0.554987	9.970055	9-584912	10-41 (068	10/020045	10:445013	58
3	9.555315	- 97000b	9-585309	10 414691	1D.019994	10.444585	57
_			9 58 5686	10-414714	10.030043	Marie Contract of the Contract	
- 9	9.555643	9-309957				10:444357	56
5	9-555971	9 900909	9.586062	10.413933	10.030091	10.444019	15
0	9.556109	9.969880	0.586439	10.413561	10.030140	10:443701	54
7	9.556616	9.969811	9.586815	10.4131 5	10.010189	10.443374	5.1
8	9-556953	9 959763	0.537840	10.412810	(0.010238	10.443047	52 4
1 9	9-557280	9.969714	9.587566	10-612434	10 030286	10 443730	SI
10		9.969665	9.587941	10-412050	ALTERNATION AND ADDRESS OF		
	A-221000	4.003002		170917500	10,030335	10-442394	50
111	0.557932	9.969616	9.588316	10-411584	10,030384	10.442068	49
12	01558258	9.959567	9.588691	10.411309	10.030433	10.441743	48
13	9.558583	9.909518	9.589000	10.410934	10,030482	10.441417	47
14							
1000	9.554909	9.969469	9-589440	10.410560	10.030531	10.441091	45
1 15	9.559234	9.969420	9.589814	10.410186	10.030580	10-440766	45.
10	9.559558	9-969370	9.590188	10,409812	10.030630	10-14044=	44
17	9.559883	9.969321	9-590562	10,409438	10.030679	10-140117	43
13	9.560207	9 969272	9-590935	10.409066	10.030728	10.419793	42
19	9.560531	9.909223	9.591308	10.408692	10,030277	10.419469	41
20	G 10 10 10 10 10 10 10 10 10 10 10 10 10		9.501081	10.408319		MICHIGAN CONTRACTOR	
200	9,560855	9.909173	412/11/04/	10,400319	10.030827	10.439145	40
21	9.561178	9.969124	9.592054	10,407946	10,030876	10.438832	39
22			9.592426	10,407574	10,030924	10.438499	38
23	FEBRUARIS (BID		9.592798	10,407 103	10.030075	10.438176	37
12				The second second			
	9.562146		9.593171	10,406839	10.031024	10.457854	35
25	9.562468		Contract Con	10.406458	10.031074	10-437532	35
2.0	9 56 2799		9 593914	10,406086	10,031123	10-437210	34
27	9.563112	9.068827	9.594285	10,405715	10.031173	10.436888	33
23	9.563433	9.968777	9.594656	10.405344	10,031223	10.436567	32
20		9.968728	9.595027	10.404973	10.031272	10.436245	10
			Marine Street, Square,		IN THE OWNER	DESCRIPTION OF THE PARTY OF THE	_
134	9.564075	9.968678	9.595398	10,404601	10,031322	10.435935	30
31	9.564396	9.968528	9.595768	10.404232	10.031373	10.435604	29
32	9 5647 16	9.968578	9.596138	10.401862	10.031422	10-435484	28
			9 596508	10.403492	10.031472		27
23	9.50(016			The second second second	THE RESERVE THE PARTY OF THE PA	10.434904	
1 23	9.565356	9.968479	9.596878	10.403122	10.031521	10.434644	20
3.5	9-565676	9.958429	9-597247	10.402753	10.031571	10-434324	25
36	9.565995	9.968379	9.597616	10.402384	10.031521	10.414065	24
37		9.968329	9.597985	10.401015	10.031671	10.433686	23
38		9.968278	9.598354	10.401646	10.031722	10.433368	22
				The second secon			31
39	9.500951	1000	9.598722	10.401178	10.031772	10.433049	
Target.	9-567269	9.968178	9.509001	10.400900	10.0312873	10.432731	20
4 41	9-557587	9.968128	9-599459	10.400541	10.031871	10.432413	19 .
42	9.507904	The second second		10.400 Mg	10.031911	10.432096	18
43		9.968027	I DOING BE SEED TO SEE	DESCRIPTION OF STREET			17
			9.600194		10.031973	10.431778	
44			9.600560		10.032023	10.431461	10
45		9.967927	9.600929		10.032073	10.431144	115
46	9.509173	9 967876	9.601096	10.398704	10.032124	10-430828	14
47		9 967826					13
48	THE RESERVE	9.967775	Mark Company	DESIGNATION OF THE PERSON NAMED IN	A STATE OF THE PARTY OF THE PAR		12
49			100000	I STORY OF THE PARTY OF THE PAR		10.429880	11
	11-05-00000000	TOTAL PROPERTY.	I MADE SHOW THE PARTY OF	TOTAL PROPERTY.	CONTRACTOR OF THE PARTY OF THE	The second second second	
150	9-570435	-	9.602761			10,429585	10
151	9-570741	9.967624	9.603127	10.396873	10.032376	10.489349	9
1 62		9.967573			10.032427		9
	10.00	9.967522				10.428620	
1 3	4.37.1300	1919-13-4	65.3030				
24	4 57 1095	9,967471	9.604223			10.42/105	
		9.907421					5
35	9-574323	9.967370	0 004953	10-393047		10.447577	1 4
1 57		9.967319				10 417364	1 2
58		9.957268				10.427050	1 =
		0.967217	9.606046				
59	200	o obvice	50511				
50	/8	9.967166		7 (100)			_
24	Co sine	Sine.	Co-tang	Tang.	Co-sec.	Secant	1 H
Section 1			-	STATE OF THE PERSON NAMED IN			

22 Degrees.

	1		1	22	Degrees.			
1	11	Sine	Co-sine.	Tang	Co-tang.	Secant	Co-sec	2 34
1	75	9 173575	9.967186	0.000410	10.393590	10.032834	10-426425	60
	1	9.573888	9:96711	y 606773	10.39324	10.032885	10.426132	
		9-174200	9.967064		10.393863		10:415800	58
		9.974948	9,96721	0 607500	10.392500		10:41458	57
		9.574884	9.96891 9.968910	A 200	10.39177		10-414864	
1	6	9-57 5447	9.900%50	1 0 00	10.39141	at the second	10-414563	
1	-	9-575758	9.98686	1000	10 39105		10-414242	53
1	13	9.576069	9.900750	The second second	10.39068		10-423931	52
ı		9.570379	9.900709		10.39033		10.423621	
ı	K		9,96665	9.610036	10.38996		10-413311	50
1	3	and the same of th	0.966503	I Complete and the second	10.38950	of processing the contract of	10:423001	49
r	13	THE COLD IN	9.966490			OF THE OWNER, WHEN PARTY AND PARTY AND PARTY AND PARTY AND PARTY.	10.422282	47
1	12		9.966447	A CARL THE PART	10.388520		10.411071	46
1	B	THE RESERVE OF THE PERSON NAMED IN	9 966 399	9.611841	10.388159		10.411764	45
1	10	E BARRON PARAMETERS	9.966344		10.387799	A PERSONAL PROPERTY AND ADDRESS OF THE PERSONAL	10.411455	44
1	12	The second second second	9.966292		10.387439		10,427.147	+3
	It	I STATE OF THE STATE OF	9.966188		10.387070		10,410838	42
1	20	A DESCRIPTION OF THE PARTY OF T	9.966136	9.613041	10.186350	A BESTELLANDON AND A STREET	10.410113	10
1	3	The state of the s	9.96608		10.386000		10.419915	39
1	23	THE RESIDENCE OF	9.900033	A Part of the last	10:385641		10.419508	33
1	23	9.580699	9.965981	9.614718	10.385382	10.034019	10.419501	177.
1	2	The second second	9.965929	4 GOVERNMENT	10.384923	The second second	10.418095	35
I	21	The second second	9.965876		10.38450		10.418688	35
1	27		9.965772	A COLUMN TO SERVICE AND ADDRESS OF THE PARTY	10.384207	The second second	10.418582	31
1	28		9.965720		10.383491		10.417771	52
1	29		9.965668		10.383133	10.034332	10.417465	3.0
1	30	9.588840	9.965615	9.617224	10.382776	10.034385	10.417160	30
1	31	9.583145	9-965563	9.617582	10.382412		10.416855	28
1	32	I SHILL SHARE I	9.965511	9.617939	10.382061		10.416551	28
1	33		9.965458	AND DESCRIPTION OF THE PARTY OF	10.381709		10.416346	27
1	34	The state of the s	9.905406		10 381348		10-415943	25
1	36	The second secon			10.380636		10-415335	4
1	37	9 584968	9.965248	9.619721	10.380279	10.034752	10.415032	23
1	38	And the second second	9.965195	9.620076	10.379924		10.414728	21
1	39		9.965143	9.620787	10.379568		10.414416	21
Į.	40		9-965090	-	10.379213	1	10.414123	
1	41	the second second	9.905037		10.378858	The second second	10.413821	10
1	43	THE RESERVE AND ADDRESS.	0.964931		10.378148		10-413217	27
1		9.587085	9.964879		10.377793		10.412915	16
1	45		9.9648z6	9.622561	10.377439	10.035174	10.412514	33
1	46		1.964773		10.377085	Commission of the last of the	10.412312	24
1	48		.964666		10.376731	EUROSCO CONTRACTOR DE LA CONTRACTOR DE L	10.411711	碧
	49		964613		10.376024	DESCRIPTION OF THE PARTY OF THE	10.411410	42
1	50		964560	A TA	10.375670	CONTRACTOR AND ADDRESS OF	10.411110	30
I	51	9.589190 9	The second second	STREET, SQUARE, OR	10 375317	10.035493	0.410810	0
	52	9,589489 9	964454	9.625036	10,374964	10.035546	0.410511	-3
					10.374612		0.410111	7
	-			9.625741			0.409912	6
		9.590586 9					0.409314	5
	57						0.409016	195
	58	9-591282 9			0,372856	10.035867	0.408718	
	59	91591580 9	964080				0.408435	4000
=			-		-		0.40X122	9
		Co-sine.	Sine.	Co-tang	Tang.	Co-sec-	Secunt	10
		-		67 1	curcest			

				23	Degrees.	1000	-31	
1	15	Sine	Co-sine.	Tang	Co-tang.	Secant.	Co-sec	138
1	0	9.591878	9.964016	9.627852	10.371148	10.035974	10,403122	60
ı	1	9 592176	9.963972	9.618203	10.371797	10.035018	10.407824	59
ı	10	9.592473	9.963919	9.528554	10.171446	10.035081	10.407517	58
ı	3	9-591770	9-963865	9 628905	10.374005	10:010133	10.407310	57
ı	-	9-593007	9.965811	9.629244	10.370745	10.016180	10-401433	56
ı	5	0-591103	9.903757	9.629006	10.570594	AD.OIDEGS	10.406637	\$5
ı	6	4-593059	9-903704	9.629956	10.370044	10.016100	10.406341	54
ı	13	H-598455	0.002500	9.630556	10.369394	10-016404	10.406045	53
П	9	9-594547	DOMESTIC OF THE PARTY OF THE PA	9.631005	10.368995	10,030468	10.405453	51
ı	10	9.594843		0 631355	10.368645	10/036612	10.401168	20
H	Til			9.631704	10.368296	10 036566	10.404863	
ı	12	9-595417	COLUMN TO SERVICE STATE OF THE PARTY OF THE	9.632053	10.367947	10.016621	10.404568	48
ı	13		THE RESERVE OF THE PERSON NAMED IN	9 032401	10.367 (49	10.036614	10.404172	47
ı			MILES CONTRACTOR IN	9 632750	10.367240	10.036729	10:401979	46
ı				9.633098	10.366901	10.035783	10 403685	45
ı	16	9.596609	9.963163	9.633447	10,366553	10.036837	10.403391	44
				0.633795		10.036892	10.403097	43
	_	MINISTER STATES IN	ALC: UNKNOWN BOOK OF THE PARTY	9.634143		10.036946	10.402804	43
			and the same of th	9-634490	DESCRIPTION OF THE PERSON OF T	10.037001	10-402510	41
				9.634838	-	10.037055	10-401217	40
		9.598075		9.635185		10.037110	10.401925	39
	22	9.598368		9.635532	10 364468	10-037164	10.401632	38
ı	23 24	9.598952		9.635226	10-363774	10.037273	10.401045	37
ı	福	9-500344	ELECTRONIC PROPERTY AND ADDRESS OF A	9 636572	10.102418	10-037328	10,4001 (6	35
ı	16			9.636919	10.367081	10.037381	10.400454	34
ı	27			0.637265		10.017428	10.400173	33
ı	48			1.637611	10.361389	0-0374	10.399882	32
ı	20	y (00409)					10-199591	31
ı		y.600700	9.962398 9	638301	10.301698	0.017601	10.399300	30
	III.	6.600990	0.002343 9	03%647	10.361353	0.037657	10.399010	19
			ACCOMMUNICATION IN				10 398720	18
		ADDRESS AND D		ALPERSON STREET			10.398430	27
							10.398140	26
					ESECTATE 191		0.397850	35
	-					1100	0.397272	24 23
	400			DESCRIPTION OF			0.396983	11
	иси в		CONTRACTOR DO				0.396695	21
		601594	961846 9	54474-1	10.358253 1	0.038154	0 396405	20
-	110	603881	9.951791 9	042091	10.357909 1	0.038200	0.396118	19
		1004170	1961735 9	OPERATOR OF THE PERSON NAMED IN	ARREST CONTRACTOR OF THE		0.395830	18
	41 9		ALCOHOL: N				0.395543	17
							0.395255	16
		ADDRESS OF THE PARTY OF THE PAR	ALCOHOLOGICA DA				0.394958	16
		ARTERIOR DE LA CONTRACTOR DE LA CONTRACT					0.394681	14
			STEED STREET GO	9100020-000			0.194194	13
		ARTERIOR AND ADDRESS TO	DESCRIPTION OF THE				0.393821	17
						CONTRACTOR OF THE PARTY OF THE	0 193535	10
8	<b>9</b> 8	.600751 0	-	The second second	the name of the local division in		0.303340	_
		.602015 9			D.354143 I		0.793964	8
		607122 9				0.018877 1		_
	月日	.607507 9	351067 9	646540 1	10.353460	0.018911	0.191191	6
	311	. 60: Sua 9	951011 0			0.018989 1		5
		. 605177 9			MICHAEL COLUMN 100	0 039045 1		41
		1.658461 G				0.039101 8		3
		A58745 9				0.039157 E 0.039214 1		2
		APRILL'S				0.039270 #		76543318
		la-sime.		o-tang		Co-see	Birth .	
	1116	MANUEL I	Sine. 'C	A. rank	THE PARTY OF	or leading to	المستوا	223

		-	24	Degrees	-		_
LM	Sine.	Co-sine.	Tang.	Co-tang.	Secant.	Co-sec.	26
-		0.050000	- 5.8c8-			10 ann68+	60
10	9.609313	9.900730	9.648583	10.351417	10.039270	10.390687	
12	9.600197	9.900674	9.648923	10.351077	10.039326	10.390403	59
2	9.600680	9.950618	9.649203	10.350737	10.039382	10/300120	58
3	9,610164	9.960561	9.649602	10.350398	10.039439	10.389836	37
4	Q:010447	9,960505	9.649942	10.350058	10,039495	10.189553	50
15	9,010719	9.960,448	9,050281	10.349719	10.039552	10.389271	155
5	0 611013	9 960392	9.650620	10.349380	10039608	10.388988	54
	9.611294	9.960335	9.650959	10.349041	10.039665	10 388706	53
14	9.611570	9 960279	9.651297	10.348703	10.039721	10.188434	31
9	9.611858	9.960222	9.651636	10/348364	10.039778	10. 188 142	31
15	The second second	9.960165	9.051974	10.348026	10.019835	10.187860	
	9.613140		-				50
111	9.612421	9.960109	9.651312	10.347688	10.039891	10.387579	49
12	9.612702	9.96005=	9.652650	10.347350	10.039948	10.181398	48
13	9.612983	9.959995	9.652988	10.347012	10.040006	10.387017	47
14	9.613264	9 959938	9.653326	10.346674	19.040061	10/586716	40
115	9.613545	9.959882	9.653663	10.346337	10.040118	10-180445	45
16	9.613825		9.654000	10.346000	10-040175	10.180175	MA.
17	9,614105	9.959768	The second second second	10.345663	10.040232	VOLTS CRUE	45
18		9-959761	9.654674	10.345326	10.040280	10.18 201 5	
19	9.614665	9.959054	9.655011	Control of the last of the las	NAME OF TAXABLE PARTY.	THE RESERVE TO SERVE THE PARTY OF THE PARTY	B-1
			The second second	10.344989	10.040346	10/185335	9/
20	9.614944	2.959596	9.055348	10.344652	10.040404	10.385016	40
21	9.615223	9.959539	9.655684	10.344316	10.040451	10.384111	39-
22	9 615501	94959482	9.656020	10.343980	10.040518	10.584498	郭
23	9.615781	9 959425	9.656356	10. 143644	10.040575	10.384210	17
24	9.616060		9.656692	10. 143308	10.040032	30.18 1040	36
25	9.6:6338	9.959310		10.348972	10.040660	10.381661	15
16	9.616616		9.657364	The second second	10.040747	30.383184	
	The second secon	COLUMN P. P.	ACCUPATION AND ADDRESS.	10.342030	10.040806		LUI I
27	9.016894	9-195			The second second	10,383166	20
	9 017172	9.459138		10.341906	10.040862	10.383839	2
29	9.617450	9.959080	9.028369	10.341631	10,040919	10.382550	31 8
30	9.617727	9:959023	9.658704	10.341296	10:040977	10.382273	製
31	9.618004	9.958965	9.659039	10.340961	10.041035	10 381006	200
32.	9.618281	9-958908	9.659373	10.340027	10.041092	10.081714	3
33	9.618558	9.958850	9.659708	10.340292	10.041100	10.181441	
	9.618834	Deliver and the last of			Section 2 to the last of the l	BERTHAM TO SHARE THE PARTY OF T	20
34		91958792		10.339958	10.041208	10.SELIAN	2.0
36	9.619110	9.958734		10.339624	10.041266	10.350595	热
36	9,619386			10.339290	10.041323	10.380614	24
177	9.619662	9.958619		10.338957	10.041381	10.380338	21
38	9.619938	9-958561	9.661377	10.338623	10.041439	(0.150061	21
39	9.620213	9-958503	9.661710	101338290	10.041497	10.079787	22
140	9.620488	9-958445	9.662043	10.337957	60.D41666	10.579515	20
39 40 41	9.620763	9.958387	9.662376	March Street, Street, St.	10.041613	and the same of	77
172	The second second			10.337624		IC SYNTHY	12.1
42	9.621038	9.958329	9.662709	10.337391	10.041671	10.37Xq112	31
43	9.621313	9.958271	9.555042	10.336958	10.041729	10.378687	17
144	9.621587	9.958213	9.663375	10.336523	10 041787	10.378413	10
45	9.621861	Contract of the last	9.663707	10.336293	101041846	10.378179	15
46	9.622135	9.958096	9.664039	10.335901	10.041904	10.377865	14
47	9.622409	9.958038	9.064371	10.335629	10 041962	10.577541	72
48	9.622682	9-957979	9.664703	10.335297	10.042021	10.377318	12
49	9.622956	9.957921	9.665035	10.334964	10.042079	10.377044	21
50	9.623729	9 957863	9.66 5266	10.134634	10/042137	10.376778	10
	-		Charles and the last	The second second	The second second		
51		9 957804	9.665697	10.334303	10.042196	10.37498	2
52	9.023774	9-957746	9.666029	10.333971	10.042254	10.376116	
53 54	9.034047	9,957087	9.666360	10.333640	10.042313	10-375953	1
54	8 (054319	9-957628	9.666691	10-333309	10.042372	ICL375681	-6
155	9.024591	9-957570	9.667021	10.331979	10.042430	10.37 5409	5
156	9.624863	9-957511	9.667352	10.332648		10.37 5137	
157				10.332318		10.374885	3
158					10.042507	10,314564	1
50	0.6=5677	9.047224	9.668744		10.042665	10.374740	1
60	0.525048	0.007226	9.66863	10,331328	10.041714		
55 57 55 55 55 55 55 55 55 55 55 55 55 5	-	-	-	12/33/3-0	The second	10.37.1032	-
	Co-sine."	bine	Co-tung.	1308	Co-sec.	Securit	. TAG
		THE REAL PROPERTY.	-	1000			

25 Degrees.

No.   Co-sene.   Tang.   Co-sene.   Co-sene.   Mo.   O.   O.   O.   O.   O.   O.   O.	-	-		400	sections.	_		_
1 9.626219 9.957217 9.6699021 10.330988 10.23738 10.27378 50 3 9.626700 9.957089 9.669931 10.330039 10.042842 10.377310 50 9.62700 9.957089 9.669991 10.330039 10.042842 10.377310 50 9.62700 9.95682 9.670300 10.339680 10.04260 10.377100 56 9.627570 9.95682 9.670300 10.339680 10.043019 10.377100 56 9.627570 9.95682 9.670300 10.339680 10.043019 10.377100 56 9.627570 9.95682 9.677306 10.339680 10.043019 10.377100 56 9.628319 9.95682 9.677306 10.338694 10.043138 10.377100 51 9.95884 9.95682 9.677306 10.338694 10.043319 10.377100 51 10.968806 9.95682 9.677306 10.338694 10.043316 10.377108 51 10.968806 9.95682 9.677209 10.338707 10.043315 10.377108 51 10.968806 9.95682 9.677209 10.338707 10.043315 10.377108 43 13 9629831 9.956849 9.95684 9.672249 10.338709 10.043314 10.370347 47 14 9.63972 9.956849 9.672249 10.338703 10.043314 10.370347 47 14 9.63972 9.956849 9.672249 10.338703 10.043314 10.370347 47 14 9.63972 9.956849 9.672300 10.338703 10.043313 10.370347 47 9.956849 9.95688 9.67237 10.338703 10.043313 10.357031 49 9.95032 9.95688 9.674374 10.338703 10.043313 10.359744 41 9.63972 9.95688 9.674374 10.338703 10.043313 10.369744 41 18 9.63972 9.95688 9.674374 10.325703 10.043513 10.369744 41 18 9.63972 9.95688 9.674374 10.325703 10.043513 10.369744 41 18 9.63972 9.95608 9.674374 10.325703 10.043513 10.36974 41 18 9.63972 9.95608 9.674374 10.325703 10.043513 10.36974 41 18 9.63972 9.95608 9.674374 10.325703 10.043513 10.36974 41 18 9.63972 9.95608 9.67437 10.325703 10.044311 10.368411 13 9.63189 9.95608 9.67437 10.325703 10.044311 10.368411 13 9.63189 9.95608 9.67437 10.325703 10.044311 10.368411 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.368411 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.368411 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.36841 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.36841 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.366811 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.366811 13 9.635814 9.958309 9.67880 10.334436 10.044311 10.366811 13 9.635814 9.958309 9.688308 1	\$ 36	Sine	Co-sine.	Tang	Co-tang	Secant.	Co-sec.	MI
1 9.626219 9.957217 9.6699021 10.330988 10.23738 10.27378 50 3 9.626700 9.957089 9.669931 10.330039 10.042842 10.377310 50 9.62700 9.957089 9.669991 10.330039 10.042842 10.377310 50 9.62700 9.95682 9.670300 10.339680 10.04260 10.377100 56 9.627570 9.95682 9.670300 10.339680 10.043019 10.377100 56 9.627570 9.95682 9.670300 10.339680 10.043019 10.377100 56 9.627570 9.95682 9.677306 10.339680 10.043019 10.377100 56 9.628319 9.95682 9.677306 10.338694 10.043138 10.377100 51 9.95884 9.95682 9.677306 10.338694 10.043319 10.377100 51 10.968806 9.95682 9.677306 10.338694 10.043316 10.377108 51 10.968806 9.95682 9.677209 10.338707 10.043315 10.377108 51 10.968806 9.95682 9.677209 10.338707 10.043315 10.377108 43 13 9629831 9.956849 9.95684 9.672249 10.338709 10.043314 10.370347 47 14 9.63972 9.956849 9.672249 10.338703 10.043314 10.370347 47 14 9.63972 9.956849 9.672249 10.338703 10.043314 10.370347 47 14 9.63972 9.956849 9.672300 10.338703 10.043313 10.370347 47 9.956849 9.95688 9.67237 10.338703 10.043313 10.357031 49 9.95032 9.95688 9.674374 10.338703 10.043313 10.359744 41 9.63972 9.95688 9.674374 10.338703 10.043313 10.369744 41 18 9.63972 9.95688 9.674374 10.325703 10.043513 10.369744 41 18 9.63972 9.95688 9.674374 10.325703 10.043513 10.369744 41 18 9.63972 9.95608 9.674374 10.325703 10.043513 10.36974 41 18 9.63972 9.95608 9.674374 10.325703 10.043513 10.36974 41 18 9.63972 9.95608 9.674374 10.325703 10.043513 10.36974 41 18 9.63972 9.95608 9.67437 10.325703 10.044311 10.368411 13 9.63189 9.95608 9.67437 10.325703 10.044311 10.368411 13 9.63189 9.95608 9.67437 10.325703 10.044311 10.368411 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.368411 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.368411 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.36841 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.36841 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.366811 13 9.63189 9.95808 9.67580 10.334436 10.044311 10.366811 13 9.635814 9.958309 9.67880 10.334436 10.044311 10.366811 13 9.635814 9.958309 9.688308 1	0	0.620048	0.052476	0.658672	10.221227	10.042724	10.274022	60.1
2 9.626490 9.95718 9.66931 10.330039 10.04301 10.373240 58								1000
3 9,636760 9,937099 9,669601 10.330139 10.043011 10.373240 57 9,667300 9,93698 9,670300 10.339381 10.043019 10.377320 56 9,667370 9,93602 9,670300 10.339381 10.043019 10.377300 53 8 9,628109 9,93662 9,670300 10.328369 10.043019 10.377300 53 8 9,628109 9,93662 9,672306 10.328369 10.043197 10.3771801 52 9 9,628378 9,93662 9,672301 10.328369 10.043197 10.3771801 52 10 9,62836 9,93662 9,672291 10.328369 10.04319 10.3771801 52 11 9,62836 9,93662 9,672291 10.328369 10.04331 10.377181 53 12 9,62836 9,93662 9,672291 10.337381 10.04331 10.377181 53 13 9,62836 9,93662 9,672291 10.337381 10.04331 10.377181 54 14 9,62836 9,93662 9,672291 10.33781 10.04331 10.377181 54 15 9,62836 9,93662 9,67229 10.32738 10.04331 10.377081 45 16 9,63231 9,93632 9,673002 10.32638 10.04313 10.377049 46 17 9,63232 9,93632 9,673002 10.32638 10.04313 10.377049 46 18 9,6323 9,93632 9,67330 10.32638 10.04313 10.37704 54 17 9,63234 9,93628 9,67438 10.325416 10.04333 10.36948 44 17 9,63234 9,93628 9,67438 10.325416 10.04331 10.36948 44 17 9,63239 9,93638 9,67438 10.325416 10.04331 10.36948 44 18 9,63259 9,95628 9,67438 10.325416 10.04371 10.36948 44 19 9,63239 9,95628 9,67438 10.32431 10.04391 10.36948 44 19 9,63239 9,95628 9,67438 10.33443 10.04391 10.36674 44 10 9,63239 9,95638 9,67438 10.33443 10.04391 10.36674 44 11 9,63259 9,95530 9,67530 10.33443 10.04391 10.36874 12 12 9,63239 9,95500 9,67530 10.33443 10.04491 10.36874 12 13 9,63249 9,95500 9,67530 10.33443 10.04491 10.36841 13 13 9,63249 9,95538 9,67684 10.33443 10.04491 10.36732 13 14 9,63239 9,95538 9,67683 10.33443 10.04491 10.36732 13 15 9,63249 9,95538 9,67684 10.3344 10.04491 10.36732 13 17 9,63249 9,95538 9,67684 10.3344 10.04491 10.36732 13 18 9,63249 9,95538 9,6768 10.3344 10.04491 10.36732 13 19 9,63249 9,95538 9,6768 10.3344 10.04491 10.36634 13 19 9,63249 9,95538 9,6688 10.3488 10.04491 10.36634 13 19 9,63249 9,95538 9,6688 10.3488 10.04491 10.36634 13 19 9,63249 9,95538 9,6688 10.3488 10.04491 10.36634 13 19 9,63249 9,95538 9,6688 10.3488 10.04491 10.36634 13 19 9,63249 9,95538					1000			20
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\$ 0.627,300  0.95061  0.670540  10.32935  10.04107  10.372700  55  9.627,540  0.95062  0.670540  10.32335  10.04107  10.37250  53  0.627,540  0.95062  0.670570  10.32836  10.04107  10.37250  53  0.627,540  0.95062  0.67130  10.32836  10.04137  10.37150  53  0.96276  0.95062  0.967130  10.32836  10.04137  10.37152  51  0.9628916  9.95062  0.67130  10.32707  10.04337  10.371084  49  0.629185  9.95662  0.67120  10.32707  10.04337  10.04337  10.371084  49  0.629185  9.95662  0.67120  10.32703  10.043391  10.04331  10.371084  49  0.629185  9.95662  0.67120  10.32703  10.04331  10.04341  40.37081  43 \\ 13.062972  0.95687  0.67120  10.32703  10.043491  10.37027  45 \\ 13.062972  0.95687  9.67120  10.32607  10.04361  10.37027  47 \\ 15.96196  0.95627  0.95627  9.95627  9.67120  10.32607  10.04367  10.36707  47 \\ 9.63027  0.99628  9.67120  10.32507  10.04367  10.36077 \\ 10.96305  0.96628  9.67120  10.32507 \\ 10.04367  10.36077 \\ 10.96305  0.95628  9.67120  10.32507 \\ 10.04367  10.36074 \\ 10.9631320  9.956089  9.67120  10.32504 \\ 10.9631320  9.956089  9.67120  10.32504 \\ 10.04371  10.36074 \\ 10.9631320  9.956089  9.67126 \\ 10.03210 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04367 \\ 10.04467 \\ 10.04467 \\ 10.04467 \\ 10.04467 \\ 10.04467 \\ 10.04467 \\ 10.04467 \\ 10.04667 \\ 10.04467 \\ 10.04667 \\ 10.04467 \\ 10.04667 \\ 10.04467 \\ 10.04667 \\ 10.0		No. of Concession, Name of Street, or other party of the Concession, Name of Street, or other pa		CONTRACTOR OF THE PARTY OF THE				
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17 9 520524 9.95628 9.674257 10.325743 10.043732 10.30478 43 18 9.620792 9.956148 9.674584 10.325416 10.043732 10.36628 41 19 9.631059 9.956148 9.674910 10.325900 10.043522 10.368941 41 20 9.631326 9.950089 9.675564 10.324436 10.043971 10.36874 40 21 9.631593 9.950089 9.675564 10.324436 10.043971 10.36874 33 22 9.631859 9.955909 9.675564 10.324436 10.044031 10.36874 33 23 9.632322 9.955849 9.676543 10.32373 10.044031 10.36874 33 24 9.632392 9.955849 9.676543 10.32373 10.044101 10.368775 37 24 9.632392 9.955789 9.676543 10.32373 10.044151 10.357608 16 25 9.632923 9.955789 9.676543 10.32373 10.044151 10.357608 16 26 9.632923 9.955789 9.676869 10.323357 10.044151 10.357608 16 27 9.632389 9.955669 9.677520 10.323859 10.044511 10.357677 34 28 9.632352 9.955669 9.677846 10.323154 10.044513 10.366811 32 28 9.633984 9.955669 9.677846 10.323154 10.044513 10.36681 32 28 9.633984 9.955669 9.677846 10.323154 10.044513 10.36681 32 39 9.53719 9.955548 9.67846 10.323154 10.044513 10.36681 32 30 9.634759 9.955368 9.67846 10.323154 10.044513 10.36681 32 31 9.634759 9.955368 9.67846 10.323154 10.044512 10.36636 30 31 9.634759 9.955368 9.67840 10.323154 10.044512 10.36636 30 31 9.634759 9.955368 9.68030 10.32154 10.044532 10.365438 31 32 9.635031 9.955489 9.67840 10.32159 10.044532 10.365432 27 32 9.635031 9.95548 9.68030 10.32159 10.044532 10.365432 27 32 9.635031 9.95548 9.68030 10.31433 10.044931 10.36404 22 33 9.634758 9.95547 9.68092 10.31433 10.044935 10.36440 24 34 9.635031 9.95548 9.68030 10.31933 10.044935 10.365428 27 34 9.635031 9.95548 9.68030 10.31935 10.04493 10.36523 10.36533 10.3633 10.04493 10.36523 10.36533 10.36533 10.04493 10.36523 10.36533 10.36533 10.04493 10.36523 10.36533 10.36533 10.04493 10.36533 10.36533 10.04493 10.36533 10.36533 10.95393 10.04493 10.36523 10.36533 10.95393 10.04493 10.36523 10.36523 10.95393 10.04493 10.36523 10.36523 10.95393 10.04493 10.36523 10.36523 10.95393 10.04543 10.36523 10.36523 10.95393 10.04543 10.36523 10.36523 10.95393 10.04543 10.36526 10.36523 10.95393 10.04543 10.3652	16	9.630257	0.956327	9 673929	10.325071	10.043673	10.369748	
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20   9.631326   9.956080   9.675237   10.324763   10.04391   10.368674   40   40   9.631859   9.955060   9.675564   10.324436   10.04401   10.368407   39   9.632832   9.955909   9.676564   10.32410   10.04401   10.3682407   37   40.632832   9.955909   9.676870   10.324783   10.04401   10.367873   37   40.952832   9.955849   9.676843   10.32477   10.04401   10.367342   35   9.632838   9.955849   9.676860   10.32333   10.04421   10.367342   35   9.632838   9.955789   9.676860   10.32333   10.04421   10.367343   35   37   39   9.632838   9.955600   9.677640   10.323860   10.04431   10.367563   31   32   9.632839   9.955600   9.677840   10.323850   10.04431   10.36681   31   32   9.632839   9.955600   9.678840   10.323850   10.04431   10.36681   31   32   9.633719   9.95548   9.67817   10.32829   10.044452   10.36626   30   31   9.634849   9.955600   9.678840   10.323850   10.044512   10.36626   31   31   9.634849   9.955488   9.67817   10.32829   10.044512   10.36626   31   31   9.634778   9.95548   9.67871   10.32829   10.044512   10.36626   30   31   9.634778   9.95548   9.67847   10.32829   10.044512   10.36626   30   31   9.634778   9.95560   9.67882   10.323540   10.044512   10.36626   30   31   9.634778   9.95560   9.67847   10.32039   10.044512   10.36622   27   31   9.635043   9.95548   9.67847   10.32039   10.044512   10.36626   28   31   9.634544   9.95560   9.67947   10.32039   10.044512   10.36622   27   31   9.635043   9.95560   9.680444   10.32039   10.044514   10.36494   22   24   24   24   24   24   24								-
11 9.631593 9.955069 9.675564 10.324436 10.044031 10.168141 38 13 1 10.041031 10.168141 38 13 13 14.058159 9.955069 9.676809 10.324310 10.044031 10.168141 38 13 14.058159 9.955069 9.676809 10.324378 10.0441031 10.168141 38 14.058169 9.65268 9.955789 9.676869 10.32133 10.044131 10.367608 16 16.06323 9.955789 9.676869 10.32133 10.044171 10.367677 34 16.963243 9.955769 9.677194 10.128366 10.044171 10.367677 34 17 9.632189 9.955669 9.677520 10.322154 10.044131 10.365811 12 18 9.631719 9.955669 9.677846 10.322154 10.044513 10.366246 32 9.633984 9.955689 9.678846 10.322154 10.044512 10.366246 32 9.633984 9.955848 9.67846 10.322154 10.044512 10.366046 30 19.633984 9.955848 9.67846 10.322154 10.044512 10.366046 30 19.632778 9.955368 9.67846 10.322154 10.044512 10.366046 30 19.63278 9.955369 9.95548 9.67846 10.322154 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.044512 10.366046 30 19.632514 10.36522 27 10.36523 10.36522 27 10.36523 10.36522 27 10.36523 10.36522 27 10.36523 10.36522 27 10.36523 10.36522 27 10.36523 10.36522 27 10.36523 10.36522 27 10.36523 10.36522 27 10.36523 10.36522 27 10.36523 10.36522 27 10.36523 10.36522 20 10.36523 10.36522 10.36523 10.36522 10.36523 10.36523 10.36523 10.36523 10.36523 10.36523 10.36523 10.3								
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25	24	9.632592	9.955849	9.676543	10.323457	10.044151	10.367608	
26	120	9.632648		9.676860	10.222131	10.044544	10.257.242	_
27 9.632189 9.955669 9.677520 10.321820 10.044331 10.366811 32 9.631454 9.955609 9.677840 10.321829 10.044439 10.305626 32 10.963298 9.955548 9.678711 10.321829 10.044432 10.366261 32 9.632984 9.955608 9.678740 10.321829 10.044432 10.366261 32 10.963298 9.955488 9.678740 10.321829 10.044512 10.366261 32 12 9.634749 9.95388 9.679140 10.321829 10.044512 10.366261 32 12 9.634778 9.95530 9.679140 10.320205 10.044512 10.36528 22 13 9.634778 9.95530 9.679140 10.320205 10.044512 10.365212 27 14 9.635042 9.955247 9.679474 10.320205 10.044592 10.365428 22 14 9.635042 9.955247 9.679474 10.320205 10.044592 10.364938 25 15 9.635300 9.95510 9.680444 10.219550 10.044874 10.364994 25 15 9.635314 9.955019 0.804044 10.219550 10.044874 10.364994 25 15 9.635314 9.955019 0.808768 10.314928 10.044935 10.364480 24 19 9.636300 9.954934 9.684091 10.31950 10.044935 10.364480 24 19 9.636300 9.954934 9.68404 10.31950 10.044935 10.36493 22 10.363634 10.954091 10.36363 11.954091 10.36363 11.954091 10.36363 11.954091 10.36363 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.36360 11.954091 10.954091 10.36360 11.954091 10.954091 10.36360 11.954091 10.954091 10.36360 11.954091 10.954091 10.36360 10.36360 11.954091 10.954091 10.36360 10.36360 10.954091 10.954091 10.36360 10.36360 11.954091 10.954091 10.36360 10.363					10.111506	10.044271		10000
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10   9-633984   9 953488   9-678496   10.321504   10.044512   10.366016   30   31   9-634759   9-95368   9-678821   10.12179   10.044512   10.365751   29   39 953488   9-678821   10.120554   10.044632   10.365751   29   3 9-634778   9-95368   9-679471   10.120554   10.044632   10.365222   27   49-685042   9-655042   9-679471   10.120554   10.044632   10.365222   27   49-685042   9-655042   9-655042   9-679795   10.32026   10.044632   10.365222   27   9-685042   9-655				THE RESERVE OF THE PERSON NAMED IN				
11 9.634249 9.953628 9.679146 10.12179 10.044672 10.365751 20 12 9.634514 9.953368 9.679146 10.120854 10.044693 10.365436 28 13 9.634778 9.955367 9.679471 10.120529 10.044693 10.365432 27 14 9.635042 9.955247 9.679795 10.320205 10.0447693 10.364938 26 13 9.635364 9.955186 9.680120 10.359285 10.044874 10.354694 25 13 9.635570 9.955186 9.680444 10.219556 10.044874 10.354694 25 13 9.635314 9.955005 9.680444 10.219556 10.044874 10.354694 25 13 9.636300 9.955005 9.681092 10.318908 10.044874 10.354592 22 14 9.636623 9.954883 9.681092 10.318908 10.044995 10.253993 22 14 9.636623 9.954883 9.681740 10.318260 10.045117 10.363277 20 14 9.637638 49.95407 9.68203 10.318260 10.045117 10.363277 20 14 9.637638 9.95462 9.68203 10.317937 10.045177 10.353114 10.363277 10.68718 10.68718 10.68517 10.36327 10.68718 10.68718 10.36265 17 14 9.637633 9.954600 9.682010 10.317290 10.045295 10.36489 17 14 9.637633 9.95450 9.68336 10.316644 10.045218 10.36265 17 14 9.637848 9.954474 9.68436 10.316321 10.045218 10.36265 17 14 9.637839 9.954519 9.68376 10.316341 10.045218 10.36265 17 14 9.63889 9.954457 9.683001 10.316321 10.045281 10.36265 17 14 9.63889 9.954457 9.683001 10.316321 10.045281 10.36265 17 14 9.63891 9.954519 9.684740 10.316321 10.045281 10.36265 17 15 9.639744 9.95474 9.68466 10.313354 10.045281 10.361542 11 16 9.63991 9.95451 9.68466 10.313354 10.045281 10.361542 11 17 9.63891 9.95451 9.68466 10.313354 10.045281 10.361542 11 18 9.639744 9.95474 9.68466 10.313354 10.045281 10.361544 10.36265 10.361544 10.96391 10.045781 10.36265 10.361544 10.96391 10.045781 10.36265 10.361544 10.96391 10.361644 10.045481 10.36265 10.361544 10.96391 10.361644 10.045281 10.361544 10.36265 10								
32	30	A-077A04	9 955400	4.078490	10-351200	10.044512	10.300010	30
32	32	9.634249	9.955498	9.678821	10,121179	10,044672	10-164751	29
31		9.034514		9.679146	10.120854	10.044632	10.365486	
34 9.635042 9.955247 9.679795 10.320205 10.044753 10.364938 26 35 9.635306 9.455186 9.680120 10.319880 10.044814 10.364694 25 36 9.635570 9.955126 9.680444 10.319556 10.044874 10.364480 24 37 9.635834 9.95505 9.680768 10.319328 10.044935 10.364180 24 38 9.636300 9.954944 9.68192 10.318908 10.044935 10.36393 24 40 9.636523 9.954883 9.681740 10.318908 10.044935 10.363640 21 40 9.636623 9.954883 9.681740 10.318268 10.045117 10.363377 20 41 9.636886 9.954883 9.681740 10.318268 10.045117 10.363377 20 42 9.636763 9.954883 9.682053 10.317937 10.045117 10.363377 20 43 9.637118 9.954701 9.682761 10.317937 10.045137 10.363377 20 44 9.637673 9.954640 9.683031 10.317613 10.045239 10.36365 17 44 9.637673 9.954680 9.683031 10.316967 10.045380 10.363265 17 45 9.638458 9.954579 9.68366 10.316364 10.045481 10.362065 15 46 9.638707 9.95458 9.683001 10.316967 10.045381 10.361801 14 47 9.638458 9.954457 9.684001 10.315999 10.045581 10.361801 14 48 9.63870 9.95458 9.68464 10.31534 10.04564 10.36180 14 49 9.63870 9.95418 9.68466 10.31534 10.04564 10.36180 14 49 9.63870 9.95418 9.68466 10.31534 10.04564 10.36180 14 49 9.63870 9.95418 9.68466 10.31534 10.04564 10.36180 14 49 9.63870 9.95418 9.6846 10.31548 10.04564 10.36180 14 49 9.63870 9.95418 9.6846 10.31548 10.04564 10.36180 14 49 9.63870 9.95418 9.6846 10.31548 10.04564 10.36180 14 49 9.63870 9.95418 9.6846 10.31548 10.04564 10.36180 14 49 9.63870 9.95418 9.68496 10.31548 10.04564 10.36180 14 49 9.63870 9.95418 9.96470 10.31648 10.31548 10.04564 10.36180 14 49 9.63870 9.95418 9.96470 10.31648 10.31548 10.04564 10.36180 14 49 9.63870 9.95418 9.96470 10.31648 10.31648 10.36180 14 49 9.63870 9.95418 9.96480 10.31648 10.31648 10.04564 10.36180 14 49 9.63870 10.95470 10.31648 10.31648 10.31648 10.36180 14 49 9.63870 10.95470 10.31648 10.	-	9:634778				10,044691	DESCRIPTION OF THE PERSON NAMED IN	
36 9.635306 9.455186 9.680130 10.319880 10.044814 10.364694 25 36 9.635570 9.955136 9.680484 10.319556 10.044874 10.364402 24 37 9.635834 9.955053 9.680768 10.319353 10.044995 10.361416 21 38 9.636037 9.95505 9.681032 10.318988 10.044995 10.263933 22 39 9.63652 9.954883 9.681416 10.318584 10.04505 10.303640 21 40 9.63665 9.954823 9.681001 10.318584 10.04505 10.363377 20 41 9.636866 9.954823 9.68206 10.318280 10.045117 10.363377 20 42 9.637613 9.954820 9.682387 10.317613 10.045117 10.363377 20 43 9.637148 9.954701 9.682361 10.317513 10.045177 10.363377 10 44 9.637673 9.954660 9.683051 10.317501 10.04518 10.36285 18 45 9.637673 9.954660 9.683051 10.317501 10.04518 10.36265 17 46 9.63879 9.95458 9.683051 10.316367 10.045181 10.36265 17 47 9.638458 9.954457 9.683051 10.316387 10.045481 10.36265 11 48 9.63870 9.95458 9.68305 10.316381 10.045481 10.36265 12 49 9.638458 9.954457 9.683001 10.315999 10.045581 10.361368 14 49 9.63870 9.95458 9.68464 10.31534 10.04565 10.361364 12 49 9.63870 9.954578 9.68466 10.31534 10.04565 10.361364 12 49 9.63870 9.95458 9.68466 10.31534 10.045787 40.360678 10 51 9.63901 9.95431 9.68590 10.31438 10.04588 10.065787 40.360768 10 51 9.63901 9.95431 9.68590 10.314388 10.04584 10.36136 10 51 9.63900 9.95431 9.68591 10.314388 10.04584 10.36136 10 51 9.63900 9.95431 10.96590 10.314388 10.04584 10.36138 10 51 9.63900 9.95431 10.96590 10.314388 10.04584 10.35096 79 52 9.639064 9.95491 10.96890 10.38491 10.31438 10.04584 10.35096 79 52 9.639064 9.95491 10.96890 10.38491 10.31438 10.04584 10.35096 79 53 9.640024 9.95491 10.96890 10.38491 10.31438 10.04584 10.35096 79 53 9.640024 9.95490 9.68593 10.31438 10.04584 10.05590 10.35599 79 53 9.640024 9.95490 9.68593 10.31438 10.04584 10.05590 10.35599 79 53 9.640024 9.95490 9.68593 10.31438 10.04584 10.05590 10.35599 79 53 9.640024 9.95490 9.68593 10.0560 10.0560 10.0560 10.0560 79 53 9.640024 9.95490 9.68593 10.0560 10.0560 10.0560 10.0560 79 53 9.640024 9.95490 9.68593 10.0560 10.0560 10.0560 10.0560 70 53 9.640024 9.9540 10.0560 10.0560 70 53 9.6400		THE RESERVE AND ADDRESS OF THE PERSON NAMED IN				MUST SHARE AND AND		
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54 0.640264 0.956029 0.686255 10.315745 10.045971 10.359710 6 55 0.640264 0.953965 0.686577 10.313423 10.046034 10.359120 5 56 0.640264 0.953966 0.686898 10.313102 10.046034 10.359120 4 57 0.641064 0.953845 0.687240 10.312781 10.046034 10.358120 3 58 0.641114 0.955781 0.687240 10.312781 10.046155 10.358036 3 59 0.641124 0.955781 0.687240 10.312460 10.046171 10.35878 2 50 0.641842 0.953760 0.688182 10.31210 10.046171 10.358158 0 56 Co-sine. Sine. Co-rang. Tang. Co-sec. Securit. M.	100	0.640001	0.054000	0.68/074	10, 214066	10.045010	10-250036	4
55 9.690644 9.953968 9.686577 10.114623 10.046032 10.359426 5 56 9.640304 9.953906 9.686898 10.113102 10.046032 10.359426 5 57 9.541054 9.953845 9.687249 10.312781 10.046053 10.358936 3 58 9.641114 9.953781 9.687640 10.312460 10.046155 10.358936 2 9.941651 9.953781 9.687640 10.312460 10.04627 10.35847 1 10.041842 9.953760 9.688181 10.111119 10.04627 10.35847 1 10.041842 9.951660 9.688181 10.111119 10.04627 10.358168 0 10.641842 9.951660 9.688181 10.111119 10.04627 10.358168 0	120	100000	2 22 4440	0 68627	10 71 771	ID-DIFORT	10 359970	2
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\$8 0.641134 0.953781 9.687540 10.112460 (30.05612) 10.358036 5 \$9 0.641134 0.953781 9.687540 10.112460 (30.05612) 10.35876 2 \$0 0.641842 0.953760 9.68781 10.11219 10.046140 10.358158 0 \$1 Co-sine. Sine. Co-tang. Tang. Co-sec. Securit. M.	126	9 949304	A1422400					100
39 9-541 (51 9-953781 9-687261 10-111465) 13-04672 10-158578 2 10 9-541 (51 9-953721 9-687261 10-11119 10-04672 10-358417 1 10 9-641842 9-951660 9-688182 10-111818 10-046740 10-358158 0 10 Co-sine. Sine. Co-rang. Tang. Co-sec. Secunt. M.	57		9953049					3
10 9.641842 9.9517560 9.688182 10.11818 10.046140 10.558158 D	58							
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		Contract to the last	26	Degrees.			
1 32	Sine.	Co-sine.	Tang.	Co-tang.	Secant	Co-sec.	1 10
1-	100000000000000000000000000000000000000	-	g.688:82		-		
0	9.64184=	9 953660		10.311818		10.358158	60
1.3	9.642101	9-953599	9.688502	10.311498		10 357899	159
2	9.642360	9.953537	9 688833	10.311177	10-046463	10.317640	58
3	9.642618	9.953475	9.689143	10.310857	10.046525	NX357381	57
.4	9.642877	9-953413	9.689463	10.310537	10/01/02/24	10.157113	56
1 5	0.643135	9 953352	9.689783	10.310217	10.046648	10.355765	55
5	9.643393	9.953290	9.690103	10 300897	10 046710	10.356507	54
7	9.643650	9.953228	6 600423	10.309577	10 046772	10.356350	53
7 8	9.643908	9.953166	9.690742	10.309258	10.046834	10.116042	52
	9.644165	9.953104	9.691062	10.308918	10.046896	10.155835	51
9	Marie Control	9.953042	9.691381	10.708619	10.046958	10.355577	
10	9.644423				-		50
100	9.644680	9.952980		10.308300	10.047010	10.355320	49
12	9.644936	9.952918		10.307981	10,047082	10.555064	42
13	9.645193	9.952855	9.692338	10.307662	10:047145	10.154807	47
14	9.645450	9 952795	9.692656	10-307344	10.047207	10.254990	46
15	9.645706	9.952731	9 692975	10.307025	10.047250	10.254894	45
10	9.645962	9-952669		10.306707	10.047311	10.3 (405)	44
17	9.646218	9.952606		10.306388	ID(D47394	10.353781	45
18	9 646474	9 952544		10.300070	10.047456	10.355mb	42
1900	9.646729	9.952481	9.694248	10.305752		BEAUTIFUL AND ADDRESS OF THE PARTY OF THE PA	
19		ACCRECATE VALUE OF THE PARTY OF			10.047519	10.355174	20
20	9.646984	9.952419	9 694566	10.305434	10:047581	10.393010	40
at	9.647240	9 952356	9.694883	10.305117	10.047644	10.351100	39
23	9.647494	9.952294	9,095201	10.304799	10.047700	10:152506	18
23	9.647749	9.952231	0.605508	10.304482	10.047760	10.342241	25"
24	9.648004	9.952168	The second second	The second second	10.047832	10.351006	38
25	9 648258	9.952106	A CONTRACTOR OF THE PARTY OF TH	10/303847	10.047894	10.351741	
26	9.648512	9 952043	BARTON CHICAGO	10.303530	10-042957	10.341483	30
	9.648766		9 696787	10.303213	10.048020	10.251254	33
27	The second second	9.951917	0 007101			A COLUMN TO SERVICE AND ADDRESS OF THE PARTY	
1000	9.649020	A PORT OF THE REAL PROPERTY.	The second second	10.303897	10.048083	10.350680	20
29	9 649274	9.951854	9.697420	10.302580	10.048148	10,350726	8.
30	9.649527	9.951791	9.097730	10.301264	10 048209	10-190473	10
34	9.649781	9 951728	9.698053	10.301047	10.048272	10 350314	20
32	9 650034	9.951665	The same of the sa	10.301631	10.048335	10.349900	ak I
33	9 650287	9.951602		10.301314	10.048398	10-140717	22
	9 650539	9.951539	9.699001	10.300000	10.048461	10 140464	20
34			Section 2017	1 1 7 1 2 2 4			24
35	9.050792	9 951470	9.699316		10.04%524	10,141,202	
36	9.651044	9.951412	9 699632	10.300368	10.048588	10.348936	24
37	9.651297	9.951349	9.699947	10.300053	10.048651	10.345701	23
38	9.651549	9.951286	9.700263	10, 299737	10.048714	10.345451	22
139	9.651800	9.951222	9.700578	10.299422	10.048778	10.348000	23
40	9 652052	9.951159	9.700893	10.299107	10.048841	19.347048	10
41	9 652304	9.951096	9 701208	10.298792	10.048904	10.347090	19.
42	9.652555	9.951032	9.701523	10.298477	THE PERSON NAMED IN	Mark Committee of the C	18
	9.652806		100000000000000000000000000000000000000		10.048968	10.347445	
43	A COLUMN TO A COLU	9.950968	9.701837	10.298103	10.049033	10.347394	77
44	9.653057	9.950905	9-702152	10.207848	10.049095	10/346943	10
45	9.653308	9.950841	9.702466	10.297534	10.049159	10.346692	33
46	9.653558	9.950778	9.702780	10.297230	10.049232	10-345442	14
47	9 653808	9.950714	9.703095	10.296905	10.049286	10-140182	13
48	9.654059	9.950650	9-703409	10.296591	10.049350	10/345941	12
49	9.654309	9.950586	9.703713	10.296277	10.049464	10-345091	24
50	9.654558	9-950522	9.704036	10.295064	10.049475	10.345142	to
	9.654808				STATE OF THE PARTY OF	-	-
St		9.950458	9.704350	10.295650	10.049542	10.345192	3
52	9.655058	9-950394	9.704063	10.295337	10 049606	10,344941	10
53	9.655307	9.950330	9.704977	10.293013	10.049570	10/344033	6
54	9.655556	9.950266	9.705290	10-294710	10.049734	10:34444	16
55	9.655805	9.950202	9.705603	10-294397	10.049798	10.344195	5
56	9.656054	9.950138	9.703916	10.294084	10.049262	10:343946	27
57	9.656302	9.950074	9.706228	10.193772	1000099886	10:343096	3.1
55 56 57 58	9.636551	9.950010	9.706541	10.293450	10.040990	16-343449	
59	9.656799	9.949945	9.706844	10.193146	10.050055	10-143201	- 0 to p.o.
59	9.657047	9-949881	9 707100	10.292834	10.050110	10 141953	0
10		-			-		
34	Co-sine.	Sine.	Co-tang.	Tang.	Co-seci-	Decapt.	At
				1000			

Sine:   Co-ine:   Tang   Co-tang   Secant   Co-ine:   1				291	Degrees.			-
1 9.686799 9.944749 9.744049 9.744050 10.255950 10.055831 10.312301 59 9.656047 9.941679 9.744049 10.255751 10.055331 10.3123773 38 9.6560454 9.9417579 9.744943 10.255751 10.055331 10.312373 38 9.656040 9.941308 9.745258 10.254750 10.0558021 10.312313 57 9.6586926 9.941308 9.745258 10.254750 10.0558021 10.312313 55 9.6587389 9.941378 9.745758 10.254750 10.058022 10.312851 53 9.9687389 9.941187 9.745029 10.253508 10.058022 10.312851 53 9.9687389 9.941187 9.745029 10.253508 10.058802 10.312854 51 9.9688929 9.940975 3.747319 10.253508 10.059883 10.31233 9.941117 9.745725 10.253508 10.059883 10.31233 9.941117 9.745725 10.253508 10.059883 10.31233 9.941117 9.745725 10.253508 10.059883 10.31233 9.941117 9.745725 10.253508 10.059883 10.31233 9.94583 9.94573 9.747619 10.253508 10.059883 10.31233 9.94583 9.94583 9.749589 9.94583 9.94583 9.94583 9.745829 9.94583 9.94583 9.94583 9.94583 9.94583 9.94583 9.74580 9.025808 10.25975 10.059574 10.311123 45 9.658543 9.94583 9.749589 9.025808 10.25975 10.059574 10.311123 45 9.658543 9.94583 9.749589 9.025808 10.25975 10.059575 10.311123 45 9.658543 9.94583 9.74958 9.025806 10.25975 10.059575 10.311123 45 9.658543 9.94583 9.74958 9.025806 10.25975 10.059575 10.311123 45 9.658543 9.94583 9.74958 9.025806 10.25975 10.059575 10.311123 45 9.658543 9.94583 9.74958 9.025806 10.259575 10.059575 10.311123 45 9.658543 9.94583 9.74958 9.025806 10.259575 10.059575 10.311123 45 9.658543 9.94583 9.74958 9.025806 10.059575 10.059575 10.311123 45 9.659575 9.94085 9.74958 9.025806 10.059575 10.05	36	Sine.	Co-sine-	Tang	Co-tang	Secant	Co-sec.	26
0.688799	0	9.685571	9.941819	9749752	10 256248	10.058181	(0.314429)	60
2	2000		Market Street,		THE RESERVE OF THE PARTY OF THE	CONTRACTOR OF THE PARTY OF THE		59
4 9.686480 9.941469 9.745140 10.254760 10.058521 10.31321) 55     9.686709 9.941469 9.745140 10.254760 10.058621 10.31321) 55     9.687169 9.941389 9.745735 10.254465 10.058602 10.31304 54     9.687869 9.941117 9.746726 10.253274 10.058831 10.312157 50     9.687869 9.941117 9.746726 10.253274 10.058831 10.312157 50     9.687863 9.941117 9.746726 10.253274 10.058831 10.312157 50     12 9.688839 9.940973 3.747319 10.253281 10.058831 10.312157 50     12 9.688321 9.940907 9.747031 10.253281 10.058831 10.312157 50     13 9.688221 9.940907 9.747031 10.253281 10.058831 10.312157 50     14 9.688747 9.94057 9.748209 10.253281 10.058831 10.312157 50     14 9.688747 9.94057 9.748209 10.253281 10.059971 10.111023 45     15 9.688439 9.940501 9.748209 10.253281 10.059971 10.111023 45     1689443 9.940621 9.748209 10.254287 10.059937 10.111023 45     1689433 9.940621 9.748209 10.25027 10.059937 10.111023 45     1699098 9.940599 9.749789 10.25007 10.059937 10.110802 44     10.969073 9.94038 9.74938 9.749391 10.25007 10.059937 10.101023 45     10.969073 9.94038 9.74938 9.749391 10.25007 10.059931 10.109002 49     10.969073 9.94039 9.75038 10.25007 10.059931 10.109002 49     10.969074 9.94039 9.75038 10.25001 10.059931 10.109002 49     10.969076 9.94039 9.75038 10.24031 10.059931 10.109002 49     10.969096 9.940409 9.75038 10.24031 10.059931 10.109002 49     10.969096 9.940409 9.75038 10.240404 10.059931 10.109002 49     10.969096 9.940409 9.75038 10.024044 10.059931 10.109002 49     10.969096 9.940409 9.750576 10.249441 10.059931 10.109002 49     10.969096 9.940409 9.750576 10.249441 10.009031 10.109032 31     10.969096 9.930849 9.751400 10.024004 10.059936 10.30880 33     10.969096 9.930849 9.751400 10.024004 10.009031 10.309061 31     10.969096 9.930849 9.751400 10.024004 10.009031 10.309061 31     10.969096 9.930849 9.751400 10.024004 10.000031 10.309061 31     10.969096 9.930979 9.754400 10.024009 10.000031 10.309061 31     10.969096 9.930979 9.754789 10.024009 10.000031 10.309061 31     10.969096 9.930979 9.754789 10.02407	2	9.686027	9.941679		10.255052	10.058331	10.313973	
\$ 0.686700 0.941460 0.745210 10.254760 10.058672 10.31364 54     9.687389 0.941728 9.745738 10.254760 10.058672 10.31364 54     9.687389 0.941728 9.74573 10.255771 10.058872 10.31361 52     9.687389 0.941717 9.746730 10.255771 10.058873 10.31354 52     9.687389 0.941717 9.746730 10.255771 10.058873 10.31354 51     9.687389 0.941717 9.746730 10.253774 10.058873 10.31354 51     9.688739 0.9497019 9.74703 10.253874 10.058873 10.313157 50     11 0.688631 9.940007 9.747010 10.253881 10.359271 10.3113157 50     12 0.688731 9.940007 9.747010 10.253881 10.059873 10.311479 47     14 9.688747 9.940074 9.747019 10.253881 10.059873 10.311479 47     15 9.688738 9.940075 9.747010 10.253881 10.059873 10.311479 47     1689438 9.940075 9.748801 10.151709 10.059878 10.311682 49     15 9.689739 9.940760 9.749880 10.250073 10.059878 10.310577 43     17 9.689439 9.940575 19.749097 10.250073 10.059878 10.310577 43     18 9.689538 9.940075 19.749080 10.250073 10.059849 40.310372 44     19.690737 9.94079 9.749680 10.250073 10.0599849 40.310372 44     19.690737 9.94079 9.750878 10.25007 10.0599849 40.310372 44     19.690737 9.94079 9.750878 10.25007 10.0599849 40.310372 44     19.690737 9.94079 9.750878 10.249719 10.059991 10.109992 40.309873 44     19.690737 9.94079 9.750878 10.24978 10.059997 10.209078 37     19.69073 9.94079 9.750878 10.24978 10.059997 10.209078 37     19.69073 9.94079 9.750878 10.24978 10.059997 10.209078 37     19.69073 9.94079 9.750878 10.24978 10.059997 10.209078 37     19.69078 9.93998 9.75187 10.24978 10.050907 10.309871 10.30987	3	9.686254	9.941609	9.744645		10.058391	10.313746	57
6	4		CONTRACTOR AND ADDRESS OF	9-744943				_
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14   9.688   221   9.940905   9.747616   10.252984   10.059995   10.351479   47     47   9.688977   9.940834   9.747915   10.252087   10.059378   10.311033   46     48   9.688978   9.940832   9.748209   10.25799   10.059378   10.310802   44     49   9.689873   9.94080   9.748301   10.25799   10.059378   10.310802   44     49   9.689873   9.94080   9.749393   10.250907   10.059378   10.310802   44     49   9.69098   9.94080   9.749393   10.250911   10.059378   10.310977   43     49   9.69073   9.94038   9.749898   10.250015   10.059961   10.309071   10.309071   10.250015   10.059961   10.309071   10.25011   10.059961   10.309071   10.25011   10.059961   10.309071   10.249719   10.059961   10.20918   10.059961   10.0	-		CARLAGRICA PAR	A CONTRACTOR OF THE PARTY OF TH	CONTRACTOR STATE			49
14 9.688747 9.940834 9.747913 10.250887 10.059160 10.311233 46 9.688978 9.940593 9.748209 10.251791 10.059378 10.310802 44 9.689483 9.940551 9.749087 10.250907 10.310802 44 9.689483 9.940551 9.749087 10.250907 10.059449 (0.10337 10.310802 44 9.689873 9.940380 9.749087 10.250907 10.059449 (0.10337 10.310802 44 9.690908 9.940040 9.749689 10.250311 10.059901 10.309002 49 9.690908 9.940109 9.749689 10.250311 10.059901 10.309002 49 9.690908 9.940105 9.750881 10.249719 10.059984 10.309072 9.940109 9.750881 10.249719 10.059804 10.20928 37 10.94009 9.940105 9.750871 10.249719 10.059804 10.20928 37 10.94114 9.93982 9.751402 10.248833 10.059875 10.30900 36 10.94114 9.93982 9.751402 10.248833 10.060089 10.30880 39 9.940115 9.750874 10.248833 10.060089 10.30880 39 9.940115 9.750874 10.248833 10.060089 10.30880 39 9.95091 9.751757 10.249748 10.060080 10.30880 39 9.95091 9.751757 10.249748 10.060089 10.30880 33 10.249831 10.249833 10.060089 10.30880 33 10.249831 10.249833 10.060089 10.30880 33 10.249834 10.060089 10.3088108 31 9.969131 9.939708 9.751757 10.249705 10.060040 10.30880 31 9.909131 9.939708 9.751757 10.249705 10.060040 10.30880 31 33 10.94981 9.93914 9.75177 10.247095 10.060040 10.30880 31 33 10.94980 9.939909 9.75182 10.247958 10.060089 10.30860 31 31 9.093859 9.939919 9.75182 10.24674 10.060040 10.307213 10.90978 10.30880 9.93919 9.75182 10.24674 10.060040 10.307213 11 9.093849 9.93919 9.754709 10.245079 10.060040 10.307213 11 9.093849 9.939389 9.754115 10.24509 10.060040 10.307213 11 9.909480 9.93840 9.75380 10.245079 10.060040 10.307213 11 9.909480 9.93840 9.753820 10.245079 10.060040 10.307213 11 9.909480 9.93840 9.753820 10.245079 10.060040 10.307213 11 9.909480 9.93840 9.753820 10.245079 10.060040 10.307213 11 9.909480 9.93840 9.753820 10.245079 10.060040 10.307213 11 9.909480 9.93840 9.753820 10.245079 10.060047 10.30880 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.306060 10.3060			COLUMN TO SERVICE			THE RESERVE AND ADDRESS OF THE PARTY OF THE		
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45 9.695671 9.938619 9.75732 10.241948 20.061381 10.304329 15 46 9.695892 9.938547 9.757341 10.242655 10.061453 10.304108 14 47 9.696113 9.938472 9.757338 10.242363 10.061453 10.303836 14 48 9.696314 9.938402 9.757931 10.242069 10.061398 10.303836 12 49 9.696775 9.938358 9.758517 10.2421776 10.061670 10.303837 10 51 9.696995 9.938185 9.758517 10.241483 10.061742 10.303215 10 51 9.696995 9.93813 9.75830 10.241190 10.061815 10.303205 9 52 9.697315 9.938040 9.75939 10.240695 10.061887 10.302785 8 53 9.697435 9.938040 9.75939 10.240605 10.061887 10.302785 8 54 9.69764 9.937967 9.759687 10.24065 10.06203 10.30256 7 55 9.697874 9.93893 9.75970 10.24003 10.06203 10.30256 7 56 9.69894 9.93822 9.760272 10.24002 10.06210 10.30256 7 57 9.698313 9.937749 9.76064 10.239728 10.062178 10.301687 3 58 9.698532 9.937604 9.76064 10.239728 10.062469 10.30168 3 59 9.698751 9.937604 9.761188 10.238561 10.062469 10.301468 3 59 9.698570 9.937611 9.761439 10.238561 10.062469 10.301408 1				THE NAME OF THE		A COUNTY CHICAGO		THE PARTY NAMED IN
46 9.696383 9.938547 9.757245 10.242655 10.061453 10.304108 14 47 9.696113 9.938475 9.757638 10.242363 10.061453 10.303887 13 48 9.696314 9.938402 9.757331 10.242069 10.061398 10.303866 13 49 9.696554 9.938330 9.758244 10.242176 10.061670 10.303666 11 50 9.696775 9.938185 9.758517 10.341483 10.061742 10.303215 10 51 9.696995 9.938185 9.758510 10.341483 10.061742 10.303215 10 52 9.697315 9.938113 9.759102 10.340896 10.061887 10.302785 8 53 9.697315 9.938040 9.759395 10.240806 10.061887 10.302785 8 54 9.697654 9.937907 9.759687 10.340313 10.062033 10.30336 6 55 9.697874 9.937895 9.75979 10.240031 10.062033 10.30316 5 56 9.698094 9.937822 9.760272 10.24031 10.062178 10.301667 3 57 9.698311 9.937749 9.76066 10.239728 10.062178 10.301667 3 58 9.698531 9.937760 9.750866 10.239436 10.062245 10.301668 3 59 9.698751 9.937604 9.761188 10.238526 10.062469 10.301468 3 59 9.698970 9.937511 9.761439 10.238561 10.062469 10.301408	94	I BOUNDARY SHOW	I Married World	Manual Control		Market Comment	A SHAREST PARTY AND ADDRESS OF THE PARTY AND A	_
47 9.696113 9.938475 9.757638 10.242361 10.061525 10.303686 12.40369 10.061528 10.303686 12.40369 10.061528 10.303686 12.40369 10.061528 10.303686 12.40369 10.061528 10.303686 12.40369 10.061528 10.303686 12.40369 10.061528 10.303686 12.40369 10.061528 10.303686 12.40369 10.30368 12.40369 10.30368 12.40369 10.30368 12.40369 10.30368 12.40369 10.30368 12.40369 10.30368 1			I LOUIS TO SELECT			THE RESERVE AND ADDRESS OF THE PARTY OF THE	The second second	
48				a bellioner and the				
49 9.096577; 9.938310 9.758241 10.221776 10.061670 10.303446 11 9.696977; 9.93818 9.758517 10.2211483 10.061742 10.303225 10 9.096977; 9.93818 9.758310 10.241483 10.061742 10.303205 9 9 9.697215 9.938113 9.7579102 10.240896 10.061887 10.302785 8 9.697435 9.938040 9.759395 10.240605 10.061887 10.302785 8 9 907874 9.937879 9.759687 10.240605 10.062033 10.302346 6 9.698874 9.937893 9.759979 10.240021 10.062405 10.302346 6 9.698874 9.937822 9.760272 10.240021 10.062405 10.302346 5 9.698873 19.937749 9.760564 10.230436 10.06221 10.101687 3 9.698532 9.25676 9.76086 10.230436 10.06221 10.101687 3 9.98875 9.937604 9.761488 10.228822 10.062396 10.301468 3 9.698537 9.937604 9.761488 10.228822 10.062396 10.301249 1	48	The second second			A STATE OF THE REAL PROPERTY.		4 (8000-00-00-00-00-00-00-00-00-00-00-00-00	
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	49			I HOUSE PARK				I III DOG TO
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	50							
53 9.697435 9.938040 9.759395 10.240605 10.064960 10.302565 7 54 9.697654 9.937067 9.759687 10.240313 10.062033 10.302346 6 55 9.698094 9.937822 9.760271 10.240321 10.062105 10.302146 5 56 9.698094 9.937822 9.760271 10.239728 10.062178 10.101687 3 57 9.6983313 9.937749 9.760564 10.239436 10.062251 10.101687 3 58 9.6985329 9.376769 9.76086 10.239436 10.062354 10.301687 3 59 9.698737 9.937604 9.761148 10.238852 10.062396 10.301249 1 59 9.698970 9.937531 9.761439 10.238561 10.062469 10.301030 0	200		1					9
53 9.697435 9.938040 9.759395 10.240605 10.064960 10.302565 7 54 9.697654 9.937067 9.759687 10.240313 10.062033 10.302346 6 55 9.698094 9.937822 9.760271 10.240321 10.062105 10.302146 5 56 9.698094 9.937822 9.760271 10.239728 10.062178 10.301406 4 57 9.698313 9.937749 9.760564 10.239436 10.062171 10.301687 3 58 9.6985329 9.376769 9.76086 10.239436 10.062346 10.301468 2 59 9.698751 9.937604 9.761148 10.238852 10.062346 10.301249 1 59 9.698970 9.937531 9.761439 10.238561 10.062466 10.301030 0	1							
55 9.6989313 9.937893 9.759979 10.240021 10.062105 10.302126 5 56 9.698094 9.937822 9.760272 10.239728 10.062178 10.301806 4 57 9.6983313 9.937749 9.760564 10.239436 10.062251 10.301687 3 58 9.698532 9.937676 9.760856 10.239444 10.062244 10.301468 2 59 9.698751 9.937604 9.761148 10.228852 10.062396 10.301249 1 10 9.698970 9.937531 9.761439 10.238561 10.062469 10.301030 0	53					A CONTRACTOR OF	OF REPORT ASSESSMENT OF THE PERSON NAMED IN	
55 9.6989313 9.937893 9.759979 10.240021 10.062105 10.302126 5 56 9.698094 9.937822 9.760272 10.239728 10.062178 10.301806 4 57 9.6983313 9.937749 9.760564 10.239436 10.062251 10.301687 3 58 9.698532 9.937676 9.760856 10.239444 10.062244 10.301468 2 59 9.698751 9.937604 9.761148 10.228852 10.062396 10.301249 1 10 9.698970 9.937531 9.761439 10.238561 10.062469 10.301030 0	154							6
	155	9.697874	9.93789	9.75997	10.24002	10.06210	10.302126	3
	155		9.93782	9.76027	10.23972	8 10.062170		4
	57	9.598313	9.93774	9.76056	10.23943	6 10.06225		3
	158					10,06232.		1 3
	159						10.301249	
se Co-sine.   Sine. Co-tang.   Tang.   Co-sec.   Sucant.	100		The second second					-
	1.80	Co-sine.	/ Sinc.	Co-tang	Tang.	Co-100	.   Sucani	107 3

28 Degrees.

	-	-	- 20	Degrees,	-	12000	
, M	Sine.	Co-sine	Tang.	Co-tang.	Secant	Co-see ,	201
10	9.671609	9-945935	9.725674	10-174326	EG-D-C4DB-C	10-125191	60
1 1	9.671847	9.946868	9-715979	10.274024	10.054112	10.328143	59.
1 2	The second second	9-945800	9.726284	80 873716	10.054200	10.121016	51
1 3	9.672321	9-945733	9.726588	10.173412	10.054267	10.117679	57
1 4	9.672558	9.945666	9.716892	10 173108	10.054334	10.337443	59
5	9.679795	9.945598	9-727197	10.272803	10.054403	10.327305	59
1 6	9.673032	9.9455 21	9-727501	10.272499	10/054460	10.320008	54
7	9.673268	9.945464	9.717805	10.171795	10.004516	10.326732	51
-8	9.673505	9.945396	#-71810p	10.171591	raidsaffaa	10 gubang.	51
9	9.673741	9-945328	9-7=8412	10.271588	10.054672	10.326259	54
10	9.673977	9-945761	9.7=8716	10.271284	10.054739	10.316013	50.1
EL	9.074213	9-945193	9.729020	10.270980	10.054807	10. 222787	69
3.5		9.945125	9.729323	10 170677	10.054876	10.325551	900
1 13	1 2 20	9.945048	9.729525	10.270174	10.054042	10.325210	47
14	9.674919	9.944990	9.729929	10.270071	10.005010	10.729081	46
1 45	9.675155	9-9449:2	9.730253	10.259767	10-055078	10.224845	45
15	9.675390	9-944854	9.730535	10.269469	10.055146	10.524610	44
17	9 67 5624	9-9447/16	9 7 308 3 5	10 269162	10.055314	10.334376	43.4
18	9.675859	9.944718	9-731141	10.268859	10.055282	10.324141	#
19	9.676094	9.944650	9-731444	10.068556	10.055350	10-313906	T
100	9.676338	9-944481	9.731746	10.268254	10.055418	10 323672	40
21	9.676562	9-944514	9-732048	10.257952	10.055486	10 311438	59
22	9.676796	9.941116	9-733351	10.067649	10.055554	10.323504	(38)
7.3	9-677030	9-911377	9.732653	20.257347	10.055623	10.315970	37
24	The second second	9-944309	9-732955	10.267045	10.055691	10.322716	791
25	9 677498	9-944341	9-733257	10.16743	10.055759	10.312501	35
1 26	9.677731	9.944172	9.733558	10.266442	10-0558#8	10.322269	34
27	9.677964	9-944104	9.733800	10.266140	10.055890	10.322036	33
28	9.678197	Control of the last of the las	9.734102	10.265838	10-055964	10.321503	33
20	9.678430	9-943967	9-734463	10.265537	10.056033	10,321570	31
130	9.678663	9-943899	9-734764	10.265236	10.056101	10.381357	150
31	9 678895	9.943830	9 735066	10 264934	10.056170	10:331105	24
32	9.679128	9.943761	9.735367	10.264633	10.050230	10.330576	2.8
33	9.679360	9.943693	9.735668	10.254333	10-056307	10.320640	17
34	9.679592	9.943614	9.735969	10/204031	10.050376	10.320408	160
35	9.679824	9-945555	9.736269	10.263731	10.056445	10.320176	35
35	9.680288	9.943486	9-736570	10.263430	10.050514	10.319941	1
38	9.680519	9.943417	9/737471	10.263129	10.056583	10.319712	#
39	9.680750	9.943279	0737471	10.162529	10.050721	10.319150	20
40	9.680982	9-943210	9.737771	10.262220	10.056790	10.314018	30
41	9.681213		9.738071	-			
41	9.681443	9.943141	9.738371	10,261629	10.056859	10.318787	12
43	9.681674	9.943072	9-738671	10,261329	10.056928	10.318557	18
1 44	9.681905	9.941934	9.738971	10.261020	10.057066	10.316095	18
45	9.682135	9.941864	9.739271	10-260720	10.057136	10.317865	15
46	9 682365	9.942795	9.739570	10.260430	10.057205	10.117619	14
47	100	9.942746	9.739870	10.160130	10.057274	10.317405	
48	1000	9.942656	9-740169	10.259831	10.057344	10.317175	No.
49	9.683055	9.942587	9-740468	10.259532		10.316945	11
50	- 60-0	9.942517	9-740767	10,259233	10.053483	10,316746	10
51	9.683514	9.941448	9.741066	10.258934	10.057550	10.316486	10
52	9.683743	9 942378	9.741365	10.298635	10.057623	10.316201	8
53	9.683972	9-942308	9.741664	10.158336	10.047602	SEDSEE.OL	7
54	9.684201	9.942239	9.741962	10.258038		10.315799	6
55	9.684430	9.942169	9.742261	10.257739		10.315570	5
56	9.684658	9.942099	9-74=559	10.257445	10.057901	10.315342	4
57		9.941019		10.257142	10.057971	10 315113	4
-	9.685115	9.941959		10.156844	10.058041	10-114885	2
59			9-743454	10,236546	10.058131	10.314057	
60			9-743752	10.250248	_	10.114439	a
34 /	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Secunt	M
		-	7.4	RALL CO.		Name and Address of the Owner, where	

_			191	segrees.			
M	Sine.	Co-sine-	Tang	Co-tang	Secant	Co-sec.	M
0	9.685578	9-941819	9743753	10.256248	10.058181	10.314419	60
1	9.685749	9-944749	9.744050	10/19990	10.058191	10.314201	59
2	9-686027	9.941679	9-744348	10.195592	10.058324	10/31/1073	58
1 3	9.686254	9-941600	9.744645	10.355555	10.058391	10.313746	57
4	9.686483	91941539	9-744943	10.255057	10,058461	10:313418	56
5	9.686709	9.941459	9.745240	10:254750	10.058938	10.111191	95
6	9.686930	9.941398	9-745538	10 254452	10.058602	10.313054	54
7	9.687163	9.941328	9.745819	rocasping	TO.058671	10.315837	53
18	q.687389	9.941258	9.746132	10.151868	10.058748		52
19.	9.687616	9.941187	9.745929	10/253571	10,048813		51
10	9.687843	9.941117	9.746726	10,253274	10.058883	10.312157	50
100	9.688069						-
325		9.941045	9-747023	10.253977	10.058954	10.311931	49
2.2	9.688295	9.940975	5-747349	10:252681	10.059025	10-311705	48
13	9.688511	94940905	9.747616	10.052350	10.059095	10.311479	47
24	9.688747	dradox34	0.747915	10-252087	10/020100	10.311153	46
125	9.685973	9,940763	9.748509	10.251791	10.059437	10.311028	45
16	9.689198	9.940693	9.748505	10,151495	10.059307	10.310801	# 1
37	9.689423	9.940622	9.748801	10.25P199	10.059378	10,310577	43
18	9 689648	9.940551	9.749097	10.150903	10.059449	10.310352	42
19	9.689873	9.940480	9-749393	10.250607	10.059510	10.310197	41
10	9-690093	9.940409	9.749089	10.250311	10.059591	10.300001	40
at	9,690323	9.940338	9.749985	10.250015	10.059662	10.309677	39
22	9.690548	9.940207	9.750281	10.249719	10.059733	10.309452	38
23	9.690772	9.940196	94750576	10.249424	10.059804	10.309218	37
24	9.690996	9.940125	9.750873	10.249128	10.059875	10.309004	36
25	9.691220	9.940054	9.751167	10.248833	10.059946	10.308780	35
16	9-691444	9.939981	9.751462	10.248 538	10.060018	10.308556	34
27	9.693558	0.939941	9.792757	10.248241	10.060089	10.308332	33
28	9.691892		9.752052	10.247948	10.060160	801808308	32
29	9.693115	9.939768	9-752347	10.247653	10.060232	10-307885	31
30	9.692339		9 7 (1642	10.247358	10.060303	10.307661	30
	9.692462	9 939625		10 2 (2062	10.066375		20
31	The Property of the Park	The second second second	9.752937	10.247063	The second second	10.309438	28
32	9.093785	9-939554	9.753831	10.246709	10.060440	10.307215	27
33	9.693008	9.939482	9.753526	10.246474	10.060513	10.306992	20
34	9.093331	A STATE OF THE PARTY OF THE PAR	9.753820	10.246180	10,060590	10.306769	_
36	9.093453	9-939339	9.754115		10.060661	10-206547	25
36	9.693676	9.939267	9-754409	10,245591	10-060733	10.306524	74
37	9-1093898		9.754703		10,060805	10.306102	23
38	9.694420		9-754997	10-245003		10.305880	22
39	9-09-8842			10-144709		10.305058	125
40	9:094504		9.795585	10/344415	10.061030	10.305436	20
43	9.694786	9.938908	9-755878	10:244522	10.061092	10-305514	19
42	9.695007	9.938836	9.796171		10.001104		18
43	95695229	9-938763	9.75646	10.241919	10.061137	10.304771	1.7
44	9.645450	9.938691	9.756759		10.061309	10,304550	16
45	4.645671	9.938619	9.797051	10.245948	10.06138	10,304329	19
46	9.69 5892	9.938547	9-757345	10:14165	10.06145	10.104108	114
47	9.696113		II SANCO CONTRACTOR OF THE PARTY OF THE PART	1 0000000000000000000000000000000000000	10,06152	10.303887	13
47	9.696334	9.938402			10.06159	10.303666	23
49	9.696554	9.938330	9-758224	10.241770	10.061670	10,303440	II
50	9.69677		T DATE OF THE PARTY OF	The second second			10
	9.69699					10.303004	'n
50	9.09721	COMMON PROPERTY.	I E-MATCHESIS				9
25	0.00741	0.0280	9.75910	10 71060	10.05105	ID SOME	1
25	0.5015	0.02705	577939	10.7104	10.06203	10 2022	6
54				10.24031			
55 56 57 58	9.697874		9.75997				
150	9.69709						1 3
120	9.59831			10.230436			
200	9-698531				10.06232		
59	9-69875					10.301249	_
100	9-093970			Street, Square, or other Dates			
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30 Degrees.

No.   Co-sine   Tang   Co-tange   Secant   Co-sine   X	-	_		30	Degrees.			
0 9.698970   9.93753   9.761439   10.238561   10.061469   10.30081   59   9.699189   9.937458   9.75073   10.238369   10.061469   10.30081   59   19.061469   10.37081   59   10.061469   10.30081   59   10.238369   10.061469   10.30081   59   10.238369   10.061469   10.30081   59   10.23836   10.061469   10.20083	10	t Sine.	Co-sine.	Tang.	Co-tang.	, Secant.	Ca-sec.	1.26
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28	Sine	Co-sine.	Tang.	Cò-tung:	Secant.	Coisec.	. 26
153			The Cake		-	10.000	
10	9.711839	91933066	9.778774	10.111125	10,066934	10.188161	00
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13	9.712260	9-932914	9-779345	10 110654	10.007086	10.287740	38
13	9.712469	9.932838	9.779632 9.779918	10,220368	20.007163	10.287531	37
4	9-712079	9:932762	9.779918	10.220082		10.287321	56
4 50	9.712889	9.932685	9.780203	10.219797		10.287122	55
	9.713091	9.932600	9.780489	80.219511	10,067391	10.286902	54
7 8	9.713308	9 932533	9.780775	10.219225		10.286692	53
8	9.713517	9.932457	9.781060	10.218940	10.067543	10.286483	52
19	9.713720	9 952380	9.781345	10.218654	10.067620	10.280274	51
10	9-713935	9.931304	9-781631	10.218369	10.067696	10.286065	50.
T.E	9.714144	9.932228	9.781916	10.218084	10.06:772	10.235856	49
22	9.714352	9.932151	9.781101	10.212299	10.067849	10.285048	42
13	9-714561		9.782486	10 217514	10.057025	10.285439	-
					10,068002	10.203439	47
14	9.714709		9-782771	10.117219	10.068079	10.385231	46
15	9.714978		9.783056	10.116944		10.28,012	45
16	9.715180	9-931845		10.216659	10.068155	10.284814	44
17	9-714394	9.931768	9.783626	10.115374	10.068232	10.284606	45
18	9-715502		9.783910	10.216090	10,068300	10.284398	47
19	9.715809	9.931614	9.784195	10.215805	10.068386	10.284191	41
20	9.716017	9.931537	9.784419	10.21 ( 521	10.058463	10.283983	40
2.1	9.716324	9 93 1400	0.784764	10 215236	19,068 540	10 28 3776	39
22	9-716432	9.931383	9.78;048	10.214052	10.068617	10 283 (68	38
23	9.716639	9.931306	9.785332	10 214068	10.06369.4	(0.283:6)	37
2.3	9.716846	9 93 1229	9.785616	10.214384	10.068771	10.283154	36
26	9-717093	9.931152	9.785900	10 214100	10.068848	10.282947	39
16	9.717259	9.931075	9.786184	10.213816	10.068925	10.282741	34
	9.717466	9.930998	9-786468	10.213532	10.069002	10 282534	33
28	0.717672	9 930921	9.786752	10.213248	10,069079	10.282327	32
	9.717673	9.930843	9.787036	10.212964	10.069257	10.282121	31
10	9.718089	9.930756		10.212681	10.069234	10.281915	
	Section 1					THE RESERVE AND ADDRESS.	30
31	9.718291	9 930688	9.787603	10.212397	10.069312	10 281709	29
33	9.718497	9.930611	9.787886	10 212114	10.069389	10.281503	28
33.	9.718703		9.788170	10/211830	10.069467	10.281297	27
34	y-718g0g	9.930456	9.788453	10.211547	10.069544	10.281091	26
35			9.788736	10.211264	10 069622	10.280886	25
36		9.930300		10.210981		10.280680	24
37	9.719525	9.930223	7.789302	10.210698	10.009777	10.280475	23
38	9.719732	9.930145	3.780585	10.210415	10.069855	10.280270	22
39	9-719935	9.930067	9.789868	(0.210132	10 060033	10.280065	21
40	9.730140		9.790151	10 209849		10,279860	20
		9.929911	The state of the s	10.209567		10.279655	19
M	- plantage			10.109384		10.079055	3
_	9-730549		9.790710	10.200000	10.070167	10.379451	18
2	9-730754	9-9-9755	701-10	10 209001	10.070345	10.279246	17.
MP.			9.791281	15.208437		10.278838	16
45			9.791503	10:208154			15
W.		9.919521	2.791846	10 207872	10.070,479	10.278634	14
P-	0.721570	9 9 29 442 9			10.070558	10.278430	13
38			2792410	10.207590	10.070636	10.278226	12
42				10.207308		10,278022	11
20	9.723181	9 429207	791974	10.207016	10.070793	10-277819	10
51				10.206744	10.070871	10/377615	9
52	9.722588			10.206468	10.070950	10.277412	8
53	9.722791	908972	793819	10.106181	10.071028	10.277200	7 6
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55			794383	10.205017	10.074185	10.276803	5
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10	6		9.928420		10.204211	10,071580	10.175790	60
ш	и		9.928342	9.796070	10.203930	10.071658	10.175585	52
ш	2	9.724614			10,203649	10.071737	10.275386	38
ш	3	9.724816	9.928183		10.203368	10.071817	10.175184	57
ш	в	9.725017	9.925104	MARKET SATISFACE AND ADDRESS OF THE PARKET SATISFACE AND ADDRESS O	10-203087	10.071896	10.274981	50
ш	5	9.735219	9.928025	0-797 94	10.202806	10.071975	10.274781	35
ш	10	9-724420	9,927946	9-797475	10.202525	10.072054	10.274510	<b>日本</b>
ш	7	9.725612	9.927867	9.797735	10.201145	30.072133	10.474378	53
ш	R	9.725823	9.927757	9.798036	10.201964	10.072213	10.27.0477	52
1	9	9.726024	9.927708	9.798316	10.201684	10.072292	10.273976	55
ш	10	9.726225	9.927029	9.798596	10,201404	10.072371	10,273775	339
и	11	9.726426	9-927549	9.798877	10.201123	10,072451	10.273574	<b>290</b>
ш	18	9.726626	9.927470	9.799157	10.200843	10.072530	10/273374	45
ш	13	9-726827	9-9=7390	9 799437	10,200583	10,072510	10-171171	42
ш	14	9.727017	9.927310	9.799717	10.200285	10.072040	10.272971	45
ш	15	9.727228	9.927231	and the second second	10.200003	10.072769	10.272773	41
ш	16	9-727428	9.927151	9.800277	10.199723	10.072849	10-272572	44
	17	9-727628	9.927071	9,800557	10.199443	10.072929	10.272372	411
ш	18	9.727828	9.926991	9.800836	10.199164	10.07,1009	10,272472	#1
м	19	9.728027	9.920911	9.801115	10.198884	10,073019	10,171971	18
IИ	20	9.728227	9.926831	0.801300	10.198604	10.073169	10,271775	45
	21	9.728427	9.925751	9.801075	10.198125	10 07 1249	10-27 (573	53-4
ш	22	9.718616	9.926671	9.801955	10.198045	10,073329	10/271374	38
ш	23	9.728825	9.926591	9.802234	10.197766	10.073400	10.271175	見
ш	24	9.729024	9.926511	9.802513	10.197487	10.073489	10.270476	20.0
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п	26	9.729422	9.926351	9.803072	10.196928	10.073649	ND.270575	29
и	27	9.729624	9.926270		10.196649	10.073730	x0x210119	22
ж	#8	9.729840	9.926190	g.803630	10.196370	10.073510	10.270180	25/1
и	29	9.730018	9.926110	9.803908	10.196092	10.073890	10.109981	35
N.	30	9.730217	9.926029	9.804187	10.195813	10,073971	10,269783	22
и	31	9.730415	9.925949	0.804466	10,195534	10.074051	10.200581	15.7
	32	9.730613	9.925868	9.804745	10.195255	10.074132	10.269187	28
	33	9.730811	9-925788	9.805023	10 194977	10.074212	10.259189	27
	34	9-731009	9-925707	9.805302	10.194698	10.074293	10,168991	311
	35	9.731206	9.925626	9.805580	10.194420	10 074374	10,26F794	21
	36	9.731404	9.925545	9.805859	10 194141	10.074455	10,268596	24
	37	9.731602	9.925465	9.806137	10.193863	10.074535	to,268398	22
ш	38	9 731799	9.925384	9.806415	10.193565	10.074585	10,268201	22
и	39	9.731996	9.925303	9.806693	10.193307	10.074697	10.258004	23
и	40	9.732193	9.925222	9.800971	10.193029	10.074778	10/201807	40.4
F	41	9.732390	9.925141	9 807 249	10.192751	10,074859	10.267510	10
	42	9.732587	9.935060	9.807527	10.192473	10.074040	10:267413	8 1
	43	9.732784	9-924979	9.807805	10.192195	10.075021	10.257215	17
	44	9-732980	9,924897	9.808083	10.191917	10.075103	10.257000	15
	45	9.733177	9 924816	9.808361	10.191639	10.075184	10.166823	15
	46	9-733373	9.924735	9.808638	10.191300	10.075265	10.266627	100
1	47	9-733569	9.924654	9.808916	10.191084	10.075346	10.265431	131
-	48	9 733765	9.924572	9.809193	10.190807	10.075418	10,266235	131
1	49	9.733961	9,924491	9.809471	10.190529	10.075509	10,166039	0
L	50	9.734157	9-924409	9.809748	10.190252	10.075591	10.265845	10
1	şı	9 734353	9.924328	9.810025	10.189975	10.075572	10.26 (647	
1	52			9.810302	10.159698	10.075754	10.26 6451	- 8
1	53		9.924164		TARGET MATERIAL PARTY AND ADDRESS OF THE PARTY	10.075820	10.265266	17
1	54		9.924083		10.189143	10.075917	10.265061	- 6
1	55		9,924001		10.188866	10.075999	10,25,4865	3
1	30		9.923919		10.188590	10.076081	10 164670	
	57		9.923837		10.188313	10.076163	10.264475	31
	58	9-735719	9-923755	9.811964	10.188036	10.076245	10,264281	3
	59	9-735914		9.812241	10.187759	10.076327	10.254036	中田の十〇
	60	-	9-923591	9.812517	10.187483	10.076409	10,263841	0
8 10	1	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec-	Secant.	34.
138			-	- 53	Degrees	-		

33 Degrees

33 Degrees	
Sine. Co-sine, Tang. Co-tang. Seemt , Co-sec	M
9.716109 9.913531 9.713517 10.187483 10.076409 10.163891	63
9.736303 0.423400 4.812744 10 187206 10.076491 10.263697	
9.736498 9 923427 9.813070 10.186930 10.076573 10.263502	30
4.7566ga q 925145 4.811147 10.186653 10.076055 ED.263208	87
9.736886 9.923261 9.813611 10.186377 10.070737 10.263114.	50
9,737080 9 923181 9.813899 10.186101 10.070819 10.262920	55
9.737274 9.925098 9.814174 10.185825 10.076902 10.262746	54
19 737467 19 917016 3. 814452 10.185548 10.016984 10.262535	41-
9 737661 (Luling ; 3 814725 10.185252 10.077067 10.262459	52
19-737859 9-9226;1 9-815004 10-184086 10-077149 151-262145	51
9.718048 9.922768 9.815279 10.184721 10.077232 10.201952	30
The state of the s	_
9-73844 9-922686 9.815555 10.184445 10.097314 10.261759	49
9.738434 9.922653 y 813831 to 184169 to 077397 to an 1666	43
9.733627 9.922 (20) 9.816107 10.183893 10.077480 10.261373	47
9.738820 9.922438 9.816382 10.183618 10.077562 10.261180	40
9.739013 9.912355 9.816658 10.183342 10.077645 10.260987	45
9.739206 9.925272 9.816933 10.183067 10.077728 10.260794	44
9.739398 9.922889 9.817309 10.182791 10.077812 10.260502	43
9.739590 9.933106 9.817484 10.182516 10.077894 10.260410	45
9.739783 9.922023 9.817759 10.182241 10.077977 10.260217	440
9.739973 9.921940 9.818035 10.181965 10.078060 10.260025	40
9.740167 9.921857 9.818310 10 181690 10.078143 10.259833	39
9-749359 9-921774 9-318485 10-181415 10-078226 10-2596-51	38
9.740550 9.921691 9.818860 10.181140 10.078309 10.259450	37
9 740741 9 921607 9.819135 10.180865 10.078393 10.259258	36
9.740934 9.021 524 9 819410 10.180590 10.078476 10.259000	35
9.741325 9.921441 9.814684 10.180316 10.078559 10.258875	34
9-741316 9-921357 9-319959 10-180041 10-078643 10-158684	33
9-741 (08 9.921 274 9.820134 10.179766 10.078726 10.248492	32
9-741644 9 931190 9 810508 10 179492 10.078810 10.258301	370-
9-74188919-921107 9 820783 10-179217 10-078893 10-258111	-
	30)
9.742080 9.921023 9.821057 10.178943 10.078977 10.257920	29
	28
9 744462 9.920856 9.821606 10.178394 10.079144 10.257538	27
	26
7 742842 9-923688 9-822154 10-177846 10-079312 10-257158	25.
	24
9-743243 9-920520 9-822703 10-177197 10-079480 10-256-77	23
9-7-63413 9-920436 9-822977 10-177023 10-079564 10-256587	22. 3
	원내
9.743791 9.920168 9 813524 10.175476 10.079732 10.256208	20
9-743982 9-9-0184 9-823798 10.176202 10.079816 10.256018	19:
9.744171 9.920099 9.824072 10.175928 10.079901 10.255820	18
9 744361 9.9 DOOR 9.824345 10.175655 10.079985 10.255639	17
9-744550 9-919936 9.824619 10.175381 10.080069 10 355450	16
9-744739 9 919840 9.824893 10.175107 10.080154 10.25 5061	15
9-744928 9-919702 9.825166 10,174834 10,080238 10.255072	14
9.745117 9.919677 9.825439 10.174561 10 080323 10.254883	6
9:745306 9-919503 9.825713 10.174287 10.080407 10.254694	12
an analysis for the country of the c	n
9.74683 9.919424 9.826259 10.173741 10.080576 10.256317	10
	-
4.745871 9.919339 9.826532 10.173468 10.080661 10.254129	2
9.746065 9.919254 9.826805 10.173195 10.080746 10.253940	8
9.746248 9.919169 9.827078 10.172922 10.080831 10.253752	3
9.746436 9.919085 9.827351 10.172649 10.085915 10.233564	6
9.746624 9.919000 9.817624 10.172376 10.081000 10.257176	5
9.745812 9.918915 9.827897 10.172103 10.081085 to 253188 9.745499 9.918830 9.828170 10.171830 10.081170 10.251001	140
9-740999 9-91853019-518170 10-171830 10-081170 10-255001	3
9-747187 9-918745 9.828442 10.171558 10.051255 10 252813	2 1
9-747374 9-918659 9 828715 10.271285 10.081341 10.252526	10
9.747502 9.918574 9.828987 10.171013 10.081426 10.252438	0
Co-sine   Sine.   Co-tang.   Ta g.   Co-sec.   Secant.	M
PA December 1	

			39	Begreen.			
Var.	Sine -	Co-sine.	Tang.	Costang.	Secant	Co-sec.	W
21		-	-	-	-	the same of	200
0	9 747562	9.918574	9.821917	10.171013	10,081416	10.252438	00
D	9-747749	9.918489	n.829260	10.170749	10.081511	10.252261	59
2	9.747936	9.918494	0.820532	10 170468	10.081596	10.252064	58
	9.748123	9.918318	9.829805	10 170/05	10.081681	10.241877	57
3							
4	9.748310	9.918233	9 830077	10.159923	10 081767	10.251590	59
5	9 748497	9.918147	9.830349	10.169651	10.081853	10.251503	35
6	9.748683	9.918062	9.830621	10.159379	10.081938	10.251519	54
7	9.748870	9-917976	9.830893	10.169107	10.082024	10.252130	53
7 8	9.749056	9 917891	9.831165	10.168835	10.082100	10.250944	54
		9.917805	9.831437	10.168563	10.083105	10-150752	
9	9.749243		The second second				51
10	9 749439	9/917719	9,831709	10.168291	10.081281	10.250574	50
2.0	9.749615	9.917534	9.811981	10.168010	10.081366	10.250386	40
12	9.749801	9.917548		10.167747	10.082452	10.150100	48
					10.08248		
13.	9.749987			10.167475		10.250011	47
14	9.750172	The second second		10.167204	10.082624	10.149818	45
19	9 750358			10.166932	10.082710	10.149641	45
15	9-750543	9 917204	9.813339	10.166661	10.082795	10.149457	44
17	9-750729			10:166380	10.082882	10.249271	43
18	9.750914		9.81128:	10 166118	10.081968	10.149086	42
		RESIDENCE AND A	MIPS AND REST	10.155846	10.083054		
19	9-751099					10.248901	91
20	9.751284			10,165575	10.083141	10.148716	40
21	9.751469	9.416773	9.834696	10.165304	10.083127	10 248 4 11	50
12	9.751654			10.165035	10.083313	10.148146	1
23	9.751839			10.164762	10.08 5400	10.248161	10.00
				10.164491	10.083486	Design Street	130
24	9.752023					10.247977	1 28
25	9.752208			10.164320	10.083573	10.747791	35
26	9.752392			10.163049	10.083659	10.247608	30
27	9.752576	9-916254		10.163628	10.083746	10.247424	33
28	9.752760		9.836593	10.163407	10.083833	10.247240	11
=9	9-752944	1 1 1		10.163136	10.083919	10.247046	31
30	9.753128	A STATE OF THE PARTY OF THE PAR	The second second	10.163866	10.084006	10.245832	
		-	And the latest the lat	Michigan Company	The second second	The second second	- 30
34	9.753312	9.915907	9.837405	10.162595	10.084003	10.245688	59
32	9.753495	9.915820	9.837675	10.162325	10.084180	10.246505	35
33	9-753670			10.162054	10.084267	10.246521	27
34	9.753862		Hardin Carlotte	10.161784	10.084354	10 246138	46
	9.754046			10.161503	10.084441		
35				The country of the country of		10-245954	_
36	9.754229	The second second		10.161243	10.084548	10,245771	100
37	9.754412			10,160973	10,084615	10.345588	128
38,	9-754595	9.915297		10.160703	10.084703	10/245405	32
39	9-754778	9.915210	9.839568	10.160432	10.084790	10.245222	21
40	9.754960		9.839838	10 160162	10 084527	10.245040	20
_	-				THE RESERVE AND ADDRESS.		=
951	9.755143	9.915035	9.840108	10-159892	10.084965	10.264857	10
42	9 755336		9.840378	10.159622	10.085052	10.244674	18
43			9.840647	10.159353	10.085140	10.255402	17
44	9.755690	9.914773	9.840017	10.159083	10.085227	10.211310	16
45	9-755872		9.841187	10.158813	10.089315	10.244128	Iç
46	9-756054		9.841457	10.158543	10.085402	10.221035	
	0.756236	-	9.841726	10.158274	10.08		
47			9.841996	CONTRACTOR OF THE PARTY OF THE	10.085490	10.241164	12
48	9-756418		The second second	10.158004	10.085578	10 243582	III III
49	9.756600	Marie Control of	9.842266	10.157734	10.085666	10.243400	EE
50	9.7567.82	9.914246	9.842535	10.157465	10.085754	10.242218	10
50	9.756963	9.914158	9.842805	10.157105	10.084842	10.242017	1
52	9.757144				HEADER TO SERVICE	DESCRIPTION OF THE PERSON OF T	6
	0 757936	0.011090	0 81174	10 7555	10.001930	10,243856	2
58	3-13/240	3.313933	9.443343	10.150064	10.086018	10/14/10/4	3
54	973730	9-913494	9.043012	10.156388		10,242493	6
55					10.086104	10,247582	· K
56	9.757869	9.913718	9 844151	10-155849	10.086281	10.242131	4
57	9.758050	9-913630	9.844430	10.1555804	10.086370	10,141950	20.00
68	9.758230	9.911041	9.844580			10.541730	1
60						10.241,89	13
55 55 57 58 59 60			9.845227		0.006615		
	Coning	-		THE REAL PROPERTY.	STEEL STATE OF THE PARTY OF THE	10.241409	0
24	Co sino	Sine	Co-tang	Tang.	Co-sec	Secunt.	- 24
		-	77.7	The Parks			

35 Degrees.

_		_		P. Carrette	-		
MI	Sine.	Co-sine.	Tang.	Co-tang.	Secont	Co-sec.	16 1
		E CONTRACT	. 8	10 101000	10.086615	A TANADA	60
1 2	9-758591	0.913305	9-845337			10.141.109	DAME:
1 1	9.758772	9-913270		10.154504		10.241228	59
10.0	9-758952		9.845704	MACHINE & SAC REL	10'089813	10.241048	38
1 3	9-759137	9.913099	9.844033		10.086901	10.140868	57
li ă	9-759314		9.846102	10:153698	10.086990	10.140688	56
1117	9-759493	0.914942	9.846590	10.153430	10.087078	10.140508	55
1113	SIMONETA		4.846819	ORGANIZATION OF THE PARTY OF TH	10.087161	10.240318	
1 9	9-759072	9.914833			DOMEST COMPANY		54
1 2	9-759-55	9.952744	9.847107	10.152893	10.087356	10-240148	53
1 8	9.760031	9.912555	9.847376	10.152614	10.087345	10,339969	52
1 0	9.260211	9.911566	9.847044	10.153356	10.087414	10.339789	60
10		9.912477	9.847913	10.142087	10.087 (13	10.339610	50
				-	and the last of th		
		9 912388	9.848181	10:151819	10.087613	10,839431	49
13		9.912299	2.842449	10.151551	10.057701	10 139152	48
73	9.760927	9.912210	9.848717	10,154483	10.087790	10.139013	47
14	9.161100	9.912121	9.848986	10.151014	10.087879	10.275894	46
15	9.761284	9.912034	9-849954		10.087969	10.238715	
16				10.130,40	10.088048	10.238416	
	9.761464	9.911943	9.549523	10.150478			44
1 47	9.761642	9 911853	9-849790		10.088147	10.05835%	43
138	9.761821	9:911763	9.850058	10.149942	10.088137	10.138119	42
19	9-761999	9-911674	9.859335	10.149675	10.088316	10.138001	41
20	9.762177	9.911584	9.850593	10.149407	10.088416	10,037813	40
				The second second	STREET, VALUE		
21			0.850361	10.149139	10.058505	10.337644	39-
2.7			9.857129	10.148874	10.088595	10.737466	38
2.5		9-911315	9 851396	10.148604	10.088685	1Q-337488	37
22		9.911226	9.251664	10.148336	10.088774	10.337414	36
2			9.851931	10.148069	10.088864	10-136933	35
18			9.852199	10.147801	10.088914	10.036045	
							34
2			9.852460	10.147534	10.089044	10.136448	33
23	9.263600		9,852753	10.147267	10.089134	10.336400	32
29	9.763777	19.919776	9.853001	10,146999	10.089224	10.216223	31
30	9.763954		9.853168	10.146737	10.089314	10-236046	30
	The second second						
31			9.853535	10,146465	10.089404	10.035869	39
1 3		9 910506	9.853802	10,146198	10.089494	10,235093	28
33		9.910415	9-854069	10.145931	10.089:85	10.235515	37
34		9.910385	9.856336			10.235338	16
3			9.854003	10.145307	10.089764	10.235162	25
11.0	Nevadada			100000000000000000000000000000000000000	100	10.233182	_
34			9.854870	10,145130		10.23498 5	24
33	9.765191		9.855.137	10,144863	10.089946	10.234809	43
38			9.855404	10,144596	10.090037	10.234633	92
34	9-765544	9.909875	9.85567 6	10.144339	10.090127	10.234456	at
100	9.764720			10,144062	10.000218	10.234280	20
				Contract of the last	Charles water		
1.4	9.765891			19-143796			19
14	9.76607	9.909601			10 090399	10.233928	18
14			9.856737		10.090490		17
14							16
12							15
13							100000
			The second second	10.142403		10.233226	14
14							13
1.4							12
4	9 9-76730	9,908964	9.858336	10.14166	10.091016	10.232700	12
15	9,76747				10.091127	10.232424	10
				-	The second	-	
5							9
1 5	2 9 76781				10.091510	10.232176	8
1 5	1 9.76799	9 9.008 599	9.859400	10.140600	10.091401		
1 5							
1 3							
1 5					TO COLUMN		
		a y yo8324		No. of Concession, Name of Street, or other Persons, Name of Street, or other Persons, Name of Street, Name of	10.091676		
1 5	2 9.76869	7 9-908233		and the same of th	10.001767	1 10 10 10 10 A 10 A 10 A 10 A 10 A 10	
1 5	8 9,76887	19.908141	9,860730				
	9 9.70904					10.230955	
1.0	0 9.76921	9,907958	9.861161	10. LTK7.30	10.091041	10.230781	0
-	N. California	3			1		-
	Co-sine	Sine.	Co-tang	Tang-	L'o-sec.	Secant	36
		_	20.0	1			-

	Charles	
N   Sine.   Co-sine. Tang. Co-tang.   Secant.	Co-sec.	76
0 9,769219 9,907958 9,861161 10.138739 10.092042 1	D 230781	60
	0.130607	59
	10.230434	58
	0.130260	57
	0.130087	150
THE CONTRACT CONTRACT CONTRACT OF THE CONTRACT	0.229740	53
	10.229(6)	183
	10.219394	52
	10.229221	51
10 9.770952 9.907017 9.863915 10.136085 10.092963 1	10.229048	50
Hinde F. H. E. Hillion J. P. L. State J. P. H. Martin, county beautiful P. State H. Bouley, J. St. P. J. Lin	10.228875	149
12/9.771298 9.906852-9.864445 10.135555 10.093148	10.128701	148
THE PERSON NAMED AND DESCRIPTION OF THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TO THE PERSON	10.228510	147
THE PROPERTY OF THE PROPERTY O	10.118357	40
L Brown Colonial Colo	O.EESOT)	44
THE RESIDENCE OF THE PROPERTY	10.227521	43
	0.1117669	42
	10.337497	11
30 9.771675 9.906111 9.866564 10.133436 10.093889 1	10,127525	AD.
21 9-772847 9.906018 9.866829 10.133174 10.093982 1	0.227455	39
	10/225082	38
13 9.773190 9.905832 9.867358 10.131642 10.094168 1	10, 2362 10	37
	0.236610	1
THE STORY OF THE S	10.226467	185
THE RESIDENCE OF THE PROPERTY	10.226296	185
THE RESERVE OF THE PROPERTY OF	10.226125	11
The state of the s	10.125787	31
THE PROPERTY AND PROPERTY OF THE PROPERTY OF T	10.225612	50
	0.115441	29
	10. 11 517 1	26
	0.115701	27
	10, 224930	.25
THE RESIDENCE OF THE PARTY OF T	0.114760	25
	10.224590	24
	D. 22442D	H
IN THE PROPERTY OF THE PROPERT	0.224250	21
The state of the s	0.223010	20
THE RESIDENCE OF THE PROPERTY	0.212743	18
THE PART OF THE PARTY OF THE PA	0.221571	17
	0.221232	36
	0.221003	25
46 9.777106 9.903676 9.873430 10.126570 10.096324 1	0.272894	14
	0.222725	移
THE RESIDENCE OF THE PROPERTY	0.222558	糖
	0.222387	10
	0.222249	
	0.222050	2
THE RESIDENCE OF THE PROPERTY	0.121221	
	0.221713	6
\$5 0.778024 0.002824 0.8758CD TO. (24300) 10.007176 10	0.111376	5 6 5
	0.221208	4
57 9.778960 9 902634 9.876326 10.123674 10.097356 10	0401110	4 5
58 9.779128 9.902539 9.870539 to 123411 10.097461 10	D 200872	2
	0.110705	
The second secon	0.110537	0
In Co-sine. Sine. Co-tang. Tang. Co-src S	ecant	24.

37 Degrees.

			37	Degrees.			-
. 26	Sine	Co-sine.	Tang	Co-tang.	Secunt.	Co-sec.	76. 4
To	9-779463	0.002340		10 111556	10.397691	10.300137	60
					10.697747		59
2					10.047542		58
13					to.borest		57
					10.098035		56
					10.098125		55
6					10.098224		54
1 2	9.780634	9.901681	9.878953	10-121047	10.098319	10-219306	53
8					10,098415		52
9					10,098410		51
30	9.781734	9.901394	9.879745	10.120259	10:098606	10.218800	50
133	9.781301	9.901098	9.880003	15.119997	10.098701	10:218699	49
12	9.781468	9.901202	9.880265	10.119735	10.008798	10,218532	48
133	9.781634	9 901106	9.880658	10.119472	10.098894	10.218366	47
14	9.781000	2,901010	9.000790	to tridato	10.098990	10.215200	46
					10,099086		45
					10,099182		44
17					10,099278		43
18					10,099374		42
119					10,099471		41
20	THE REAL PROPERTY.				10,000162	Name of Street, or other Persons, Name o	40
2.1	9.782961	9.900339	9.882625	10/117375	10.099663	10.217039	39
					10.099760		38
=3	9.783292	9,900144	9.883148	10.116854	10.099856	10.216708	32
						10.215542	39
25					10.100049		125
	9.783768	9.899854	9 881914	10.110065	10.100146	10.216212	134
27				10.115804		10-215047	33
28					10.100145		38
						10.215718	38
30	9-784447	9.899407	0.884630	10.115020	10.100533	10,215553	10
31	9.784612	9.899370	9.815242	10.114758	10,100630	10.215388	29
32	9.784756	9.899273	9.885503	10.114497	10:100727	10.215224	28
33	9-784941	9.899276	9.885765	10.114235	10.100824	10.215059	42
34	9.785105	9.899078	9.886026	10.113974	10.100922	10-214895	20
					10.101019		45
					10.101116		24
						10.214403	23
						10-214239	22
39	9.785925	9.898592	9.887333	10,112667	10.101408	10-114075	33
47					10.101506		20
41	9.786252	9.898397	2.887855	19.112145	10-101603	10-213748	19
42	9.786416	9.898299	9.883116	10.111384	10.101704	10.213584	18
1 43	19.780579	9.898202	9.888377	10.111623	10.101708	10-243424	17
44	9.786742	9.898104	9.888639	10.111361	10.101896	10.213258	16
45	9.786906	9.898006	9.888900	10,111100	10,101994	10.213004	155
46	9-787069	9.897908	9.889160	10.110840	10.103092	10.212931	184
47	9.787232	9.897810	9.889421	10,110579	10.102100	10-212769	43
48					10.102288		82
		0.897014	9.889943	10-11005	10.105286		(165)
59	-	The second second	1	10.109790		10.512230	10
1 51	9-787883	9.89741	9.89046	10.10953	10-108585	10-212117	9
32	9.788054	9.897320	9.890729	10,10927	10.102080	10.211955	3
58	9:788208	9.397121	g.Xggg%(	10,10901	10.10277		7
	91788370	9.897.123	9.891247	10,10875	10.10287	10-211630	6
55	9.788531	9 897024	0-891507	10.10849	10-102074	10-211458	5
	9.788694			in inkaj:			4
57	9.788856	9.896848	g.Agzun's	10-10797	10-103170		3
58	9-789018			10-10771			1 3
				10.10745			100
60	9:789342	9.896530	9.59281	10-107116	10.10346		0
100	Cosine	Sine.	Co-tang	Taug.	Codec.	Securit.	1 31
-		April 1997					

-			- 50	archices.		_	
36	Sine.	Co-sine:	Tang.	Co-tang.	Secant.	Co-sec.	×
0	9.789342	9.396538	9.892810	10.107190	10,103458	10.210548	60
1	9.789504		0.803070	10 106010	10.103467	10.210496	69
	9.789005	0.890334	9.893331	10.106660	10.103665	10.210335	58
3	9.789817	9.590230	9.893591	10.100400	10.103764	10 210173	97
	9.789988		9.893851	10,106140	10.103863	10.810013	56
14	9.790149	9.596018	9.894111	10.105869	10.103961	10.209851	55
56	9.790310	No. of Concession, Name of Street, or other party of the Concession, Name of Street, or other pa	9.894371	10.10(620	10.104061	10.200000	32 54
	9.793471	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN COLUMN 1	9.894632	10-105368	10.104160	10.009539	53
1 2	9.790632		9.894893	10.105108	10.104259	10.209368	52
	9.790793		The second second	10.104848	10.104359	10.100207	31
12		9.895041	9.895158	THE RESERVE AND ADDRESS.	10.104458	10.309046	50
10	9.790954	9.895541	9.895413	10-104588		-	
12	9.791115	CONTRACTOR AND ADDRESS OF	9.895072	10.104328	10.104557	10.208885	49
12	9.791275	9.895343	9.895932	10.104008	10:104657	10.208725	48
13	91791430	9.595244	9.896192	10.103808	10,104750	10.208554	47
14	9.791596	9.895145	9.896452	10.103548	10.104855	10.108103	46
15	9:791757	9.895045	9.896711	10/10/198	10.104955	10.308243	45
10	9.791917	9.894945	9.896971	10,103029	10.105055	10.108087	44
17	9.792077	9.894846	9.897231	10.102769	10.105154	10-107923	43
18	9.792237	9.894746	9.897491	10.102509	10.105254	10.007763	42
19	9.792397	9.894646	9.897751	10.102249	10.105354	10 10/603	41
20	9-792557	9.894546	9.898010	10.101990	10.105454	10.307445	40
21	9.792716	9.894446	9.898270	10.101730	10.105554	10.007284	19
22	9.792876		9.898530	10:101470	10.10(554	10.207124	38
13	9.793035	9.894246	9.898789	10.101211	10,105754	10. 100g0 c	37
24	9.793195	9.844146	9.899049	10.100951	10:105854	10.206804	16
25	9.793354	THE PERSON NAMED OF	9.899308	10.100593	10.105054	10 205045	35
26	9-793514		9.899568	10:100432	10.106014	10.201486	54
27	9.793075	9.893846	9.899827	10.100173	10.106144	10.206127	11
128	9.793832	9.893745	9.900086	10 000014	10 106200	10.006168	1
29	0.793001	9.893645	9.900346	10 099654	10.106355	10.20600g	31
10	9.794150	9.893544	9.900605	10 090395	10.106856	10 10 15 150	20
	the same of		Statement with		-	-	_
31	9.794308	9.893444	9.900864	10.099136	10.106556	10.205692	39
32	9.794467	9.893343	9.901114	10.098876	10.106657	10.205533	28
33	9.794636	Contract of the last	9.901383	10.098617	19.100757	10.205374	敖
34	9.794784	9.893142	9.901642	10.098358	10-106898	10.109216	20
35	9-794942	9.893041	9.901901	10.008099	10.100959	10.005052	25
196	9.795101	9.892940	9.902160	10.097840	10.107060	10.104895	25
37	9-795259	9.892839	9.902419	10.097584	10.107161	10.104741	23
38	9.795417	9.892739	9 902679	10.097325	10.107161	10.104583	22
39	9.795575	9.892638	9.902938	10.097062	10.107361	10-204425	23
40.	9.795733	9.892536	9.903197	10.096803	10.107464	10.204267	20
41	9.795891	0.892414	9.909455	10.096545	10.109(6)	10/104109	19
42	9.790049	9.892334	9.903714	10.096286	10.109666	10/20/19 (1	15
43	9.796206	9.892275	9.903973	10 046017	10.107767	10.203794	17
44	9.796364	9.892132	9.904111	10.095768	10.107868	10/201616	16
45	9.796521	9.892030	9.994461	10.007500	10.107970	10/103470	15
46	9.796679	9.891929	9.904750	10.009150	10.108071	10.203301	14
47	9 796826	9.891827	9.905008	10.004991	10.108173	10.401164	100
48	9.790993	9.891726	9.905267	10.094733	10.108274	10.203007	12
49	9-797150	9.891624	9.905126	10.094474	10.108176	10.202810	100
50	9-797307	9.891523	9.905784	10.094216	10.108477	10.200501	10
				-		-	
51	9-797464	9.891421	9,906043	10.093937	10.108579	10.303536	3
SE	9.797021	9:891319	9.906302	10.093698	10.108681	10.301179	2
93	9-797777	9.091217	9.900500	15.093440	10.100753	10.101111	1
54	9-797934		9.905819	10 093181	10.108885	10.202066	6
55	9.798091		9.907077	10,092923	10-108987	10/101909	***
50	9-798347	9.890911	9.907336	10.092664	10.109089	19/201753	100
57 58	9.798403	9.890809	9-907594		10.109191	10.201517	3
58	9.798560		9.907852		10.109293	10,201440	
59	9.798716		9.908111	10.091889	10.109395	101201284	2
00	9.798872	9.890503	9.908369	10.091631	10.109497	10 201133	0
59 00 3	Co-sine.	Sine.	Co-tang.	Tang.	Co-sec.	Separat	340
	-	-	75.7				

M.   Sine.   Co-sine   Tang.   Co-tang.   Secant   Co-sice   M.	J	-	100000	200		Degrees.	-		100
O   9,798871   9,890303   9,908369   10.091631   10.109497   10.201128   60.90988   10.091631   10.109497   10.200516   57   10.99598   10.109701   10.200516   57   10.99598   10.109701   10.200516   57   10.99598   10.109701   10.200516   57   10.99598   10.99948   10.09914   10.109070   10.200506   57   10.99598   10.109070   10.200506   57   10.99598   10.109070   10.200506   57   10.99598   10.109070   10.200506   57   10.99598   10.109070   10.200506   57   10.99598   10.109070   10.200506   57   10.99598   10.109070   10.200506   57   10.200508   588588   9.990477   10.20058   58   10.20058		1 36	Sine.	Co-sine.	Tang.	Co-tang.	Secant	Co-sec.	M
1	1	0	9.798872	9.890503	9.908369	10.001621	10.100407	10,201128	-
2 9,799184   3,890498   9,009144   10,00985   10,10985   10,20066   57   9,79945   9,809093   9,00940   10,00938   10,10102   10,20050   56   9,79965   9,88988   9,09918   10,00938   10,11012   10,20094   54   9,79965   9,88988   9,09918   10,00983   10,11012   10,20094   54   9,79966   9,88988   9,09918   10,00983   10,11012   10,20094   54   9,79966   9,88988   9,9918   10,00983   10,11012   10,20094   54   9,80047   9,889687   9,910693   10,08965   10,11012   10,20094   54   10,00883   10,11012   10,20094   54   10,00883   10,11012   10,20094   54   10,00883   10,11012   10,20094   54   10,00883   10,11012   10,10973   51   10,00893   10,11012   10,10973   51   10,00883   10,11012   10,10987   51   10,00883   10,11012   10,10987   51   10,00883   10,11012   10,10987   51   10,00883   10,11012   10,10987   52   10,00883   10,11012   10,10987   52   10,0087   10,11042   10,10987   52   10,0087   10,11042   10,10987   52   10,0087   10,11042   10,10987   54   10,0087   10,0087   10,0087   10,11042   10,10987   47   10,0087   10,0087   10,11042   10,10987   47   10,0087   10,0087   10,11042   10,10987   47   10,0087   10,0087   10,11042   10,10987   48   10,0087   10,0	Ī	1001	9.799028						
3 9-799339   9-809105   10.009086   10.10905   70.20005   57 5 9-79961   9.880989   9.909660   10.009081   10.10907   10.200050   55 5 9-79961   9.880988   9.909918   10.009081   10.110010   10.200349   55 6 9-79962   9.880988   9.909918   10.009081   10.110010   10.200349   55 7 9-799962   9.880988   9.909918   10.009081   10.11012   10.200098   53 8 9.800117   9.889682   9.910435   10.089367   10.110128   10.199883   52 9 9.800217   9.889682   9.910435   10.08936   10.110128   10.199883   52 10 9.800217   9.889679   9.91063   10.08094   10.110123   10.199267   50 11 9.800382   9.889374   9.911209   10.088376   10.11073   10.199263   48 13 9.800892   9.88968   9.911724   10.088376   10.110323   10.199263   48 14 9.801210   9.88866   9.911204   10.088376   10.11033   10.199263   47 14 9.801210   9.88866   9.911204   10.088376   10.11036   10.199263   47 14 9.801210   9.88866   9.911204   10.088376   10.11036   10.199263   47 14 9.801210   9.88866   9.911204   10.088376   10.111036   10.19965   47 14 9.801210   9.88866   9.912498   10.087502   10.111142   10.198644   44 17 9.801210   9.88865   9.912498   10.087502   10.111142   10.198644   44 18 9.801665   9.88865   9.912498   10.087502   10.111452   10.198644   44 19 9.801810   9.888544   9.91371   10.086273   10.111452   10.198644   44 19 9.801810   9.888544   9.91371   10.086273   10.111452   10.198644   44 19 9.801810   9.888344   9.91371   10.086729   10.111452   10.198644   44 19 9.801810   9.888344   9.91371   10.086729   10.111452   10.198644   44 19 9.801810   9.888344   9.91371   10.086724   10.111556   10.198077   38 20 9.801840   9.888344   9.91371   10.086724   10.111556   10.198077   38 21 9.801840   9.888344   9.91371   10.086724   10.111556   10.199764   30 22 9.801840   9.888344   9.91371   10.086748   10.111656   10.19764   30 23 9.801860   9.88760   9.91457   10.086743   10.111659   10.19764   30 24 9.801860   9.88760   9.91450   10.086749   10.111678   10.19764   30 25 9.801870   9.88760   9.91450   10.086749   10.111763   10.19767   30 25 9.	ı	2				10.091114	10.109702	10 200816	58
4   9.799495   9.89093   9.090602   10.090340   10.110012   10.200349   56   9.799651   9.889988   9.090918   10.090082   10.11012   10.200149   54   79.799602   9.889785   9.910177   10.080823   10.11012   10.200149   54   8.800177   9.889628   9.910477   10.080823   10.11012   10.120008   53   9.800273   9.889579   9.910693   10.080807   10.110421   10.199728   51   10.980823   0.889579   9.910693   10.080807   10.110421   10.199728   51   10.880823   0.889879   9.910693   10.080807   10.110421   10.199728   51   10.880823   0.889827   9.911467   10.088533   10.110729   10.199263   48   49   9.800823   9.889374   9.911467   10.088533   10.110729   10.199263   48   49   9.800824   9.88964   9.911240   10.08533   10.110729   10.199263   47   49.800879   9.888548   9.911240   10.085760   10.111145   10.196644   49   9.800849   9.888548   9.912240   10.085760   10.111145   10.196644   49   9.800849   9.888548   9.912240   10.085760   10.111145   10.198644   49   9.888548   9.913274   10.0856720   10.111452   10.198644   49   9.888548   9.913274   10.0856720   10.111452   10.198644   49   9.888648   9.913274   10.0856720   10.111452   10.198644   49   9.888649   9.888649   9.913274   10.0856720   10.111452   10.198644   49   9.888649   9.888649   9.913274   10.0856720   10.111452   10.198644   49   9.888649   9.888649   9.913274   10.0856720   10.111452   10.198644   40   9.888649   9.888649   9.913274   10.0856720   10.111452   10.198644   40   9.888649   9.888849   9.913274   10.0856720   10.111452   10.198644   40   9.888649   9.888849   9.913274   10.0856720   10.111452   10.198644   40   9.888649   9.888849   9.913274   10.0856720   10.111452   10.198647   40   9.888647   9.914540   10.0856720   10.111452   10.198677   3.9807473   9.887670   9.918471   10.0856720   10.111452   10.199670   3.9807473   9.887670   9.918471   10.0856720   10.111452   10.196647   3.9807474   9.887670   9.916674   10.0856720   10.111458   10.196647   3.9807474   9.887670   9.916674   10.086733   10.11268   10.196647   3.9807474	ı	3			9.909144	10.090856	10 109805	10,200661	57
5 9,7996;19,389990,9.99660;10.003340;10.1100tc 10.200349;57 6 9,79966,9.888588 9.99918;10.00083;10.11018;10.200018;33 8 9,80017,9.889682,9.910435;10.08893;10.110318;10.19928;35;10.980047,9.889682,9.910435;10.089367;10.110318;10.19928;35;10.9800427,9.889477,9.910951;10.089367;10.110318;10.19928;35;10.9800427,9.889477,9.911045;10.088936;10.110328;10.19928;35;29.800737,9.889371,9.911047;10.088376;10.110031;10.19928;35;29.800737,9.889371,9.911047;10.088376;10.110032;10.19928;34;44,9.901304;10.088376;10.110036;10.19928;34;44,9.901304;10.988376;10.110338;10.110928;35;40.9800429;9.888858;9.912498;10.08876;10.110338;10.19928;34;40.9800429;9.91108;10.88968;10.111036;10.198644;40.9800429;9.91108;10.88968;10.111036;10.198644;40.9800429;9.91104;10.88968;10.1111349;10.198644;40.9800429;9.91104;10.88676;10.111142;10.198644;40.9800444;40.9800429;10.88676;10.111145;10.198644;40.98004444;40.980044444;40.98004444;40.98004444;40.980044444;40.980044444;40.980044444;40.980044444;40.980044444;40.980044444;40.980044444;40.980044444	ı		9-799495	9.890093	9.909402	10.090598	10.109907	10,200505	56
7 9-79996a   888785   9-910177   10.089823   10.110318   10.102088   53   9-800174   9.889679   9-910951   10.089367   10.110321   10.199725   50   9-800427   9-889477   9-910951   10.089397   10.110321   10.199725   50   9-800427   9-889477   9-910951   10.085391   10.110321   10.199267   50   50   50   50   50   50   50   5	N				9.909660	A 100			55
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4 2	A STATE OF THE PARTY OF THE PAR	9.882871	9.927147		of the latest designation of the latest desi	10.189983	47
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103		9 882657	9.927659			10.189684	45
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		9 882443	9.928171	10.071829	A DESCRIPTION OF THE	10.189386	43
13	A DESCRIPTION OF THE PARTY OF		9 928427	10.071573	A COUNTY OF THE PARTY OF	10.189237	4
115	A DECEMBER OF THE PARTY.	9.882229	9.918683	10.071317		10.189088	41
20	9,811061	9.882121	9.928940	10.071060	10.117879	10.158939	40
23	9.811210	9.882014	9.929196	10.070804	10.117986	10.188700	39
22	S Company of the last of the l		9.929452	10.070545	A STATE OF THE PARTY OF THE PAR	10.188642	38
23	A CONTRACTOR OF THE PARTY OF TH		9.929708	10.070191		10.188493	37
24	The second second		9.929964	10.070036		10.188345	38
24	The second second second	9.881584	9.930220	10:069780	A DESCRIPTION OF THE PERSON NAMED IN	10.188105	36
26		9.881477	9.930475	10.009529	Control of the Control	10.188048	34
4. 45			9.930731	10.069269		10.187950	33
28	The second second second second	9.881261	9.930987	10.060013	The second second	10.187752	32
29	C. COMMON PROPERTY.	9.881153	9.931243	10.068757		10.187504	31
30	The second second	9.881046	9.931499	10.068501		10.187456	20
_	Commence of the last of	-	-	_			_
3		9.880938	9-931755	10.068249	THE OWNER OF THE OWNER, WHEN PERSON NAMED IN	10.187308	29
32			SHAPE WATER	10.067990	The second secon	10.187160	23
33		THAT IS IN	D. P. Carlotte, March	10.067734		10.187012	27
34			9.932522	10 067478		10.186865	20
35			9.932778	10,067122		10.186717	7.5
36			9.933033	10.066967		1001865-0	24
37	9.813578	W147 - W	9.933289	10,066711	A STATE OF THE PARTY OF THE PAR	10.186422	23
38			9.933545	10 000455		10.186275	22
-59			9-933800	10.066200	THE RESERVE AND ADDRESS OF THE PARTY OF THE	10.186128	21
40			9-934056	10,065944	10.120037	10.185981	20
41			9-934311	10.065689	10.120145	10.185834	19
42			9.934507	10.065433		10.185687	18
43			9.934823	10.065177	10.120363	10.185540	17
44	9.814607	9.879529	9.935078	10.064922	THE SECOND SECON	10.185305	16
45		9.879420		10.064667	CONTRACTOR OF THE PARTY.	10.185247	15
46		9.879311	9-935589	10.064411	200	10.185100	14
47	9.815046	9.879202	9.935844	10 064156	The second second	10.184054	173
48	0.815193		9.936100	10.063900		10.184807	12
49	0.815139	9 878984		10.063645		10.184661	11
50	9 815485			10.063390		10.184c1c	10
51			0.036866	10.063134		10 184158	_
52	9 815778	878656	0.027127	10.063834	10.121334	0 104328	9
53	9.815924	2.878	0.027006	10.062679	10 13144	10 18 223	
	9.816069	W. W. W.			10,121453		6
55	9.816216	878775	0.93,032	10.062308	10.121671	10.183931	
26	9.816361	878710	0.028	10.06.01	10.121072	10,183783	54 %
57	9.816507	878100	0.028200	10.061600		10.183639	2
58		The second second second				10.183493	3.1
50	9 816798		0.018008	10.061347	10.122001	10.183348	4
60	9.816943	Tr. 10 15			10.122210	10.183302	
M			9.939163			0.183057	0
1	Co-sing,	Sine. I	Co-tang.	Tang-	Ca-sec-	Secant.	M 3
	-		- 20	Degrees.	-	No.	-

41 Degrees.

	4: Degrees.		
M Sine Casane, The	ig. Co-tang.	Secant. Co.	. c. v
ala 8 (6 ) 12 () ( = = = 2 80 (0 , 0 2)	6. 10.062537	13.123225 15 15	3.05 6.0
Alakanakk a Combot balata	15 13.5°34°2	13.122337 10.1	2 12 50
しょうしきょうきょう ひきつくじょう りつご	16 * 1 (0.01* 12*	15.122443-15.1	
3 9.1.1-3-9 9 8450 0.1.30	1015 10.000 mg	13-12255- 10-15	1021 5"
	3183 150039817	10 122600 10 18	24"6 ,6
1 -1, 5, 5, 5, 6, 5, 7, 7, 2, 2, 0, 0, 1, -		13 144 0 15.1	• • • • • • • • • • • • • • • • • • • •
6,9 817813 9 877120 9-94	644 10 549436	10.122580 1 .15	218- 54
7 0 1 0 2X 0.37"313 U 143	54; , 10 5 <sub>1</sub> 92 <sub>5</sub> 1	10 12399C F 15	2. 12. 53
e'c ikina a 356km u cat	12.3.125.8746	15.123151 1 1 18	1567 53
6.6. 5.32:- 0.8-0-80 9 921	1., 4 10 7, 6, 2	10.113211 15 15	
10 9.8183.2 9 8: 66-8 9 941	171 . 10 15 15 15	10:00 02:1:00	1.55 30
		12.123432-17-15	111 9
11 0 . 8530 6.2 6.26 6 . 41		4 1 1 2 2 2 2 2 1 1 1 1	111
12-3 518651 9 8"01; 7 9 943 1319,818825 9.876347 9.944		13.122622 6.13	11-; 4
14 4 818969 9.8-623914 942		10.12.701 1 .18	1.151, 43
14 9 813919 9.3 01314 942	1088 10 357017	10.12257211311	3-145
15 9.819113 9.876125 9 941 16 9 81925 9.8 0014 9 943	930 10 05 072	10 12:48011 415	13 11
1- 9 810 101 4 8 200 1 4 9 443			
18 9.819 545 9.875 793 9.943	2 10.0562.9	13.12.2 - 118	24.51 4
19 9 81 968 9 9 5 7 5 6 3 2 9 9 4 9	.207110 3444421	10 1213 8 10.15	-4-31 4 - 3-11 11 .
2019.819832 9 575571 9-944	262110 0	10 121,21 11 18	11
20,4.0.0015 4 . 17,1 4.44		: = 1	
21:9.819971 9-5 5459 9 944	151-10.575153	10 13 14 14 17 17 17	
22 9.820120 9.875, 41 9 944	771115 11229	12.12.405 11.0 1	·
23 9 720263 9.875237 9.945	2050110 0210.4	1	"
24'9 520426 9 875126 9 945	2 1 1 3 1 3 1 1 1 1 1	13.12.13(1.21-	
25,0.820556,9.875014 9.945	553 110 014 1111	10.11, 12	
26 9.823993 9.874933 9.945	195 117 117 117	10 1252 1 1 . 1	
27'9 820836 9 874"51 9.946 28 9.827,79 9 874680 9.946	1243 2 2393		
28;9.821;22;9.87.4568,9.946	1299 . 3 3 . 3 . 4	12 12:12 10:1-	
33.9 821265 9 874456 9.946	25541	10 12-21 112 17	· : ( ): (
31 9 821407 9 874,44 9 947	G6 (C 3.5)	1 12 36 1	311.1
32.9 821550 9 814232 9-94	314 ( 144 ) 443 (	1.2. 12.	
33.9 821993 9 8 4(21 9.91	· ; - 5, i - 5 · ·	12,87,11,11	
74 9.821835 9 87 1259 9.91		:" 125"9	
1 26 0.52[37" 0 573500[9 935			14.
3-9-12262 7.8-70-2 9.945	3 - 110 671 - 1		,
28 9 822424 9.8-3565 9.94	244115	1 1 100 33, 3 4 4 5	
39 0.822546 9 873445 1.434	1, 137 (194)	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
40 9 822488 9 5-3333 9 94	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 . 1	
41 9.822825 9.5-3224 7.949	A. 10. (19)	1, 17, 22, 1, 1,	7: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1: 1:
1 12 0 822072 9 873113,9 939	POLICE VICES	3 1 1 2 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-
( # 2 0 823114 0 6 2995)9 Pe	410 12 14 24		
44 9. 123255 9 . 2005.00	11 12 - 14 1 <u> </u>	1 12-115 1-1-	' · : 10
45 9 523317 9 572772 9 95	1. 1157 ( 177)	1 42 28 1 1	: 1 2 3 1 1 5 1
1		1212	
47 9.825583 9 (-7, 47)9 451	133713-37212	Dir ( )	13 15
1 18 9.823821 9.67*13119 951	1200 1000 2000	1917 . 6 . 17	9 (4 12
1 49 9 823953 9 5 3 3 4 1 10 9 1	17 (3) (4) (1) (3) (4)	10.12 11 13	3 11
	(Ng0) 12 (4 11 )		
51 9 52 522 5 76 72 0 , 0 952	1133 10 30 5032	Social 27, 1391*	<b>**</b> *
1 -2 9.524386 9.57198 - 3.952	\$425;13 (" <b>595</b> )	12.15. 11.17.	
re a veriese a tent fille to	2	19101 2191	
. :4 0. :246619 31.5534 713	2	1 - 1 15 1 [5 4- 5 ]	•••
i ray 82 (808 9 8) 10 (1 ) i '		1211124 1211	1
la en la desta de la calacteria de la companya de l	112. 1.	10 12 3 3 10 17	
l em a bas na metal i sin sa i	(1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	13 12 300 1237	1.1
3 4 9 5253 5 9 5 1 5 1 9 5 1	(4.9) (2.1) 9371.	3 1.32 9 9 83 17	4
. ) 6 2 5 5 5 1 1 9 2 1 7 2 4 7 5	property opening	10.121713 1-11	• • • •
0.14 .5.11 6 5 1 12 9:05	ration (1974) safeti	1911-152-1911	-
4 Co- 16 . Str . C. 1	·. i ç. ·	Absolution Fig.	
	5. Degrees.		
•	'er avi Biogai		

42 Degrees.

-	- 0'ms -	Co-sine	Tang.	Cotang	Secant.	Co-sec	W
26	Sine.	Section 19		Co-tang			-
0	9.825511	9.871073	9.954437	10,045563	10.128927	10.174349	60
1 2	9.825651	9.870846	9.954691	10.045309	10,129154	10.174309	59
13	9.815931	9.870732	9.955200	10.044800	10.120268	10-174069	57
1 4	5 825071	9.870618	9-955454	10.044546	10.129382	10.173939	56
5	9.826211	9.870504	9.955707	10.044293	10.129496	10 173789	55
6	9.826351	9.870390	9.955961	10.044039	10 129610	10.173649	54
7 8	9.8.6491		9.956215	10.043785	10.129724	10.173509	53
	9.826631		9.956469	10.043531	10.129839	10.173369	52
9	9.826770		9.956723	10,043277	10.129953	10.173230	51
10	9.826910			10.043023	10.130067	10.173090	50
110	9.827049				10.130181	10.172951	#
13	9.827189		10.000		10.130196		45
113	9.827328		I KIND OF THE		10-130411	STATE OF THE PARTY	12
14	9.827407						45
16		9.869245					44
	9.827884				10.130870	10.172116	ar .
17	9 828023					A SECTION AND ADDRESS.	42
19	9.828162	9.868900			10.131100	10.171818	41
20	9.828301	9 868785			10.131214	10.171699	40
21	9.828420	9.868670	9.959760	10.040231	10.131330	10.171557	10
22		9.868555			DECEMBER OF THE PARTY OF THE PA	10.171422	38
23		9.868440				10.171184	31
24	9.82885	9.868324	9.960531		10-131676	10 171145	16
25	9.82899	9. 68209	9.960784				25
26	9.829131	9.868093	9.961038				131
27	9.82926	9 867978	9.961291	THE RESERVE THE PARTY NAMED IN			33
28	9.82940	9 867862	9.961549			THE RESERVE OF THE PERSON NAMED IN	(E)
29		9.867747					
30	-	9.867631	-				10
31		9.867515			The second second second	A RESIDENCE OF THE PARTY.	29
32		919.867399					2
33		19.867283					26
34		9.867051		10.036933			=5
35		9.86693					21
37	0.82064	9.86681	9.96382			A DESCRIPTION OF THE PARTY OF T	23
38		9.866703					92
39		9.866586					21
40	9 83105		9.964581		A CONTRACTOR OF THE PARTY OF TH		20
41	9.83119	1					19
42		9.866237				A SECTION OF THE PARTY OF THE P	18
43		9.866120				A STATE OF THE PARTY OF THE PAR	17
44		9 866003	9.96560	10.034398		4 Received and Co.	10
45		9.865887				10.168258	15
46		9.865770	9 96610	10.033891	10.134330	10.168121	14
47	9.83201						12
48		2 9.865531					12
49		9.865419					11
50	9.83241	2					10
51	9 83256			of the particular agencies.	I I THE RESIDENCE AS A SECURE		9
52		7 9.865061					8
53		3 9.86.1950			Annual Reservation		.0
154		9 9 86483			STORESON MADE A		3
155	9.83310	5 9 864711	9.96864	10.031611	E TOWNS CO. LANSING		
56	9.83337	9.56448	9.96889	10.031104			
58	0 83351		9.96914				1
59		8 9.86414				10.166151	1
60	9.81178	3 9.86412	7 9.9595			10.166217	0
1	Co-sine		Cosan		Com	The san	TH
	Co office	- Control	- Comment	is to			

43 Degrees.

				Degrees.			
M	Sine.	Co-sine-	Tang.	Co-tang.	, Secant.	Co-sec.	M
<u> </u>	0 822782	264127		10.030344	10.135873		7
ĭ	9.033703	9.864010	9.909050	10.0,0544			60
	9.033919	9.864010	9.909909	10.030091	10.135990	10.166081	19
2	9.834054	9.303892	9.970102	10.029838	10.136108		58
3	9-834189	9-863774	9 970416	10.029584	10.136226	10.165811	57
4	9.834325	9.863656	9.970669	10.029331	10.136344	10.105675	56
5	9.834460	9.862638	9.070922	10.029078		10.165545	
lő	9.834595	0.863410	0.071175	10.028825		10.165405	
-	0.821720	0 862201	0.071120	10.028571		10.165270	54
8	9.034/30	9.003301	9.9/1429	10.038571			53
	,,,,,,			10.028318		10.165135	52
	9.834999			10.02806;			51
13	9-835134	9.862946	9 972188	10.027812	10.137054	10.164866	50
111	0.875260	9.862827	0.072441	10.027559	10.137172	10 161721	
12	0.825102	9.862709	0.072604	10.027306			42
	9.835538	0.862.00	9.972094				48
1 ::	9.035530	9.802590	9 972940	10.02#052			47
	9.835672	9.802471	9 973201	10.026799			46
15	9.835807	9.802353	9-973454	10.026546	10.137647	10.164193	45
16	9.835941	9.862234	9.973707	10.026293	10.137766	10.164259	44
17	9.836075	9.862116	9.973960	10.026040	10.137885		43
18	9.836200	9.861996	0.074212	10.025-87			
	9.836343	9.861877	0.07.1.166	10.025534			42
20	0.836477	9.861758	0.074714				41
1—	12:23:24/-/	3.551/38	7.7/4/19	10.025281	10 138242		40
21	9.836611	19.861638	9-974973	10.025027	10.138362	10.163389	39
ľ 22	9.836744	19.861210	0.076226	15.024774			38
23	:9.836878	19.861100	0.075470	10 021521	10.138600		37
24	9.837012	0.861280	0.075722	10.02 1268	10.138720		
25	9.837146	2.861161	0.075085				36
26	9.837279	9.661044	9.975905	10.024015			35
2-	19.03/2/9	9.861041	9.970238				34
	9.837412	9.000922	9.9-0491	10.023509			33
20	9.837546	9. 65832	9.976-44	10.023256			32
	9.837679			10 023003	10.139318	10.162321	31
_30	9.837812	9.860562	9.97 250	10.022750	10.139.138	10.162188	30
	9.837945						1
35	19.03/945	9.503442	9 9 7 503	10.02249,	10.139558		29
3.2	9.838078	9.805322	9.977750	12.022244	10.139678		28
33	9.838211	9.800202	9.978009	10.021991	10.139798	10.161789	27
34	9.838344	9 863082	9 9-8262	10.021738	10.139918	10.161656	26
35	9.838477	9.859962	9.978515	10.021485	10.140038	10.161423	25
36	9.838610	9.859842	4.7-8-68	10.021232			24
37	9.838742	0.850721	0.010021	10 020979		10.161258	
38	9.838875	u 850601	0.070171	10.020726			23
30	9 839007	08:0.80	9.979274		10.140399		22
13	Ja 82017	3.039400	9.979527	10.0204~3	10.140520		21
				10.020220	13.140646	10.160860	20
41	9.839272	9.859234	9.980022	13.019967	10.140761	10 160728	19
42	9.839404	0.8:0110	0.480286	10 019 14			18
43	19.839536	4 8 5800 S	0.682558	10.019462	•		
نه	9.839668	0.868877	0.08020	10.019402			17
1 4	9.839865	2.83.4	9.900/91	10 019209			16
1 72	9.039300	9.050750	9.93:514	10.018956			15
1 7	9 839932	9.358035	9.951297	10 018703	10.141365		14
47	19.940304	9.853514	3.981550	10.018450			13
40	9.840196	9.858393	9.981805	10.018197		10.159804	12
1 49	9.840328	9.858272	9.982056	10.017944	10.141728	10.159672	11
50	9.840459	9.858157	9.982 200	10.017691	10.141849	10.159541	10
							<u> </u>
1	13.040201	9.05029	9-922503	10017438	10.141971	10.1594-9	9
12:	,9.040722	19-55790X	19.982814	10.017186	10.142092		8
255	9 840854	19.857786	9-973067	10.016022	10.112214	10 1:0176	7 1
1 54	19.840985	19.857665	9 983320	10.016680	10.142335	15.15,015	6
1 25	9.841116	9.857543	9.983573	10.016127	10.14245-	10.1:8882	5
1 50	9.84124~	9.857422	9.983826	10.016174	13 142578	10.128753	
57	9.8411-8	0.8 57300	0.081070	10 01 02	10.142700	10 158622	4
58	9.841500	0.857178	0.08:22	10.015669	.0.142/05		3
1	0.8116	085-056	3.9.4331	10.015009	10.142022	10 158491	2
60	3.041040	19.057050	9.904504	10.015416	10.142944	12.129300(	\ I.(
J	4.041771	14-050934	9.904537	10.015163	10.143066	110.13250	1 0
/ M .	Co-sinc.	Sine.	Co-tang.	Tang.	Co-sec.	Serini	

				-99 IM	grees.			200
E	W	Sine.	Co-sine.	Tang.	Co-tang-	Secant.	Co-sec	×
ż	-		-	-			10.158220	
1	0			9.984837	10.015103	10,143066	DESCRIPTION OF THE PARTY OF THE	00
и	. 1		9.856812	9.985090	10.014910	10.143188	10,1580gE	59
1	2	9.842033	9.856690	9.985343	10.014657	10.143310	10.157967	58
и	3	9.842163	9.856568	9.985596	10.014404	10.143431	10.157837	57
u	4	9.842294	9.856446	9.985848	10.014152	10.143554	10.157706	50
1	5	9.842424	9.856323	9.986101	10.013899	10.143677	10.157576	55
П	16	9.842555	9.856201	9.986354	10.013646	10 143799	10.157445	54
u	7		9.856078	9.986607	10.013393	10.143922	10.157315	53
1	8		9.855956	9.986860	10.013140	10.144044	10.157185	52
ı	9		9.855833	9.987112	10.012888	10.144167	10.157054	54
1	10			9.987365	10.012635	10,144289	10 156924	50
٦	-		-	The second second	-	The second second	Salaration or the last	
и	AX	9.843206		9,987618	10.012382	10.144412	10.150794	19
п	1.2	9.843336		9.987871	10.012129	10.144535	10.156664	451
u	13	9.843466	9.855342	9-988123	10.011877	10 144658	10.155534	47
и	14	9.843595	9.855219	9.988376	10 011624	10.144781	10.156405	46
ı	25	9.843725	9.855096	9 988629	10.011371	10.144904	10.155275	43
и	16	9.843855	9.854973	9.988882	10,011118	10.145027	10.196145	44
ı	17	9.843984	9.854850	9.989134	10.010866	10.145150	10.156016	43
ı	18	9.844114	9.854727	9.989387	10.010613	10.145273	10 155886	42
П	19	9.844243	9.854603	9.989640	10.010360	10:145397	10.155757	46
ı	20	9 844372	9.854480	9 989893	10.010107	10.145530	10 155633	40
ł		_			_	-	-	
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ı	29		9.853366	9.992167	10.007833	10.146634	10.154467	51
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# TABLE, III.

## Natural Sines.

In this table the natural sines are exhibited to every degree and minute of the quadrant, and arranged so that the degrees corresponding to the sines are to be taken from the top of the page with their minutes in the left side columns, and the degrees answering to the co-sines from the bottom with their minutes in the right side columns

The natural sine or co-sine of any number of degrees, &c. more than 90, is the same as the natural sine or co-sine of its supplement, found by subtracting them from 180°; or the natural sine or co-sine of an arch greater than 90° is the natural co-sine or sine of its excess above 90°.

To find the natural Sine or Co-sine of a given Number of Degrees,
Minute,, and Seconds:

Or, to find the degrees, Minutes, and Seconds, corresponding to a given natural Sine or Co-sine.

These are to be found as directed for the logarithmic sines, &c. except that the differences to 100" are to be taken from the bottom of that column containing the given degrees in the former case, or the nearest natural sine or co-sine in the latter.

## EXAMPLE I.

Required the natural Sine of 32° 21' 45", or its Supplement I The natural sine of 32° 21' is	147° 38′ 15″. 535090
The difference at the bottom of the column containing the natural sine of the given degrees and minutes is 409, the multiplied by 45, pointing off two figures in the production.	is ( , 10,
	535274
Sum is the natural sine required	5352/4

#### EXAMPLE II.

Required the natural Co-sine of 71					
The natural co-sine of 71° 40' is -					
The difference 460, multiplied by 25, po	inting	; off tw	o figu	ıres,	is —115
Remainder is the natural co-sine requir	ed	-	-	-	314430

## EXAMPLE III.

Required the Degrees, Minutes, and Seconds, answering to the natural Sine 495994.

The natural sine next less to that given is 495964, answering to 190 41'; the difference between this natural sine and the given one is 30, to which two cyphers being added, and that divided by 422, the difference at the bottom of the column, gives the quotient 7" to be annexed to 290 44'. Hence 29' 44' 7", or its supplement 1500 15' 50'; are the degrees, &c required.

## EXAMPLE IV.

Required the degrees, Minutes, and Seconds, answering to the natural Co-sine 368805.

The natural Co-sine next greater to that given is 368936, to which answers 68° 21'; the difference between this natural sine and the given one is 131, to which two cyphers being added, and that divided by 451, the difference found at the bottom of the column, gives the quotient 29". Hence 68° 21' 29", or its supplement, 111° 38' 31" are the degrees, &c. required.

To find the natural versed Sine of a given Number of Degrees, Minutes, and Seconds.

If the given arch be less than 90°, find its natural co-sine, which subtract from 1000000, and the remainder will be the natural versal sine required. But if the given arch exceed 90°, find the natural co-sine of its supplement, which add to 1000000, and the sum will be the natural versed sine required.

#### EXAMPLE 1

Required the natural versed Sine of 20° 39'.

The natural co-sine of 20° 39' is 935752, which subtracted from 1000000, leaves 064248, the natural versed sine of 20° 39'.

#### EXAMPLE II.

Required the natural versed Sine of 1460 38' 40."

The natural co-sine of 330 21'20" (the supplement of 1460 38' 40') is 835274, which added to 1000000, the sum 1835274 is the natural versed sine required.

To find the Degrees, &c. corresponding to a given natural versed Sist

Take the difference between the given natural versed sine and 1000000, and the remainder will be a natural co-sine; the degree, &c. corresponding to which, will be those required, if the given natural versed sine be less than 1000000, but if otherwise, it will be their supplement.

## EXAMPLE 1.

Required the Degrees, &c. answering to the natural versed sine 098565.

The above subtracted from 1000000, leaves 901035, which taken as a natural co-sine, corresponds to 25° 42′ 20″.

# EXAMPLE II.

Required the Degrees, &c. answering to the natural versed Sine 1160172. Here 1000000 subtracted from the above, leaves 160172, which taken out as a natural co-sine, corresponds to 80° 46′ 59″; therefore its supplement 99° 13′ 1″ are the degrees, &c. required.

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55 357010 3	73258 3	89392 4	05408	21300 4	37063	452694	168187 4	83537 4	198740	5
56 357281 3	73528 3	89660 4	05673 4	21563 4	37325 4	152953	168444	183792 4	98992	
57 357553 3 58 357825 3									199244	31
59 358046 3	74327	90463 4	06471	22956	38110	53731	109115	84555	99748	E
60 358368 3	74607 3	99731 4	56737 4	22618 4	38371	15399P	16947=	484810	00000	4 5 H 4 0 M
M 1/99	682 17	679	660	650	640	039	624	er.	600	M
THE REAL PROPERTY.			N	atural C	o-sines	Day .	23			1
Diff.to	458	148	145	441	438	434	430	1 424	1400	1

31	300	110	3.10	33*	.14*	330	369	370	380	395 4
0	500000	515058	529919	544514	559191	57 1576	582785	601816	615061	629345 60
1	500252			54=883	559454				615891	
2	500504	A SECTION AND ADDRESS.		545127	559675	574053	588156	601180	616133	619772 58
3	500750				559916					629998 51
13	501007	45 4 27			500157				616578	
1 6	501259	A COLUMN TO SERVICE AND ADDRESS OF THE PARTY	A CONTRACTOR OF THE PARTY OF TH		500398	574707			616807	
7	140 000			A COLUMN TOWN	560880				617265	Groups or
8		A COLUMN TO SERVICE							617494	631117 50
10	Maria San				501361		589901			
10	502517	17529			56+602	\$75457			617951	6315 N FE
11	101769	517778	552630	507320	501843	\$76199	590571	604367	518180	641801 11
¥6			1000000		502083		590000	604599	6,18408	6330111
F3	1000	518276			562324		1 590840		618637	632255 47
13					562564			605062		032412 414
16	15055000	Section 1997			562805			100000000000000000000000000000000000000	higoga	0327054
10	No. of Concession, Name of Street, or other Persons, Name of Street, or ot	The second second			563045		591544		619551	632937144
17	504528				563526			605988	619779	62248142
Ly		510758			563766			10 20		633606 4
10						578332		No. of the last	620135	633831 6
2.0	505281	520165	-	-	564247	578570	592716	606682	610464	5230c6 to
2.2	508532	Market and		549995		578807		606914		634281
23	505783		535,81	550238	564727		593185		520920	634506 37
2.4		221010	The second second		564967			607376		034731 34
25					565207		59.653			934955 39
26	506788	521506		551200			593887		621831	PERSONAL PROPERTY.
28	10.	I Deposition for the					594355	608300	022059	035405 17 0050000 12
129	17-11-50	522251			506166				622287	figgligg 116
30			The second second				594823	608761	622515	63furl 30
31	507780	522747	537545	552180	566646	580940		608992	fi22742	016101 22
32	Name and Address of						595290		6azgra	616527.16
13		523242	The Contract of the	552664					623197	636751 17
125		523490			567365				623425	036976 19
35		523738					595991		623652	057200 24
37	ALC: UNKNOWN	524234		553392	68082	582220	596225	610145	614107	027414 F46 627546 F5
38		524481	539261	553876	568323	582506	596692	610606	b14134	522572 22
139		524729		554118	568562	581831	596925	610836		5150y6 41
40	510043	544977		554360		583069		611067	624789	616320 23
41	510293	525224	539996	554602	569040	583305	597392	611297	625016	015544 18
42		525472	540040	554844	569280	583541	597625	611527	025248	635768 11
43	510793	525719	540485	555080	569519	593777	597858	611757	625470	63,8493
12	511043	525967	540730	5555328	509758	584014	598092	611987	613697	639215
45 46	CITCAS	526214	541210	555812	570236	582486	598558	612217	625923	639439 11
47		526709	The second second				528791		626377	619886 11
48		526956							616604	640110 11
49	512293	527203	541933	556537	570952	585194	599256	613137	616830	640333 11
50	512543	527450	542197	556779	571191	585429	200780	613307	627057	04D\$57 10
51	512792	517697	542442	557025	571430	\$85665	599722	613596	627284	SANTED 9
52	513042	547944	542686	557262	571000	585901	599955	613826	627510	641003
53	513202	528141	142933	\$5750#	571907	580137	600188	014056	627737	041225
57	513701	52869	543174	557745	572140	586608	6006	614285	627963	MAINT .
56	514010	528422	543602	337907	572602	\$86844	60088-	61474	628416	541806
57	514290	529179	543607	558460	572861	487074	601118	614972	628642	042310 1
58	514539	529426	544151	558710	573100	587314	601350	615203	628868	642341 1
59	519789	529073	544395	558952	578818	587550	601583	61545E	029094	642565
22	515038	The second second	544639	559193	573676	-	001215	015551	609320	
201	599	58ª	250	308	510	549	339	030	510	50° ×
12	-			N	storal w	Co-sine	IL.		1	
Dil	40,00	THE R. P. LEWIS CO., LANSING	Ten 1	1	D. F. I	C 27 1	217.12	e. 1	N 11	10
4/07	ARE ALSO	1913 Y	2149 L	404	1399	394	139911	128511	780	274

м	400	41°	4'79	4.7	410	4.0	46	47"	480	4.,"	. 1
_		656054	666131	0 1998	1004053	70-107	71934	-31354	743145	*54"10	65
1	673010	656279	669347	662211	808:40	707312	719142	1,1552	745534	74430	: 59
2	643233	656498	669563	642424	69,5077	737518	719741	731750	743534	754091	158
3	643456	656717	669779	6826,6	795286	-0-723	719946	-31040	743728	.755282	5
4		656937	60499	682849	09;49;	707929	72014%	732147	743923	755472	
5	243901	6 - 7 2 2	070211	683261	605013	708213	720221	34) + 3	1.4411 11.212	55663	
				1033486						~55853 ~56544	
ś	644340	5:-811	6-2855	68,045	696333	728750	720051	- 3 29 20	11-23	- 5° 234	. ; ;
9	644791	658033	6-107.	683911	696539	757956	72117"	-3313-	-4.,894	-50425	`Ś1
10	0.,5013	101-1-	071200	1.02 61 23	.040"48	3.161	1-2135"		4 (24)	750015	:52
11	645236	6,8471	671505	6.4325	095057	709300	-21554	- 53.5.	74,272	- 50805	44
12	045468	053084	071721	"DN#24"	1047105	1739571	721703	173773-	1,111,15	754995	15
13	045680	6;8908	671456	4654754	96-374	:-047-6	721902	733427	745073	5-185	47
14	645902	659127	672151	10/49-1	1697582	i=39981	1722103	734124	74;5%;	757375	46
1.3	6.61.6	029340	67230	035183	,657000	13145	j=22504	1734623	76351	75750,	45
77	646568	650782	672707	68560	608227	13:0:	-22-66	-2.1-	3511	7 . 7 . 9 .	++
ıś	616-00	6000002	673013	68,818	603415	17137,0	72295	-3 715	-10638	758124	42
19	647012	060220	07 7 228	1;0:7030	028023	1_1125*	1-33100	1-351121	1700132	-5×321	41
	647133	660439	673443	686242	668832	1-11200	~2;379	- 3 3 30.00	74"12;	7 (8 (1)	: 10
21	647455	6606:7	67 365	685453	994949	711413	-2:50	10000	74-218	1-38-57	30
22	64-677	660875	673873	686695	0992;1	7:161-	723771	-33-03	-4-412	-544.7	šŠ
23	647898	661094	674288	6.005-6	.694455	711322	723971	735930	-4-6:5	759252	
24	648120	661312	67430	63-288	.66,4663	712020	1724172	735-4-	1776	~592~1	;6
135	048341	661530	67451	687299 687510	649571	712233	1724372	73027	· 7 ; 7 [	- 59461	35
20	048503	001.49	6-4-3	687510	1 <b>73</b> 3379	7 7 7 6 7 9	1724573	1730491 1-26022		759073	34
28	640006	662181	67:15	68-932	70026		7211-1	- 26801	-18-0	-650039	; ; ;
20	619227	662102	675376	688144	- 30702	-1-71	725174	-:-351	720763	-63217	31
;5	64444	662520	6-559	688144	700909	71,250	بُ-يني-نِ	-3-27-	50;6	-65406	30
2.1	hankha	61.2828	169とそつか	· (688-66)	1-2111-		. 7 . 2 2	1000401	- 1 t 1X	! - 100 - 0 -	• • • •
32	649890	60,050	676510	6380	701 72.	713.5	-255	-3-6-3	744341	-60-81	28
33	650111	663273	676233	เอลยังรัว	101531	17,502	7250-5	73-307	749534	700972	27
34	6,0332	663491	6-644	5.68 <b>91</b> 9°	701739	:=14066	726175	-3:3063	744726	61161	
35	6,0553	663704	67666	: 689177	731946	-14269	726;-5	738259	740919	761350	25
30	650-74	663926	6768-0	689620	1732153	,714473	720575	737455	7,50111	761538	2.4
37	651316	66.761	67709	1 695541 1 686835	702300	; "149"0 " "188"	1726	1-38051	750133	701-27	, 23
30	6:1427	661570	6	090041   690251	7027	713253	1-2-1-1	110011		1762154	21
40	651657	664-46	63	690462	1-52401	.714115	72-31	- 142 30	5333	1762242	20
1	6c18-x	66:012	601	0 . 6- 2	732133		-,	1		1	_
12	652008	60:230	6-816	0,06-2	703305	71500	·	3,011	7,1271	02568	8
43	652319	1605443	107837	3 091091	1:33601	.j715) az	727072	1-,,52-	1751456	. 1028.6	17
[44	052539	005005	0-229	71091303	1703861	170000		1-40023	(~5'045	'703544	16
ز 4 ا	652760	160:382	เดาหลว	11091513	170.1013	17103 2	. 725571	1-45218	[751540	1703233	: 15
				169172						763425	14
				3 691933						-03008	. 13
40	652611	666740	67.6	1 69214;	1 2.034	1010411	123 /00 120165	1.110.55	. 752415   752030	1763796	, 12
50	653861	666056	67489	8 6925n3	-2521-	-1721	29100	1 41 105	1.52008	764171	
5 1				1 692773		1		41501			
5 2	054301	66:200	68020	5 692983	70:4:	-1772:	2.11.10	7.1.30	, 529 9 (743181	"01359 "64347	9 9
	654521	667016	68050	693102	70:06:	71792	, 72 , 63	1-41-81	.753372	-6:-3	, ,
5-1	654741	667833	68072	5 693192 1 693402	-058-	-18124	35162	-414-6	753593	(10.14.2)	
55	654961	668049	6×093.	1 643611 7 093821	70607	1,718129	737,361	7.;2171	53733	j=65100	, 4
150	655180	668265	68114	7 09 3821	756284	471 531	3 307	1-42300	7,3940	. 0 . 246	, 4
57	055400	008485	1091300	2109.1230	)·700456	4716733	734758	47.42304	, 113	,"054*3	; ;
50	6	66801	168 0	6604240	70004	1718035	7.734757	1.42.35	75.432	1-05670	
123	6:62:0	660121	68100	694449 694658	700901	719158	1.731155	1744957	1.194919 1723717	76621	, i
-	270079	100	470	400	1/3/13/	1/ 43 +	111111111111	1 1 1 1 1 2 2		1-1-1	
71	49*	467	4/	· 40*							
-					Natura	l Co-sin	¢s.				
	Diff. to	369	363	357	352 3	<b>;6</b>   3 ;	. 221	1 127	3:1	315	
	130#	J-9	1 3,	337	27- 3	T , ! 3 .	1 331	1	(	(	_

	-	-	-	-	-	-	-	-		
124	50°	1,510	52°	530	540	55°	560	570	580	59"  =
1	766044		788011	798636	809017			838671	848048	857167 60
12		The second second	788190			819319			848201	857317 (1
	10000	777512		798985	800530	819652	820525	820146	848610	Serting a
ı	THE RESERVE		788727	799335	809700	819819	829688	839304	848664	857766
8	766979	778060	788905	799510	809871	819985	829850	834462	848818	357915 65
l B	and the second	778243		799685					848972	Spoot f
l	767352	778420	789263			820318		839778	849125	8c8c644
12	767729	778791	789620	800208	810553	820651	830499	840094	849433	Reserve
10				800383				840251	849586	858662 50
10	768097	779156	789977	800557	810894	820983	830824	840409	849739	85881140
13	768284	779338	790155	800731	811064	821149	830984	840567	849893	85896048
B	7686-6	779520	790333	800900	811234	821315	821208	840882	850046	8 59 100147
l iii	768842	779884	790690	801254	811574	821647	831470	841039	850352	8 cq.406/40
E		780067	790868	801428	811744	821813	831631	841196	850505	859555 40
I.		780240							850558	859704 13
IR	100000	780430			812253	822310	823716	841668	850964	Stones
20	d BUPSONS	AND DESCRIPTION OF THE PERSON NAMED IN	791579			822475		841825	851117	Storage
2		-	791757	802297	812592		832438	841982	851260	Shorterion
2		781147	791935	802476	812762	822806	832599	842130	Scrapp.	86044158
3			792112	801644	812931	822971	832760			\$60je.5
2		781520				823136		842452	851525	\$607450M
2		781883				823467		842766		860390 35 8610 ph 34
27		782065		803337	813608	823632	833404		852184	Sátriágy
2		782246				823797		843079	852336	851234 (#
21	CONTRACTOR STATE	782427			814116	823961 824126		843235 843391	852488	861F28FF
30				8040;0	_		-		852640	-
3		782970	793530			824456	834046	843548 843704	852791 852944	86 suza al
3.		783151				824620		843860	E53000	Réspusies
3.		783332				824785	834527	844016	853248	862210 10
3		783513		804721	814950	824949	834688	844172	853399	801366 N
3		783874				825278			853551 853702	86166145
31	773103	784055	794768	805239	815465	825442	835168	844640	853854	861808 tt
35	of passessment to	784235	DESCRIPTION OF THE PERSON NAMED IN			825606			854005	852955 21
45		784416	795121			825770		844951	854150	20210120
4		784596			815969	825934 826098	835648	W	854308	863249 10
4:		784957	745650	806100	816306	826262	835967	845417	854450 854610	86354347
I X	774209	785137	795826	806273	816474	826426	836127	845573	854761	863080 16
4	S DEPRESSION		796002	806445	816642	826590	836236	845728	854912	86381611
45	N INTERNATION		796178	806788		826753			855063	86398214
45		1 2 -	796530	806960	817145	827081	836764	846193	855254	864275 12
45	775128	786037	796706	807132	817313	827244	836924	846348	855515	86442111
55		786217		807304				846503		864567 10
5)	775496	786396	797057	807475	817648	827571	837242	846658	855816	864713 9
3	775079	786576 786756	797233	807047	817815	827734	837401	846813	855966	864800 3
54	776046	786935	797584	807000	818150	828060	837710	847122	846267	865151
153	776230	787114	797754	858161	818317	828223	827878	847277	846449	86 cans   4
156	776413	787294	797935	808333	818484	828386	838036	847431	846467	86 5441 4
	770596	787473 787652	798110	808674	818651	828549	828195	847585	850718	1 685508
55	776962	787832	798460	808846	818085	828875	838612	847804	867047	80,580 1
60	277146	788011	798636	809017	819152	829038	838671	848048	852167	866025 4
26	390	380	379	360	354	840	35°	320	310	30" "
		-	1		Natural	Co-sing	S.			
	100	72 1		and her		1	1		7-	TO I STATE OF

302 295

1	60°	. 61°	620	63"	. 640	659	66°	. 67°.	68"	69°	м
-	866025	100	-	891007	-	906308	913545	920505	927184	933580	60
1	866171		883084	891139	898922	906431	913664	920618		933685	59
12		874902					913782			933789	58
13	866607		883357				914018				57
15	866752	1000			899431	906922		921072			55
6	1200000000						914254				
1 8	867187	875746	883902		899812		914372	921412		934308	1000
2	867331	875886	884174				914607		928161		
10	867476	876026		892323	900065	907533	914725	921638	928270	934619	50
2.3	867621		Section Contracts		900192		914842			934722	100
13		876307					914900			934-26	
74		876587			900572		915194				HIDRON I
15			884988				915311		928810	100000000000000000000000000000000000000	
16		\$76867 \$77005		893110	900825	908205	915429	922313	928917	The second	
18		877146			901027		915663				1000
19		877286			901203		915779				
2	-	8-7425	-	893633	-	908751	-	922762	-	-	
11	869064	877565 877704	885799	893763	901455	908872		922874	929455	935752	
23	DOM: NOT THE OWNER, TH	877844	DOWN		901707				929669		
24		877983		894154	901833	909236	916363	Marie Contract	929776	936060	1804
25		878111		894284					929884		
10		878400		894545		909478			930097		
28	810069	878539	886742	894675	902335	909720	916828	923657	930204	936468	1000
29	DOCUMENTS.	878678			902460				930311	936570	
120	870356	-	-	894934	902585	-	-		930418	-	
34	870499		887145	895064 895194		100000000000000000000000000000000000000	917170		930524		
33		879233			902961					936977	
34		879372					917523			937079	
35	871071	879510	887815				917639				
37	871357		887949	895841			917870			937383	
38		879925	888083				917986			1000	
39		880201	888310	896229		911164	918101	924878		937580	
41	-	880339	888484	895358	903958	911284	918331		931586	937788	
42	-	880477	888617	896486		Children and the	918446				
43		880615	888751		DESCRIPTION OF		918561				
133	872354	880753	888884	896744 896873	904331	911762	918676	925430	931902		15
46	872038		889150	897001	904579	188116			932113		
47	874780	Total Control	889283	897130	904703		919021	925761	932219	938393	13
48	872922	881441	889416 889549	897258	904827	912120	919135	925871	932324	938493	12
50	873206		889582	897515	905075	912358	919364	925900	The second second	938694	_
51	873347	881710	889815	897643	905198	912477		-	932639	-	9
5=	873489	100 0	884948	897771		CONTRACTOR OF THE PARTY OF THE	MINISTER, MARIE	THE RESERVE OF THE PERSON NAMED IN	CONTRACTOR AND ADDRESS OF THE PARTY AND ADDRES		8
53	873631	881990	890080	803000	905445	912715	919707	926419	932849	938994	7
55			890345								
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THE

# ANGLES

Which every Point and Quarter Point of the Compa makes with the Meridian.

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		21	28 7	30	21	No. of Concession,	COLUMN TWO
****		23	30 56	15	23 3	0.51.0	
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BE-25.50	- Participant		36 33	45	31	W-144	100
Block or other	V-0.2 (1.5)	31/2	39 22	30	31	SEATOND	100
N. E.	N. W.	33	10/08/2020	15	334	C P	10 ***
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		41	47 48 50 37	30	44	-354	5339
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	(1.12.1.1.1.1		70 18	45	61	D. C. 2.	****
market 1 14	44-07-1-06		73 7	30	61	ALL HERSE	72341
Service of	100	63	75 56	15	63	No. of Street,	42.3%
E. b. N.	W. b. N.	7	78 45	0	7	E. b. S.	W. b.
and the same	TA TANGERY	71	81 33	45	71	ALC: THE	1000
	1,41-17	71	84 22	30	71	MEG1948	1-3
	71	7 1/4 7 1/2 7 3/4	87 11	15	71 71 71 73 73	14000-0000	100
East.	West.	8	90 0	0		East.	West.

# TABLE V.

( 90 )

# A TRAVERSE TABLE,

Degree and Quarter Degree of the Compass or Horizon.

## EXPLANATION.

ble is calculated for the easy and expeditious solution of cases of Right-angled Plane Trigonometry. It is general-d a useful and requisite assistant to the Surveyor, the and to every one, who has any concern with trigonometry cise of his profession. The manner of using it must be very ull, who are acquainted with the principles of that excellent cometry; but to those, who have only a superficial knowes subject, the following description and examples will be

able, one of the acute angles—whether given, or required—45°, is found, to the nearest 15' at the top of the page; but n 45°, it must be sought at the bottom, where the numbers n a retrograde order. And whether the angle under considat the top, or bottom, the Hypothenuse, if less than 120, is Distance column; against which, in a column marked Latind the side contiguous to the angle; and in a column, parture, the side opposite the angle.

e given numbers exceed the limits of the table, any aliquot as a half, one third, &c. may be taken; and those founding are to be doubled, trebled &c. that is, multiplied by the that the given number is divided by.

# EXAMPLES.

e Hypothenuse of a right angled triangle=96 and one or igles=33° 45'; required the sides.

45' at the top of the table, and against 96 in a Distance found 79.84 in a Latitude column for the side contiguous angle, and 53.34 in a Departure column for the side opponent angle.

e sides of a right angled triangle be=89.23 and 66.02; e angles and Hypothenuse.

ting this table, till these two sides are found against each oining columns of Latitude and Departure, the angle opongest side is found to be 53° 30′, the other, 36° 30′ and enuse, 111.

anner all the cases of Right-angled Plane Trigonometry ly solved; but for more particular directions, beoks on this aid be consulted.

n	-	-	_	-	***		_	-	-
٦	3	1	5	0	3	01	Dist	43	
-1	1810	Lat.	Dep	St	Lut.	Dep.	1 2	Losto	Dep
н	1	1.00	0.00	1	1.00	10.0	1	1.00	0.01
н	2	2,00	0.01	1 2	2.00	0.02	1 2	2.00	0.03
	3	3.00	0.01	3	3.00	0.03	1 3	3.00	0.04
я	4	4 00	0.02	4	4.00	0.03	4	4.00	0.05
н	5	5.00	0.02	1 1	5,00	0.04	5	5.00	0,07
в	6	6.00	0.03	6	600	0.05	6	6.00	0.08
н	7 8	7.00	0.03	1 7	7.00	0.06	7	7.00	0.09
п		8.00	0.03	E	8.00	0.07	8	8.00	0.10
н	9	9.00	10.04	9	9.00	80.0	9	9.00	0.12
×	10	10,00	0.04	10	10.00	0.09	10	10,00	013
м	11	11.00	00%	1 23	11.00	0.10	11	11.00	0.14
и	12	12.00	0.05	12	12.00	0.10	13	12.00	0.16
и	13	13,00	0.06	13	13.00	0.11	14	13.00	0.17
М	15	15.00	0.07	15	15.00	0.13	15	15.00	0.20
в	16		-	-15	16,00	0.14	16	16.00	
н	17	17.00	0.07	17	17.00	0.15	17	17.00	0.21
н	18	18.00	0.08	18	18.00	0.16	18	18.00	0.24
	1.0	19.00	0.08	19	19.00	0.17	19	19.00	0.25
1	20	20,00	0.09	20	20.00	0.17	20	20,00	C.16
1	21	21.00	0.09	21	21.00	0.18	21	21/00	0.27
1	22	22.00	0.10	22	32.00	0.19	22	22.00	0.29
1	23	23.00	0.10	23	23 00	0.20	23	23.00	0.30
В	24	24.00	0.10	24	24.00	0.21	34)	24.00	0.31
н	25	25.00	0.11	25	15.00	0.22	24	25.00	0.33
М	26	26.00	0.11	26	25.00	0.13	26	26.00	0.34
н	27	27.00	0.12	127	37.00	0.24	27	27 00	0.35
н	28	18,00	0,12	28	28.00	0.24	48	28.00	9.37
ч	29	29.00	0.13	29	29.00	0.25	29	29.00	0.38
u	30	30,00	0-13	30	30.00	0.26	30	30.00	0.39
П	31	31.00	0.14	31	31.00	0.27	31	31.00	0-41
н	32	32.00	0.14	32	32.00	0.18	32	32.00	0.41
1	33	33.00	0.14	33	33.00	0.20	33	33.00	0.43
и	35	34.00	0.15	34	34.00	0.30	34	34.00	0.44
В		-	-	35	35,00		35	35.00	045
н	36	36 00	0.16	36	36,00	0.31	36	30.00	0.47
ı	38	37.00	0.17	37	37.00	0.33	37	37.00	0.43
п	39	39.00	0,17	39	39,00	0.34	19	39.00	0.50
3	40	40.00	0.17	40	40.00	9.35	40	40.00	0.52
н	41	41 00	0.18	41	41.00	0.36	41	41.00	
1	42	42.00	0.18	42	42.00	0.37	42	42.00	0.54
1	43	43.00	0.19	43	43.00	038	43	43.00	0.50
1	44	44 00	019	44	44.00	0.38	44	44.00	0.58
1.	45	45 00	0.20	45	45.00	0.39	45	45.00	0.59
1	46	46.00	0,20	46	46.00	0.40	40	46.00.	0.60
1	47	47.00	0.21	47	47.00	0.41	47	47.00	0.62
İ	48	48.00	0.21	48	48 00	0.42	48	48.00	0.63
1	49	49.00	0.21	49	49.00	0:43	49	49.00	0.64
1-	50	50.00	0.22	50	50.00	0.44	50	50.00	0.65
1	51	51.00	0.22	SI	51.00	0.45	51	57.00	0.67
1	52	52.00	0.23	52	52.06	0.45	52	52.00	0.68
1	53	53.00	0.23	53	53.00	0.46	53	53.00	0.99
1	54	54.00	0,24	54	54.00	0.47	54	54.00	0.71
1		55.00	0.24	55	55.00	0.48	55	55,00	0.71
1	56	56.00	0.34	56	56.00	0.49	56	56.00	0.73
1	57 58	57.00	0.25	57	57.00	2.50	57	57.00	0.75
1	59	59.00	0.25	58	58.00	0.51		57.99	0.76
1	59 60	60.00	0.26	59	60.00	0.52	59	59.99	0.79
1		Dep.	Lat.		Dep.	Lat		Dep.	
1	Dist	-	-	Dist.			Dist		Lat
1	-	45	1		30	_	Bear.	13	1000
	100		7	80	Degree	0.03	1		

89 Degrees.

t		15		, E	30	,	8	45	~
1	Dist.	Lat.	Dep.	Dist.		De p.	Dist	Lat	Dep.
	61	61.00	0.27	61	61.00	0.53	61	60.99	0.80
	62	62.00	0.27	62	62.00	0.54	62	61.99	0.81
	•	63.00 64.00	0.27	63	63.00 64.00	0.55	63 64	62.99 63.99	0.82
-	65	65.00	0.28		65.00	0.57	65	64.99	0.85
i	66	66.00	0.29	66	66.00	0.58	66		0.86
	67 68	67.00 68.00	0.29	67 68	67.33 68.00	0.58	67 68	66.99 67.99	0.88
	69	69.00	0.30	69	69.00	0.59	69	68.99	0.92
	70	70.00	0.31	70	70.00	0.61	7Ó	69.99	0.92
	71	71.00	0.31	71	71.00	0.61	71	70.99	0.93
	72 73	72.00 73.00	0.31 0.32	7 <b>2</b> 73	72.00 73.00	0.63	72	71.99 72.99	0.94
	74	74.00	0.32	74	74.00	0.65	73 74	73.99	0.97
j	75	75.00	1.33	75	75.00	0.65	75	74-99	0.98
1	76	76.00	0.33	76	76.00	0.66	76	75.99	0.99
1	77 78	77.00	0.34	77	77.00 78.00	0.67 0.68	77 78	76.99 77.99	1.01
	79	79.00	0.34	79	79.00	0.69	79	78.99	1.03
- 1	80	80.00	0.35	80	80.00	0.70	80	79.99	1.05
1	81	81.00	0.35	81	81.00	0.71	81	80.99	1.06
j	82 83	82.00 83.00	0.36	82 83	82.00 83.00	0.72	82 83	81.99 82.99	1.07
	84	84.00	0.37	84	84.00	0.73	84	83.99	1.10
	85	85.00	0.37	85	85.00	0.74	85	84.99	1.11
	86	86.00	0.38	86	86.00	0.75	86	85.99	1.13
	87 88	87.00 88.00	0.38	87 88	87.00	9.76 0.77	8 <sub>7</sub> 88	86.99 87 99	1.14
j	89	89.00	0.39	89	89.00	0.78	89	88.99	1.16
	90	90.00	0.39	90	90 00	0.79	90	89.99	1.18
1	91	91.00	0.40	91	91.00	0.79	91	90.99	1.19
1	92 93	92.00	0.40	92 93	92.00	0.80	92 93	91.99 92 99	1.20
	94	94.00	0.41	94	94.00	0.82	94	93.99	1.23
- 1	95	95.00	0.41	95	95.00	0.83	_95	94.99	1.24
	96	96.00	0.42	96	96.00	0.84	96	95.99	1.26
	97	97.00 98.00	0.42	97 98	97.20 98.00	0.85	97 98	96.99 97.99	1.27
	99	99.00	0.43	99	99.00	0.86	99	98.99	1.30
Ì	100	100.0	0.44	100	100.0	0.87	100	99.99	1.31
	101	101.0	0.44	101	101.0	0.88	101	101.0	1.32
į	102	102.0	0.45	102	102.0	0.89	102	102.0	1.34 1.35
į	104	104.0	0.45	104	104.0	0.91	104	104.0	1.36
	105	105.0	0.46	105	105.0	0.92	105	105.0	1.37
	106	106.0	0.46	106	106.0	0.92	106	106.0	1.40
ļ	107	108.0	0.47 0.47	108	107.0	0.93	108	107.0	1.41
	109	109.0	0.48	109	109.0	0.95	109	109.0	1.43
	110	110.0	0.48	110	110.0	0.96	110	110.0	1.44
j	111	1110	0.48	111	111.0	0.97	111	111.0	1.45
	113	113.0	0.49	113	113.0	0.99	113	113.0	1.48
i	114	114.0	0.50	114	114.0	0.99	114	1:4.0	1.49
ł	115	115.0	0.50	115	115.0	1.00	115	115.0	1.51
i	116	116.0	0.51	116	116.0	1.01 1.02	116	116.0	1.52
1	118	118.0	0.51	118	118.0	1.03	118	118.ວ	1.54
	119	119.0	0.52	119	119.0	1.04	119	119.0	1.56
	120	1200	0.52	120	120.0	1.05	120	Dep	1.57 Lat.
	Dist.	Dep.	Lat.	Dist.	Dep	Lat.	Dist		<u> </u>
•	<u> </u>	45		<del></del>	DECIU			<u></u>	

Dep Lat.
30'
89 DEGILAYS.

-	. 0	1.0	1 1	5/	1 0	(1) ·	1 451	
Dist	-	Dep.	Lat.	-	3	_		
	Lat		-	Dep.	Lat	Dep.	Lat.	Dep.
1 1	1.00	0.02	2.00	0.02	1.00	0.05	1.00	0.03
3	3.00	0.05	3.00	0.07	3.00	0.08	3.00	0.09
4	4.00	0.07	4.00	0.09	4.00	0.10	4.00	0.12
5	5.00	0.09	5.00	0.11	5.00	0.13	5.00	0.15
6	7.00	0.10	7.00	0.13	7.00	0.16	7.00	0.15
2	8.00	0.14	8.00	0.17	8.00	0.21	8.00	0.24
9	9.00	0.16	9.00	0.20	9.00	0.24	9.00	0.27
10	10.00	0.17	10.00	0.22	10,00	0.26	10.00	0.31
11	11.00	0.19	11.00	0.24	12.00	0.29	10.99	0.34
13	13.00	0.23	13.00	0.28	13.00	0.34	12.99	Ougo
14	14,00	0.24	14.00	0.31	14.00	0.37	13.99	0.43
15	15.00	0.26	15.00	0.33	14.99	0 39	14.99	0.46
16	15.00	0.30	16,00	0.35	15.99	0.43	16.99	0.49
17	18.00	0.31	18,00	0,39	17.99	0.47	17.99	0.55
19	19.00	0.33	19.00	0.41	18.99	0.50	18.99	0.58
20	20.00	0.35	20.00	0.44	19.99	0.51	19.99	0.61
21	21.00	0.37	21.00	0.46	20.99	0.55	20,99	0.64
33	23.00	0.40	22.99	0.50	22.99	0.60	22.99	0.70
24	34.00	0.42	23.99	0.52	23.99	0.63	13.99	0.73
25	25.00	0.44	24 99	0.55	24.99	0.65	24 99	0.76
25	27.00	0.45	25.99	0.57	26.99	0.68	25.99	0.79
28	28.00	0.47	26.99 27.99	0.61	27.99	0.73	26.99	0.86
29	29.00	0.51	28.99	0.63	18.99	0.76	28.99	0.59
30	30.00	0.52	19.99	0.65	29.99	0.79	29.99	0.92
31	31,00	0.54	30.99	0.68	30.99	0.81	30.99	0.95
32	32,00	0,56	31.99	0.72	31.99	0.86	31.99	1.01
34	33.99	0.59	33.99	0.74	33-99	0.89	33.98	1.04
35	34-99	0.61	34 99	0.76	34.99	0.91	34.98	1.07
36	35.99	0.63	35.99	0.79	35.99	0.94	35.98	1-10
37	36.99	0.65	36.99	0.83	36,99	0.97	35.98	1.13
39	38.99	0.68	38.99	0.85	38.99	1.02	38.98	1.19
40	39.99	0.70	39.99	0.87	39.99	1.05	39.98	1,22
41	40.99	0.72	40.99	0.89	40.99	1.07	40.98	1.25
43	41.99	0.73	41.99	0.92	41.99	1.10	41.98	1.28
44	43 99	0.77	43.99	0.96	43.98	1.15	43 98	1.34
45	44-99	0.79	44-99	0.98	44.98	1.18	44.98	1437
46	45.99	0.80	45.99	1.00	45.98	1.20	45.98	1.40
47	47.99	0.84	46.99	1.03	46.98	1.23	46.98	1.44
49	48.99	0.85	48.99	1.07	48,98	1.28	48.98	1,50
50	49.99	0.87	49 99	1.09	49.98	1.31	49.98	1.53
51	50.99	0.89	50.99	1.11	50.98	1.34	50.98	1.56
53	51.99	0.91	51.99	1.13	51.98	1.36	51.98	1.59
54	53.99	0.94	53.99	1.18	53.98	141	53 97	1.65
55	54.99	0.96	54-99	1.20	54.98	1.44	54-97	1.68
56	55.99	0.98	55.99	1.22	55.98	1.47	55.97	1.71
57	57.99	0.99	57.99	1.24	56.98	1.49	56.97	1.74
59	58,99	1.03	58.99	1.29	58.98	1.54	58.97	1,80
60	59 99	1/05	59-99	1.31	59 48	1.57	59 97	1.83
Dist.	Dep.	Lat.	Dep.	Lat	Dep.	Lat	Dep.	Lat
9	0'		45		30	0.0	151	Sec.

	-	-	100	11	EGRE	En	300		-87	
4	Dist	0		15		30/		457		
K	\$	Lat	Dep.	Lat.	Dep-	Lat	Dap.	Lat.	Dep.	ı
Į	61	60.99	1.06	60.99	1.33	60.98	1,60	60.97	1.86	1
١	62	61.99	1.10	61.99	1.35	61 98	1,62	61.97	1.89	ı
١	64	63.99	1.12	63.98	1.40	63.98	1.68	63.97	1.95	ı
Į.	65	64.99	1.13	64.98	1.42	64.98	1.70	64.97	1-99	ä
1	66	65.99	1.15	65.98	1.44	65.98	1.73	65.97	2.01	ı
ı	68	66.99	1.17	66.98	1.46	65.98	1.75	66-97	2.08	ı
۱	69	68.99	1.20	68.98	1.51	68.98	1.81	68.97	2.11	ı
ł	70	69.99	1.22	69.98	1.53	69.98	1.83	69.97	2.14	ı
ì	71	70.99	1.24	70.98	1.55	70.98	1.86	70.97	2.17	ı
ı	72 73	71.99	1.26	71.98	1.57	71.98	1.91	71.97	2.23	ı
ŧ	74	73-99	1.29	73.98	1.61	73-97	1.94	73-97	2.26	ı
II.	75	74-99	1.31	74.98	1.64	74.97	1.95	74-97	2 29	ı
1	76	75.99	1.33	75.98	1.66	75-97	1.99	75.96	2.32	ı
1	77 78	76.99	1.34 1.36	76.98	1.68	76.97	2.02	76-96	2.35	I
1	79	78.99	1.38	78.98	1.72	78.97	2.07	78.96	2.41	
1		79.99	1.40	79.98	1.75	79.97	2.09	79.96	2-44	
1	81	80.99	1.41	80.98	1.77	80.97	2,12	80.96	2.47	ı
H	82	81.99	1.43	81 98	1.79	81.67	2.15	81.96	2.50	ı
H	84	83.99	1.45	83.98	1.83	83.97	2.20	83.96	2.53	ı
ĸ	85	84.99	1.48	84.98	1.85	84.97	2.23	84.96	2.60	ı
ı	86	85.99	1.50	85.98	1.88	85.97	2.25	85.96	2.63	ı
ı	87	\$6.99	1.52	86.98	1.90	86.97	2.28	86.96	2.66	ı
ı	88 89	87.99 88.99	1.54	87.98 88.98	1.92	87-97	2.30	87.96 88.96	2.69	۱
ı	90	89.99	1.55	89 98	1.96	89.97	2.36	89.96	2.75	ı
ı	91	90.99	1.59	90.98	1.00	90.97	2.38	90.96	1.78	1
ä	92	91.99	1.61	91.98	201	91.97	2.41	91.96	2.81	1
ı	93	92.99	1.62	92.98	2.03	92.97	2.43	92,96	2.84	ı
8	94	93.99	1.64	93.98	2.05	93-97	2.40	93.96	2.87	ı
B	96	95:99	1.68	95.98	2.09	95-97	2.51	95.96	2.93	ł
ı	97	96 99	1.69	96.98	2.12	96,97	2.54	96.95	2.96	ı
n	98	97.99	2.7.2	97.98	2.14	97-97	2.57	97-95	2.99	1
ľ	100	98.98	1.75	98.98	2.16	98.97	2,59	98.95	3.02	۱
Ę	101	101.0	1.76	101.0	2.20	101.0	264	101'0	3.08	I
	102	102.0	1.78	102.0	2.23	102.0	2.67	102.0	3.12	1
V	103	103.0	1.80	103.0	2.25	103.0	2.70	103.0	3.15	1
	104	104.0	1.83	1040	2.27	104.0	2.72	104.0	3.18	1
	105	105.0	3	105.0	2.29	105.0	2.75	105.0	3.21	1
	106	106.0	1.89	106.0	2.31	105.0	2.77	106.0	3.24	1
	108	108.0	1.88	108.0	2.36	108.0	2.83	108.0	3.30	1
	109	109.0	1.90	109.0	2.38	109.0	2.85	1090	3.33	1
	110	110.0	1.92	110.0	2.40	110.0	_	110.0	3.36	1
	111	111,0	1.94	111.0	2.42	111.0	2.91	1111.0	3.39	1
	113	113.0	1.95	113.0	2.44	112.0	2.93	113.0	3.42	1
	114	114.0	1.99	114.0	2.49	1140	2.98	114.0	3.48	1
	115	115.0	2.01	115.0	2.51	115.0	3.01	115.0	3.51	1
	116	116.0		116.0	2.53	116.0	3.04	116,0	3.54	1
	117	1170	2.04	117.0	2.55	117.0	3.06	117.0	3.57	1
	119	119.0	2.08	119.0	2.60	119.0	3.12	119.0	3.63	1
	120	120.0	1.09	120,0	2.62	120.0	3.14	120.0	3 66	
	1 2	Dep	Late	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	
	Dist	0.		4	5/	30	1	1.5	1 -	
	STATE OF THE PARTY.	-	-	62.0	DEGI	SPDG		_	_	-

88 DEGREES.

T D	0	1	1/ 2	11	1 30	9/	43	10
Dist	Lat.	Dep.	Lat.	Dep.	Latt.	Detr.	Lat.	Dep.
1	1.00	0.03	1.00	0.04	1.00	0,04	1.00	0.05
2	2.00	0.07	2.00	0.08	2,00	0.09	2.00	0.10
3	3.00	0.10	3.00	0.12	3.00	0.13	3.00	0.14
4	4.00	0.14	4.00	0,16	3.99	0.17	4.00	0.19
5	5.00	0.17	5.00	0.20	5.00	0.23	4.99	0.24
6		0.21	6.00	0.24	5.99	0.26	5.99	0.29
7 3	8.00	0.28	7-99	0.31	7-99	0.31	7-99	0.38
9	8.99	0.31	8.90	0.35	8.99	0.39	8.99	0.43
10	9.99	035	9.99	0.39	9.99	0.44	9.99	0.48
11	10.99	0.38	10,99	0.43	10,99	0.48	10.99	0.53
12		0.42	11,99	0.47	11.99	0.52	11.99	0.58
13	12.99	0.45	12.99	0.51	12.99	0.57	12,99	0.61
14	13.99	0.49	14.99	0.59	14.99	0.65	14.98	0.72
16	15.99	0.56	15.99	0.63	15.98	0.70	15.98	0.77
17	15.99	0.59	16 99	0.67	16.98	0.74	16.98	0.82
1 18	17.99	0.63	17.99	0.71	17.98	0.79	17.98	0.86
19	18.99	0.66	18 99	0.75	18,98	0.83	18,98	0.91
20	19.99	0.70	19 98	0.79	19.98	0.87	19.98	0.96
21	21.99	0.73	20.98	0.82	21.98	0.91	20.98	101
22	22.99	0.80	22.98	0.90	22.98	1.00	21.97	1.10
24	23.99	0.84	23.98	0.94	23.98	1.05	23.97	1.15
25	24.98	0.87	24 98	0.98	24 98	1.09	24.97	1.20
26	25.98	0.91	25.98	1.02	25198	1.13	25.97	1.25
27	26.98	0.94	26.98	1.06	26.97	1.18	26.97	1.30
28	27.98	0.98	27.98	1.10	27197	1.22	27.97	1-34
30	29.98	1.05	29.98	1.18	29.97	1.31	29.97	1.39
31	30.98	1.08	30.98	1.52	30.97	1.35	30.96	1.49
32	31.98	1.12	31.98	1 26	31.97	1,40	31.96	1.54
33	32.98	1.15	32.97	1.30	32,97	1.44	32.96	1.58
34	33.98	1.19	33-97	1.33	33 97	1.48	33.96	1.63
35	34.98	1.22	34-97	1.37	34.97	1.53	34.96	1.68
36	35.98	1.20	35.97	1-41	35.97	1.57	35.96	1.73
37	37.98	1.33	37.97	1.49	37-96	1.66	37.96	1.78
39	38.98	1.36	38.97	1.53	38.96	1.70	38.96	1.87
40	39.98	1.40	39.97	1.57	39.96	1.74	39.95	1.01
41	40.98	1 43	40.97	1.61	42.96	1.79	40.95	1.97
42	41.97	1.47	41.97	1.65	41.96	1.83	41.95	201
43	43.97	1.54	42.97	1.69	42.96	1.88	43.95	2,00
45	44.97	1 57	44-07	1-77	44.96	1.96	44.95	2.16
46	45.97	1.61	45.96	1.81	45.96	201	45-95	221
47	46.97	1.64	46 96	1.85	46.96	2.05	46.95	2.25
48	47.97	1.68	47.96	1.88	47-95	2.00	47-94	2,30
40	48.97	1.71	48.96	1.92	48.95	2.14	48.94	2.35
50	49.97	1.75	49.96	1.96	49.95	-	49-94	2,40
51	50.97	1.78	50.96	2,00	50.95	2.22	50.94	2.45
53	52.97	T.85	52.96	2.08	51.95	2.31	51.94	2.54
54	53.97	1.88	53.96	2.12	53.95	2.36	53-94	259
55	54.97	1.92	54.96	2,16	54.95	2-40	54-94	2,64
56	55-97	1.95	55.96	2,20	55.95	2.44	55-94	2.69
57 58	56.97	1.99	56.96	2.24	56.95	2.49	56.93	2-73
59	58.96	2,06	58.96	2.28	57 94 58.94	2.53 2.57	57.93	2.78
60	59.96	2.09	59.96	3.36	50 94 1	2.62	59.93	2.88
4	Dep-	Lat	Dep.	Lat.	Dep.	Lat	Dep.	Lat
Dist	0.		45	-	30	1	15	
			1300		GREES.		-	-
					- Contract			

1 1	1 0	,	15	<del>,                                     </del>	30	·	1 4:	,
Diet.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
61	60.96	2.13	60.95	2.39	10 94	2.66	60 93	2.93
62	61.46	2.16	01.95	2.43	61.94	2.73	61.93	2.97
63	62.96	2.20	62.95	2.47	62.94	2.75	62.93	3.72
64	63 96	2.23	63.95	2.51	63.94	2 79	63 ,3	3 07
66	64.96		64.95	2.55	64.74	2.84	64.93	3 12
67	65.96 66.96	2.33	65.95 66.95	2.59 2.63	65.y.ı 66 y.ı	2.92	65.92 66.92	3.17 3.21
68	67.96	2.37	67.95	2.67	67.94	2 97	6:.92	3.26
69	68.y6	2. 4 [	68.95	2.71	68.93	3.01	6×.92	3.31
73	69.96	2.44	69.95	2.75	69.93	3.05	69.92	3.36
71	70.96 71.96	2.48 2.51	70.95 71.94	2.79	70.93 71.93	3.10	70.92 71.92	3 41
72 73	72.95	2.55	72.94	2.57	ر72.93	3 14 3.18	72.92	3.45 3.50
74	73.95	2.58	73 94	291	73 93	3.23	73 91	3.55
75	74.95	2.62	74 94	2.94	74.93	32-	7491	₹.60
76	75.95	2.65	75.44	2.98	75.93	3.32	75.91	3.65
77 78	76 95	2.6y		3.C2 3.06	76.93	3.36 3.40	76.91	3 69
7°   79	77-95 78.95	2.76	77·94 78 94	3.10	77 93 78.42	3.45	77.91 78.91	3.74 3.79
80	79.95	2.79	79 94	3.14	79.92	3.49	79.91	3 84
81	80.95	2.83	80 y4	3.18	80.92	3.53	10.04	3.10
82	81.95	2.80	81.94	3.22	81.42	3.58	81.91	3.43
Хз 84	82.95	2.90	82.94 83.94	3.26	82.92 83.92	3 62 3.66	82.90 83.90	3.98
85	84.95	2.93	84.93	3.30 3.34	84.42	3.71	8140	4.58
86	85.95	3.00	85.93	3.38	X5.92	3.75	83.95	4.1;
87	86 95	3.04	86.93	3.42	80 1,2	3.79	80.90	4.17
88	87.95	3.07	87.93	3.45	k y2	3.84	87.40	4.22
89	88.95	3.16	88.93	3.49	88.92	3.88	88.40	4.27
90	89 95	3.14	89.43	3.53	89. 11	3.93	X9.93	4.32
91 92	90.9. <sub>1</sub>	3.18 3.21	90.93	3.57	90.91	3.97	90 90 91.89	4 37
93	92.94	3.25	92.93	365	92.91	4.06	92 89	4.46
94	93-94		93.93	3.69	93.91	4.10	93.89	4.51
95	94 94	3.32	94.93	3 ";	94.91	4.14	94.89	4.56
96	95 94	3.35	95.93	3.77	95.91	4 19	95.89	4.61
97 98	96 94 97-94	3.39 3.42	96.93	3.85	96.91 97.91	4.23	96.89 97.89	4.65
99	98.94	3.46	98.92	3.89	19.89	4 32	98.89	4.75
100	99.94	3-49	99.42	3.93	9., 3	1.36	99.88	4.50
1 1	109	3.53	133.9	3.96	100.y	441	100 9	4.85
102	101.4	3.56	101.9	4.00	101.9	4+>	101.9	4.89
103	102.9	3.59 3.63	102.9	4.04 4.08	102.3	4-14	102.9	4-94
10,	124 9	3.66	104.9	.) 12	104.9	4.58	1-4.9	5.04
136	105 9	3.70	105.9	4.16	1059	4.61	105.4	5.09
11.77	136.9	3.73	156 9	4 20	106 y	4 67	100.9	5.13
109	107.9	3٠77 د3.8	107.9	4.24	107 9	4.71	107.9	5.18
110	108.9	3.84	104.9	4.32	100.9	4.50	100.9	5.28
111	110.9	3.87	110.9	4.36	1129	4 1	110.9	5.33
11.2	111.9	3.91	111.9	4.40	111.9	4.89	111.9	5-37
1.3	112.9	34+	112.9	4-44	112.9	495	1129	5.42
1. +	1139	3 98	113.9	4-48	113.9	4.6" 5.01	113.9	5.47
115	114.9	4.21	114.9	451	114.9		114.9	5 52
115	1159	4.05	115.9	4.55	115.9	5.06	115.9	5.57 5 6 i
118	117.9	4.12	117.9	4.63	1179	5 15	117.9	5.66
1119	118.	4.15	118.9	4.67	118.9	5.19	118.9	5.71
120	1199	4.19	119.9	1:"1	119.4	5.23	1199	5.76
ا بر ا	1),	La.	Dep	1	D		15-16	Lai
Dist	0/		45	, 1300 (1)		J'	1./	

1 H	1 0	,	1 15/ 1		1 30'		45"	
Dist.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
THE R.	1.00	0.05	1.00	0.06	1.00	0.06	1.00	0.07
1 2	2.00	010	2.00	0.11	2.00	0-12	1.00	0.13
3	3.00	0.16	4.00	0.17	3.00	0-18	2.99	G100
5	3-99	0,16	4.99	0.28	4 99	0.31	3.99	033
6	5.00	0.31	5:99	0.34	5.00	0.37	5.99	0.39
7 8	6.99	0.37	6.99	0.40	0.99	0:43	6.99	0.40
	7-99	0.42	7.99	0.45	8.98	0.55	7-98 8-98	0.59
10	9.99	0.47	8.99	0.51	0.08	0.61	9.98	0.65
11	10.98	0 58	10.98	0,62	10.98	0.67	10.98	0.72
12	11.98	0.63	11.98	0.68	11.98	0.73	11.97	0.78
13	14 98	0 68	12.98	0.74	12.98	0.79	12.97	0.85
14	13.98	0.73	13.98	0.85	13.97	0.85	13.97	0.98
16	15 98	0.84	15.97	0.91	15.97	0 98	15.97	1.05
1 17	16.98	0.89	16.97	0.96	16 97	1.04	16.96	1-11
18	17 98	0.94	17-97	1.02	17.97	1.10	17.96	1.18
19	18.97	0.99	18 97	1.08	18.96	1.16	18.96	2/24
21	19.97	1/10	19.97	1.19	19.90	1.22	19.96	1/21
21	20.97	1.15	20.97	1.19	20.96	1.25	20.96	1.67
23	11.97	1.20	21.90	1.30	22.96	1.40	21 95	1.50
24	23.97	1.16	23.96	1.36	23.96	2.47	23.95	1457
25	24.97	Light	24.96	1.42	24.95	1.53	24-95	1,64
20	25.96	1.36	25.96	1.47	25.95	1.65	25.94	3.77
28	27.95	1:41	27.96	1.59	27.95	1.71	27.94	3.81
129	28.96	1152	28.95	1.64	28.95	1.77	28.94	1.90
30	29.96	1,57	29.95	1,70	29.94	1.83	29.94	1.96
31	30.96	1.62	30.95	1.76	30.94	1.89	30.93	2.03
32	31.95	1.07	31.95	1.81	31.94	1.95	31.93	2.16
34	33.95	178	33.95	1.93	33.94	208	33.93	2.22
35	34-95	183	34-94	1.98	34-93	2.14	34-93	2.29
36	35.95	1188	35.94	2.04	35.93	2.20	35.92	2.39
37	36.95	1.94	36.94	2.10	36.93	2.26	36.91	2.42
39	37-95	2.04	37-94	2.15	37-91	2.32	37.92	7.55
40	39.95	2,00	39.94	2.27	39.93	2.44	39.91	2.02
41	40.94	2.15	40.93	2.33	40.92	2.50	40.91	2.68
42	41 94	2/20	41.93	2.38	41.91	2.56	41.91	2175
43	42.94	2.30	42-93	2.44	42.91	2.69	42.97	2.88
45	44-94	2.36	44.93	2.55	43.91	2.75	43.91 44.90	2.94
4ñ	45.94	2.41	45.93	2.61	45.91	2.82	45.90	3.00
97	46.94	2.46	46.92	2.66	46.91	2.87	46,90	3.07
48	47-93	2.51	47.92	2.72	47.91	2.93	47.90	3-14
50	48.93	2.56	49.92	2.78	48.91	3.05	48.90	3.20
51	50.93	2.67	59.92	2.89	50 90	3.11	50.39	1
52	51.93	272	51.92	2.95	51.00	3.17	51.80	3-34
55	52.93	2.77	52.91	3.00	52.00	3.24	52.89	3-47
55	53-93	2,83	53.91	3.06	51-90	3.30	53.88	3-53 3.50
36	54-93	2.91	54.91	-	54.90	-	55.88	1.66
57	55.92	2.98	55.91 56.91	3.17	55.90	3.42	56.88	3-73
57	57.92	3.04	57.91	3.29	57 89	3.54	57.88	3-79
59	58.92	3.09	58.91	3-34	58.89	3.60	58.87	1.86
-	50.92	3-14	59.90	3.40	59.89	3.66	59.87	3-92
Dist.	Dep. 1	Late	Dep. 1	Lat.	Dep_1	Lat	Dep.	Lat.
-	07	100	45	DECR	30		1.5	

86 DEGREES.

-			-			207		-
(3)	0,			17		0/	45	
No.	1.at	Dep	Let	Dep.	- kette	Dep.	Lat.	Dep.
64	60.92	3.19	60.90	3.45	61.83	3-72	60.87	3-99
62	61.92	3.24	61.90	3.52	62.88	3.79	61.87	4.05
64	63.91	3-35	63.90	3.63	67.88	3.91	63.86	4-19
0.5	64.91	3.40	64.90	3.69	64.88	3:97	64.86	4.25
66	65.91	3-45	64.89	3.74	65.88	4.03	65.86	432
67	66.91	3-51	62.89	3.8a	66.88	4.09	66 86	4.38
68	62.91	3.56	68.39	3.86	65.87	4.15	68.85	4.45
70	69.90	3.66	69.89	3-97	69.82	4.27	69.85	4.58
71	70 40	13.92	70.89	4.03	20.87	4-33	70 85	4.04
7-92	71.90	3-77	71.88	4.08	71.87	4.40	74.85	4:28
78	72.90	3.82	72.88	4.14	72.86	4.46	72.84	4-77
74	73.93	3.87	73.88	4.20	73.86	4.52	73.84	4.84
75	74.90	3.98	74.88	4.34	75.86	4.64	74.84	4.91
77	75.00	4 03	76.88	4-37	76.86	4.70	76.84	4.97
78	77-89	4.08	77.87	4.42	77.85	4.76	72.82	5.10
7.0	78.89	4.13	78 87	4.48	78.85	4.82	78.83	5.17
80	79.89	4.19	79.87	4-54	79.85	4.88	79.83	5.23
81	80.89	4-24	80.87	4.59	80.85	4/94	80.83	5.30
82	81.89	4-29	81.87	4-05	81.85	5.01	81.82	5.36
1 84	81.88	4.40	87.86	4.76	83.84	5-13	81.82	5-43
85	84.88	4.49	84.86	4.82	84.84	5.10	84.82	5,56
86	84.88	4.50	8; 86	4.88	85.84	5.25	85.82	5.62
87	86.88	4-55	86.86	4-93	86.84	5-31	86.81	5.69
88	85,88	4.61	87 86 88 86	4-99	87.84	5-37	87.81	5.75
89	84.88	4-55	89 86	5.06	88.83	5-43	88.81 89.81	5.82
91	VO. 63	4.76	90.85	5.16	90.83	5.56	40.81	5.95
91	91.87	4.81	91.85	5.22	91.83	5.62	91.80	6.01
03	91.87	4.87	92.85	5-47	92.83	5.68	92.80	6.08
94	93-87	4.92	93.85	5-33	93.82	5-24	93.80	6,15
95	94.87	4.97	94.8;	5.39	94.82	5.80	94.80	6,21
95	95.87	5.02	95.85	5-44	95.82	5.86	95.79	6.28
97	96.87	5-08	96.84	5.50	90.82	5-07	97 79	6.41
90	V8.86	5.48	98.84	5.64	98.82	6.04	98.79	6.47
190	99.86	5.23	99 84	5.67	99.81	6.10	99-79	6.54
tot	100,9	5.29	100.8	5-23	100.8	b. 17	100.8	6.61
102	-101.9	5-34	101.8	5-78	101.8	6 23	101.8	6,67
103	102.0	5.39	103.8	5-84	101.8	6.29	102 8	6,74
104	103.9	5-44	1048	5.90	104-3	6.41	103.8	6.87
106	1059	5-55	104.8	5.01	105.8	0.47	105.8	6.93
107	106.9	5.60	106.8	6.07	106.8	6.63	106.8	7.00
1:08	107.9	5.65	107.3	6.12	107.8	6.54	107.8	7.05
100	108.9	5.70	108.8	6.18	108.8	6.65	108.8	7-13
110	109.3	5.76	159.8	6 24	109.8	6.72	109.8	7.19
CALL		5.81	110.8	6.29	110.8	6.78	110.8	7-26
1113	1128	5.86 5.91	1112.8	6.41	112.8	6.84	111.8	7-33
216	112.8	5.97	113.8	6.46	113.8	6.96	113.8	7 39 7-46
915	1148	6.01	114.8	6.52	114.8	7.02	114.8	7 52
0 16	1158	6.07	115.8	6,58	115.8	7.08	8.211	7.59
217	3,611	6.42	116.8	0.63	116.8	7-14	110.7	7.55
318	117.8	6.18	117.8	6.64	117.8	7-20	117.7	7-22
110	118.8	6.28	118,8	6.75	118.8	7.20	119.7	7 78
	Dep	The same of	Dep.	Litte	Dep.	7-39 Lat	Thep	7-45
Dist	1	Julia .	45	_	-	-	-	Let
IIA					30		35	

TE	1 0	1		51	P 2 2	0×.	1 70	7-1
160	11-00	-					7	TYPE
1	Lat	Dep.	Lat.	Dep.	Lat.	Hep-	Lat	Dep
I N.		0.07	1,00	0.07	1.00	0.65	1:00	80.0
1 3	The second second	0.14	1.99	0.15	1.99	0.16	1.99	0.17
3		0.21	2.99	0.22	3.99	0.34	1.99	0.25
	100	0.28	3.99	0.10	3-99	0.31	3.99	0.13
3		031	4 00	0.37	4-98	0.39	4.98	0.41
1 6		0.42	5.98	0.44	5.98	0.47	5.98	0150
1 3	6 98	0.40	6.98	0.53	6.98	0.55	6.98	0.58
	1 (190	0.56	7.98	0.59	7.98	0.63	7-97	0.56
10	8.98	0.03	8.98	0.67		0.71	8.97	0.75
11100	1	-	9.97	9.74	9-97		9.97	
1 33	1 1 1 1 2 2 3 1	0 77	10.97	0.82		0.86	10090	0.91
72	1000000	0.84	11.97	0.89	17.00	0.94	86.11	0.99
13	L P DOMES	0,91	12.96	0.96	1296	1.02	12.96	1 16
15	The state of	0.98	13.96	1.17	13.96	1.18	13.95	1.24
		1.05	14.95	-	14.95			
16	1 7 3 9 2	1,12	15.96	1.19	15.95	1.26	15.95	1.33
17	ALC: NAME OF PERSONS ASSOCIATED IN	1,19	16 95	1 26	16.95	1.33	16.94	141
10	1	1,26	17.95	1.33	17.94	1.49	17-94	1.49 1.57
10		1.40	19.95	1.41	10.94	1.57	19.01	1.66
21	2000	The second second						-
_	1 93	1.46	20 94	1.50	20.94	1.65	20,93	1.74
23	11-133	1.53	21.94	1.63	21.93	173	21.92	1.82
24		1.60	42.94	1.70	12.93	1.80	32.92	1,90 1,99
25	11 3193	1.74	23.93	1.85	23.93	1.96	23.92	3,67
26	The state of the s	The second second	-					
27	1 - 2-9-9	1.81	25.93	1.93	25.92	2.04	25.91	2.15
28		1.88	26.93	2.00	26,92	2.13	26.91	2.24
20	1 -1193	2.02	27.92	2.15	28.91	2.20	27.90	2:32
30		2,00	29.02	2,22	20.01	1 35	29.90	2.48
	233	-	_	Tona Control				
31	30.92	2,16	30.91	2,30	30.90	2.43	30.89	2457
33	2000	2.23	31.91	2.37	31.90	2.51	32.89	2.65
34	32.92	2.30	32.91	2.45	31 90	2.59	33.88	2.81
35	33 92	2.44	33.91	2.59	34.89	2.75	34.88	2.90
36			1000	-	-			$\overline{}$
	35.91	2.58	35.90	2.67	35.89	2.82	35.88	3.00
37	36.91	2.65	36.90	2.74	36.89	2.90	37.87	3.15
39	37:91 38:91	2.73	37.90	2.80	38.88	3.06	38.87	3-25
40	39.90	2.79	39.89	2.96	39.88	3.14	39.86	331
41		2.86	-	-		-	40.86	_
42	40.95	and the same of	40.89	3.04	40 87	3.82	41.86	340
43	41.90	3.00	41.88	3.19	42.87	1.30	42.85	3-50
44	43.80	3.07	43.88	3.26	43.86	3-37	43.85	3.64
45	44.89	3.14	44.88	3.33	44.86	3.53	44.85	375
46	45.80	3.21	-	-	45.86	3.61	45.84	3.81
47	46.89	3 18	45.87	3.41	46.86	3.00	40.84	1.59
48	47.88	3.35	47.87	3 56	47.85	3.77	47.84	3.97
49	48 88	3.42	48-87	3.63	48.85	3.84	48.93	4.06
50	49.88	3 49	49.86	3.71	49.85	3.01	49.83	4.15
SI	00	12.5×1	0.00				-	75.1
52	51.87	3.63	51.86	3.78	51.84	4.00	51.82	4-31
53	52.87	3.70	52.85	3.93	52,84	416	52.82	4-39
54	53.87	3.77	53.85	4.00	53,83	4.74	\$3.81	447
55	54.87	3.84	54.85	4.58	54.83	4.32	54 81	4.55
56	55.86	-	55.85		Marie Control		55.81	4.68
57	56.86	3.91	56.84	4-15	55.83	4:47	56,80	4-72
38	57.86	4-05	57.84	4-30	57.82	455	57.80	4.80
59	58 86	412 1	c8.84	4-37	58 82	4.63	58.80	4 80
60	59.85	4-19	59.84	4.45	59.82	4.77	59.79	4.97
1	Dep	Lat	Dep.	Lat	Dep	Lat.	Dep	Lat.
Dist	_	1301	45	,	-		15	_
=	01	1	-		30'		13	-
-	1-11-11	10000	A	25 15E3	REES.	-	-	-

100	-	0'	-	000	- 2		45'		
Jin C	Lat		Lat	-	Lat.	Dep	-		ı
01	60.85	Dep. 4-26	60.81	Dep	50.81	-	Late	Dep.	ı
62		4-32	61.82	4-52	61.81	4.79	60,79	5-05	ı
63	62.85	4-19	62.83	4.67	62.81	4.94	62,78	3.22	ı
64		4.46	63.82	4-74	63.80	5.02	63.78	5.30	ı
66	64.84	4-53	64.82	4.82	64.80	5-10	64:78	5.38	l
67	66.84	4.67	66.X1	4.89	65.80	5.13	65.77	5-47	ı
68	67.87	4-74	67.81	5.04	67.79	5-54	67.77	5.63	ı
69	68,83	+31	68.8r	1 2	68.79	5.41	68.76	\$.7E	ı
70	69,83	4.88	69.81	5.19	69.78	5.49	69.76	1.80	ı
71 72	74.83	4-95	70,80	5 34	70,78	5.65	70.76	5.88	ı
1 73	72,12	5.09	71.80	5.41	72.78		72.75	6.05	ı
74	73.82	5.16	73.80	5.48	73-77	5.73	73:75	6.13	ı
75	74.82	5.23	74.79	5.50	74.77	5.88	74:74	6.21	ı
75	75.81	5-30	75:79	5.63	75.77	6.04	75:74	6.39	ı
78	77.81	5-37	77-79	5.72	77476	6.12	27-73	6.46	
79	78.81	5.58	78.78	5.85	18.76	6.10	18.73	6.54	
	-	9.98	79.78	5.93	79:75	6.28	79-73	6.62	
81	80.80	5.65	80.78	6.00	80.75	6.43	80.72 81.72	6.79	ı
83	82.80	5.79	82.77	6.15	82.74	6.91	82.71	6.87	ı
84	83.80	5,86	83.77	6.23	83.74	6.59	83/71	6.96	ŀ
-85	84.79	5 93	84.77	6.30	84.74	6.67	84.71	7.04	ı
36 87	86.79	6.00	86.76	6.45	85.73 86.73	6.75	86.70	7.12	ļ
88	87.79	6.14	87.76	6,52	87 73	6.90	87.70	7.49	ı
89	88.78	6.21	88.76	6.00	88.73	6.98	88.69	7.37	ı
90	29.78	6.28	89.75	6.67	89.72	7.06	89.69	7.45	ı
91	90.78	6.35	90.75	6.74	90.72	7.14	90.69	7.54	ı
93	91.78	6.43	91.75	6.83	91.72	7.30	91.68	7.70	ı
94	93.77	6.56	93-74	6.97	93.71	7.38	93.68	7.78	ı
95	94-77	663	94.74	7.04	94-71	7-45	94.07	7.87	
96	95-77	6.70	95.74	7-14	95.70	7-53	95.67	7.95 8.03	b
97	95.76	6.84	96.73	7.10	95.70	7.61	96.67	8.11	
99	98.76	6.91	98.73	7-34	98.69	7.77	98.66	8 20	
100	99.76	6.98	99-73	7.41	99.69	7.85	99.66	8.28	
101	100.8	7.05	100.7	7-49	100.7	7.92	100.6	8.36	
103	101.5	7.18	101.7	7.56	101.7	8.00	101.6	8.45	
104	103.7	7.25	103.7	7.71	103.7	8.16	103.6	8.61	
105	104.7	7.32	1047	7.78	1047	8.24	104.6	8.69	
106	105.7	7.39	1057	7.86	105.7	8.32	106.6	8.78	
108	107.7	7 46	107.7	7-93 8.00	107.7	8.47	102.6	8.94	
109	108.7	7.60	108.7	8.08	108.7	8.55	108.6	9.03	
110	1097	7.67	109.7	8.15	109.7	8.63	109.6	9.11	
131	110.7	7-74	110.7	8.23	11007	8.71	110.6	9.19	
112	1127	7.82	110.7	8.3D 8.37	1127	8.79 8.87	111.6	9.27	
114	113.7	7.95	113.7	8.40	113.6	894	113.6	9.44	
115	114.7	3.02	1147	8.52	114.6	9.03	114.6	9.52	
116	115.7	8.09	115-7	8.60	115.6	9.10	115.6	9.61	
118	117.7	8.16	117-7	8.67	116.6	9.18	116.6	9.69	
911	218.7	8.30	118.7	8.82	118.6	9.34	118.5	9.85	
110	119.7	8.37	119.7	8.89	119.6	9.42	119.6	9.94	
世	Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.	Lat.	
Dist	- 0'	I	45		34	0'	1:	)*	
	-	-	95.1	MGRE	PR.	-			

10	- 0			1	1	010	45	
Dist.	Lat	Dep.	Lat.	Dep.	Lat	Dep.	Lat	Dep.
3	1.00	0.09	1,00	0.00	1,00	0.10	1.00	0.10
3	1.99	0.17	2,99	0.18 0.17	1.99	0.19	1.99	0.20
3 4	3.98	0.35	3.98	0.37	3.98	0.38	3.98	0.40
5	4.98	0 44	4.98	0.46	4.98	0.48	4.97	0.50
6	5.98	0.52	5.97	0.55	5-97	0.58	5-97	0.65
7 8	7-97	0.70	7.97	0.64	7.96	0.57	7.96	0.70
10	8.97	9.78	8,96	0.82	8.96	0.86	8.95	0.90
10	9.96	0.87	9 96	0.92	995	0.96	9.95	1.00
II	10.96	0.96	10.95	1.01	10.95	1.05	10 94	1.10
13	11:95	1.05	11.95	1.10	17.94	1.15	11.94	1.30
14	13.95	1.12	13.04	1.28	13-94	1 34	13.93	(.40
15	14194	1.37	14-94	1-37	14.93	1.44	14.92	1.50
16	15.94	1.39	15.93	1-46	15.93	1.93	15.92	1,60
17	10.94	1.48	16.93	1.56	17.92	1.03	17.91	1.80
19	17.93	1.66	18.92	1.74	18.91	1.82	18.90	1.90
20	19.92	1.74	19.92	1.83	1991	1.92	19.90	2.00
21	20.92	1.83	20.91	1.92	20.90	2.01	20.89	2.10
22	11.92	2.00	1L91	2.01	21.90	2.11	21.89	1.20
25	12.91 23.91	1.00	23.90	2.20	11.89	2.30	22,88	1. JD
25	24.90	1.18	24.90	2.29	14.88	1.40	24 87	2 50
26	15.90	2.27	25.89	2.38	35.88	4-49	45.87	1.60
27	26.90	7-35	26.39	3.47	26.88	1.59	26.86	771
28	27.89	2-44	=7.88 =8.88	2.65	27.87	1.58	27 86	2.81
30	19.89	2.61	#9.87	2.75	29.86	1.88	29.85	1.01
31	30.88	2.70	30.87	2.84	30.86	2.97	30.84	5.11
32	31.88	2.79	31.87	2.93	31.85	3.07	31.84	3.00
33	32.87	2.88	31.86	3.11	33.84	3.16	33.83	3.31
35	34 87	3.05	34.85	1.20	34-84	3.35	34.82	3.51
36	35.86	3.14	35.85	3.29	35.83	3-45	35.82	3.61
37	36.86	3.22	36.84	3-39	36.83	3.55	36,81	3.72
38	37.86	3.31	37.84	3.48	37.83	3.64	37.81	191
40	39.85	3.49	39.83	3.66	39.82	3.83	30.80	401
41	40.84	3.57	40.83		40.81	3.03	90.79	411
42	4184	3.66	41.82	3.75	41.81	403	41.79	4.21
43	43.81	3.75	43.82	3.93	41.80	4-12	43.78	441
45	44 83	3.91	44.81	4.12	44-79	431	44-77	4.58
46	45.83	4.01	45.81	4.21		4.41	45-77	4.64
47	46.82	410	46.80	4.30	46.78	4-50	46.76	4.71
48	48.81	4.18	47.80	4.39	47.78	4.60	47.76	4.91
50	49.81	435	49.79	4.48	49-77	4.79	48.75	5.01
QT.	50.81	4-44	50.79	4.67	50.77	4.89	50.74	GING
52	51.80	4.53	51.78	4.76	51.76	4.98	51.74	5 24
53	52.80	4.62	59.78	4.85	52.76	5 08	52.73	5.31
55	53-79	4.71	53-77	4·94 5.03	53-75	5.10	53-73	5-51
56	\$5.79	4.88	55.77	5.12	55.74	5.37	55.72	5.64
57	56.78	4.97	56.76	5.22	56.74	5.46	36.71	5.71
58	57.78	5.06	57-76	5.31	57.73	5.56	57-71	3.81
59	58.78	5-14	59.75	5 49	59.72	5.05	59.70	6.01
-	Dep	Lat.	Dep.	Lat	Dep.	Lat	Dep	Lat.
Dist.	0	-	45		30		15	
-	-	-	THE REAL PROPERTY.	-	RWS.			-

-	1 0			5/	9	0'	45'	
1 St.	Lat.	Dep.	Late	Dep	Lat.	Dep.	Lat.	Dep
61	60.77	1 5.32	60.74	5.58		3.85	60.60	6.11
62	61.76	5.40	61.74	5.67	61.71	5.94	61.69	6.41
63	61 76	5.49	62.74	5-76	62.71	6.13	62.68	6.31
64	64.75	5.58	6473	5.95	64.70	6.23	63.68	6 GE
56	65.75	5.75	65.72	6.04	65.70	6.33	65.67	6.61
67	66,75	5.84	66.72	6.13	66.69	6.42	66.66	6.71
69	68.74	5.93	68.71	6.31	67.69	6.61	68.65	6.81
70	69.73	6 10	69.71	6.41	69.68	6.71	69.65	7.01
7.8	70.73	6.19	10,70	6.50	70.67	6.81	70.64	7-11
7.3	71,73	6.48	71170	6.59	71.67	2.00	71.64	7.21
73	73.72	6.35	73.69	6.68	73.66	7.09	72.63	7-31
75	74-71	6.54	74.69	6.86	74165	7.19	74.62	7/5t
76	75-71	6.62	75.68	6 95	75.65	7.28	75.62	7.61
77	77.70	6.80	76.68	7.05	76.65	7.38	75.61	7.71
79	78.70	6.89	73.67	7.23		7-57	78.60	7.91
80	79-70	6.97	79.66	7:32	79.63	7.67	79.60	8.04
82	80.69	7.06	80.66	7-41	80.63	7.76	80.59	8.12 8.22
83	82.68	7.15	82.65	7.50	81.62	7.96	82.58	8.32
1 84	83.68	7-34	83.65	7.69	83.61	8.05	83.58	8.42
85	84.68	7.41	84.64	7.78	84-61	8.15	84-57	8.52
86.	85.67	7.50	85,64	7-87	85,60	8.24	85.57	8.62
88	87.67	7.67	87.03	8.05	87 59	8.43	87.56	8.82
89	88.66	7.76	88,63	8.14	88.59	8.53	88.55	8.92
90	90.65	7.84	89.62	8.24	89.59	8.63	89.55	9.02
91	91.65	7.93 8.02	90.62	8.33	82.00	8.72	91.54	9.12
93	92.65	8.11	92 61	8.51	92.57	8.91	92.53	9.32
94	93.64	8.19	93 61	8.60	93-57	9.01	93.53	9-42
95	95.63	8.28	94.60	8.69	94.50	9.11	94-51	9.52
97	96.63	8 45	95.60	8.88	95.56	9.30	95-52	9.72
98	97.63	8.54	97-59	8 9	97-55	9.39	97-51	9.82
99	98,62	8.63	98.58	9.06	98.54	9.49	98,50	10.02
101	100.6	8.80	100.6	9.15	100.5	9.68	100.5	10.13
102	101-6	8.89	101.6	9.33	1015	9.78	IDE.S	10.22
103	103.6	9.06	102.6	9 42	102.5	9.87	103.5	10.32
104	104.6	9.15	103.6	9.52	103 5	9.97	104.5	10.42
106	105.6	9.24	105.6	9.70	105.5	10:16	109.5	10.62
107	106.6	9-33	106.6	9.79	106.5	10.26	106.5	10.72
108	107.6	9.41	107.5	9.88	107.5	10.35	107.5	10.52
110	109.6	9.59	109.5	9.97	109.5	10.54	109.4	11.02
111	110.6	9.67		10.16			110,4	
112	10000	9.76	111.5	10.25	111.5	10.73	irr.4	11,22
113	112.6	9.85		10.34	112.5	10.93	113.4	11,42
115	1146	10.01	114.5	10.52	114.5	11.02	1144	11,52
116	115.6	10.11	115.5	10.61	115.5	11.12	115.4	11,62
117	117.6	10.20		10.71	116.5	11.21	CONTRACTOR OF THE PARTY OF THE	11.72
119	118.5	10.37	117.5	10.80	117.5	11.40		11,52
120	119.5	10.46	119.5	10.98	119.5	11.50	119.4	12/02
2	Dep.	Lat	Dep.	Lat	Dep.	Lat	Dep.	Lat.
Dist	0,		45	1	30		1.5	23
1000		1	94	DEGR	D.D.O.		_	

84 DEGREES.

-	0	-	15	-	20	-	45		
Dist	_	Des	-		30	-	Lat.	Dep.	
	Lat.	Dep	Lit	Dep.	Lat	Dep.	THE OWNER OF THE OWNER, THE OWNER	0.12	
2	0.99	0.10	1.99	0.11	0.99	0.11	0 99	0.11	
3	2.98	0.31	2.98	0.33	2.98	0.34	2.98	0.35	
4	3.98	9.42	3.98	0.44	3-97	0.45	3.97	0.47	
- 5	4.97	0.52	4.97	0.54	4-97	0.57	4-97	0.59	
6	5-97	9.63	5 96	0.65	5-96	0.68	5.96	0.81	
7 8	7.96	0.84	7.95	9.87	7-95	0.91	7.94	0.04	
9	8.95	9.94	8.95	0.98	8.94	1.00	8.94	1.00	
10	9.95	105	9.94	1.09	9.94	1.13	9.93	1.18	
36	10.94	1.15	10.93	1.20	10-93	1.15	10.92	1.29	
12	11 93	1.15	11.93	1-31	11.92	1.47	11.92	1.53	
13	13.92	1.46	13.92	1.52	13.91	1.58	13.90	1.65	
15	14.92	1.57	14 91	1.63	14.90	1.70	14.90	1.76	
16	15.91	1.67	15.90	1.74	15.90	1.81	15.89	1.88	
17	16.91	1.78	16.90	1.85	16.89	1-92	16.88	2.11	
18	17.90	1.88	17.89	1.96	17.88	2.15	17.88	2.23	
20	19.89	1.00	19.88	2.18	19.87	2.26	19.86	2-39	
21	20.89	3.30	20.88	1.19	20.86	1.38	20.84	2-47	
22	\$1.88	4.30	21.87	1.40	21.86	2.49	21.85	1.59	
23	32.87	240	\$2,86	\$.50	32.85	2.60	22.84	2-70	
24	23.87	2.61	13.86	2.61 3.77	33.85	1.72	14.83	3.94	
26	25.86	1.72	26.85	2.83	25.81	2.94	25.82	3.06	
27	26.85	282	26.84	3.94	26.83	3.06	26.81	3.17	
28	37.85	2-93	37-53	3.05	17.81	3.17	27.81	3-29	
39	28 84	3.03	48.83	3.16	18.81	3.28	48.80	3-41	
30	29:84	3.14	29.88	3-97	29.81	3.40	19-79	3-53	
31	30.83	3.24	30.82	3-37	30.80	3.51	30.79	3.64	
33	32.82	3-45	32.80	3.59	31.79	3-74	32.77	3.88	
34	13.81	3.55	33.80	3-70	33.78	3.85	13.76	4-00	
35	34.81	3.66	34-79	3-81	34.7%	3.95	1476	4-11	
36	35.80	3.76		3.93	35.77	4-08	15.75	4-23	
37	36.80	3.87	36.78	4-93	30.76	4-19	37-74	4-35	
39	38.79	4.08	18.73	4-85	38.75	441	38.73	4.58	
40	39.78	4.18	39.76	4-35	39-74	4-53	39.70	4.70	
41	40.78	4.29	40.76	4.46	40.74	4.64	4072	4.82	
43	41.77	4.49	41:75	4-57	41.73	475 487	41.71	5.05	
44	43.76	4.60	43-74	479	43-73	4-98	43.70	5-17	
45	44.75	4.70	44-73	4-90	4471	5/09	44.69	5-29	
46	45.75	4.81	45.73	5.01	45.70	5-21	45 68	541	
47	46.74	491	46.72	5-13	46.70	5.32	46.67	5.64	
48	47.74	5.12	47.71	5.33	47 69	5-43	48.56	5.76	
50	49.73	9.23	49.79	5.44	49 68	9.66	49.65	5.88	
51	10.73	5-33	50.70		50.67	5-77	90.65	5-99	
52	51.72	\$-44	51.69	5.66	91.67	5.89	51.64	6.11	
53	52.71	5.54	52.69	5.27	53.65	6.00	53.63	6.35	
54 55	53-79	5.75	54.67	5.99	54.65	6.23	54.60	6,46	
56	55.69	9.85	55.67	6.10	55 64	6.34	55.61	6.58	
57 58	56.69	5.95	56.66	6.21	\$6.63	6.45	\$6,60	6.70	
58	57.68	6,06	57.66	6.31		6.57	57.60	6.81	
59 60	59.67	6.17	58.65	6.42	59.61		59.58	7.05	
2000	Dep.	Lat	Dep.	Lat	Dep.	Late	Dep.	Late	
Dist		A THE	Liep.	-		O/	- Defe	57	
Proping N			1	ALC: UK	DEDUE				

, =	1 0	)/	1 1	,/	1 2	υ'	1 4	./
1 2			Lat		Lat.		Lat.	
61	60.67	Dep	63.64	6.64		D p.	·	()+p.
62	61 66	6.38	61.63	6.75	60.61	7.02	60.58	7.17 7.29
63	6265	6.59	62.63	6.86	62.60	7.13	62.56	7.40
64	63.65	6.69	63.62	6.97	63.59	7 25	63.56	7 52
65	64.64	6.79	64.61	7 28	64.58	36	64.55	7.64
66	65 64	7.00	65.61	7.19 7.29	65 58 66.57	7.47	65.54	7.76
68	67.63	7.11	67.60	7.40	67.56	7.70	67.53	7.99
69	68.62	7.21	68.59	7.51	68.56	7.81	68.52	8.11
70	-69.62	7.32	69.58	7.62	69 55	7.42	69.51	¥.22
7.5	70.61	7 42	70 58	7.73	70.54	8.34	70.51	8.35
72 73	71.61	7.53	71.57	7 84 7.95	71.54	8.15	71.50	8.46
74	73.59	7-74	73.56	8.06	73.52	8.38	73.49	8 70
75	74.59	7.84	74.55	8.17	74.52	8 49	74.48	8.83
76	75.58	7.94	75.55	8.27	75.51	8 60	75.47	8.93
77	76.58	8.05	76.54	8.49	76.51	8.72 8.83	76.47 77.46	9.2¢ 9.17
70	77.57 78.57	8 26	77.54	8.60	77.50 78.49	8.94	77.45	9.17
80	79.56	8.36	79 52	8 71	79 49	9.06	79.45	9.45
81	80.56	8.47	80.52	8.82	80.48	9.17	80.44	9.52
82	81.55	8.57	81.51	-93	81.47	9.28	81.43	9.64
83 84	82.55 83.54	8.68	82.51 83.50	9.04	82 47 83 46	940	82.42	9.76 9.87
85	84.53	8.88	84 49	9 25	84.45	962	84.41	9 99
86	85.53	8.99	85.49	9.36	85.45	9.74	85.40	10 11
87	86.52	9.09	86 18	9-47	86.44	9.85	86.43	10.23
88	87.52 88.51	9.20	87.48 88.47	9.58 9.69	87 +3 88.43	13.58	87.39 88.38	10.46
89 93	89.51	9.30	89.47	9.80	89.42	13.14	89.38	10.58
91	93.50	9.51	90.46	9.91	90.12	10.30	90 37	13 73
92	91.50	9.62	91.45	10.02	91.41	19.41	91.36	10.81
93	92.49	9.72	92.45	:012	91.40	10 53	92.35	15.93
94	93.49	9.83	93.44	10.23	9340	10.64	93-35	11.05
95	94.48	9.93	94-11	10 37	94.39	10.75	94.34	11.23
97	96.17	10.14	95.43	10.56	96 38	10.98	95.33 96.33	11 10
98	97.46	1024	97.42	10.67	97-37	11.59	97.32	11.52
99	98.46	10 35	98.41	10.78	98.36	11.21	98.31	11.04
100	99.45	10.45	99 41		99.36	11.32	99.31	11.87
101	103.4	10.66	100.4	11.10	102.3	11.55	100.3	1199
103	102.4	10.77	102.4	11.21	102.3	11.66	102 3	12.11
104	103.4	10.87	103 4	11.32	103.3	11.77	103.3	12.22
105	1014	12 48	104.4	11.43		11.89	104.3	12.34
106	1054	11.08	105.4	11 54	106.3	12.00	105.3	12.48
108	107.4	11.29	107.4	11.76	1	12.23	157.3	12.69
109		11.39	1084	11.87	108.3	12.34	108.2	12.81
110	1094	1150	109.3	11.98	179 3	12.45	109.2	12.93
111		11.65	110.3	12.58	- 1	1267 1	1102	13 O; 13.16
112	111.4	11.71	111.3	12.19	- 1	12.68	111.2	13.28
114	113.4	11.92		1241		1291	113.2	
115	1144	1202	114.3	12.52	1143	13.02	114.2	13 52
116	115.4	12.13	115.3	1263		13.13	1152	13.63
117	116.4	12.23	116.3	12.74		13.24 13.36 -	116.2	13.75
119	118.3			12.05		15 50 13 47 .		13 09
125	11931	12 54	1193	13 06		13.58		14 10
ايد	17 ,	11	1) p	La	Dep.	1.1	Dep	lat.
Dist			4	,	٠,0	7	15/	
			07	Dr. iR	1 13			

1 -	1 -0	1	1 14	1	1 20	1	45'	
) ist	Lat	-	Lat.	Dep.	Lat	Dan	-	Dep.
-		Dep		_	-	Dep.	Lat.	
13	0.99	0.12	0.99	0.13	0.99	0.13	0.99	0.13
3	1.99	0.37	1.98	9-38	2.07	0.39	2.97	0.40
1 4	3-97	0.49	3.97	0.50	3.97	0.52	3.06	D.54
1 3	4.96	D.61	4.96	0.63	4.96	0.65	4.95	0.67
6	5.06	1073	5.95	0.76	5.95	0.78	5.95	0.81
7 8	0.95	0.85	6.94	0.88	6.94	0.91	6.94	0.94
8	2.94	0.98	7.94	10.0	7 93	1.04	7.93	80.4
9	8.93	1 10	8.93	1.14	8.92	1.17	8.92	1.21
10	9-93	1/22	9.92	1.26	9.91	1.31	9.91	1.35
188	10.92		10.91	1.39	10.91	1.44	10.00	1.48
(88	11.91	1.46	11.90	1.51	11.90	1.57	11.89	1.75
13	12.90		13.89	1.77	12.89	1.70	13.87	1.89
15	14.89	1.83	14.88	1.89	14.87	1.96	14.86	2.02
10	15.88	1.95	15.87	2.02	15.86	2.00	15.85	2.15
12	16.87	207	16.86	2.15	16.85	2.22	16.84	2.29
1.8	17.87	2.19	17.86	2.27	17.85	2.35	17.84	2-43
19	18.86	2.32	18.85	3.40	18.84	2.48	18.83	2.56
20	19.85	2.44	19.84	2.52	19.83	2.61	19.82	2.70
2.1	20.84	2.50	20.83	2.05	20.82	2.74	20.81	2.83
22	21.84	2.68	21.82	2.78	21.81	2.87	21.80	2.97
23	22.83	2.80	22.82	2.90	22.80	3.00	22.79	3.10
24	23.82	3.05	24.80	3.03	23.79	3.13	25.78	3-75
25	-		-		24.79			3.37
26	26.80	3.17	25.79	J 28 3.41	25.78	3.39	25.76	3.51
1 28	27.79	3.41	27.78	3.53	27.76	3.52	27.74	3 78
29	28.78	3.53	28.77	3.66	28 75	3.79	28.74	3.91
30	29.78	3 66	29.76	3-79	29.74	3.92	29.73	4.05
31	30.77	3.78	30.75	3.91	30 73	4.05	30.72	4-18
4 32	31.76	13.90	31.74	4.04	31.73	4.18	31.71	4.32
33	32.75	4.02	32.74	4.16	32.72	4-31	32.70	445
34	33.75	4.14	33-73	4.29	33-71	4 44	31-69	4.58
35	34-74	4 27	31-72	4-42	34-10	4.57	34.68	4.72
36	35.73	4.39	35-71	4 54	35.69	4.70	35-67	4-85
37	30.72	4.51	36.70	4.67	36.68	4.83	36.66	4-99
38	38.71	4.75	38.69	4 92	37,67	5.00	37.65	5.12
40	39.70	4.87	39.65	5.05	39.66	5.22	39.63	5-39
42	40.69	5 00	40.67	5.17	40.65	5.35	40.63	5-53
42	41.60	5.12	41.66	5.30	41.64	5.48	41.62	5.66
43	42.68	5 24	42.66	5.43	4# 63	5.61	42.61	5.80
44	43 67	5.36	43.65	5-55	43.62	5.74	43.60	5.93
45	44 66	3.48	44.64	5.68	44.62	5.87	44-59	6.07
46	45.66	5.61	45.03	5.81	45.01	6.20	45.58	6.20
47	46.65	5-73	46 62	5.93	46.00	6.13	40.57	6.34
48	47.64	5.85	47.62	6 18	47-59	6.40	47.56	6.47
49	49.63	6.09	49.60	6.31	48.58	6.53	48.55	6.61
CX	50.62	6.22	10.10	6.44	100 16	h 05	10.11	F 22
52	51.61	6.34	51.58	6.56	51.56	6.79	51.53	7.01
53	52.60	6.46	52.58	6.69	5255	6.92	52.52	7.85
54	53.60	6.58	53-57	6.81	53-54	7.05	53.91	7.28
55	54-59	6.70	54.56	6.94	54-53	7.18	54.50	7.42
56	55.58	5.82	55.55	7.07	55-52	7.31	55-49	7.55
57 58	56.58	6,95	56.54	7.19	56.51	7-44	56.48	7.60
58	57.57	7.07	57.54	7.32	57.50	7:57	57-47	7.82
59	58.56	7-31	58.53	7-45	58.50	7.70	58.46	7.96
	59-55 Dep.	Lat.	1)ep.	Lat.	59:49		59.45	8.00
Dist		-	-	Lant	Dep.	Lat.	Dep.	Lat
	G.	10000	45	Mary .	30	-	1	5
	-	Acres and	82 1	DEGRE	ES.		-	7-9-4

			15/ I		1 30'		45/	
Vist.	0.		1:					
7	Lat.	Dep.	Lat.	Dep.	Lat.	D	Lut.	D-p.
61	60 55	7-43	60.51	7.70	60.48	7.90	60.44	8.23
62	61.54	7.56	61.50	7.82	61.47	8.09 8.22	61.43 62.42	8.36 8. <sub>5</sub> 0
63	62.53	7.63 7.80	62.50	7.95 8.08	<b>62.46</b> 63.45	8.35	63 42	8.63
64 65	63.52 64.52	7.00	64.48	8,20	64 44	8.48	64.41	8.77
66	65.51	8.04	65.47	8.33	65.44	8.01	65.40	8.93
67	66.50	8.17	66.46	8.46	66.43	8.75	66.39	9.04
68	67.49	8.29	67.46	8.58	67.42	8.88	67.38	9.17
69	68.49	8.41	68.45	8.71	68.41	9.01	68.37	y 30
70	69.48	8.53	69.44	8.83	69.40	9.14	69 36	9.11
71	73.47	8.65	70 43	8.96	70.39 71.38	9.17	70.35 71.34	9.57
72	71.46	8.77 8.90	71.42 72.42	9.09	72.38	9.53	72.33	9.84
73 74	72.46 73.45	9.02	73.41	9.34	73.37	9.66	73.32	9.98
75	74-44	9.14	74.40	9.46	74.36	9.79	74.31	10.11
76	75.43	9.26	75-39	9-59	75-35	9.92	75.31	10.25
77	76.43	9.38	76.38	9.73	76.34	10.05	76.30	10 38
78	77.42	9.51	77.38	9.84	77.33	10.18	77.29 78.28	10.55
79	78.41	9.63	78.37	9.97	78.32 79.32	10.31	79.27	15.79
80	79.40	9.75	79.36		80.31	10 57	83.20	10.92
81 82	80.40	9.87	80.35 81.34	10.22	81.30	10.70	81.25	11.06
83	81.39 82.38	10.13	82.34	10.47	82.29	13.83	82.24	11.19
84	83.37	10.24	83.33	10.60	83.28	15.96	83.23	11.33
85	84.37	10.36	84.32	10.73	84 27	1109	84.22	11 46
86	85.36	10.48	85.31	10.85	85.26	11.23	85.21	1160
87	86.35	10.60	00.50	10.98	86.26	11.36	86.21 87.20	11.73
88	87.34	10.72	87.30 88.29	11.11	87.25 88.24	11.49	88.19	12.00
89	88.34 89.33	10.97	89.28	11.36	89.23	11.75	89 18	12.14
90		11.09	90.27	11.48	90.22	11.58	90.17	12.27
91 92	90.32	11 21	91.26	11.61	91.21	12.01	91.16	1241
93	92.31	11.33	92.26	11.74	92.20	12.14		12.54
94	93.30	11.46	93.25	1186	93.20	12.27	, , ,	12.65
95	94.29	11.58	94.24	11.99	94 19	12 40	94.13	
96	95.28	11.70	95.23	12.12	95.18	12.53	95.12 96.11	13.08
97	96.28	11.82	96.22	12.24 12.37	96.17 97.16	12.79	97.10	13.22
98	97.27 98.26	11.94	97.22 98.21	12.49	98.15	12.92	98.10	13.35
99 100	99 25	12.19	99.20	12.62	99 14	13 05	99.09	13.49
101	100.3	12.31	100.2	12.75	100.1	13.18	100.1	13.02
102	101.2	12.43	101.2	12.87	101.1	13.31	101.1	13.75
103	102.2	12.55	102.2	13.00	102.1	13.44	102.1	13.89
104	103 2	12.67	103.2	13.12	103.1	13.57	103.1	14 16
105	104.2					13.8.1	105.0	14.29
106	105.2	12.92	105.2	13.38 13.50	105.1	13.97	106.0	14 43
107	100.2	13.16	107.1	13.63	107.1	14 10	107.0	14.56
109	108.2	i 3 28	108.1	13.76	108.1	14.23	108.0	14.70
110	109.2	1341	109.1	13.88	109.1	14.36	109 0	14.83
111	110.2	13.53	110.1	14.01	110.1	14.49	110.0	14 97
1112	1112	1365	111.1	14.13	111.0	14.62	111.0	15.10
113	112.2	13.77	112.1	14.26	112.0	14.88	113.0	15.37
114	113.2	13.89	114.1	14.24	114.0	15.01	-	1551
115	_	14.14	115.1	14.64	115.0	15.14		15.04
116	115.1	14.14	116.1	14.77	116.0	15.27	1159	15 78
118	117.1	14.38	117.1	14.89	117.0	15 40	116.9	15.91
119	118.1	14.50		15.02	118.0	15.53	117.9	16.05
120	119.1	14.62	119.0	15.14	1190	15.60		
Dist.	Dep.	lat.	Dep.	: Lat	Dep.	Lac	Dep.	1 1 1
≊	()	<del>,</del>	45	,	30	,	1.	, ,

10	0		15	,	30	)'	4:	1	i
13.5	Lat.	Dep.	Lat.	Dep.	1,at.	Dep.	Lat.	Dep.	١
1 2	0.99	0.14	1.98	0.14	0.99	0.15	0.99	0,15	l
3	2.97	0.42	2.97	0.43	2.97	0.44	2.97	0,46	l
4	3.96	0.56	3.96	0.57	3.96	0.59	3-95	10,0	I
5	4-95	0.70	4-95	0.72	4-95	0.74	4-94	0.76	ı
6	6.93	0.97	5.94	1,00	5.93	1.03	5.93	1,06	Į
7 8	7.92	Litt	7.92	1,15	7.91	1.18	7-91	1,22	ı
10	8.91	1.39	9.90	1.43	9.89	1.33	9.88	1,37	ı
11	10.89	1453	10.89	1.58	10.88	1,63	10.87	1.67	ı
12	11.88	1.67	11.88	1 72	11.87	1.77	11.86	1.83	ı
13	12.87	1.81	12.87	2.01	12.86	2.07	12.85	2,13	ı
15	14.85	2.09	14.84	2.15	14.84	2.22	14.83	2.28	ı
16	15.84	2.23	15:83	2.30	15.82	2 37	15.81	2.43	ı
17	16.83	2 37	16.82	2,44	16.81	2,51	16.80	2,74	ı
19	18.82	2.64	18.50	2,73	18.79	2.81	18.78	2.89	l
20	19.81	2.78	19.79	2.87	19.78	2.96	19.77	3104	ı
21	20.80	2.92	20.78	3.01	20.77	3.10	20.76	3119	Į
23	21.79	3.06	21.77	3.30	21.76	3.25	21.74	3.35	ı
24	23.77	3.34	23.75	3.44	23.74	3.55	23.72	3165	l
25	24.76	3,48	24.74	3.59	24 73	3.70	24.78	3 80	l
26	25.75	3.62	25.73	3.73	25.71	3:84	25.70	3.98	ı
28	27.73	3.90	27.71	4.02	27.69	414	27.67	4:16	l
30	28.72	4-18	28.70	4.16	28.68	4-29	28.06	441	i
31	30.70	4-10	30.68	4 45	30.66	4-43	30.64	4.56	ı
32	31.69	4.45	31.67	4-59	31.65	4-72	31.63	487	ı
33	32.08	4 59	32.66	474	32.64	4.88	32.62	5102	ı
34	33 67	4.73	33.65	5.02	33.03 34.02	5.03	33.60	5:32	ı
30	35.65	5.01	35.63	5/17	35.60	5.92	35.58	5148	ı
37	30.64	5.15	36.62	5431	30.59	5-47	36.52	1.63	ı
38	38.62	5.43	37.61	5.45	37.58	5.62	37.56	5.78	ı
40	39.61	3.57	39 59	5-74	39.56	5.91	39-53	80.0	ı
42	40.60	5-71	40.58	5.88	40.55	6,05	40.52	6:24	ı
42	41.59	5.85	47.57	6.03	41.54 4±53	6.36	41.51	figg figs	ı
44	43-57	6.12	43-54	6.31	43.52	6.50	43-49	6.69	ı
45	4+56	6 26	44-53	6.46	44-51	6,65	44.48	4.85	
46	45.55	6.40	45.52	6.74	45-49	6.80	45.46	7100	
48	47-53	6 68	47.50	6.89	47-47	7:09	47-44	7-130	
49	48.52	6.82	48.49	7.03	48.46	7/24	48.43	7445	
50	49.31	6.96	49.48	7.17	49:45	7 39	49:42	7.6L	
53	51:49	7.10	51.46	7-46	51.43	7 69	50 41 51.39	7-76	
53	5248	7.38	52,45	761	52.42	7.83	52.38	8.06	
54 55	53.47	7.52	54-43	7.75	53.41	7.98	53-37 54-36	N:27	
156	55.46	7.79	55.42	8.04	55.38	8.28	55-35	Sign I	
57 58	56.45	7 93	56 41	8.18	56.37	8.43	5h:34	8,67	
56	57.44	8.07	58.39	8.32	57-36	8.57	57-33 58:31	8,98	
59	59.42	8.35	59.38	8.61	59:34	\$ 87	59-30	9/13	
THE STATE OF	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	
Dirt	01		-45	No. of Street, or other	50		15		
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P	10			5'	ا <u>ع</u>	U <sup>1</sup>	l —4	<u>'</u>
ت	Lat.	Dep	Lat	: Dep	Lat.	D. p.	læt.	Dep.
61	60.41	8.49	60.37	8.75	60.33	902	63.29	4.28
62	61.40	8 63 8.77	61.36	8.90	61.32	9.16	61.28	9.43
63	62.39 63.38	8.91	62.35	9.04 9.18	62.31	9.31	62 27	9.58
65	64.37	9.05	64.33	9.33	64.29	961	64 24	1.89
66	65.36	9.19	65.32	9 47	65.28	9.76	03.23	10.04
67	66.35	9.32	66 31	9.61	66.26	9.90	66.22	10.19
68	67.34	9.46	67.30	9.76	67 25	10.05	67.21	10.34
69	68.33	9.60	68.29	9.90	68 14	10.20	68 20	10.50
70	69 32	9.74	69.28	10.01	fy.23	10 35	69.19	10 65
71	70.31	9.88	70.27	10.19	70.22	15.49	73.17	16.80
72	71.30	10.02	71.25	10.33	71.21	10.64	71.16 72.15	10.95
74	73.28	10.30	73.23	10.62		10.94	73.14	11:6
75	74.27	10.44	74.22	10.76	74.18	11.09	74.13	1 41
76	75.26	10.58	75.21	10.91	75-17	11.23	75.12	11.56
77	76.25	10.73	76.20	11 05	76.15	11.38	76.10	11.71
78	77.24	10.86	77.19	11.19	77-14	11.53	77.09	11.87
79 80	78.23	10.99	78 18	11.34		11.68	78.08	12.02
	79 22		79.17	11.48	79.12		79.07	12:17
81	80.21	11.27	80.16	11.62	81.10	,11.97 :12.12	81.05	12.32
83	82.19	11.55	82.14	11.91		12.27	8203	12.63
84	83.18	11.69	83.13	12.05	83 08	12.42	83.02	12.78
85	84.17	11.83	84.12	12.20	84 07	12.56	84.01	12.93
86	85.16	11.97	85.11	i 12.34	85.06	12.71	85.00	13.08
87	86.15	12.11	86.10	12.48	86 04	12.86		13.23
88	87.14	12.25	87.09	12.63	87.03	1301	86 98	13.39
89	88.13 89.12	12.39	88.08	12.77	88.02	113.16	87.96 88 95	13.54
90		12.53	· -					
91	90.11	12.66	90.06	13.06	90.00	13.45	89 94 90.93	13.84
93	92.09	13.94	92.54	13.34	91.98	13.75	91.93	14 15
94	93.09	13.08	93.03	13.49	92.97	13.89	9291	14.30
95	94.08	13.22	94.02	13.63	93 96	14.04	93.89	14.45
96	95.07	13.30	95.01	13.78	94.95	14.19	94 88	14.60
97	96 06	13.50	96.00	13.92	95.93	14.34	95.87	14-6
98	97.05	13.64	96.99	14.06	96.92	14.49	96.86	14.91
99	98.04	13.78	97.98	14.21	97.91	14.63	97.85	15.06
101	100.0	14.06		14.49	99 89		99.82	
102	101.0	14.20	99.95	14.64	100.9	14.93	100.8	15.36
103	102.0	14 33	101.9	14.78	101.9	15.22	8.101	15.67
104	103.0	14.47	102.9	14.92	101.9	15.37	103.8	15.82
105	104.0	14.61	103.9	15.07	103.8	15.52	103.8	15.97
106	105.0	14.75	104.9	15.21	104.8	15.67	104.8	16.13
107	106.0	14.89	105.9	15.35	105.8	15.82	105.8	16.28
108	105.9 107.9	15.03	106.9	15.50	106.8	15.96	106.7	16 43 16 58
110	107.9	15.31	108.9	15.78	107.8	16,26	107.7	16.73
111	109.9	15 45	109.9	15.43	109.8	16.41	109.7	16.89
112	110.9	15.59	110.8	16.07	110.8	16.55	110.7	17.04
113	111.9	15.73	111.8	16.21	111.8	16.70	111.7	17.19
114	112.9	15 87	112.8	16.36	112.7	16.85	112.7	17.34
115	113.9	16.00	113.8	16.50	113.7	17.00	113.7	17.49
116	114.9	16.14	114.8	16.65	114.7	17.15	114.7	1765
117	115.9	16.28	115.8	16.79	115.7	17.29		17.80
1119	116.9 117.8	16.42 16.56	116.8	16.93	116.7	17.44	116.6	17 95
120	118.8	16.70	118.8	17.22	118.7	17.59	118.6	18.25
	Dep.	Lat.	Dep	Lat.	Dep	lat	Dep.	Lat.
Dist	- DCp.		4.		36		15	
12	U		4:		باد		13	

200	-	)/	1 1	51	1 .	0'		-
Disi	-					the same of		5'
6	Lat	Dep.		Dep		Dep	Lee .	Dep.
1	COLUMN TO SERVICE		0.99	0.16	THE RESERVE	ART DESCRIPTION AS		0.17
1 3			2.96	0.48				
1 4			3.95	0,64	3.99	0.66	3 94	0.68
3		0.78	4 94	0.80	4 93	0.83	4.93	0.85
6	5.93		5.98					
7 8	6.91	1.10	6.91	1.13				
1 9	2-2-	1.41	8.88	1.45	10000		8.87	1.58
10		1.56	9.87	1.61	9.86		9.86	1 69
11	10.86	1.72	-10.86	1.77	10.84	1.82	10.84	1.86
12		1.88	11.84	1.93	11.84		11.83	2.03
13		2.03	12.83	2.09	13.81		12.81	2.20
114	13.83	2.19	14.80	2.25	14.79		14.78	2.37
16		2,50	15.79	2.57	15.78		15.77	2.71
		2.66	16.78	2.73	16.77	an enterement	16.75	2.88
18		2.82	17.77	2.89	17-75	2.97	17.74	3.05
19	18.77	2.97	18.75	3.05	18.74		18.73	3.22
20	19.75	3.13	19.74	3.21	19.73		19.71	3.39
21	20.74	3.29	21.71		20.71		20.70	3.56
23	21.73	3.44	22.70	3 54	21.70	3.63	22.67	3-73
24	23.70	3.75	23.69	3.86	23 67	3.96	23.65	4.06
25	24.69	3.91	24.67	4.02	24.66	4.13	24.64	4-23
26	25.68	4.07	25.66	4.18	25.64	4.29	25.52	4.40
27	26.67	4.22	26.65	4-34	26.63	4.46	26.61	4-57
28	27.66	4.38	27.64	4.50	27.62	4.62	28.58	474
30	29.63	4.54	29.61	4.66	29.59	4-79	29.57	5.08
31	30.62	4.85	30 60	4.98	30.57	5.12	30.55	5.15
32	31.61	5.01	31.58	5.14	31.56	5.28	31.54	5-43
33	32.59	5.16	32.57	5.30	32.55	5.45	32 52	5-59
34	33 58	5.32	33.56	5.47	33.53	5.61	33.51	5.76
35	34-57	5.48	34-54	5.63	34.52	5.78	34-49	5.93
36	35.56	5.03	35.53	5.79	35.51	5.94	35.48	6.10
38	37-53	5.94	37.51	5.95	37.48	6.27	37-45	6.44
39	38.52	6.10	38.49	6.27	38.47	6 44	38.44	6.50
40	39.51	6.26	39.48	6.43	39.45	6.60	39.42	6/27
41	40.50	6.41	40.47	6.59	40 44	6.77	40.41	6.94
42	41.48	6.57	41.45	6.75	41.42	6.93	41.30	7-11
43	42.47	6.88	42.44	7.07	43.40	7.10	42.38	7-28
45	44-45	7.04	44.41	7.23	44-38	7-43	44-35	7.6±
46	45-43	7.20	45.40	7.39	45-37	7-59	45-34	7.79
47 48	46.42	7-35	46.39	7.55	46.36	7.76	46.32	7.96
	47.41	7.51	47.38	7-72	47:34	7.92	47-31	8-13
49	48.40	7.66	48 36	7.88	48.33	8.09	48,29	8.30 3.47
P 700	49.38	- 0	49.35	0	49.31	0	10000	8.64
52	50.37	7.98	50.34	8.36	50.30	8,42	51.25	8.81
53	52.35	8.29		8.52	52.27	8.75	52.23	8.98
54	53-34	8.45	53.30	8.68	53.26	8.91	53.22	9-14
55	54.32	8.60	54 28	8,84	54.25	9.08	54 21	9-31
56	55.31	8.76	55-17	9.00	55-23	9.24	55-19	9.48
57	56.50	8.92	56.26	9.16	56.22	9.47	56.18	9.81
59	57.29	9.07	57.25	9.32	57.20	9-57	57.15	9.99
59	59.26	9 39	59.22	9.64	59.18	9.90	59.13	10,15
	Dep.	Lat	Dep.	Lat	Dep-	Lat.	Dep	Late
Dist.	0/		45/		30		151	
				DEG	THE RESERVE TO SHARE THE PARTY OF THE PARTY			

,			9	DEGRI			103		
Dist.			154			0'	4.5		
ا أ	Lat	Dep.	Lat.	Dep	Lat	Dep.	Lat	D-p	
61	60.25	9-54	60 21	9.81	60.16	10.07	60.12	10.33	
62 63	61.24	9.73 , 9.86	61.19	9.97	61.15	10.23	61 10	10 50	
64	63.21	10 01	63.17	10.29	63.12	10.40 10.56	62.09 63.08	10.67	
65	64.20	10.17	64.15	10 45	64.11	10.73	64.06	11.01	
66	65.19	10.32	65.14	10.61	6; 09	10.89	65.05	11.18	
67	66.18	10.48	66.13	10.77	66.08	11.06	66.03	11.35	
68 69	67.16	10.64	67.12 68.10	10.93	67.07 68.05	11.22	67.02	11.52	
70	69.14	10.79	6g.0g	11.25	69 04	11.39	68.99	11.69	
71	70.13	11.11	70.08	11.41	70.03	11.72	69.97	12.02	
72	71.11	11.26	71.06	11.57	71.01	11.88	70.96	12.19	
73	72.10	11.42	7205	11.73	72.00	12.05	71 95	12.36	
74 75	73 Og 74 O8	11.73	73 04 74.02	11.90	72.99	12.21	72.93	12.53	
76	75 06	11.89		12.22	73.97	·	73 92	12.70	
77	76.05	12.05	75.01 76.00	12.22	74.96 75.94	12.54	74.90 75.89	13.04	
78	77.04	12.20	76.99	12.54	76.93	12.87	76.87	13.21	
79 85	78.03	12.36	77.97	12.70	77.92	13.04	77.86	13.38	
80	79.02	12 51	-8.o6	12.86	78.90	13.20	78.84	13.55	
82	80.00 80.99	12.67	79 95 80.93	13.02	79.89 80.88	13.37	79.83 80.82	13.72	
63	8198	12.98	8192	13 34	81.86	13.70	81.80	14.06	
84	82.97	13 14	8291	13.50	82.85	13.86	82.79	14.23	
. 85	83.95	13.30	83 89	13.66	83.83	14.03	83.77	14 39	
86 87	84.94	13.45	84.88	13.82	84.82	14.19	84 76	14.56	
88	85 93 86 92	13.77	85.87 86.86	13.98	85.81 86.79	14.56	85.74 86.73	14.73	
89	87 93	13.92	87.84	14 31	87.78	14.69	87.71	15.07	
90	88.89	14.08	88.83	14 47	88.77	14.85	88 70	15.24	
91	89.88	14.24	84.82	14.63	89.75	15.02	89.69	15.41	
92	90.87	14.39	90.80	14 79	90.74	15.18	90.67	15.58	
93 94	91.86	14 55	91.79	14.95	91.72	15.35	91.66	15.75	
95	93.83	14.86	93.76	15 27	93.70	15.68	92.63	15.92 16.09	
96	94.82	15.02	94.75	15.43	94.68	1584	94.61	16.26	
97	9581	15 17	95.74	15.59	95.67	16.0i	95.60	16.43	
98	96.79	15.33	96.73	15.75	96.66	16.17	96.58	16.60	
100	97.78 98 77	15.49	97 71	15.91	97.64	16.34 16.50	97.57 98.56	16.77 16.94	
101	99.76	15 80		10.07		16 67		17.10	
102	100.7	15.96	99 69 100.7	16.40	99.61	16.83	99·54 100·5	17.27	
103	101.7	16.11	101.7	16 56	101.6	17.00	101.5	17.44	
104	102.7	16 27	102.6	16 72	102.6	17.17	102 5	17.61	
106	103.7	16.43	103.6	16.88	103.6	17.33	103.5	17.78	
107	104.7	16 58	104.6	17.04	104.5	17.50	104.5	17.95	
108	105.7	16.90	106.6	17.36	105.5	17.83	106.4	18.29	
109	107.7	17.05	107.6	17.52	107.5	17.99	107.4	18.46	
110	108.6	17.21	108.6	17.68	108.5	18.16	108.4	18.63	
1112	109 6	17.36	109.6	17.84	109.5	18.32	109.4	18.80	
113	110.6	17.52	110.5	18.00	110.5	18.49	111.4	18.97	
114	113.6	17.83	112.5	18.32	1124	18.82	1:24	19.31	
115	113.6	17.09	113.5	18 49	1134	18.98		19.48	
116	114.6	18.15	1145	18.65	114.4	19.15	114.3	19.64	
117	115.6	18.30	115.5	18.81	115.4	19.31	115.3	19.81	
119	116.5	18.46	116.5	j 18.97 19.13	116.4	19.48	116.3	19.98	
120	118.5	18.77	1184	19.15	117.4	19.80	118.3	20.32	
نیا	Dep.	Lat.	Dep.	Lat.	IN P	Lat.	Dep.	Lat.	
Dist.		),	45	<u></u>	30		1		
	`			Timot	<u></u>			-	

7 -	1 0	_	-	-	- 00			
Dist	-	-	-		30		1	1
-	Lat.	Dep.	Late	D:p.	Late	Dep.	Last.	Dep.
1 14	0.98	0.17	0.98	0 18	0.98	0.18	1 0.98	0.10
1 3	1.97	D. 35 D. 62	1.97	0.30	7.95	0.55	1.95	0.55
1 4	3.94	0.69	3.94	0.71	3.93	0.73	3.93	0.75
5	4.93	0.87	4.92	0.89	492	0.91	4.91	0.93
6	5.91	1.04	5.90	1.07	5.90	1.04	5.89	1.12
7	6.89	1.22	6,89	1.25	6.88	1.28	6.88	1.32
8	7.88	1.39	7/87	1.42	7-87	1.46	7.86	1,43
9	8.86	1.56	8.86	1.60	8,85	1 64	8.84	1.68
10	9.85	1.74	9.84	1.78	9,83	1.82	0.82	1.57
31	10.83	2.08	10,82	1.95	10,82	2.00	10.81	2.05
12	12.80	2,26	11.81	2.14	11,80	2.37	11.79	2.42
13	13.79	2.41	13.78	2.49	13.77	2.55	13.75	2.01
15	14.77	2.60	1476	2.67	1475	2.93	14-74	1.50
16	13.76	2.78	15.74	2.85	15.73	2.92	15.72	198
17	16.74	2.95	16.73	3.03	16.72	3.10	16.70	3-17
18	17.73	3.13	17-71	3.20	17.70	3.18	17.68	3-36
19	18.71	3.30	18 70	3.38	18.68	3.46	18.67	3-54
20	19.70	3-47	19.68	3.56	19.67	3.64	19.65	3-73
21	20.68	3.05	20.66	3-74	20.65	3.83	20.63	3 92
22	21.67	3 82	21.65	3.91	21.61	401	21.61	4-10
24	23 64	3.99	21.61	4.09	23.60	4-19	23.58	4-48
-20	14.62	4.34	24.60	4.45	24-58	4.56	24,6	4.66
26	25.61	4.51	25.59	4.01	25.56	4-74	25.54	481
20	26.59	4.60	26.57	4.80	26.55	4-02	20.53	5.04
28	27-57	4.86	27.55	4.98	27 53	5.10	27.51	5.22
29	28 56	5.04	28.54	5.16	28.51	5.28	28.49	5-41
30	29.54	5.21	29 52	5.84	39-50	5 47	29.47	5.60
3.1	30.53	5-38	39.51	5.52	30 48	5.65	30.40	5 7%
38	31.51	5.50	31.49	5.69	31 46	5.83	31-44	5.97
33	32,50	5.73	32 47	5 87	32.45	6.01	1949	0.46
34	33.48	6.08	33.45	6.05	33-43	6.20	33-40	6.53
-	35-45	6 25	-	6.41	10000		34-39	6.74
36	36.44	6.43	35 43 36 41	6.58	35.40	6.56	35-37	6.90
38	37-43	6.60	37.39	676	37-36	6.92	37-33	7.09
39	38.41	6.77	38.38	6 94	38 35	7-11	38 32	3.27
40	39 39	6.95	39.35	7-12	39.33	7.29	39.30	9.45
41	40.38	7.62	49.35	7.30	40.31	7 47	40.28	7.65
42	41.36	7.29	41.33	7-47	41.30	7.65	41.26	7.83
63	42.15	7-47	42 31	7 65	42.28	7.84	42.25	8.02
44	43-33	7.64	44-18	7.83	43.30	8.02	43 22	S 21 S 30
45		-	-	-	44.25	_	4431	
46	45.30	7.99	45.27	8.19	49.23	8.38	45-19	8.58 8.77
48	47.27	8.34	47.23	8.54	47.20	8.75	47.15	8.95
49	48.26	8.51	48.22	8.72	48.18	8.93	48 14	0.14
50	49.24	8.68	49.10	8.90	49.16	9.11	49 12	9-11
51	50.23	8.86	50.19	9.08	50.15	9.29	50.11	9-51
52	51.31	9.03	51.17	9.25	51.13	9.48	51.09	9.70
53	52.19	9.20	52.15	9.43	52.44	9.66	52.07	9.891
54	54.16	9.38	53.14	9.61	53-10	9 84	54.03	10.07
	-	-		9.79				
56	56.15	9.72	55.11	9.96	55.06	10.31	56.00	10.45
57	57.12	10.07	57.07	(0.12	57.03	10.57		10.82
59	100000000000000000000000000000000000000	10,25		10.50	58.01	10.75	and the same of	11.00
60	59.00	10.42	59.04	10.68	59.00	10.95		11.10
_	Dep	Late	Depe	Late	II.p.	Lat.	Dogo	Logical
Dist	0.		45	The state of	30		13	Section 1
				DEGE	1			

1	. 0	-	15	-	30		4	10:
4 %	Lat.	Dep.	Late	Dep.	Lat	Dep	-	1
61	60.07	-	60.03	10.85	59.98	11 12	La	Dep.
1 64	61.00	10.77	61.01	11.03	60.96	11.30	59.93	11.56
1 63	62.04	10.94	01.119	11 21	61.95	11.48	61.89	11.75
64	63 03	IE II	01.98	11.39	62.93	11.66	62.88	11.94
65	6401	11.29	03.96	11 25	63.91	11.85	63.86	12/12
66	65.00	11.46	64.95	11.74	64,89	12,03	64.84	12,31
68	05.98	11.63	66.91	11.92	65.88	12.31	65.81	12.50
69	67.95	11 98	67.90	12.28	67.84	12.57	67.79	12.87
125	68.94	12.16	68 88	12.46	62.83	12.75	68.77	13:06
7.8	69.92	12-33	69.67	12.03	09 81	12.94	09.75	13,24
35.	73.98	12.68	70.85	12.01	79-79	13.12	70.74	5-43
1 强	71.88	12.85	72.82	12,99	71.78	13.49	71.73	13.30
75	73.86	13.02	73.80	13.39	73 74	13.67	73.68	13 90
76	74.85	13.25	74.79	13-52	74-73	13.85	74.67	14 18
77,	75.83	13.37	75 77	13 70	75.71	14.03	75.85	14.35
	76.82	13.54	76.76	13.88	76.60	14 21	76.03	14.3
79	77.80	13.72	77.74	14.06	77.68	14.40	77.61	1474
_	-	14.07	79.71					
81	19:77	14.14	80.60	14-59	79.04	14.70	80.56	15.10
81	81.74	14.41	81,68	14-77	81.61	15.13	81.54	15.48
84	82.72	14.59	82.66	14.95	82.59	1531	82,53	15 07
85	83.71	14.76	83.04	15.13	\$3.58	15.49	83,51	15.85
86	84.69	14-93	84.63	15-30	8436	15.67	84.44	16,04
87	86,66	15.28	86.60	15.48	86.53	15.85	86 46	16.23
80	87.65	15.45	87.58	15.84	87 55	16.22	87 44	15.60
100	88.63	15.03	88.50	1601	88,49	16.40	88.42	16.79
91	89.62	15.80	89.55	15.19	89 48	15.58	89.40	15.97
92	90.60	15.98	90.53	15.37	90.46	16.77	95.39	17.16
1 93	91 59	16.15	91.52	16.55	91.44	17.43	9239	17-35
94	93.57	16.50	93148	10.90	9340	17.31	93 33	17-53
yti	94-54	15.67	94-47	17.08	94.39	17.49	94-34	17 91
97	95.53	15.84	95-45	17.16	95.38	17.58	95.30	18.09
98	96.51	17.02	96.44	17-44	96.36	17 86	96.28	18.28
99	97-50	17-19	97.42	17.62	97-34	18.04	97.20	18.47
100	98,48	17.36	98.40	17.79	98.33		98.25	-
101	99.47	17-54	99.39	18.15	99.31	18.41	100.2	18.84
103	101.4	17 89	101.4	18.33	101.3	18-77	101.1	19 21
1104	102.4	18.06	101.3	18.50	102.3	18.95	102.1	(9:40
105	103 4	18.23	103.3	18/68	103-4	19:43	103.3	19.59
106	104.4	18 41	104:3	18.36	104.2	19.33	104-1	19.77
107	105.4	18.58	1053	19.04	105 2	19.50	105.1	19.96
rog	107.3	18 93	107.3	19:40	107.2	19 86	107.1	20.32
110	108 3	19.10	108.2	1957	105.2	25.05	108.1	10 52
B'EL	109 3	19.28	109.2	19:75	109.1	20.43	109.1	20/70
FXX	110.3	19.45	110.2	1993	E10.1	20.41	110.0	20189
1113	171.3	19.62	111.2	30.29	112.1	20-59	111.0	21,08
TES	113.3	19.80	113.2	20.46	113.1	20.46	1110	21,45
116	1143	20 14	119.1	20.64	FRAN	21/14	1110	21.60
227	115.2	20.32	115-1	20 81	FISO	21 32	1149	21.82
2:2	116.2	20.49	1.0.1	11.00	116,0	21.50	115.9	10,01
119	117.2	20.66	F17-1	21.18	117.0	21.69	116.9	22.30
110	118.2	20.84	118.1	1.35 Lat.	118.0	21.87	117.9	12.58
Dist	Dep.	Late	Hep	I death.	Dep.	Lat	Dep.	Let
110	1	-	4	Table Di	-	su'		St. 7

-	-		-	1	0	0/	-		
Dis	01	-	15			0/	4		
12	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep	
7	0.98	0.19	0.98	0.20	0.98	0.20	0.98	0.20	1
2	1.96	0.38	1.96	0.39	1.95	0.40	1.96	0.41	۱
3	2.94	0.57	3.92	0.78	3.92	0.60	3.92	0.61	I
5	3-93	0.95	4.90	0.98	4.90	1-00	4-90	1.01	
6.	5.89	1.14	5.88	1.17	C.88	1 20	5.87	Litt	
	6.87	1.34	6.87	1.37	6.86	1.40	6.85	1-43	
7 8	7.85	1.53	7.85	1.56	7.84	1.59	7.83	1.63	ı
9	8 83	1.72	8.83	1.76	8.82	1.79		1.23	ı
10	9.82	1.91	9.81	1.95	9.80	1.99	9.79	2.04	ı
2,1	10.80	2.10	10.79	2.15	10.78	2.19	10.77	1.24	ı
12	11.78	2.29	12.77	2.54	11.76	3,39	11.75	2.65	ı
13	13.74	2.67	13.73	2.73	13.71	2.59	13.71	1.85	ł
15	14.72	2.86	14(21)	2.93	14/70	2.99	14/69	3.05	ı
16	15.71	3.05	15.69	1.12	14.68	3-10	15.00	3.20	ı
17	16.69	3.24	16.67	3.32	16.66	3.39	10.04	3 46	ı
18	17.67	3.43	17.05	3.51	17.64	3.59	17.42	3.62	ı
19	18.65	3.63	18 63	3.74	18.62	3.79	18,60	3.87	ı
20	19.63	3.82	19.62	3.90	19.60	3.90	19:58	4-01	ı
21	21.60	4.01	20.60	4.10	20.58	4.19	20-56	4-18	
22	22.58	4.39	22,56	4.40	21.56	4.39	22.52	4.08	ı
24	23 56	4.98	23.54	4.68	23.52	4 78	23.50	4.84	ı
25	24.54	4.77	24.52	4.88	24,50	4.98	24:48	1.00	ı
28	29.52	4.95	25.50	5.07	25.48	5.18	125.46	5 19	ı
27	26 50	5.15.	26.48	5.27	26 46	5.38	26,43	5-50	ı
28.	27-49	5.34	27.46	5 46	77.44	5.58	, 27-61	5-79	ı
29	28.47	5.53	28,44	5.66	28.42	5.78	28.39	5.91	ι
30	29.45	5 72	29,42	-	29,40	5.98 B.18	29/37		B
31	30.43	6.11	30.40	6.24	30.38	6.38	30.35	8.11	ı
33	32.39	6.30	32.37	6.44	32 34	6.58	34.31	6.71	ł
34	33-38	6.49	33-35	6.63	33-32	6.78	33.29	6,92	ı
35-	34.36	6.68	34.33	6.83	34.30	6.98	34-17	7.13	ı
36	35-34	6.87	35.31	7.02	. 35.28	2.18	35-15	7-33	ı
37	36.32	7.06	36.29	7.22	36.26	7.38	36.22	7.83	ı
38	37.30	7.25	37,27	7.44	137-24	7 58	37.25	7-74	ı
39	38.28	7-44	38-25	7.61	38.22	7.78	38 15	7-54	ı
		7.82	40.21	8.00	40.18	8.17		8.95	ı
41	40.25	8.01	41 19	8.19	41.16	8.37	40.14	8,55	ı
43	42.21	8:20	42.17	8.30	42.14	8.47	42 10	8.7fi	ı
44	43.19	8.40	43.15	8.58	43.12	8,77	43 08	8.95	
45	44-17	8.59	44.14	8.78	44-10	8.97	44.06	9.16	
46	49.15	8.78	45.12	8.97	45.08	2-17	45.04	9:37	
47	46.14	8.97	46.10	9,17	46.06	9.37	46.01	9.57	
48	48.10	9.15	48.06	9.36	47.04	9-57	47:97	9-77	
\$ 50	49.08	9.54	49.04	9-75	49.00	9.97	48.95	9.98	
51.	50.06	9-73	The Real Property lies	9.95	49.98	10.17	49-93	10.39	
52		9:92	51.00	10.14	50.96	10.37	50.91	10,59	
53	52.03	10.11	51.98	10.14	51.94	10 57	51.89	10.79	
154	53.01	10.30	50.96	10.53	52.92	10.77	52.87	11.00	
550	53.99	10.49	53-94	10/73	53.90	10.97	53.85	11.20	
56	54-97	10.00	54.02	10.03	54.88	11.16	54.83.	11,40	
57	55-95	10,58	55.90	11.32	55 86	11.36	55.81	11,61	
1 59	57.92	11.26	57.87	11.51	57.82	11.76	57-76	11,81	
60	98.90	11-45	58.85	1871	58.80	11.96	58.74	12,22	
1	Dep	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Eat.	
Dis.	_	01	4	-		20	T		
=				8 DEG			_		-

1=	1 0	-		15/	1	30/	1 45/		i
1季	Lat	I Dep	Lat	Dep	Lat.	Dep	Lat.	Dep.	ì
61	59.88	11.64	59.83	11.90	59.78	12 16	59.72	12.42	1
62	60,86	11.83	60.81	12.10	60.76		60.70	12.63	ı
63	61.84	12.02	61.79	12.29	61.74	12.56	61.68	12.83	ł
1 24	62.82	12.21	62.77	12.49	63.70	12.76	62.66	13.03	ı
65	-	12.40	63.75	12.68	64.68	12,96	63.64	13.24	۱
66	65.77	12.59	64.73	13.07	65.66	13.16	64.62	13.44	1
68	66.75	12.98	66.69	13.27	66-63	13.56	66.58	13.85	ı
69	67 73	13.17	67 67	13.46	67-61	13 76	67.55	14.05	ı
70	68.71	13.36	68.66	13.66	68.59	13.96	68.53	14 25	ı
73	70 68	13.55	70.62	13.85	69.57	14 16	69.51	14.66	ı
7.5	71.06	13.93	71.60	14.24	71.53	14-35	70.49	14.87	ı
7.4	72,64	14-12	72.58	14.44	72.51	14-75	72.45	15.07	ı
75	73.62	14.31	73.56	14.63	73-49	14.95	73 43	15.27	ı
76	74.60	14 50	74-54	14.83	74.47	15.15	74.41	15.48	ı
77 78	75.59	14.69	75:53	15.02	75-45	15.35	75.39	15.68	ı
	77-55	15.07	77.48	15 41	77-41	15.75	77.34	16.00	ı
79	78.53	15.26	78.46	15.61	78.39	15.95	78.32	16 29	1
81	79.51	15 40	79:44	15.80	79.37	16.15	79.30	16.50	ŧ.
82	80,49	15.65	80.42	16.00	80.35	16.35	80.28	16.70	1
83	81.48	15.84	81.41	16.39	81.33 82.31	16.55	81.26	15.90	ı
84	83.44	16.22	83.37	16.58	83.29	16.95	83.22	17:51	ı
86	84.42	16.41	8435	16.78	84-27	17:15	84.20	17.51	ı
87	85.40	16.60	85 33	16.97	85.25	17.35	85.18	17.72	ı
88.	86.38	16 79	86.31	27-27	86.23	17-54	86.16	17.92	ı
90	87 36 88.35	16.98	87.39 88.27	17.56	87.21	17.74	87.14	18.12	ł
QI	89.33	17.38	89 25	17.75	89.17	18.14	80.00	18.53	ı
ga	90 31	17.55	90.23	17-95	90.15	18.34	90.07	18:74	Ł
93	91.29	17.75	91.21	18. 14	91,13	18.54	91.05	18.94	ŀ
94	92.27	17.94	92.19	18 34	92.11	18.74	91.03	19:14	ı
95	93-25	18.13	93-17	18.53	93.39	18.94	93:01	19.35	ı
90	94.24	18.32	94.16	18 73	94-07	19/14	95-99	19:55	ı
98	95.20	18.70	96.12	19.12	96.01	19.54	95.95	19.95	
99	97.18	18.89	97.10	1931	97.01	19.74	96.93	10.16	ı
100	1:3.46	14.08	98.08	19.51	97-99	19.94	97 90	20/36	П
101	99.14	19.46	100.0	19.70	98-97	20,14	98.88	20.57	ı
103	101.1	19 65	101.0	20.00	99-95 100-9	20 34	100.8	20.98	1
104	102.1	19 84	102.0	20.29	101-9	20.73	101.8	21.18	ı
10,	103.1	10.04	103.0	20.48	101.9	20,93	1018	21.38	8
106	104.1	20.23	104.0	10.68	103.9	21,13		21.59	
108	1050	20.42	104.9	10.87	104-9	21,33		21.79	
100	107.0	10.80	100.9	21.36	106.8	21-73		11.10	
110	108.0	20 00	1079	21.46	107.8	21.93		22.40	
211		21,18	108.0	21,60		22113		22 00	
112		21.37	109.8	21.85	109.8	22/33		22,81	
113		21.56	111.8	22.24	110.7	21 53		13.01	
115		21 94	112.8	22 44	112.7	22 93		3 42	
116	-	22.12	113.8	22.63	113.7	25.13		13.62	
117	114.9	22-32	114.7	22.83	114.6	23.33		13.53	
118		12.52	115.7	23.02	115.6	23.53		24.23	
119		22.71	117.7	23,22	115.6	23.72	CONTRACTOR OF THE PARTY OF THE	24 44	
TY	D-	Est.	Dep	Lot	Dep.	Lat.	Dep.	The	1
8	0/					01	-	31	
			-	INCO			-	-	-

78 DEGREES-

1	62	1 0	17	1	-	1 - 3	Di		57
ľ	15	Las	Dep	Lat	1 Dep	Tan.	Dep.	Lat	Dep
n	1	0.98	0.21	0.98	0.21	0.98	0.22	0.98	0.22
N	0	1.95	0.42	1.95	0.42	1.95	0.43	1.95	0.44
K	3	2.93	0.62	2.93	0.64	2 93	0.65	2.93	0.66
ı	4	3.01	0.83	3.91	085	3 91	0.87	3.90	0.88
	_ 5	4.89	1,04	4.89	1.06	-4.88	1.08	4.88	1,10
	6	5.87	1.46	5.86	1.27	5.86	1.30	5.85	1.32
	7 8	7.83	4.66	7.82	1.49	7.81	1.52	7.80	1.54
	9	8.80	1.87	3.30	1.91	8.79	1.95	8.78	1.99
В	10	9.78	2.08	9.77	2.12	9.76	3,16	9.75	2.21
R	11	10.76	2.29	10.75	1.33	10.74	2.38	10.73	1 3.43
	12	11.74	2.49	11-73	2.55	12.69	2.81	11.70	2 65
	13	13.69	2.70	13.68	2.97	13.67	3.03	13.65	3.00
п	15	14.67	3.12	14.06	3.18	14.64	3 45	14.63	3.31
	16	15.05	3.33	15.64	3.39	15,62	3.46	T5.61	3:53
	17	16 63	3.53	16,61	3.61	16.60	3.68	16.53	3.75
ı	18	17.61	3.24	17.59	3.82	17 57	3.90	17.56	3-97
ı	19	18.58	3.95	18 57	4.03	18.55	4.11	18.53	4.19
ľ	20	19.56	4.16	19 54	4 24	19.53	4-33	19.51	#
B	31	20.54	4-37	20.52	4.67	20.50	4 55	20.45	4.63
ľ	23	22.50	4.78	22,48	4.88	22.45	4.98	25.43	5.08
K	24	23.48 .	4 99	13:45	5.00	#3-43	5.19	23-41	5.30
K	25	24:45	5.20	24 43	5,10	24.41	5 41	24 38	5.52
K	26	25.43	5-41	25.41	5 52	25.38	5.63	25.30	5-74
K	27	26 41	5.61	26,39	5-73	26.36	5-84	26.33	5.96
ľ	28	27.39	5.82	28.34	6.15	27.34	6.06	27.31	6.18
ı	30	29.14	6.24	29.32	6 37	20.20	6.49	10.26	6.62
ľ	31	3-32	0.45	30,20	6.58	30.27	6.71	30.24	654
ı	32	31,30	6.69	31,27	6.79	31 24	6.93	31.21	7.00
ı	33	32.28	6 86	32 25	7.00	32.22	7.14	32.19	7.28
ı	34	33.26	7.07	33.23	7.21	33.19	7.36	33-15	7.50
ı	35	34-24	7.28	34.20	7-43	34-17	7.58	34 14	7-72
ı	36	35.21	7.48	35 18	7.64	35.15	7.79	35.11	7-95
ı	38	36.19	7.69	36.16	7.85	36.12	8.DI 8.23	37.06	1.17 1.39
ı	39	38.15	8 11	38.11	8.27	38.08	8 44	38.04	8.61
ı	40	39 13	8,32	39.00	8 49	39.05	8.66	19,01	8.83
ı	41	40.10	8.52	40.07	8.70	40.03	8.87	39.99	9.05
ı	42	41.08	8.73	41.04	8.91	41.00	9.09	40.96	9.27
1	43	42.06	8.94	4=.02	9.12	41.98	9.31	41.94	9 49
	44	43.04	9.15	43.00	9.34	42.90	9.52	43.80	9-71
1	46	-		-	9.76	44.91	9.74	44 87	10.15
1	47	44.99	9.56	44.95	9.97	45.89	10.17	45.84	10.15
1	48	46.95	9.98	46.91	10.18	46.86	10.39	46.82	10.50
1	49	47-93	10.19	47.88	10.40	47.84	10.61	47-79	10.81
1	50	4891	10.40	48.86	10.61	48.81	10.82	48.77	11.03
1	51	49.89	10 60	49.84	10.82	49.79	11.04	49.74	1 1 26
1	52	50.86	10.81	50.82	11.03	59.77	11.25	50.72	11.48
4	53	53.82	11 23	51.79	11.46	52.72	11.47	52.67	15.70
1	55	53 80	11.44	53.75	11.67	53.70	11.90	53.64	12.14
1		54.78	1164	54.72	11.88	54.67	12.12	54.62	12.36
ı	57	55.75	11.85	55.70	12.09	55.65	12.34	55 59	12.58
1	58	56.73	12.06	56.68	12.31	56.63	12.55	\$6.57	11.80
1	56 57 58 59 60	58.69	12.27	57.66	12.52	57.60	12.77	58 52	3.92
l	10	Dep.	Lar	Dep	Lat.	Dep	Lat	Dep	13-24 Late
1	五	-	-	asch	7	30		-	THE PERSON NAMED IN
	_	0	-	-	100	-	_	- 12	
				77	DEGRE	at St.			

1	- 11	,		110	1 3	at .	1 44	,
I Z	10	_	_	1	Lat	Dep.	Link	-
1	Lat.	Dep.	hate	The pa	-		-	Dep.
61	65.65	11.68	59.61	13.10	59-55	13.42	59.50	13.46
63	61.62	13.10	61.57	13.37	61.51	13.64	61.45	13.90
64	62.60	13.31	62.54	13.58	62.48	13.85	62 42	14.12
65	63.58	13.51	63.52	17.79	63.46	14.07	67.40	14:35
66	64.56	13.71	64.50	14:00	64.44	14-29	64 17	14:57
68	65.54	13.93	65.47	14-43	65.39	14.50	05.35	14.79
69	67-49	14.35	67.43	14.04	67.36	14.93	67.30	15.23
70	68.47	14-55	68.41	14 85	68:34	15.15	68.27	15.45
77	69.45	14-76	69.38	15.06	69.32	15-37	69 25	19.67
72	70-63	14-97	70.36	15.28	70.29	15 58	70.12	15.89
73	71.40	15-18	74 34 72-32	15.49	71.27	15.80	71.10	16.11
75	73.36	15-39	73.29	15.91	73.22	16.23	73.15	16.55
76	74-34	15.80	74.27	16 13	74.20	16.45	74.13	16.77
77	75.32	16.01	75.25	16 34	75.17	16.67	75.10	16.99
78	76.30	16 22	76.21	16.55	76.15	16.88	76.08	17.21
79	77.27	16.63	77.20	16.76	77/13	17.10	77.05	17 44
81		16.84		-			-	17.88
82	79.23	17.05	79-16	17.40	79.08	17 53	79.00	18.10
82	81.19	17.26	81.44	17.61	81.03	17.96	80.95	18.32
84	82.16	17.46	82.00	17.81	82.01	18.18	81.93	18.54
85	83.14	17 67	83,06	18.04	82.99	18 40	82.90	18.76
36	84.12	17.88	84 04	18.25	83.96	18.61	83.88	18.98
87	86.08	18.09	86,00	18.46	84.94	19.05	84.85	19.43
\$9	87.06	18.50	86197	18.88	86.89	19.26	86.81	19.64
90	8803	18.71	87.95	19.10	87.87	19.48	87.78	19.86
91	89:01	18 92	28.93	19.31	88 84	19 70	88.76	20.08
93	89.99	19 13	8991	19.52	89.82	19.91	69.73	20.30
91	90,97	19-34	90.88	19.73	90.80	20.13	90.71	20.52
94	91.95	19.54	94.84	10.16	92.75	20.50	92.66	20.07
96	93.90	19.96	93.81	20.37	93.72	20.78	93.63	21-19
97	94.88	20.17	94-79	20.58	9470	20.99	94 61	21.41
98	95.86	20.38	95-77	20.79	95.68	21.21	95.58	21.63
99	96.84	20.58	96.75	21.21	95.65	21.64	90.56	21.85
100	THE REAL PROPERTY.	-	98.70		98.61	21.86	98.51	
101	98.79	11.00	09.58	21.43	99.58	22.08	99.49	22.51
103	100.7	21-41	100.7	21.85	100.6	12.19	100.5	22.73
104	101.7	21.62	101,6	22.07	101.5	22.51	101.4	22.95
104	102.7	21.83	102.6	22.28	102.5	22.73	1024	23 17
106	103.7	22.04	103.6	22 49	103 5	22.94	101.4	23.39
107	104.7	22.45	104.6	22.70	104.5	23 38	104.4	13.61
100	106.6	22 66	106.5	23.13	106.4	23.59	106.3	24.06
110	107.6	22.87	107.5	23.34	107.4	13.81	107.3	24 28
111	108.6	23.08	108.5	23.55	108.4	24.02	108.3	24.50
112	109.6	23.29	100.4	23.76	109.3	24.24	109.2	24.73
113	110.5	23 49	111.4	23.98	110.3	24 67	110.2	24.94
115	112.5	23.91	1154	24.40	112.3	24.89	112.2	25.38
116	113.5	24 12	113.4	24.61	1133	25.11	113.1	25.60
117	114-4	24 33	114.3	24.82	114.2	25.32	114.1	15.81
118	1154	24-53	115.3	25.04	115.2	25.54	1151	26.28
119	116.4	24.74	110.3	25 25	116.2	25.70	115.1	26.58
130	Dep.	Lat	Dep	Lat	Dep.	Lat	Dep.	Lat
Dist	Dep-	-	45	-	30		10	
loss	- 9			DEGR			-	

110	-	_				-	1 45'			
1 8	0	_	1	1.10	31		-	1		
-	Lat	Dep	Late	Dep.	lat_	Dep.	Lat	Di-pa		
4 1	0.97	0,13	2.97	0.23	0.97	0 23	0.97	0 14		
1 3	1.95	0.45	2.92	0.60	2,92	0.47	2.01	0.41		
3 4	3.90	0.00	3.89	0.93	3.8g	0.03	3.80	3.45		
- 5	4.87	1.12	4.87	3.15	4.86	1.17	4.85	L19		
6	5.85	1.35	5.84	1.38	5.83.	1.40	5.63	1.43		
7 8	b.82	1.57	6.81	1.60	6.81	1.63	5,80	1,00		
_	7.80	1.80	7.79	1.83	7.78	1.82	7.77	1 90		
9	8.77	2.02	8.76	2.06	9.75	1.10	9-74	2.14		
1.1	9.74		10.71		10.70	2.57	10.08	2.01		
12	11.60	2.47	11.68	2.52	11.67	2.80	11.00	2.85		
13	12.07	2,92	12.65	2.98	12.64	301	12.03	3.09		
114	13.64	3 15	13.63	3.21	13.61	3.27	13 00	3-33		
45	14.62	3 37	14.60	3 44	14-99	3 10	14:57	3-57		
16	15 59	3.60	15.57	3 07	15-56	3-74	15.54	3.30		
17	16.56	3.82	16.55	3.90	16 53	3-97	17.48	4.04		
18	17.54	4-05	18.49	4.13	17.50	4.44	18-45	4.52		
20	19.49	4.50	19.47	4 58	19:45	4.67	19.43	475		
21	20.46	4.72	20.44	4.81	20.42	4.90	20.40	4.99		
1 22	21.44	4-95	21.41	5.04	21.39	5-14	21.37	6.23		
23	22.41	5.17	22.39	5.27	22.36	5.37	12.34	5-47		
24	23.38	5-40	23.36	5.50	23.34	5.60	33.31	5-79		
25	24.36	5.62	24-33	5.73	24.31	19.84	24,28	5.94		
26	35.53	5.85	25.31	5.96	26.25	6.30	25.25	6.15		
28	26.31	6.30	27.25	6.42	27.13	6.54	27.20	6.05		
20	18.16	6 52	28.23	6.65	28.20	6.77	18.17	6.89		
30	29.23	6.75	29.20	6.88	29-17	7.00	29.14	7-13		
31	30.21	6.97	30.17	7.11	39-14	7.24	30.11	7-37		
32	31.18	7,10	31:15	7 33	31.12	7.47	31.08	7,61		
33	32.45	7.42	32,11	7-56	32.09	7 70	38.05	7.84		
34	33-13	7.65	33.09	8.01	33.06	7.94 B.17	33.03	8.52		
36	35.08	8.10	35.04	8.25	35.01	8.40	34-97	1.56		
37	36.05	8.32	30.02	8.48	15.98	8.64	35.94	8.79		
38	37.03	8.55	36.99	8.71	36.95	8.87	36-VI	9,03		
39	38.00	8.77	37,96	8.94	37,48	9.10	37.88	9-27		
40	38.92	9.00	18.94	9-17	38.89	9-34	38.85	y.gr		
41	39.95	9 22	39.91	9.40	39.87	9.57	3y.83	9.75		
43	40,92	9.45	40.88	9.63	40,84	9.80	40.80	9.98		
43	41.90	9.67	41.83	10.08	41-81	10.04	41.77	10.45		
45	43.85	10 12	43.80	10.31	43-76	10.51	43.78	10.70		
46	44 82	10 35	44.78	10.54	44.73	10.74	44.68	10.03		
47	45.80	10.57	45.75	10.77	45.70	10.97	45.65	TELE		
48	46.77	10.80	46.72	11.00	46.67	11.21	40.62	18-41		
49	47.74	11.02	47.70	11.23	47.65	17-44	47.66	11.65		
50	-	11.25	48.67	11.40	48.62	11.07	48.57	11,88		
51	50.67	11.47	50.61	11.92	49-59	11.91	44.54	12.36		
53	51.64	11.92	51.59	12.15	50.56	12.37	51.48	12.00		
54	51.62	12.15	52,56	12.38	52.51	12.61	52:45	12.84		
35	53.59	12.37	53-54	12.61	53.48	12,84	53.42	15.07		
50	54-56	12.60	54-51	12.84	54.45	13.07	\$4.40	13.51		
57	55.54	12.82	55.48	13.06	55.43	13.31	55:37	13-55		
1 58	56.51	13.05	56.46	13.29	50 40	13-54	50 34	13.79		
1 59	57-49	13:50	57.43	13.75	57.37	13-77	57.51	14.02		
100	. Dep.	Lat.	Up	Late	12000	Lut	Dep.	Late		
100	0	-	4	_	30			5'		
-	-		- 75	TIPET		-	,	-		
	76 DEGREES									

10	0		-	,	3	)*	45	-	ľ
12	Nati	Dep	Rest .	Dep.	Lat	Dep.	Lat	No.	ı
61	59 44	13.72	59.38	13 98	\$9:31	14.24	59.25	14-50	ı
63	60.41	13 95	60.35	14.21	60.29	14-47	60.22	14.74	ı
64	61.39	14-40	61.13	14-57	61 26	14 71	61.17	14 97	ı
65	63.33	14.61	63.27	14.0	63.20	15.17	63.14	15-45	ı
66	64.31	14.85	64.14	15.13	64.18	1541	64.11	15.64	ı
67	65 28	14.07	65.22	15.36	65.15	15.64	6,08	15 93	ı
69	65.26	15.52	65.19	15.59	67.09	15.87	67.01	16.15	ı
70	68.21	15-75	68.14	16.04	6 .07	16.14	67.99	15.114	ı
75	69.18	15-97	69,11	16.37	69.04	10.57	68.97	16 85	ı
175	70/15	16.10	70'08	16.50	70,01	15.81	69.94	17-55	ı
73	71.13	16.41	71.06	16 95	70.98	17.88	70.91	17-35	ı
75	73.08	16 87	73.00	17.19	72.93	17-51	72.85	17.50 17.61	ı
76	74.05	17.10	73.98	17:42	73.40	17.74	73.82	18 06-	ı
77	75.03	17.32	7495	17.65	74.87	17-98	74.79	18.30	
78	76,98	17-55	75,92	17.58	75.84	18.21	75.76	18.54	
80	77.95	17 77	76.90	18 34	77-79	18.68	77-71	19.01	
81	78.92	78.23	78.84	18.57	78.76	18.91	78.68	14.25	
82	79.90	18.45	79.82	18-79	79.75	19.14	79.65	19.49	ı
83.	80.87	18.07	80.79	19.02	81.68	19.38	80.62	19.73	ı
85	82.82	18.90	81.76	19.48	82.65	19.84	82.56	19.97	ı
86	83,80	19-35	83.71	19.71	83.62	20.03	83.54	20,44	ı
87	84.77	19.57	84.68	19.94	84.60	#0.3F	84.51	20.68	ı
88	85.74	19.80	85.66	20.17	85.57	20.54	85.48	20,92	ı
90	86.12	20.02	86-63	20.63	86.54	20.78	80.45	21.30	ı
91	83.67	30.47	88 58	20.86	88.49	11.24	88.39	21.61	B
92	89.64	20.70	89.55	21.09	89.45	21.48	89.35	21.87	ı
93	90.01	10.92	90.51	21.32	90.43	21.71	90133	22.10	ı
94	91.59	21.15	91,50	21.54	91.40	22.18	91.31	22.58	ı
96	92.57	21.37	92.47	23.00	93.35	22-41	-	22.82	ı
97	93.54	21.81	93-44	22.23	94.32	22.64	93.25	23.06	П
98	95.49	22.05	95-39	22.46	95.29	22.88	95.19	23.29	ı
100	96.46	22.27	96.36	22.69	96.26	23.11	95.16	23.53	ı
101	97,44	22.50	97-34	22.92	97.24	23-34	97,13	23.77	ı
102	98.41	22.72	98.31	23.15	99.18	23.58	98.11	24.14	ı
103	100.4	23.17	100.3	23.61	100.2	24.04	100.0	24.48	ı
104	101.3	23.40	101-2	23.84	101 1	24-28	101.0	24.72	ı
105	102.3	23.52	102.2	24.07	102.1	34.51	102.0	24.96	
107	1013	23.84	103.2	24.51	104.0	24.75	103.0	25.19	1
108	105.2	24.29	105 1	24.75	105.0	25.24	104.9	25-67	1
109	106.2	24 52	105.1	24.98	1060	25.45	105.9	25.91	
110	107.1	24.74	157.1	25 21	1070	25.68	106.8	26,13	1
1110	108.2	24.97	1080	25.44	107.9	25.91	107.8	26.52	1
1113	109-1	25.42	110.0	15.90	109 9	26 38	109 8	26.86	1
514	111.1	25.64	0.111	26.13	110.9	26.61	110.7	27.10	1
115	TIE.T	25.87	111.9	16,16	111.8	26.85	177.7	27.33	1
115	11310	26.09	112.9	26.59	112.8	27.08	112.7	27.57	
118	114.0	26.32	113.9	26.82	143.8	27.55	113.6	28.05	1
119	116.0	26.77	115.8	27 27	115.7	27.78	115.6	28.28	1
320	THE REAL PROPERTY.	26.99	116.8	17.50	116.4	28.01	116.6	28 52	1
1 #	1 Dep.	Ent	Dep	Lat	Dep	Links	Dep	Late	1
15	Contract of	0.	1 4	5"	1	101	1 -1	3/	

1	-	0		1 15	,	11 200	100	1 4	2.0
1	ist.	Lat	Dep	Lat-	I Bep.	Lat.	Dep.	Late	Dep
ı	-	0.97	0.24	0.07	0.15	0.97	0.35	0.47	3.25
ľ	2	1,94	6.48	1.94	0.49	1.94	0.50	1.93	0.51
ı	3	2.91	0.73	2,91	0.74	1.90	0.75	=.90	0.76
ı	4.	3.88	0.97	4.85	1.11	3.87	1.25	3.87	F-07
ı	6	6.82	1.45	4.82	1 48	5.81	1.50	5.80	6-53
ı		6.79	1.69	6.78	1.72	6.78	1.75	677	1.78
ı	7.8	7.70	1.94	7.75	1.97	7.75	2.00	7.74	2.04
ı	9	9.70	2.18	9 69	2.46	9.68	2.25	8.70	2.20
ı	10	10.67	2.42	10.66	3.71	10.05	#75	9.67	2.55
ľ	11	11.64	2.92	1663	2.95	11.62	3.00	11.00	2.06
ı	13	12 61	3.15	12 60	1.20	12 59	3.25	12.57	3-31
۱	14	13.58	3.39	13-57	3.45	13.55	3.51	13-54	3.56 3.82
ı	15	14.55	3.63	14.54	3.94	14.52	4.01	14-51	-
ı	16	16.50	3.87	15.51	4-18	15.49	4.26	15:47	4-33
ı	18	17.47	435	17.45	4-43	17 43	4.51	17:41	4.58
ı	19	28.44	4.60	18.42	4.08	18.39	4.76 5.01	18 37	4 84
ı	20	20.38	5 08	19.38	5-17	19.36	5.20	19.34	5,09
ı	21	21.35	5.32	20,35	5.41	21 30	5.54	21.28	5-35
ı	23	22,32	5.56	22.29	5 66	22.27	5-76	22 24	1.86
۱	24	33.29	5.81	23.26	5-91	23.24	6.01	23.21	6.11
ı	35	24.26	6.05	24.23	6.40	74 20	6.51	24.18	6.62
ı	26	25.23	6.59	26.17	6.65	25,17	6.76	25.14	6.87
ı	28	27-17	6.77	27.64	6.89	27.11	7.01	37.08	7:13
۱	29	28.14	7.02	58.11	7 14	28.08	7.26	28.04	7.48
ı	30	19.11	7-26	29.08	7.38	29.04	7.51	29.01	7.64
ı	31	30.08	7-50	30.05	7.63	30.08	7.76	30.95	7.8y 8.15
ı	33	32,02	7.98	31.98	8.12	31.95	8.25	31.91	8.40
ı	34	32,99	8.23	32.95	8.37	32,92	8 51	12.88	8.66
ı	35	33.96	8.47	33.92	8.62	33.89	8.76	33.85	8.91
ı	36	34.93	8.71	34.89	9.11	34-85	9.01	34.81	9-17
ı	37	36.87	9.19	36.83	9.35	36.79	9.51	36.75	9.07
ı	39	37.84	9-43	37.80	9.60	37-76	9.76	37-71	9 93
ı	40	38.81	9.68	38.77	9.85	38.73	10.01	18.68	10:18
ı	41	39.78	9 94	39.74	10.09	39.69	10.17	40.61	ID:44
ı	43	41 72	10.40	41.68	10.58	41.63	10.77	41 58	10.95
ı	44	42.69	10.64	42 65	10.83	12.60	11.02	42.55	17.20
i	45	43,66	10 89	43 62	11.08	43.57	11.27	43.50	11:46
I	45	44-63	11.37	44.58	11.57	44-53	11.52	44.48	11.97
1	48	46.52	11.61	46.52	11.82	46 47	1202	46.42	11.22
1	49	47.54	rt.85	47.49	12 06	47-44	12.27	47.39	12.48
H	50	48.51	12 10	48.40	12 21	48,41	£150	48.35	學學
ı	51	50.46	12.34	49.43	12.55	49.38	13 01	50 29	13.98
1	53	51.43	12.82	51.37	13 05	51.31	13.27	54-25	13 49
1	54.	53.40	13.06	52.34	13.19	52.28	13-52	52.22	13-75 14:00
F	55	-	13:31	53:11	13:54	55.25	13:77	53-19	
I	56 57 58	59-31	13.55	59.25	14.03	54.22	14.27	54-15	14/52
1	58	56.28	14.03	56.22	14.28	56.15	14.52	56.09	14.77
I	59	57.25	14.27	57.18	14-52	57 13	14.97	57.00	F5.02
F		158.20	14.52	58 15	14177	-	16.02	58.01	15:00
I	list.	Dep	Late	Dep.	lat	Dep	Lat	Dep.	Lat.
à		- 62	-	074	TWCD	30	-	Li	

Table   Dep.   Lat.   Dep.						KEr.S.			
61		0.		15	<u>.                                     </u>	l3	30'	4.	5'
63 65.16 15.00 66.00 15.46 60.03 15.53 59.96 15.79 66.96 16.10 15.48 61.00 15.48 61.00 15.48 61.00 15.48 61.00 15.48 61.00 15.91 60.20 16.02 16.02 16.02 16.04 65.91 16.07 16.00 62.93 16.07 62.91 16.07 63.90 16.02 64.93 16.07 62.01 16.21 61.04 16.49 64.93 16.73 64.70 17.06 66 66.95 16.45 66.88 16.98 66.80 17.83 60.73 17.13 67.60 17.11 68.89 17.42 69.78 17.74 69.71 18.03 69.78 17.74 69.71 18.03 69.78 17.74 69.71 18.03 69.63 16.57 69.70 17.74 18.03 70.75 17.74 18.03 70.75 17.74 18.03 73.75 17.75 69.71 18.03 69.63 16.55 17.74 71.75 17.75	٣	Lat	Dep.	Lite	Dep	lat_	Ο р.	Lut	; D ,
64 61.01   15.48   61.06   15.51   60.99   15.77   60.62   16.04   61.01   15.48   61.03   15.75   61.96   16.27   61.89   16.29   65.01   15.27   63.00   16.00   62.93   16.27   62.86   16.55   65.98   16.45   63.91   16.74   65.83   17.03   65.76   17.01   68.89   17.18   68.82   17.18   68.82   17.18   68.82   17.18   68.82   17.18   68.82   17.18   68.82   17.18   68.82   17.18   68.83   17.18   66.96   66.82   17.18   68.83   17.62   69.95   17.10   69.86   17.18   69.									
66									
65  61.07  15.72  63.00  16.00  62.93  16.27  62.86  16.55  66.64  1.04  16.21  63.96  16.35  63.83  16.30  67.66  64.94  16.44  16.49  64.97  16.75  63.83  16.30  68.66  65.96  16.43  16.44  16.49  64.97  16.75  67.79  17.03  16.57  67.79  17.03  16.59  16.93  67.85  17.03  16.75  67.79  17.17  68.89  17.18  68.82  17.48  68.74  17.78  68.66  17.18  69.86  17.42  69.78  17.72  67.77  17.53  67.69  17.37  17.17  68.89  17.42  69.78  17.72  69.71  18.23  70.59  17.62  18.23  70.59  18.23  17.65  17.23  69.75  17.62  17.77  18.14  71.90  77.75  77.75  77.75  77.75  18.14  71.69  18.31  77.64  18.53  71.59  18.24  72.59  18.24  72.59  18.25  72.59  18.24  72.59  18.25  72.59  18.24  72.59  18.25  72.59  19.25  12.59  19.25  12.59  19.25  12.59			1	1 .					
66 64.34 15.97 63.97 16.25 63.90 10.55 63.83 16.30 67 65.91 16.21 64.94 16.49 64.97 16.75 64.79 17.06 68 65.98 16.45 16.94 65.93 17.03 65.96 17.38 60.53 17.35 65.96 17.37 17.06 65.93 17.03 65.93 17.03 65.96 17.38 60.73 17.37 65.92 16.93 67.85 17.32 67.77 17.53 67.60 17.37 17.60 67.92 16.93 67.85 17.38 68.77 17.53 67.60 17.37 17.80 17.37 69.71 18.23 71.66 70.77 17.73 18.23 17.66 70.77 17.73 18.23 71.54 18.23 71.54 18.23 71.57 18.24 72.59 18.24 72.50 18.24 72.57 18.25 72.77 18.39 73.66 18.71 71.53 19.03 17.50 72.77 18.39 73.66 18.71 71.53 19.03 17.50 19.34 72.57 18.39 73.66 18.71 71.53 19.03 17.50 19.34 72.57 18.39 73.66 18.71 71.54 18.53 71.59 19.34 72.59 19.35 72.77 18.87 72.50 19.20 72.51 18.23 72.50 19.35 72.50 19.									
68 65.98 16.21 64.34 16.49 64.97 16.73 16.73 17.36 68.96 16.69 66.88 16.98 66.80 17.38 60.73 17.37 67.92 16.93 67.85 17.33 67.77 17.53 67.61 17.32 72.60 85.99 17.42 68.89 17.42 68.78 17.74 69.71 18.03 69.63 16.57 69.78 17.74 69.71 18.03 69.63 16.57 77 77.77 18.14 72.69 18.32 71.60 69.63 17.42 69.78 17.74 69.71 18.33 69.63 16.57 77 77.77 18.14 72.69 18.46 72.61 18.23 71.50 18.24 72.77 18.14 72.69 18.46 72.61 18.28 72.59 18.5, 7.74 71.80 17.90 77.72 18.13 71.50 18.24 72.69 18.30 17.90 77.77 18.14 72.69 18.46 72.61 18.28 72.59 18.5, 7.75 72.77 18.14 72.69 18.46 72.61 18.28 72.53 19.10 77.77 74.71 18.03 74.63 18.95 74.55 19.28 74.40 19.60 77.74 18.03 74.63 18.95 74.55 19.28 74.40 19.60 77.75 19.45 72.51 19.20 75.52 19.33 74.53 19.50 19.50 77.62 19.15 77.51 19.60 75.51 19.28 74.50 19.50 74.51 19.60 75.51 19.28 74.50 19.50 77.62 19.15 77.51 19.60 77.62 19.35 74.63 18.95 74.55 19.28 74.50 19.50 77.62 19.35 77.62		-	15.07	62.07			16.55	62.82	
68 65,98 16.45 66.88 16.98 66.80 17.28 60.73 17.03 65,76 17.1 66.86 16.45 66.88 16.98 66.80 17.28 60.73 17.57 67.92 16.33 67.87 17.23 67.77 17.53 67.60 17.21 68.89 17.28 68.80 17.28 68.80 17.28 68.80 17.28 69.80 17.28 69.80 17.28 69.80 17.28 69.80 17.28 69.80 17.28 69.80 17.28 69.80 17.28 69.80 17.28 69.80 17.28 69.70 18.28 72.77 18.13 17.66 70.75 17.97 70.67 18.28 72.59 18.5, 72.77 18.13 72.69 18.21 71.64 18.53 72.59 18.5, 72.77 18.13 72.69 18.21 71.64 18.53 72.59 18.5, 72.77 18.13 72.69 18.26 72.61 18.78 72.59 18.5, 72.77 18.13 72.69 18.26 72.61 18.78 72.59 18.5, 72.77 18.13 72.69 18.20 73.50 19.2									
70   67-92   16-93   67-85   17-23   67-77   17-53   67-69   17-42     71   68-86   17-12   68-82   17-12   68-76   17-77   68-86   17-12   69-78   17-74   71-69   18-03   69-63   18-37   72-77   18-13   72-69   18-23   71-64   71-72   72-77   18-13   72-69   18-23   71-64   18-73   71-69   71-69				45.91				65.76	
71 68.89 17.18 68.82 17.48 68 74 17.78 68.06 18.7. 73 70 83 17.66 70.75 17.24 69.78 17.74 71.80 17.40 70.75 17.27 71.80 17.40 71.72 18.22 71.64 18.53 71.50 18.14 72.69 18.46 72.61 18.78 72.59 18.14 72.69 18.46 72.61 18.78 72.59 18.14 72.69 18.46 72.61 18.78 72.59 18.14 72.69 18.46 72.61 18.78 72.59 18.14 72.69 18.46 72.61 18.78 72.59 19.17 74.71 18.03 74.63 18.95 74.55 19.28 74.40 19.05 78 76.65 19.11 76.57 19.45 75.88 19.78 74.40 19.05 79 76.65 19.11 76.57 19.45 76.48 19.78 76.40 20.18 80 77.62 19.15 77.54 19.69 77.45 20.03 77.62 20.37 88 78.93 20.08 80.45 20.45 80.36 20.78 80.53 20.08 80.45 20.48 20.32 81.41 20.68 81.32 20.28 78.33 2.62 82.89 20.56 82.88 20.56 82.88 20.53 82.88 20.94 82.38 81.42 20.28 78.33 2.139 85.28 82.29 20.8 20.8 20.8 20.8 20.8 20.8 20.8 20.8									
72	_								
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100   97.03   24.19   96.92   24.62   96.81   25.04   96.70   25.46     101   98.00   24.43   97.89   24.80   97.78   25.29   97.67   27.71     102   98.97   24.68   98.86   25.11   98.75   25.54   98.64   25.97     103   99.94   24.92   98.83   25.35   99.72   25.79   99.61   26.22     104   100.9   25.16   100.8   25.85   100.7   26.04   100.6   26.48     105   101.9   27.40   101.8   27.85   101.7   26.19   101.5   26.73     106   102.9   27.64   102.7   26.09   202.6   26.54   102.5   26.99     107   103.8   25.89   103.7   26.34   103.6   26.79   103.5   27.24     108   104.8   26.13   104.7   26.86   104.6   27.04   104.4   27.50     109   105.8   26.37   105.6   26.83   105.5   27.29   105.4   27.75     110   106.7   26.61   106.6   27.08   106.5   27.54   106.4   28.01     111   107.7   26.85   107.6   27.32   107.5   27.79   107.3   24.26     112   108.7   27.10   108.6   27.57   108.4   28.04   108.3   26.52     113   109.6   27.34   109.5   27.82   109.4   28.29   109.3   28.77     114   110.6   27.58   110.5   28.06   110.4   28.54   110.2   29.02     115   112.6   28.36   112.4   28.55   112.3   29.04   112.2   29.28     116   112.6   28.56   112.4   28.55   113.3   29.29   113.1   29.9     118   114.5   28.55   114.4   29.05   114.2   29.54   114.1   30.04     119   115.5   28.79   115.3   29.94   115.1   3.30     120   116.4   29.03   116.3   29.94   115.1   3.30     120   116.4   29.03   116.3   29.94   116.2   29.55   116.0   30.95     120   120   120   120   120   120   120   120   120     120   120   120   120   120   120   120   120   120     120   120   120   120   120   120   120   120   120     120   120   120   120   120   120   120   120   120     120   120   120   120   120   120   120   120   120     120   120   120   120   120   120   120   120   120   120     120   120   120   120   120   120   120   120   120   120   120     120   1									
101   98.00   24.43   97.89   24.86   97.78   25.29   97.67   27.71     102   98.97   24.68   98.86   25.11   98.75   25.54   98.64   25.97     103   99.94   24.92   99.83   25.35   99.72   25.79   99.61   26.22     104   100.9   25.16   100.8   25.65   100.7   16.04   100.6   26.81     101   9   24.40   101.8   25.85   101.7   26.89   101.5   26.73     106   102.9   25.64   102.7   26.99   402.6   26.54   102.5   26.99     107   103.8   25.89   103.7   26.34   103.6   26.54   102.5   26.99     108   104.8   26.13   104.7   26.58   104.6   27.04   104.4   27.50     109   105.8   26.37   105.6   26.83   105.5   27.29   105.4   27.75     110   106.7   26.85   106.6   27.08   106.5   27.54   106.4   28.01     111   107.7   26.85   107.6   27.32   107.5   27.59   105.4   27.75     112   108.7   27.10   108.6   27.73   107.5   27.79   107.3   23.25     113   109.0   27.34   109.5   27.82   109.4   28.29   109.3   28.77     114   110.6   27.58   110.5   28.06   110.4   28.54   110.2   29.02     115   116.6   27.82   111.5   28.31   111.3   28.79   111.2   29.28     116   112.6   28.90   112.4   28.55   112.3   29.04   112.2   29.53     118   114.5   28.55   114.4   29.05   114.2   29.54   114.1   30.04     119   115.5   28.79   115.3   29.29   115.1   3.30     120   116.4   29.03   116.3   29.54   116.2   29.95   116.0   32.55     20   106.4   29.03   116.3   29.54   116.2   29.95   116.0   32.55     20   106.4   29.03   116.3   29.54   116.2   29.95   116.0   32.55     20   106.4   29.03   116.3   29.54   116.2   29.95   116.0   32.55     20   106.4   29.03   116.3   29.54   116.2   29.95   116.0   32.55     20   106.4   29.03   116.3   29.54   116.2   29.95   116.0   32.55     20   106.4   29.05   116.4   29.05   116.2   29.95   116.0   32.55     20   20   20   20   20   20   20		-							
102   98.97   24.68   98.86   25.11   98.75   25.54   99.64   25.97     103   99.94   24.92   99.83   25.35   99.72   25.79   99.61   26.22     104   100.9   25.16   100.8   25.65   100.7   16.04   100.6   26.73     106   102.9   25.64   102.7   26.09   402.6   26.54   102.5   26.99     107   103.8   25.89   103.7   26.34   103.6   26.79   103.5   27.24     108   104.8   26.13   104.7   26.58   104.6   27.04   104.4   27.50     109   105.8   26.37   105.6   26.83   105.5   27.29   105.4   27.75     110   106.7   26.61   106.6   27.08   106.5   27.54   106.4   28.01     111   107.7   26.85   107.6   27.32   107.5   27.79   105.4   28.01     112   108.7   27.10   108.6   27.57   108.4   28.04   108.3   26.32     113   109.0   27.34   109.5   27.82   109.4   28.29   109.3   28.77     114   110.6   27.58   110.5   28.06   110.4   28.54   110.2   29.02     115   116.6   27.82   111.5   28.31   111.3   28.79   111.2   29.28     116   112.6   28.96   112.4   28.55   112.3   29.04   112.2   29.53     118   114.5   28.55   114.4   29.05   114.2   29.54   114.1   30.04     119   115.5   28.79   115.3   29.29   115.1   3.30     120   116.4   29.03   116.3   29.54   116.2   29.95   116.0   32.55     130   130.0   115.1   3.00     140   110.0   110.0   110.0   110.0     110	;							·	-
103 99.94 24.92 99.83 25.35 99.72 25.79 99.61 26.22 10.4 10.9 25.16 100.8 25.65 100.7 26.04 10.5 26.48 10.5 101.9 25.64 102.9 25.65 101.7 26.29 101.5 26.73 10.6 102.9 25.64 102.7 26.09 302.6 26.54 102.5 26.73 10.7 10.8 25.89 103.7 26.39 103.6 26.79 103.8 25.89 103.7 26.38 104.6 27.04 104.4 27.50 109 105.8 26.37 105.6 26.83 105.5 27.29 105.4 27.75 110 10.6.7 26.61 10.6.6 27.08 105.5 27.29 105.4 27.75 110 10.7 26.85 107.6 27.32 107.5 27.59 107.3 21.25 108.7 27.10 108.6 27.58 109.4 28.04 108.3 28.51 111 107.7 26.85 107.6 27.82 109.4 28.29 109.3 28.77 114 110.6 27.58 110.5 28.06 110.4 28.54 110.2 29.02 111.6 27.82 111.5 28.31 111.3 28.79 111.2 29.28 116 112.0 28.05 112.4 28.55 112.3 29.04 112.2 29.53 113 113 129.9 113.5 28.30 113.4 28.80 113.3 29.29 113.1 29.9 113.1 129.9 118 114.5 28.55 114.4 29.05 114.2 29.54 114.1 30.04 119 115.5 28.79 115.3 29.29 115.1 3.30 116.4 29.03 116.4 29.03 116.2 29.03 115.1 3.30 116.4 29.03 116.4 29.03 116.5 29.03 115.1 3.30 116.4 29.03 116.4 29.05 114.2 29.55 114.2 29.55 114.2 29.55 116.0 32.55 116.0 32.55 116.0 32.55 116.0 32.55 116.0 32.55 116.0 32.55 116.0 30.7 13.7 13.7 13.7 13.7 13.7 13.7 13.7 13									
101.9		99.94				99.72	25.79		
106									
103.8   25 29   103.7   26.34   103.6   26.79   103.5   27.24   108   104.8   26.13   104.7   26.58   104.6   27.04   104.4   27.75   110   105.7   26.61   106.6   27.08   105.5   27.29   105.4   27.75   110   106.7   26.65   107.6   27.32   107.5   27.79   107.3   24.26   112   108.7   27.10   108.6   27.57   108.4   28.04   108.3   26.52   113   109.6   27.34   109.5   27.82   109.4   28.29   109.3   28.77   114   110.6   27.58   110.5   28.06   110.4   28.54   110.2   29.02   111.6   27.82   111.5   28.31   111.3   28.79   111.2   29.28   117.5   28.30   113.3   29.04   112.2   29.53   113.5   28.30   113.3   29.24   113.1   29.95   114.5   28.55   114.5   28.55   114.5   28.55   114.5   28.55   114.5   29.05   114.2   29.53   115.1   30.04   119   115.5   28.79   115.3   29.29   115.1   29.30   115.1   3.30   110.4   29.05   114.2   29.55   114.2   29.55   114.2   29.55   114.3   29.55   114.4   29.05   114.2   29.55   115.3   29.39   115.1   3.30   115.1   3.3									·
108			25.04						
109									
111   107.7   26.85   107.6   27.32   107.5   27.79   107.3   24.26     112   108.7   27.10   108.6   27.57   108.4   28.04   108.3   26.52     113   109.6   27.34   109.5   27.82   109.4   28.29   109.3   28.77     114   110.6   27.58   110.5   28.06   110.4   28.54   110.2   29.02     115   111.6   27.82   111.5   28.31   111.3   28.79   111.2   29.28     116   112.6   28.06   112.4   28.55   112.3   29.04   112.2   29.53     117   113.5   28.30   113.4   28.50   113.3   29.29   113.1   29.53     118   114.5   28.55   114.4   29.05   114.2   29.54   114.1   30.04     119   115.5   28.79   115.3   29.29   115.7   29.30   115.1   3.30     120   116.4   29.03   116.3   29.54   116.2   30.75   116.0   30.55     Jun.   Jun.   Jun.   Lat.   Dep.   Lat.   Dep.   L.	109		26.37	105.6	26 83	105.5		105.4	27.75
112   108.7   27.10   108.6   27.57   108.4   28.04   108.3   26.52     113   109.6   27.34   109.5   27.82   109.4   28.29   109.3   28.77     114   110.6   27.58   110.5   28.06   110.4   28.54   110.2   29.02     116   112.6   28.06   112.4   28.55   112.3   29.04   112.2   29.53     117   113.5   28.30   113.4   28.50   113.3   29.29   113.1   29.51     118   114.5   28.55   114.4   29.05   114.2   29.52   114.1   30.04     119   115.5   28.79   115.3   29.29   115.7   29.30   115.1   3.30     120   116.4   29.03   116.3   29.54   116.2   30.75   116.0   32.55     30   30'   30'   30'   30'   30'     30   30'   30'   30'   30'   30'   30'   30'     30   30'	110	106.7	26.61	106.6	27.08	106.5	27.54	106.4	28.31
113   109.0   27.34   109.5   27.82   109.4   28.29   109.3   28.77     114   110.6   27.58   110.5   28.06   110.4   28.54   110.2   29.02     115   111.6   27.82   111.5   28.31   111.3   28.79   111.2   29.28     116   112.6   28.06   112.4   28.55   112.3   29.04   112.2   29.53     117   213.5   28.30   113.4   28.80   113.3   29.29   113.1   129   9     118   114.5   28.55   114.4   29.05   114.2   29.54   114.1   30.04     119   115.5   28.79   115.3   29.29   113.1   29.90   115.1   3.30     120   116.4   29.03   116.3   29.54   116.2   30.05   116.0   32.55     27   30'   30'   30'   13'     28.77   30'   30'   30'   30'   30'   30'     28.77   30'   30									
114 110.6 27.58 110.5 28.06 110.4 28.54 110.2 29.02 115 111.6 27.82 111.5 28.31 111.3 28.79 111.2 29.28 116 112.4 28.55 112.3 29.04 112.2 29.53 117 113.5 28.30 113.4 28.30 113.3 29.04 112.2 29.53 118 114.5 28.55 114.4 29.05 114.2 29.54 114.1 30.04 119 115.5 28.79 115.3 29.29 113.7 29.90 115.1 30.04 119 115.5 28.79 115.3 29.29 113.7 29.90 115.1 30.04 120 116.4 29.03 116.3 29.54 116.2 29.90 115.1 30.30 120 116.4 29.03 116.3 29.54 116.2 29.90 115.1 30.30 120 116.4 29.03 116.3 29.54 116.2 30.05 116.0 32.55 11	. ,								
116   112.6   28.06   112.4   25.55   112.3   29.04   112.2   29.53   117   213.5   28.30   113.4   28.50   113.3   29.29   113.1   129   59   114.5   28.55   114.4   29.05   114.2   29.54   114.1   30.04   119   115.5   28.79   115.3   20.29   115.1   29.50   115.1									
116 112.6 28.06 112.4 25.55 112.3 29.04 112.2 29.53 117 113.5 28.30 113.4 28.30 113.3 29.29 113.1 '49 '9 118 114.5 28.55 114.4 29.05 114.2 29.54 114.1 30.04 119 115.5 28.79 115.3 29.29 113.2 29.30 115.1 3.30 120 116.4 29.03 116.3 29.54 116.2 30.05 116.0 30.5				-					
117   113.5   28.30   113.4   28.50   113.3   29.29   113.1   29.9   114.5   28.55   114.4   29.05   114.2   29.54   114.1   30.04   119   115.5   28.79   115.3   29.29   113.1   29.30   115.1   3.30   120   116.4   29.03   116.3   29.54   116.2   30.75   116.0   30.55									
119			28.30			_			
120   116.4   29.03   116.3   29.54   116.2   20.25   116.0   32.55   12.0									-
Dep.   Lat.   Dep.   Lat.   Dep.   Lat.   Dep.   L.							-		
13' 30' 13'									-
	ist			1 <del></del>					
75 DEGREES.	<u> </u>	U						1.	J.

-	0	-	1 15	1	30		145	
Dist.	Lat.	Dep.	Lat	Dep	Lat	Dep.	Lat	Dep.
1	0.97	0.26	0.96	0.26	0.96	0,27	0.96	0.87
1 3.	1.93	0.52	1.93	0.53	1.93	0.53	1.92	0.54
3 4	3.86	1.04	2.89	1.05	3.85	0.80	3.85	1,09
5	4.83	1.29	4.82	1.32	4.82	1.34	4.81	136
6	5.80	1.55	5-79	1.58	5.78	1.00	5.77	1,63.
1 3	6 76	1.81	6.75	184	6.75	1.87	6,74	1.90
S	7-73 8.6g	2,07	8.68	2.10	8.67	2.41	8.66	2.44
10	9.66	2.59	9.65	2.63	9.64	2.67	9.62	2.71
11	10.63	2.85	10.61	2.89	10,60	2.94	10.59	2.99
12	11.59	3.11	11.58	3.16	11.56	3.21	11.55	3.26
13	12.50	3.36	12.54	3.42	12.53	3-47	13-47	3.51
15	14.49	3.88	14-47	3.95	14-45	401	14-14	4.07
16	15.45	4.14	15.44	4.21	15 42	4.28	15.40	4-34
17	16.42	4.40	16.40	4-47	16.38	4.54	16.36	4.61
18	17-39	4.66	17.37	5:00	17.35	5.08	18.29	5.16
20	19.32	5.18	19.30	5.26	19.27	5-34	19.25	5-43
21	20.28	5-44	20.20	5.52	20.24	5.61	20-21	5.70
22	21.25	5.69	21.23	5-79	21.20	5.88	21.17	5.97
24	23 18	6,21	22.19	6.31	23.13	6.41	23.10	651
25	24-15	6.47	34.12	6.58	24.09	6.68	24.06	6.79
26	25.11	6.73	25.08	6.84	25.05	6.95	25.02	7,00
27	27.05	7.25	26.05	7.10	26.02	7-22	25.99	7.60
2.9	28.01	7.51	27.98	7.63	27.95	7.75	27.91	7.87
30	28 98	7.76	28.94	7 89	28.91	8.02	28.87	8.14
31	29.94	8.02	29 91	8.15	39.87	8.28	29.84	8.41
32	30.91	8.54	30.87	8.42	30 84	8.55	30.80	\$.69 \$.95
34	32.84	8.80	32,80	8.94	32.76	9.09	32.72	9.23
35	33.81	9.06	33-77	9.21	33-73	9.35	33.69	9.50
36	34-77	9.32	34-73	9.47	34.69	9 62	34.65	9-77
37	35.74	9.58	35 70	9.73	35.65	9.89	35.57	10.11
39	37.67	10.09	37.63	10.26	37.58	10.42	37.54	10.59
40	38.64	10.35	38.59	10.52	38.55	10.69	38 50	10,86
41	39.60	10.61	39.56	10.78	39.51	10.95	39.46	11.13
42	40.57	11.13	41.49	11.05	40.47	11.22	40.42	11.07
44	42.50	11.39	42.45	11.57	42.40	11.76	42 35.	11.94
45	43.47	11.65	43.42	11.84	43.36	12 03	43 31	12.28
46	44.43	12.16	44.38	12.36	44-33	12.29	44.27	12.49
48	46.36	12.42	46.31	12.63	46.25	12 83	46.20	13.03
49	47.33	12.68	47.27	12.89	47.22	13.09	47.16	13.30
50	48.30	12,94	48 24	13.15	48.18	13.36	48.12	13-57
51	49.26	13.46	49.20	13.41	49.15 50.11	13.63		13.84
53	51.19	13.72	51.13	13 94	51.07	14.16	51.01	14 39
54	52.16	13.98	52.10	14.20	52.04	14-43	51-97	14 65
55	53.13	14.24	53.06	14.47	53.00	14.70	52.94	14.93
56	54.00	14.49	54.99	14-73	53.96	14-97	53.90	15,20
58	50.02	15.01	55.96	15.26	55-89	15.50	55.82	45.74
59 60	57-99	15.27	56.91	15:52	50.85	15,77	56.78	16,03
	57.96 Dep.	15-53.	57.83 Dep.	15.78	57.82	16.03	57-75 Den	Lat.
Dist	The party	Lat.	Dep. 43	Late	Dep.	List	Dep.	5/
I Daniel	0			DEGR		Or.		No.

					REES. 115			
Di ç	O'		1:	<u>'</u>	30	)'	45	1
•	Lat.	υ·p.	Lat	Dρ	Lat	Dep.	Lat.	D p.
61	58.92	15 79	58.85	16.04	58 78	10.30	58.71	14.50
62	59.89	16.05	59.82	16.31	59.75	16.57	59.07	16.53
63	65 85 61.82	16.31	65.78	16.57	60.71	16.84	65.63	17.10
64 65	61.62	16.56 16.82	61.75 62.71	16.83	61.67 62.64	17 10	61.60 62.56	17.37
66	63.75	17.08	63.68	17.36	63 60	17.64	63.53	1 92
6-	6 . 72	17.34	64.64	17 62		17.91	64.48	18 19
68		17.60	65.61	17.89	65.53	18.17	615	18.46
69	66.65	17.86	66 57	18.15		18.44	66 41	18.73
70	67.61	18.12	654	18.41	67 45	18.51	67.37	19 00
71 72	68.58	18.38 18.64	68.50 64.46	15.68	68.42 ·	18.97 19.24	68 33	19.27
73	70.51	18 80	70.43	19.20	ر د.70 د د.70	19.51	73.26	19 82
74	71.48	19.15	71.39	19.46	71.31	19X	722	2009
7.5	72 44	19 41	72.36	19.73	72.27	20.54	72.18	23 30
76	73.41	19 67	73.32	19.99	73 24	20 31	73 15	ز ۵۰.۵
77 78	74.38	19.93	74.29	20.25	74.20	20.58	74.11	20.90 21.17
79 79	75.34 76.31	20.19	75.25 76.22	20.78	75.16 76.13	21.11	75.07 76.03	21 44
Śź	77.27	20.71	77.18	21 04	77.09	21.38	700	21.77
81	78.2.1	20.96	78.15	21.31	78.05	21.65	77. 96	21.99
82	79 2 i	21.22	79.11	21.57	79 02	21.91	78.92	22.20
83	80 17	21.43		21 83	79 98 i		79.88	22.53
84 85	81.14	21.74 22.00	\$1.04 82.01	22.36	80 95 '	22 45	85 85 S	22.80
38	83.07	22.26	82.97	22.62	82.87	22.98	82	23.3+
87	84-04	22.52	83.94	22.88		23.25		13.52
88	85.00	22 78	84.90	23.15	84.80	2; 52	84.70	
89	85.97	23.03	85.87	23.41		23.78	85.66	24.16
90	86.93	23.29	86.83	23.67	86 73	24.55		24.43
91	87.90 88.87	23.55 23 81	87.80	23.94 24.20	87.69 88.65	24.32	87.58 88 55	24.70 24.97
92 93	89.83	24.07	89.73	24.46	89.62	24-59	89.51	25.24
94	9၁.೬၁	24.33	90.69	24.72		25.12	93.47	25.52
95	91.76	24.59	91.65	24 99	91.54	, <u>25.39</u> 1	91 43	25.79
96	92.73	24.85	92.62	25.25	92.51	25.65	92.40	26.50
97	93.69	25.11	93.58	25 51	93 47	25.92	93.56	26 33 26 60
99	94.66	25.36 25.62	94.55	25.78 26.04	94.44	26.19	94 32 95.28	20.57
165	96 59	25.88	96.48	26 30	96.36	26.72	yń 25	27.14
101	97.56	20 14	97 44	26.57	97.23	20.99	97.21	27-42
102	98.52	26 45	98.41	26.83	98 29	27 26	98.17	27.69
103	99.49	26 66	99.37	27.09	99 25	27.53	99.13	27.96
105	101 4	26 92	101.3	27.56	107.2	27 79 28 06	1.00.1	28.50
136	102.4	27.43	102.3	27.8K	102 1	28.33	102.0	20.77
107	103.4	27.69	103.2	2 .14	103.1	28.59	103.0	29.54
:08	104 3	27.95	104.2	28.41	104.1	25.50	103.9	29 32
139	105.3	28/21	105.2	288.7	165.0	29 13	1049	29.50
<b> </b>	106 3	28 47	106.1		106.0	29.40	105.9	19.56
111	107.2	25.73	107.1	129.30 129.46	107.0	29.66	1 150.8	142.40
113	109.1	29.25	109.0	129.73	108.9	320	108.8	32 47
114	110.1	29.51	110.0	129.99	109.9	30 47	159.7	35.04
115	111.1	24.76	111.5	35.35	110.8	30 -3	110.7	31.21
116	112.0	3 7 62	1119	30.51	111.8	31 00	111.6	31.19
118	113.0	30.28	112.9	30.77	112.7	31.27	1112.6	31.76
1119	114.9	30.54	114.8	31.34	1137	31.53	114.5	32.35
120	1159	31.06	115.8	31.56	115.6	3207	11155	32.57
	De.	Line	Dep	Lat.	D. p.	1.1.	D p.	lat
.\ <u>`</u>	<u> </u>	7	·	,,	1		1.5	
'L "		·				-		·

110	-	-			_			
D.	_ 0	-		5/	50		45	
-	Lat	Dep.	Lat	Dep.	Lot.	Dep.	Lat	Dep.
1	0.46	0.28	1.92	0.28	0.95	0.28	1.92	0.58
3	1.92	0.55	2.88	0 84	2.88	0.85	2.87	0.86
1 4	3.85	1 10	3.84	1.12	3.84	1.14	3 83	1.15
15	4.81	1.38	4 80	1.40	4.79	1.42	4-79	1.44
0	5.77	1.05	5.76	1.68	5.75	1.70	5475	1.73
7 8	7.69	1.93	7-68	1.96	7.67	1.99	7.66	2.31
9	8.65	2 48	8.64	2.52	8.63	2 56	8.62	2.59
10	9.61	2.76	9.60	2.80	9.59	2.84	9.58	-2.88
IL	10,57	3.03	10.56	3.08	10.55	3.12	10.53	3-17
1.7	11 54	3-31	12.48	3.64	11.51	3.41	11.49	3-46
13	12.50	3.58	13:44	3.92	73.42	3.98	13.41	401
15	14.42	4.13	14-40	4.10	14 38	4.26	14.36	4-32
16	15.38	4.41	145.35	4.48	15-34	4-54	15.32	4-61
17	16 34	4.69	16 32	4.76	16.30	4.83	16 28	490
18	17:30	4.96	17.28	5.04	17.26	5.40	17.14	5.19
20	19.23	5.51	19:20	5.60	19.18	5 08	19-15	5.76
110	20. TQ	5-79	20.16	5.88	20 14	5.96	20,11	Dios
22	21 15	6.06	21,12	6.16	21.09	6.25	21.07	6 34
23	22.11	6.34	72.08	6.44	22.05	6.53	22.02	6.63
25	23.07	6.62	24.00	7.00	23.97	7.10	22.98	7.30
26	24 99	7 17	24.90	7 28	24.93	7.38	24.90	7:49
27	25.95	7-44	25.92	7.56	25.89	7.67	25.85	7.78
28	26,92	7.72	26,88	7.84	26.85	7.99	26.81	8.07
70	27.88	7.99	27.84	8.12	28.76	8.24	27-77	8.36
30	29.80					8.52	28 73	-
31	30.76	8.54	30 72	8.67	30.68	9.00	30.64	8.93
33	31-72	9.10	31,68	9.23	31.64	9-37	31.60	9.51
34	32.68	9.37	32.64	9.51	32.60	9.66	32 56	9.80
35	53 64	9 65	33.60	9.79	33 56	9.94	33-52	10.09
30	34.61	9.97	34 56	10.07	34-52	10.22	34-47	10.58
38	35.57	10.47	35-52	10.35	35.48	10.51	35.43	10.95
39	37-49	10.75	37-44	10.91	37-39	11.08	37-35	12.24
40	38.45	11 03	38.40	11.19	38.35	11.36	38.30	11.53
45	39.41	11.30	39.36	11.47	39 31	11.64	39.26	11.82
42	40.37	11.58	40.32	11.75	40-27	11.93	40.22	12.39
44	42.30	12 13	42.24	12.31	42.19	12.50	42.13	12.65
45	43.26	12,40	43 20	12.59	43.15	12.78	43.09	12.97
46	44.32	12.68		12.87	44.11	13.06	44.05	13.26
48	45.18	12.96	45.12	13/15	45.06	13.35	45.01	13-55
49	45.14	13.23		13-43	46.98	13.63	46.95	13.83
50				13.99	47 94	14.20	47.88	1441
51	49.02	And the second second	48.96	14.27	48.90	14.48	42.84	E4.70
52	49.99	14-33	49.92	14.55	49.86	14:77	49.79	14.99
53		14.61	50 88	14.83	50.82	15.05	50.75	15.27
55		15.16	52.80	15.11	51.78	15.34	51.71	15.55
. 56		15-44	53 76	15.67	53.69	15.00	53.62	16.14
57	54-79	15-71	54-72	15.95	54.65	16.19	54 58	16.43
58		15.99	55.68	16.23	55 GE	16.47	55-54	16.72
59		16.26	57.60	16.51	50.57	16.76	56.50	17.29
Hist.	Dep	Lat	Dep.	Lat	57-53 Dep.	17.04	57.45 Dep-	Lat.
Ties I	O/		40	S. A. Salar	307	Late		No. 150
	- 0'	-		DEGR			15	

10	1 01	12	1 30'	1 45'		
1 8	Lat Dep	Lat.   Dep.	Lat   Dep.	Lat   Dep.		
61	(8.04 16.81	58.56 17.07	58.49 17.32	58.41 17.58		
62	59 60 :17.09	59-52 17-35	59.45 17.61	59.37 17.07 1		
63	60.56 17.37	60.48 17.63	60.41 17.89	60.33 18.16		
64	62 48 17.92	62.40 18.19	62.32 18.46	61.28 18.44 62.24 18.73		
66	63.44 18.19	63.36 18 47	-	63.20 19.02		
67	64.40 18.47	64.32 18.75	64.24 19.03	64.16 19.51		
68	66.33 19.01	66.24 19.03	65.20 19.31	65.11 19.60		
70	67.19 19.29	67.20 19.59	67-12 19.88	65.07 19.89		
71	65,25 19.57	68.16 19.87	68.08 20.17	67.99 10.46		
72	69.21 1985	69.12 20 15	69.04 20.45	68.95 20.73		
73	71.13 20.40	70.08 20.43	70.95 21.02	70.86 21,33		
75	72.09 20 67	72.00 20.99	71.91 21.30	71.82 21.61		
76	73.06 20.95	72.96 21.27	72.87 21.59	72.78 21,90		
77	74-02 21 22	73.92 21.55	73.83 11.87	73-73 22.19		
78	74.98 21.50	74.88 21.83	74-79 22.15	74.69 22.48		
80	76.90 12.05	76.80 22 39	76.71 22.72	76.61 23.06		
81	77.86 *22.33	77-76 22 67	77.66 23.01	77.56 23.34		
82	78.82 22,60	78.72 22.95	78 62 23.29	78.52 23.63		
83	79.78 11.88 80.75 13.15	79.68 23.23 80.64 23.51	79.58 23.57 80.54 23.86	79.48 23.92 80.44 24.21		
85	81.71 23.43	81,60 23.79	81.50 24.14	81.39 24.50		
86	82.67 23.70	82.56 34.07	82.46 24.43	82.35 24.78		
87	83.63 23.98	83.52 24.35	83.42 24.71	85.31 25.07		
89	84 59 24.26	84.48 24.63 85.44 24.90	84 38 24-99 85-34 25-28	84.27 25.36 85.22 25.65		
90	86.51 24.81	86.40 05.18	86.29 25.56	86.18 15.94		
91	87.47 25.08	87.36 25.46	87.25 25.85	87 14 26.23		
92	88.44 15.36	88.32 25.74	88.21 26.13	88,10 26.51		
93	90.36 25.63	90.24 26.30	90.13 26.70	90.01 27.09		
95	91.32 26,19	91.20 26 58	91.09 26.98	90.97 27 38		
96	92.28   16.46	92.16 25.86	92.05 27.27	91.93 27 67		
97	93.24   26.74	93.43 27.14	93.96 27.55	92.88 27.96		
99	94.20 27.01	94.08 27.42	93.96 27.83	93.84 28.24		
100	95.41 27.56	96.01 27 98	95.88 28.40	95.76 28.82		
101	97 09 17.84	96.97 28,26		96.71 29.11		
103	98.05 28.12	97 93 28.54 98.82	97.80 28.97	97.67 29.40		
104	99.97 28.67	99.84 29.10	94 72 29.54	99-59 29-97		
105	100.9 28.94	100,8 19.38	100.7 29.82	100.5 30,26		
106	101.9 129.22	101.8 29.06	101.6 30.11	101.5 30.55		
107	102 9 29.49	103.7 30.22	102.6 30.39	103.4 31.13		
109	104.8 30.04	1946 30.50	104.5 30.96	104.4  31.41		
110	105.7 30 33	1256 30.78	105 5 31.24	105.3 31.70		
III I	106.7 30.60	106.6 31.00	106.4 31.53	106.3 31.99		
113	107.7 30 87	107.5 31.34	107.4 31.81	107.2 32.28		
114	109.6 31.41	109.4 31.90	109 3 32.38	109.2 32.85		
115	T10 5 31.70	110.4 32.18	110.3 32.66	110.1 33.14		
116	FILS 31.97	114.4 32.46	111.2 32.95	117.1 33.43		
117	113 4 32.53	112.3 32.74	113.1 33.61	112.0 33.72		
119	1144 32.80	1142 33 30	114.1 33.80	114-0 34-30		
120	115.4 33.08	115.2 33.58	115.1 34.08	114 9 34.58		
Dist	Dep.   Lat.	Dep Lat.	Dep. Lat	D.p. Lat.		
0	0 1	45'	30'	151		
	THE RESERVE OF THE PERSON NAMED IN	73 DEGI	DUC			

-		-		51	1 0		_	-
Dis	- 0			_	30	-	-	51
12	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep
T	0.96	0.29	0.96	0.30	0.95	0.30	0.95	0.30
1 2	1.91	0.58	1.91	0.59	1.91	0.60	1.95	O.fit
3 4	3.83	0.88	3.82	1.10	3.81	1.20	2.86	0.91
4	478	1.46	4.78	1.48	4-77	1 50	3.8± 4.76	1.22
5			-	1.78		1.80		1.52
6	5.74	2:05	5.73 6.69	2.08	6.68	2.10	6.67	1.83
7 8	7.65	2:34	7.64	2.37	7.63	2.41	7.62	2.44
9	861	2.63	8 60	2.67	8.58	2.71	8.57	2.74
10	9.56	2.92	9.55	2.97	9.54	3.01	9.52	3.05
It	10.52	3,22	10.51	3-16	10.49	3.31	10.48	3 35
12	11.48	3:51	11.46	3:50-	11:44	3.61	11.43	3.66
13	12.43	3.80	12.42	3.86	12 40	3.91	12.38	3.96
114	13-39	4.09	13-37	4:15	13.35	4.21	13:33	4-17
15	14-34	4-39	14.33	4.45	-14 31	4-57	14.29	457
15	15.30	4.68	15.28	4-74	15:35	4.81	15.74	4.88
1 17	16.26	4.97	16.24	5.04	16.21	5.11	16:15	5.18
18	17.21	5.26	17.19	5.34	15.17	5.41	17.14	5 49
19	18.17	5.50	19.10	5.93	19.07	6.01	19.05	6 10
20	20.08		20.06	6.23	20.03	6.31	20.00	
22	21.04	6.14	21 01	6.52	20.98	6,62	20.00	6.71
23	22.00	6.72	21.97	6.82	21.94	6.92	21.91	7,01
24	22.95	7 02	22.92	7:12	22 89	7 22	22.86	7/31
25	23.91	7.31	23.88	7:41	23.84	7.52	23.81	7.62
26	2486	7.60	24.83	7.71	24 80	7,82	24.76	7.93
27	2582	7.89	25.79	8.01	25/75	8.12	29.71	8,23
28	26.78	8.19	26 74	8 30	26.70	8/42	26.67	8.54
29	27.73	8.48	27.70	8.60	27.66	8.72	27.62	8.84
30	28.69	8.77	28.65	8.90	28.61	9.02	28.57	9.15
31	29.65	9.06	29.61	9.19	29.57	9.32	29.52	9.45
32	30:60	9:36	30 56	9.49	30.52	9.62	30.48	9.75
33	34.56	9.65	31.52	9.79	31.47	9.92	31.43	10.05
34	32.51	9.94	33.43	10.38	32 43	10.52	32.38	10,37
36	-	10.53	34.38	10.68		10 83		
37	34 43	10.82	35:34	10.00	34-33	11.43	34-29	10.98
38	36.34	11.11	36.29	11.27	36.24	11.43	36.19	11.58
39	37.30	11.40	37.25	11.57	37.20	11.73	37-14	11.84
40	38:25	11.09	38 20	11.86	38.15	12.03	38.10	12.19
feri	39.21	11199	39.16	12.16	39.10	12-33	39.05	12 (0
42	40.16	12.28	40.11	12:45	40,06	1263	40.00	12.80
43	41.12	12.57	41.07.	12.75	41.01	12.93	40.95	13.11
44	42,08	12.86	42.02	13.05	41.96	13.23	41.91	13:41
45	43.03	13:16	42.98	13.34	42.92	13.53	42.86	13:72
46	43.99	13.45	43.93	13.64	43.87	13.83	43.81	14.02
47	44.95	13.74	45.84	13 94	44.82	14-13	44-70	14-33
49	46.86	14.33	46.80	14-23	45.78	14-43	45.72	14-63
50	47.02	14 62	47.75	14.83	7 1 1 2 CHILL	14.73	47.62	14-94
51	48.77		-	-	The second	-	10000	_
52	49.73	15.20	48.71	15.12		15.34	48.57	15.55
53	50 68	15.50	50.62	15.72		15.94	50.48	16.16
54	51.64	15.79	51.57	16.01		16 24	51.43	16.46
55	52.60	16 08	52-53	16.31		16.54	52.38	16.77
56	53-55	16.37	53.48	16.61		16.84	53-33	17.07
57	54.51	16.67	54-44	16 90		17-14	54-29	17.38
58	55-47	16.96	55 39	17-20	55 32	17-44	55-24	17.68
60	56.42	17.25	56.35	17.50	OF THE PERSON	7-74	56.19	17.99
100	57.38	17.54	57,30	17.79	Colone Press	18,04	57:14	18.29
25	Dep	Late	Dep.	Lat	Dep.	Lat.	Dep.	Lat.
Dist.	0	1	4.5	10	30	1	15	100
			75	DEG	REES.	-	-	

	0	<del>,</del>	15	<del>,</del>		30' , 45'		
Dist								
	lat.	Dep.	Lat	D.p.	Lat.	Dep.	Lat.	Dep.
61	58.33	17.83	58.26	18.09	58.18	18 54 18.64	58 10	18.60 18.90
62	59 29 60.25	18.13	59.21 60.17	18.39	59.13 60.08	18.94	59.05 60.00	19.21
64	61 20	18.71	61.12	18.98	61 04	19.25	60 95	19.51
65	62 16	19 20	62.08	19.28	61.99	19.55	61.91	19.82
66	63.12	19 30	63 23	19.57	62.95	19.85	62.86	20.12
67	64.07	19.49	63.99	19.87	63.45	23.15	63.81	20.43
68	65 03	19.88	64.94	20.16	64.85	20.45	64.76	23.73
1 69	65.99	20.17	65.85	20.46 20.76	65.81	20.75 21.05	65.72 66.67	21.34
		20 47					6- 62	
71 72	68.85	20.76 21.05	•	21.05	65.67	21.35	64.47	21.05
1 53	6,81	21.34		21.05	60.62	21.95	60. 12	22.26
74	75.77	21 64	-5 67	21.94		22.25	70.48	22.56
75	71.72	21.93	~1.63	22 24	71.53	22 55	71 43	22 86
70	72 68	22.22	72 58	22.54	72.48	22.85	72.38	23.17
77		22.51	73.54	22.83	73-44	23.15	73.33	23.47
78	74.59	22.81	74-49	23.13	74-39	23.46	74.29	23 78 24.58
79 80	75.55	23.10 23.39	75.45 76.40	23 43 23.72	75-34 ;6.30	24.06	76.19	24 39
81		23.68	77.36	24.02		24. 16	77 14	2.1.6y
82	77.46 78.42	23.97	78.31	24.32	77.25 78 20	24.66	78.10	25.00
83	79.37	24.27	79 27	24.61	74 16	24.96	79.05	25.30
84	80.33	24.56	80.22	24.91	80.11	25. 16		25.61
85	81.29	24 85	81.18	25 21	81.07	25.56	80 95	25.91
86	82.24	25.14	82.13	25.50	82 02	25.86	81.91	26.22
87	83 20	25.44	83.09	15.60	82.97	26.16	82.86	26.52
88	84.15	25.73 26.02	84.04 85.00	26.10 26.39	8; 9; 84.48	26.75 26.75	83.81 84.76	26.83
00	86.37	26.3.1	85.95	26.69	85.83	27 56	85.72	27-44
91	87.02	26.61	86.91	26.99	86.79	27.36	86.67	27.74
92	87.98	26.90	87.86	27.28	87.74	27.66	87.62	28.0,
93	88.94	27.19	88.82	27 58	88.70	27.97	88.57	28.35
94	89.89	27.48	89.77	27.87	89.65	28.27	89 53	28.66
95	90.85	27 78	90.73	28.17	90 60	28.57	90 48	28.96
96	91.81	28.07	9168	28 47	91.56	28.87	91.43	29.27
97 98	92.76	28.36	92.64	20.76	92.51	29.17	92 38	29.57 29.88
99	93.72 94.67	28 65 28 94	93.59	29.06 29.36	93.46	29.47	93.33	130.18
100	95.63	29.24	94.55	29.65	95.37	3 <b>5.</b> 37	95.24	30.49
101	96.59	29.53	96.46	29.95	903;	30.37	95.19	33.79
102	97.54	29.82	97.41	30.25	97.28	30.67	97.14	31.15
103	98.50	30.11	98.37	30.54	98.23	33.97	98.10	31.40
104	99.46	30.41	99.32	33.84	99.19	131 27	99.05	31.71
105	100.4	30 70	100.3	31.14	1.00.1	31.57	100 0	32.01
106	101.4	30 gy	101.2	31 43	1011	31.87	101.0	32.32
108	102.3	31.28	103.2	31.73	102.0	32.48	101.9	32.62
109	1033	31.58	104.1	31.32	104.0	328	103.8	33.23
110	105.2	32 16	105 1	32 62	1019	33.08	1048	33.54
111	130.1	32.45		32.92	1059	33.38	105.7	33.84
112	107.1	32.73	107.0	33.21	106.8	33.68	106.7	34-14
113	1.801	33.04	107.9	33 51	107.8	33.98	107 6	34.45
114	1090	33.33	103.9	33.51	108.7	34.28 24.28	108.6	34.75
116	1100	33.62	109.8	34.13	ICy 7	34 58	109 5	
117	110.9	33.92	110.8	34.40	113.6	3.43s 3,18	115.5	35.6
118	111.9	34.21 34.50	111.7	34.49	112.5	3;.48	112.1	35.97
1119	113.8	34.79	113.6	35.29	113.5	35.78	113.3	34.28
120	114.8	35.08	1146	35.59	114.4	34 08	114.3	8, در
ند آ	D.p.	Lat	Dep.	Lat	Dep	Lat.	Dep	Lat
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9	-	1 0'	_	1 13	-	1 30' 45'			-
П	Dist.	1-		Annual Contract of the Contrac	Section 2	-	-		
ı	-	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
ŀ	1	1.90	0.62	0.93	0.63	1.90	0.32	1.89	0.64
ı	3	2.85	0.93	2.85	0.94	2.85	0.95	2.84	0.96
ı	4	3.80	1,24	3.80	1,25	3.79	1.27	3.79	1.29
ı	5	4.76	1.55	4-75	1 57	4.74	1.59	4.73	1.61
ı	6	5.71	1.85	5.70	1.88	5.69	1.90	5.68	1.93
3	7 8	7.61	2.15	7.60	2.19	7.59	2.22	7-58	2.25
ı	9	8.56	2.78	8.55	2.82	8.53	2.86	8.52	2.89
R	10	9.51	3.09	9.50	3,13	9:48	3.17	9.47	3.21
ı	11	10.46	3.40	10.45	3.44	10.43	3 49	10.42	3.54
r	12	12.36	4.02	11.40	3.76	11.38	3.81	12.31	3.86
н	13	13.31	4-33	13.30	4.38	13.28	4-44	13.26	4-50
ı	15	14.27	4.64	14.25	4.70	14.22	4.76	14.20	4.82
ı	16	15 22	4.94	15.20	5.01	15.17	5.08	15:15	5-14
1	17	16.17	5.25	16.14	5.64	16 12	5 39	16.10	5-46
ı	19	18.07	5.87	17.09	5.95	18.02	6.03	17.04	6.11
1	20	19.02	6.18	18.99	6.26	18.97	6 35	18.94	6.43
R	21	19.97	6 49	19 94	6.58	19.91	6.66	19.89	6.75
8	22	20.92	6.80	20.89	6.89	20.86	6.98	20.83	7.07
ı	24	21.87	7.11	21.84	7.52	21.76	7.30	22.73	7-39
ı	25	23.78	7.73	23.74	7.83	23.71	7.93	23.67	8.04
	26	24.73	8,03	24.69	8,14	24 66	8.25	24.62	8.36
ı	27	25.68	8.34	25.64	8.46	25.60	8.57	25.57	8.68
ı	28	26.63	8.65	26.59	9.08	26.55	8.88	26.51	9.00
ı	30	28.53	8.96	27.54 28.49	9.39	27.50	9.20	28.41	9.32
ı	31	29.48	9.58	29.44	9.71	20.40	9.84	29.35	9.96
ı	32	30.43	9.89	30.39	10,02	30 35	10.15	30.30	10 29
ı	33	31.38	10.20	31.34	10.33	31.29	10.47	31.25	10.61
и	34	32.34	10.51	32.29	10.65	32.24	10.79	32.20	10.95
ı	36	33.29	11.12	33.24	11,27	33.19		33.14	18-45
Ŋ.	37	34.24	11.43	34.19	11.59	34.14	11.42	34.09	11.57
ı	38	36.14	11.74	36.09	11.90	36.04	1206	35.98	12.21
ı	39	37.09	12.05	37.04	12.21	36.98	12.37	36.93	12.54
1	40	38.04	12.36	37.99	12.53	37 93	12.69	37.88	12.86
1	48	38.99	12.67	38.94	13.15	38.88	13.33	38.81	13.18
1	43	40.90	13.29	40.84	13.47	40:78	13.64	40.72	13.82
ı	44	E41 85	13.60	41.79	13.78	41.73	13.96	41 66	14.74
1	45	42.80	13.91	42.74	14.09	42.67	14 28	42,61	1445
1	46	43.75	14.21	43 69	14-41	43.62	14.60	43.56	14.79
1	48	45.65	14.83	45.59	15.03	44-57	15,23	45-45	15.43
1	49	46.65	15.14	46.54	15 35	46.47	15.55	46.40	15.73
1	50	47.55	15.45	47.49	15,66	47-42	15.87	47-35	16.07
1	52	48.50	15.76	48.43	16.28	No. of the last of	16.50	48.29	16.39
1	53	49-45	16.38	49.38	16.60	49-31	16.82	50 19	15.71
1	54	51.36	16.69	51.28	16.91	51.21	17.13	51.13	17,35
ŀ	55	52.3E	17.02	52.23	17.22	52.16	17.45	-	17.68
1	56 57 58 59 60	53.26	17.31	53.18	17.54		17.77		18.00
1	58	55.16	17-61	55.08	18.16		18.40		18 32
1	59	56.11	18.23	56.03	18.48		18.72	55.87	18.95
1	60	57.06	18-54	56.98	18 79	56.40	19.04	56.82	1429
1	Dist.	Dep	Lat.	Dep.	Lat	Uep 1	Lat.	Dep.	Lic
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l	Lat.	1)cp.	lat.	1) p.	Lat. 57.85	100	1 41	Dep.
61	58.01 58.97	'18.85 1916	57.93 58.88	19.10 19.42	58.80	19.30	57.76 58.71	14.63
63	59.92	19.47	59.83	19 73	59.74	19.99	59.00	20 25
64	60.87	19.78	60.78	20.04	60.69	20 31	60 60	2.5
65	61.82	23 09		20. (6	61.64	23.62	61.55	23. 0
60 67	62 77	20.70	62.68 63.63	20.67	62.54	·20.94 ;21.26	دز ⊆6 4ز6	21.22
63	63.72	21.01	64.58	21.30	64 49	21 58	64.39	21.50
69		21.32	65.53	2161	65 13	21.89	65.34	32.18
70	66 57	21.63	66.48	21.92	. 66.38	22.21	06.20	22.13
71	67.52	21.94	67.43	22 23	67 33	22.55	67.23	22.82
72 73	68.48 69.43	22.25	68.38 69.33	22.55	68.28 69.23	123.10	69.18 69.13	123 14
74	70.38	22.87	70 28	23.17	70 18	2; 18	70.07	23.70
75	71.33	23.18	71 23	23.49	71. 2	23.53	71 02	24.11
76	72.28	23.49	72 18	23 80	72 07	24.12	71.97	. 24.43
77	73.23	23 79	73.13	24.11	73.52	24 43	72.91	24.73
78 79	74.18 75.13	24.10	74.08 75.03	24.43 24.74	73.47	124.75  25.07	73.86 74 81	25.39
83	76.08	24.72	75.98	25.05	75.87	25.38	75.75	.25.72
81	77.04	25.03	76.93	25 37	76.81	25.70	76.70	
82	77 99	25 34	77.88	25.68	77.76	26 02	77 45	;26 ,6
83	78.94	25.65	78.83	25.99	78.71	26 34	78.60	;26 65
84. 85	79.89 80.84	25.96 26.27	79.77 80.72	26.31	79.66 80.61	26.65 26.97	79-54 80.49	:27,30
86	81.79	26.58	81.67	26.93	81.56	2" 29	81 44	27 04
87	82 74	26.88	82.62	27.25	82 50	27.61	82.38	27 9
88	83.69	27.19	83.57	27.56	83.45	27.91	83.33	23.29
89	84.64	27.50	84 52	27.87	84 43	28.24	84.28	25.61
90	85.60	27.81	85.47		86.30	128 56	85.22	
91 92	86 55 87 50	28.43	80.42	28.50 28.81	87.25	25.87	80.17	29.25
93	88.45	28.74	88.32	29.12	88 19	29.51	88.06	29.89
94	89.40	29.05	89.27	29.44	89.14	29.83	89 21	30.22
95	90.35	29.36	90.22	29.75	90.09	37.14	89 96	37.54
96	91 30	29.67	91.17	30.06	91.04	35.46	92.91	36.85
97 98	92.25 93.20	39.97 . 30.28	93.07	30.38 30.69	91.99	30.78 31.10	9: 85 92.80	318
99	94.15	30 59	94.02	31.00	93.88	31.41	95.75	3182
100	95 11	33.90	94.97	31.32	94 ×3	31 -3	7+ 69	32.14
10	9 <b>6.</b> 06	31.21	95.42	31.63	95.78	32.05	95 64	32.46
1. 2	97 OI 97.96	31.52	96.87	31.94	963 97.68	32.36	96 59	32.79
103	98.91	32.14	98.77	32.57	18.63	33.30	97-53 98.48	33 + 1 33 +3
10;	99.86	32.45	99.73	32.83	99 57	32.52	99.43	33.75
ιού	100.8	32.76	100.7	33 20	100.5	33.63	100.4	34.57
107	101.8	33.06	101.6	33.51	101 5	33.95	101.3	34-39
100	102.7	33-37 33.68	102.6	33.82 34.13	102.4 103.4	34.27	102.3	34.72 35.04
110	1046	33 99	104 5	34.45	1.43	34.90	1C4 2	35 36
111	12: 6	21.20	105 4	34.76	103.3	35.22	105.1	35.68
112	106.5	34.61	106 4	35.07	106.2	35.54	106 1	36.00
113	107.5	34.92	107.3	35.39	107.2	35.86	107.0	36.32
1114		35.23	108 3	35.70 36.01	108.1	36.17 36.49	108.0	36 04 36 07
116	110.3		110.2	36.33	1100	36 81	109 8	324
117	111.3	36.16	111.1	36 64	0.111	37.12	110.8	3- 61
118	112.2	36.46	112 1	36.94	111.9	37-44	111.7	37.9
119	1:3.2		113.0	37.27	112.9	3- 76		38.25 38 57
120	114.1	37 08	114.0	37.58	113.8	1,	11 3.0	Lat
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10.1	0/		1.5	Γ.	30	1	4.5	1
181	Lat.	Dep.	Lat.	Dep	Lat.	Dep/	Late	Dep
1	0.95	0.33	0.94	0.33	0.94	9.33	0.94	0.34
2	1.89	0.65	1.89	0,66	1.89	1.00	2.82	1.01
3 4	3.78	0.98	2.83	0.99	3 77	1.34	3.76	1,35
5	4.73	1 63	4-72	1.65	471	1.67	4/71	1.09
6	5 67	1.95	5.66	1.98	5.06	1.00	5.65	2.03
7 8	6.62	2.28	6.61	2.31	6.60	2 34	0.59	2/37
9	7.50	2,60	7.55	2.64	7 54 8.48	3,00	7453	3.04
10	9.46	3.26	9 44	3.30	9.43	3 34	9.41	3.38
11	10:40	3.58	10:39	3.63	19.37	3.67	10.35	3.72
12	11 35	3.91	11.33	3.96	11.31	4-01	11/29	4.06
13	13.24	4-23	12.27	4.39	13.20	4-34	13.18	4-73
15	14.18	4.88	14.16	4.95	14:14	5.01	14.32	5.07
16	15.13	5.21	15.11	5.28	15.08	5-34	15.06	5-41
17	16.07	5-53	16.05	5.60	16.02	5 67	16,00	5.74
18	17.02	5.86	16.99	6.26	16.97	6.34	17.88	6.08
20	17.96	6.19	17.94	6.59	18.85	6.68	18.82	6.76
21	19.85	6 84	19 83	6.92	19.80	7.01	19.76	7.10
22	20.80	7716	20.77	7125	20.74	7-34	20.71	7-43
23	21.75	7149	21.73	7.58	21.68	7.68	21.65	7-77
24	23.64	7:81	22.60	7/91 8:24	23.57	8.35	22 59	8.45
26	24.58	8:46	24.55	8:57	24:51	8.68	24.47	8.79
27	25.53	8:79	25.49	8.90	25:45	10:0	25.40	9.11
28	26.47	9112	26.43	9123	26039	9.35	26435	9.46
29	27.42	9-44	27.38	9.56	27-34	9.68	27:25	9.80
30	28.37	9.77	28.32	9.89	28.28	10.01	28/24	9.14
31	30.26	10.09	30.21	10.22	30,16	10.68	30.12	10.48
33	31.20	10.74	31.15	10.88	31.11	11.02	31,06	11.15
34	32.15	11:07	32 10	11/21	32,05	11.35	33,00	11-49
35	33.09	11.39	33.04	11.54	12.99	11.68	32.94	11.83
36	34-04	11:72	33 99	11.87	33-94	12.02	33.88	12,17
37	34.98	12.05	34.93	12.20	34.88	12.68	34.82	12.50
39	36.88	12.70	36.82	12.86	36.76	13.02	36.71	13.18
40	37.82	13.02	37.76	13.19	37-71	13.35	37.65	13.52
41	38.77	13.35	38.71	13.52	38.65	13.69	38.59	13.85
42	39.71	13.67	39.65	13.85	39.59	14.02	39-53	14-19
43	40:66	14.00	40.60	14.51	40.53	14-35 14-50	40.47	14.53
45	42.55	14.65	42.48	14.84	42.42	15-02	42.35	15.21
46	43.49	14.98	48-43	15:17	43 36	15-36	43.29	15:54
47	44-44	15.30	44.37	15.50	44.30-	15:59	44-24	15.88
48	45.38	15.63	45.32	15.83	45.25	16.02	45.18	16.22
50	46.33	15.95	46.26	16.48	46.19	16.36 16.69	47.06	16.56
51	48 22	16.60	48.15	16.81	48.07	17.02	48.00	10.90
52	49.17	16.93	49.09	17-14	49.02	17.36	48.94	17.57
53	50.11	17.26	50.04	17-47	49.96	17.69	49.88	17.91
54	51.06	17.58	50.98	17.80	50.90	18.03	50.82	18.15
55	52.00	17.91	51.92	18.13	51.85	18.36	51.76	18.39
56	53.89	18.23	52.87	18.46	52.79	18.69	52.71	18.92
58	54.84	18.88	54.76	19.12	53-73	19.03	54.59	19.26
59	55.79	19.21	55.70	19-45	55.62	19.69	55-53	19.94
	56.73	19.53	56.65	19.78	56.56	20.03	56,47	20.28
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10	0	1	45	Table .	30	(	10	1-16-6
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	17 DEUREES. 1										
Dist	10		.11	<u> </u>		311	4)				
	lat	Dep	lat.	Dep.	Last.	Dep.	Lat	, Dea			
61	57.68	19 80	57.59	20.11	57.50	25.36	5".41	10 01			
62	5862	20.19	58.53	20.44	58.44	20 ~0	58.35	27.15			
63	59.57	20.51	59.4	20.77	59.39	21.03	54.20	21.63			
64	61.46	20.84	63.43	21.10	60.33	21 36	61.18	21.06			
-66	62.40	21.49	62.31	21.76	62.21	22.0;	62 12	22.5.			
67	63.35	2 .81	63.25	22.00	63.16	22.3	63.56	22 04			
68	64 35	22 14	64.23	22.42	64.10	22 70	64.33	22 48			
69	65.24	22 46	65 14	22 75	65.04	25.03	64 94	23.,2			
.70	66.19	22 79	669	23 OS	65.98	23.3-	05.88	2; 4;			
71	6- 13	23.12	67.03	23.41	66 93	23.	66.82	23 90			
72	68.0%	43 44 23-77	65.y2	23.74	68.81	24.03	65.76	2.4 ::			
74	69.97	24 09	69.86	24 40	69.76	24.70	69.65	25 21			
75	0 91	24 42	18 65	24 73	70.70	25.04	~2 59	25 34			
76	71 86	24.74	71.75	25.06	71.64	23.37	71.53	2,.6			
77	72.8C	25.07	72.69	25.39	72 58	25.70	72.47	219 02			
78	73.75	25.39	73.64	25.72	73.53	26.04	73.41	26 36			
79 85	74.70	25 -2	74.58	26.05	74-47	20.3~	74-35	20.7			
I	75.64	26.75	75-53	26 38	75.41	26 ~3	<u>~5 24</u>	27.63			
81	76.59	26.37 26.70	76.47 77.43	26.73	76.35 77.30	27.04	76.18	27.37			
83	77.53 78.48	27.02	78.36	27.36	78 24	27.71	8 12	2 3			
84	79.42	27.35	79.30	27 69	9.13	28.0	79.26	28 30			
85	80.37	27.67	80.25	28.02	80 12	28 ;-	8ວິດລ	25.72			
Ko	81.31	28.00	81.19	28 35	RI 07	28 ; 1	80.04	2 7.56			
87	82.26	28.32	82.11	28 65	82.01	29.94	84.53	29.40			
88	83.21	28 65	83.08	29.01	82 95	29.37	32 32	29.74			
89	84.15	28.98 29.30	84.97	29.34 24.67	83 90	29 71 30 04	83.76 84.71	30.57 3 41			
1	86.04	29.63	_		85.78	30.38	8, 6,	30 7;			
91	86.99	29.03	85 yı 86.86	30.00 30.33	86.72	30.71	86.59	31.09			
93	87.93	30.28	87 80	30.66	867	31.0.1	87.53	5143			
94	88.88	30.60	83.74	30.99	83.61	31.38	88.47	31.50			
95	89.82	30.93	89 69	31 32	89.55	31.7:	89 41	32.17			
96	90 77	31.25	90 63	31.65	90.49	34.05	93.35	32.24			
97	91.72	31.58	91.58	31.98	91 44	32.38	912)	32.78			
98	92.66	31.91	92.52	32 31	92.38	32."I 33.05	92.1S	33.12 33.45			
100	94-55	32.56	93.46	329-	93.32 94.26	33.38	93.13	33 -9			
101	95.50	32.88	95-35	33.32	9;.21	33.71		31.13			
102	96.44	33.21	96.30	53.63	96.15	34.05		34.4			
103	97.39	33.53	97.24	33.46	97.Cg	34.28		34.81			
104	98.33	33.86	98.19	34 2y	98.03	34-72		35 14			
105	99.28	34.18	99 13	34.62	98 98	35.05	98.82				
106	100.1	34.51	133.1	34 95	99.92	35.38	99.76	35 82			
107	101.2	34 84 35 16	101.0	35.28 35.61	101.8	36.05		35.16			
15g	102.1	35 49	102.0	35.04	131.6	36.38	132.6	35.83			
1110	13,1.0	35.81	103 8	36 27	103	36.72	133.5 .	37.17			
111	135.0	36.14	124.8	36.60	104.6	37.05	154.5	;~.et			
112	1059	36.45	10:.7	36 93	105.6	37-39	105.4	37.53			
113	196.8	36 - ,	106.7	37.26	106.5	37.72	106.4	35.18			
114	1 7.8	37.11	107.6	37.58	107.5	38 25	127.3	38.52 38.50			
115	——·	<u>37.44</u> :		37 91	:	38.39					
116		37.77 38 09	109.5	38.24 38.57	109.3	38.72 j 39 06 j	159.2 110.1	39.20			
118		38 42	111.4	38.90	111.2	39 39 1	111.1	30 37			
119		38 74	- ,	39.23		39.72	1120	421			
:20		39.07		39 56		40.06	112.0	10.55			
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57 53-56 19-50 53-48 19-73 53-39 19-96 53-10 20.19 58 54-50 19-84 54-42 20.07 54-31 20.31 54-42 20.55 59 55-44 20.18 55-35 20-42 55-26 20 60 55-17 20.90 60 56-38 20-53 56-29 20.77 56-20 21.01 56-11 21 26  Dep Lati Dep Lat. Dep. Lat. Dep. Lat. S6-17 20.90 60 0 45 <sup>2</sup> 301 15 <sup>2</sup>	1				52.54	1938	SCHOOL ST					
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61	57-32	23.86	57.23	21.11	57-14	21.36	i — ·— '	21.61
62	58.26	21.21	58.17	21.46	58 07	21.71	57.04 57.98	21.97
63	59.20	21.55	59.11	21.81	\$9.01	22.06	58.91	22.32
64	60.14	21.89	60.04	22.15	59.95	22 41	\$9.85	22.67
1.55	61.05	22.13	60.98	22.50	60.88	22.76	65.78	23.0;
66	62.02	.22.57	61.92	22.84	61.82	23.11	61.72	23 37
67	62.96	22 92	62.86	23.10	62.76	23.40	62.65	23.74
68	63 40	23.26	63.80	23.54	63.69	23.81	6 3.59	24.00
69	64.84	23.60	64.74	23.88	64.63	24.16	64.52	24.45
73	65.78	23.94	65.67	24.33	65 57	24.51	65.46	21 45
	66.72	24.28	66.61	24.57	66.50	24.86	66.39	25
72	67.66	24.63	67.55	24.92	67.44	25.21	67.33	25.,
73	68 60	24.97	68.49	25.27	68 38	25.57	68 26	23 15
74	69 54	25.31	6943	25 61	69.31	25.92	69.20	25 3:
75	70.48	25.65	70.36	25.96	70.25	26 .7	73.14	26 : 7
76	71.42	25.99	71.30	26.30	71.19	26 62	71.07	20 93
77	72 36	26.34	72.24	26.65	72.12	27.97	72.01	27.25
78	73.30	26 68	73.18	27.00	73.06	27 32	7194	27.6
79 80	74.24	27.02 27.36	74.12	27.34	74.00	27 67 28 32	73 88	27.99
	75.18		75.06	27.69	7+ 93		74.81	28.34
81	76.13	27.70 28.05	75 99	28.04	75.87	28.37	75.75	28.7C
82	77.05	28.39	76.93	28 38	76.81	28.72 29 07	76.68 77.62	29.05 29 4 1
84	78.93	28.73	78.81	29.07	78.68	29.42	78.55	29.76
85	79 87	29.07	79.75	29 42	79.62	29.77	79-49	30.11
86	8281	29.41	80 68	29.77	80 55	32 12	80 42	30.47
87	81.75	29.76	81.62	30.11	81.49	30.47	81.36	30.82
88	82.69	30 10	82.56	30.46	82.43	30.82	82 29	31.18
89	83.63	30.44	83.50	30.80	83 36	31.17	83.23	31.53
90	84 57	30.78	84.44	31 15	84 30	51 72	84.16	31.89
91	85.51	31.12	45.38	31.50	85.24	31.87	85.10	32.24
92	86.45	31 47	86.31	31.84	86 17	32 22	86 03	32.59
93	87.39	31.81	87.25	32.19	87.11	32.57	86 97	32.95
94	88.33	32.15	88.19	32 54	88.05	32.92	87.90	3 .30
95	89 27	32.49	89.13	32.88	88 98	33.27	88 84	33.66
96	90.21	32.83	90.07	33.23	89.92	33.64	89 77	34.01
97	91.15	;3 18	91.00	33.57	95.86	33.97	90.71	34 37
98	92.09	33.52	91.91	33.92	91 79	3+32	91.64	34.72
99	93 23	33.86	92.88	34 27	92 73	34.67	92 58	35.07
100	93.97	34.20	93.82	34.61	93 67	35.02	93.51	35.43
101	94.91	34.54	94.76	34 96	94 60	35-37	94.45	35.78
102	95.85	34.89	95.70	35.30	95.54	35 72	95.38	36.14
103	95 79 97 73	35.23	96.63 97 57	35.65	90.48	36 07 36.42	96 32	36 49 36.85
105	98.67	35 37	98.51	16.34	98.35	36.77	98.19	37.20
	99.61	36.85		36.69		57 12		
106	100.5	36.60	99.45	37.23	99 29	37 12 37 47	100.1	37 55 37.91
108	101.5	36 94	101.5	37.38	101.2	37.82	101.0	38.26
109	102.4	37 28	102.3	37 73	132.1	38.17	101.9	38.62
110	133.4	37.62	103.2	38.07	1030	38 52	101.9	38.97
111	101 3		134.1	,8.42	1240	38.87	103.8	39.33
112		38.31	125.1	38.77	-	39.22	104.7	39.68
113	106 2	38.65	106.0	39.11	105.8	39.57	105.7	40.03
114	107.1	38.99	107.0	39.46	106.8	39.92	126.6	40.39
115	1 801	39 33	107.9	39.80	107.7	40 27	107.5	40.74
116	109.0	3 1.67	108.8	.10.15	108.7	40.62	108.5	41.10
117	10y.9	43 32	109.8	40.50	139.6	40.97	109.4	41.45
118	110.9	40 36		40.84	110.5	41.32	110.3	41.81
119	111.8	40 -0		41.19	111.5	41.67	111.3	42.16
120	112.8	41.04	112.6	41.53	112.4	42.02	112.2	42.52
¥ /	D	Lot.	Dep	Lat.	Dep.	Int	Nep.	<u>  [m</u>
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1	Dist.	Lat	Dep.	Lat	Dep.	Lat	Depo	Lat	Dep.
H		-	-	-		0.93		0.93	0.37
1	2	0.93	0.36	1.86	0.36	1.86	0.37	1.86	0.74
ı	3	2,80	1.08	2,80	1.09	2.79	1.10	2.79	LIE
ı	4	3.73	1.43	3.73	1-45	3/72	1.83	3.72	1.85
1	5	5.60	1.79	4.66	1.81	4.65	2.20	5.57	2.22
ı	2	6.54	2.15	6.52	2.17	6.51	2.57	6.50	2.50
ı	8	7-47	2.87	7.46	2.90	7.44	2.93	7:43	2.95
ı	9	8,40	3.23	8.39	3.26	8,37	3.30	9.29	3-34
ı	10	10,27	3.58	10.25	3.99	10.23	4.03	10.22	4.08
ı	12	11-10	4.30	11.18	435	11.17	4.40	11.15	4-45
ı	13	12.14	4.66	12,12	4-71	12.10	476	12.07	4-8:
ı	14	14.00	5.38	13.05	5.07	13.96	5.50	13.93	5.19
1	16	14.94	5.78	13.98	5.80	14.89	5.86	14.86	5.93
ı	17	15.87	6.09	15.84	6.16	15.82	6.23	15.79	6 30
ı	18	16.85	6.45	16.78	6.52	16.75	6.60	16.72	0.67
4	19	18.67	7.17	18.64	7.25	17.68	7.33	17.65	7-04
ı	21	19.61	7.53	19.57	7.61	19.54	7.70	19.51	7.78
ı	22	20.54	7.88	20.50	7.97	20.47	8.05	20.43	8.15
1	23	21.47	8.24	21.44	8.34	21.40	8.43	31.36	8.52
1	34	23.41	8.60	22.37	9.06	23.26	9.16	23.20	8.1g 9.26
1	25	24.27	9.32	24.23	9.42	24.19	9.53	34.15	9.63
ı	27	25.21	9.68	25.16	9.79	25.12	9.90	25.08	10.01
ı	28	36.14	10.03	26,10	10.15	26.05	10.26	20.01	10.38
ı	29	27.07	10.39	27.03	10.51	26.98	11.00	26.94	10.75
ł	30	28 94	11.11	28.89	11.24	28.84	11 36	28.79	11.40
ı	32	29.87	11.47	29.82	11.60	39.77	11.78	29.72	11.86
ı	33	30.81	11.83	30.76	11.96	30 70	1209	30.65	12.23
ı	34	31.74	12.18	31.69	12.50	31 63	12.46	31.58	12.60
ł	35	33.61	12.90	33-55	13.05	33.50	13.19	33-44	13.34
ı	37	34-54	13.26	34.48	13.41	34-43	13 46	34-37	13.71
ı	38	35.48	13.62	35.42	13 77	35.36	13.93	35.29	14.08
ł	39	36.41	13.98	36 35	14.14	36.29	14.29	37.15	14 45
ŀ	40	38.28	14.60	38.21	14.86	38.15	15.03	38.08	15.10
ı	42	39 21	15.05	39.14	15.22	39.08	15.39	39.01	15.56
ı	43	40.14	15.41	40.08	15.58	40.01	15.76	39.94	15.93
H	44	41.08	15.77	41.94	15.95	40.94	16.49	40.87	16.50
1	45	42.94	16.48	42 87	16.67	42.80	16.86	42.73	17.05
1	47	43.88	16.84	43.80	17.03	43 73	17.23	43.65	17.42
1	48	44.81	17.20	44-74	17-40	44.66	17.59	44-58	7-70
1	50	45.75	17.56	45.67	18.12	45.59	17.90	46.44	18.16
1	_	47.61	18.28	47.53	18 48	47-45	18.69		18.90
1	51	48.55	18.64	48 46	18.85	48.38	19.06	48.30	19.27
1	53	49.48	18.99	49.40	19.21		19.42		19.04
1	54	51.35	19.35	50 33	19.57		20.16	100000	10.01
1	56	52.28	20.07		20.30	-	20.52		20.75
1	57	53.21	20.43	53.12	20.66	53.03	20,89	52.94	21.12
1	58	54.15	20.79		21.02	30 3	21.26		21.49
	60	55.08	21.14		21.38		21.62		21,86
1		Dep.	Lat.	Dep.	Lat	Dep.	Lat	Dep	Lat.
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61 56.95 21.86 50.85 22.11 56.76 22.36 (6.66 22.50 57.88 24.97 69 22.71 57.59 22.97 63.58 24.94 59.75 23.94 59.65 23.40 60.68 23.29 60.58 23.40 60.68 23.29 60.58 23.40 60.65 23.80 60.58 23.29 60.58 23.40 60.67 24.09 60.66 25.5 24.01 62.41 24.88 62.34 24.56 62.24 24.98 60.37 24.96 60.68 24.40 62.44 24.88 62.34 24.56 63.27 24.96 60.68 24.40 65.20 6	<b>1 2 3</b>								
61	J								<u> </u>
64									1
6; 60.68 23.29 60.58 23.66 60.48 23.82 60.37 14.09 66.66 62.54 24.01 62.44 24.88 62.34 24.56 63.27 14.66 62.44 24.88 62.34 24.56 63.27 14.56 62.46 62.46 62.46 62.47 64.20 25.29 64.09 25.57 65.53 25.09 64.42 25.57 65.13 25.00 64.21 25.66 60.99 62.42 25.29 64.09 25.57 70.65 25.20 64.09 25.57 70.65 25.20 64.09 25.57 70.65 25.20 64.09 25.57 70.71 66.28 25.44 66.17 25.73 65.00 26.00 67.92 26.75 67.00 26.88 69.90 26.26 67.92 26.75 67.80 27.05 27.77 70.92 25.83 69.90 71.06 27.07 12.00 26.88 69.90 27.10 26.			• -						
66         61.63         23.65         61.51         23.92         61.41         24.19         61.30         24.46           68         63         24.471         63.38         24.473         63.38         24.576         63.23         14.83           69         64.41         24.73         64.31         25.01         62.20         25.29         65.02         25.57           71         66.28         25.40         66.17         25.73         66.09         26.39         65.29         25.57           72         67         22         25.80         67.10         26.10         66.99         26.39         66.87         26.66         67.92         26.73         67.80         27.65         20.31         77.60         26.68         67.92         26.73         67.80         27.70         26.83         76.72         26.83         76.72         27.70         28.21         27.70         27.70         28.21         27.70         27.70         28.27         77.71         27.72         28.27         77.71         27.72         28.27         77.73         28.31         73.63         28.27         72.75         28.37         74.22         28.57         72.23         30.02         77.23									
6. 62 55									(-`- <del>-</del> -
68 6348 24.73 63.38 24.65 63.27 24.92 63.16 25.20 64.94 25.77 70.65.75 125.90 65.24 25.77 65.13 25.66 64.20 25.94 125.71 66.28 125.80 65.24 25.37 65.13 25.66 65.00 25.94 125.77 66.28 125.80 66.29 125.97 125.80 125.70 12	-						1 ' 5		
69         64.42         24.73         64.71         25.07         65.25         25.99         65.24         25.37         65.13         25.66         65.00         25.97         25.66         65.00         25.97         25.66         65.00         25.97         26.10         66.00         26.00         26.92         26.33         65.92         26.68         26.07         26.00         26.07         26.07         26.68         27.02         26.68         27.02         26.88         69.90         27.18         69.78         27.49         69.66         27.79           76         70.95         27.24         70.83         27.95         70.71         18.99         77.29         71.64         28.27         72.79         71.64         28.27         71.52         28.59         73.38         29.27         72.45         28.99         74.25         29.00         74.91         29.26         74.94         29.27         74.92         29.26         75.36         29.69         75.23         30.02         76.16         30.39         76.12         30.02         76.12         30.02         76.12         30.02         76.12         30.02         76.13         30.02         76.13         30.02         76.12         30.02 <td></td> <td></td> <td>, ,</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>			, ,						
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85         79.35         30.46         79.22         30.81         79.09         31.15         78.95         31.50           86         80.29         30.82         80.15         31.17         80.02         31.52         79.88         31.87           87         81.22         31.18         81.68         31.53         80.95         31.89         80.81         32.25         81.68         32.25         81.68         32.25         81.68         32.25         82.81         32.26         82.81         32.26         82.81         32.29         82.66         32.98         83.74         32.29         82.66         32.98         83.74         32.29         85.59         33.35         84.66         32.98         84.67         33.35         84.52         33.72         85.65         33.72         85.65         33.72         85.45         34.40         89.47         34.79         86.53         34.40         89.47         34.79         89.32         35.18         89.17         35.70         97         90.56         34.40         89.47         34.79         89.32         35.18         89.17         35.57         99.56         34.40         89.47         34.79         89.32         35.18         89.17				1 7 2 5	i –				
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100         93.36         35.84         93.20         36.24         93.04         36.65         92.88         37.06           101         94.29         36.20         94.13         36.61         93.97         37.02         93.81         37.43           102         95.23         36.55         95.06         36.97         94.90         37.38         94.74         37.80           103         96.16         36.91         96.00         37.33         95.83         37.75         95.67         38.17           105         98.03         37.63         97.86         38.06         97.69         38.48         99.55         38.49         99.55         38.91           106         98.96         37.99         98.79         38.42         98.62         38.85         98.45         39.28           107         99.89         38.35         99.72         38.78         99.55         39.22         99.38         39.65           108         100.8         38.70         100.7         39.14         100.5         39.58         100.3         40.23           110         101.8         39.06         101.6         39.51         101.4         39.95         101.2         40.	98				35.52	-		-	
Tot   94 29   36.20   94.13   36.61   93.97   37.02   93.81   37.43   37.60   39.61   36.55   95.06   36.97   94.90   37.38   94.74   37.80   37.69   96.16   36.91   96.00   37.33   95.83   37.75   95.67   38.17   104   97.09   37.27   96.93   37.69   96.76   38.12   96.60   37.59   96.93   37.69   96.76   38.12   96.60   38.91   106   98.96   37.99   98.79   38.42   98.62   38.85   97.53   38.91   107   99.89   38.35   99.72   38.78   99.55   39.22   99.38   39.65   107   99.89   38.35   99.72   38.78   99.55   39.22   99.38   39.65   108   100.8   38.70   100.7   39.14   100.5   39.58   100.3   40.02   101.8   39.06   101.6   39.51   101.4   39.95   101.2   40.39   101.2   40.39   101.2   40.39   101.2   40.39   101.2   40.39   101.2   40.39   101.3   105.5   40.50   105.5   40.23   102.3   40.68   103.1   41.13   105.5   40.50   105.3   40.96   105.1   41.41   105.0   41.87   115   107.4   41.21   107.2   41.68   107.0   42.51   105.9   42.24   115   107.4   41.21   107.2   41.68   107.0   42.51   105.9   42.24   116   108.3   41.57   108.1   42.04   108.9   42.85   108.7   43.36   110.2   42.29   110.0   42.77   109   42.51   107.7   42.98   110.9   43.13   110.7   43.61   110.5   44.10   110.9   43.13   110.7   43.61   110.5   44.10   110.9   43.13   110.7   43.61   110.5   44.10   110.9   43.13   110.7   43.61   110.5   44.10   110.6   42.77   109   43.73   110.5   44.41   105.0   43.73   110.7   43.61   110.5   44.10   110.8   43.49   111.7   43.9°   111.5   44.41   43.75   106.0   42.77   109   43.13   110.7   43.61   110.5   44.10   110.6   42.77   109   43.13   110.7   43.61   110.5   44.10   110.6   42.77   109   43.13   110.7   43.61   110.5   44.41   43.49   111.7   43.9°   111.5   44.41   43.49   111.7   43.9°   111.5   44.41   43.75   106.0   42.77   109   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42.75   109.0   42			35.48						
102   95.23   36.55   95.06   36.97   94.90   37.38   94.74   37.80   96.06   36.91   96.00   37.33   95.83   37.75   95.67   38.17   104   97.09   37.27   96.93   37.69   96.76   38.12   96.60   35.54   105   98.93   37.63   97.86   38.06   97.69   38.48   97.53   38.91   106   98.96   37.99   98.79   38.42   98.62   38.85   97.53   38.91   107   99.89   38.35   99.72   38.78   99.55   39.22   99.38   39.65   108   100.8   38.70   100.7   39.14   100.5   39.58   100.3   40.02   109   101.8   39.06   101.6   39.51   101.4   39.95   101.2   40.39   101.2   40.39   101.2   40.39   101.2   40.39   101.2   40.39   101.2   40.39   101.2   40.39   101.3   105.5   40.50   105.5   40.23   103.3   40.68   103.1   41.13   105.5   40.50   105.3   40.96   105.1   41.41   105.0   41.87   114   106.4   40.85   106.2   41.32   106   41.78   105.9   42.24   115   107.4   41.21   107.2   41.68   107.0   42.51   105.0   42.34   116   108.3   41.57   108.1   42.04   107.9   42.51   107.7   42.98   118   110.2   42.29   110.0   42.77   109   42.51   108.7   43.30   111.8   43.49   111.7   43.61   110.5   44.41   105.0   43.73   110.7   43.61   110.5   44.10   110.9   43.13   110.7   43.61   110.5   44.41   105.0   44.77   109   43.13   110.7   43.61   110.5   44.41   105.0   44.70   105.0   43.73   110.7   43.61   110.5   44.41   105.0   44.51   105.0	_								_
103									
106   98.03   37.63   97.86   38.06   97.69   38.48   97.53   38.91     106   98.06   37.99   98.79   38.42   98.62   38.85   98.45   39.28     107   99.89   38.35   99.72   38.78   99.55   39.22   99.38   39.65     108   100.8   38.70   100.7   39.14   100.5   39.58   100.3   40.02     109   101.8   39.06   101.6   39.51   101.4   39.95   101.2   40.39     110   102.7   39.42   102.5   39.87   102.3   40.32   102.2   40.76     111   103.6   39.78   103.5   40.23   103.3   40.68   103.1   41.13     112   104.6   40.14   104.4   40.59   104.2   41.05   104.0   41.50     113   105.5   40.50   105.3   40.96   105.1   41.41   105.0   41.87     114   106.4   40.85   106.2   41.32   106   41.78   105.9   42.24     115   107.4   41.21   107.2   41.68   107.0   42.15   106.8   42.61     116   108.3   41.57   108.1   42.04   108.9   42.88   108.7   43.36     118   110.2   42.29   110.0   42.77   109   43.35   109.6   43.73     119   111.1   42.65   110.9   43.13   110.7   43.61   110.5   44.10     110   112.0   43.00   111.8   43.49   111.7   43.9°   111.5   44.4°     10ep.   Lat.   Dep.   Lat.   Dep.   Lat.   Dep.   Lat.	103		36.91						
106   98.96   37.99   98.79   38.42   98.62   38.85   98.45   39.28     107   99.89   38.35   99.72   38.78   99.55   39.22   99.38   39.65     108   100.8   38.70   100.7   39.14   100.5   39.58   100.3   40.02     109   101.8   39.06   101.6   39.51   101.4   39.95   101.2   40.39     110   102.7   39.42   102.5   39.87   102.3   40.32   102.2   40.76     111   103.6   39.78   103.5   40.23   103.3   40.68   103.1   41.13     112   104.6   40.14   104.4   40.59   104.2   41.05   104.0   41.50     113   105.5   40.50   105.3   40.96   105.1   41.41   105.0   41.87     114   106.4   40.85   106.2   41.32   106   41.78   105.9   42.24     115   107.4   41.21   107.2   41.68   107.0   42.51   105.0   42.24     116   108.3   41.57   108.1   42.04   108.9   42.85   108.7   43.36     118   110.2   42.29   110.0   42.77   109.8   43.25   109.6   43.73     119   111.1   42.65   110.9   43.13   110.7   43.61   110.5   44.10     120   112.0   43.00   111.8   43.49   111.7   43.9   111.5   44.4     10ep.   Lat.   Dep.   Lat.   Dep.   Lat.   Dep.   Lat.								1 -	
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108         100.8         38.70         100.7         39.14         100.5         39.58         100.3         40.02           109         101.8         39.06         101.6         39.51         101.4         39.95         101.2         40.39           111         103.6         39.78         103.5         40.23         103.3         40.68         103.1         41.13           112         104.6         40.14         104.4         40.59         104.2         41.05         104.0         41.50           113         105.5         40.50         105.3         40.96         105.1         41.41         105.0         41.87           114         106.4         40.85         106.2         41.32         106 I         41.78         105.9         42.24           115         107.4         41.21         107.2         41.68         107.0         42.15         106.8         42.61           116         108.3         41.67         108.1         42.04         107.9         42.51         107.7         43.98           117         109.2         41.93         100.0         42.41         109.9         42.88         108.7         43.36           118 <td></td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td></td> <td></td>						_			
101.8   39.06   101.6   39.51   101.4   39.95   101.2   40.39   102.7   39.42   102.5   39.87   102.3   40.32   102.2   40.76   101.1   103.6   39.78   103.5   40.23   103.3   40.68   103.1   41.13   102.5   40.50   105.3   40.96   105.1   41.41   105.0   41.87   114   106.4   40.85   106.2   41.32   106   1   41.78   105.0   42.24   115   107.4   41.21   107.2   41.68   107.0   42.51   106.8   42.61   116   108.3   41.97   109.0   42.41   108.9   42.88   108.7   43.36   118   110.2   42.99   110.0   42.77   109.8   43.25   109.6   43.73   119.1   111.1   42.65   110.9   43.13   110.7   43.61   110.5   44.10   120   120   43.00   111.8   43.49   111.7   43.9%   111.5   44.47   109.0   42.51   10.50   44.77   109.8   43.25   109.6   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.10   110.5   44.51   10.5   44.10   110.5   44.51   10			38.70		-				
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114   106.4   40.85   106.2   41.32   106   41.78   105.9   42.24   115   107.4   41.21   107.2   41.68   107.0   42.15   106.8   42.61   116   108.3   41.57   108.1   42.04   107.9   42.51   107.7   42.98   118   110.2   42.29   110.0   42.77   109.8   43.25   108.7   43.36   110.1   42.65   110.9   43.13   110.7   43.61   110.5   44.10   120   112.0   43.00   111.8   43.49   111.7   43.9   111.5   44.4   111.5   44.5			40.50	105 3					
115   107.4   41.21   107.2   41.68   107.0   42.15   106.8   42.01     116   108.3   41.57   108.1   42.04   107.9   42.51   107.7   42.98     117   109.2   41.93   109.0   42.41   108.9   42.88   108.7   43.36     118   110.2   42.29   110.0   42.77   109.8   43.25   109.6   43.73     119   111.1   42.65   110.9   43.13   110.7   43.61   110.5   44.10     120   12.0   43.00   111.8   43.49   111.7   43.9°   111.5   44.4°     120   120   120   120   120   120   120     120   120   120   120   120   120   120     120   120   120   120   120   120   120     120   120   120   120   120   120   120     120   120   120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120   120     120   120   120   120   120   120   120     120   120   120   120   120   120   120     120   120   120   120   120   120   120   120     120   120   120   120   120   120   120   120   120     120	114	106.4	40.85	106.2	41.32	106 1	41.78	105.9	42.24
117   109.2   41.93   109.0   42.41   108.9   42.88   108.7   43.36   118   110.2   42.29   110.0   42.77   109.8   43.25   109.6   43.73   119   111.1   42.65   110.9   43.13   110.7   43.61   116.5   44.15   120   112.0   43.00   111.8   43.49   111.7   43.9°   111.5   44.4°   44.4°   111.5   44.4°   111.5   44.4°   111.5   45.5°   30.5°   15.5			41.21		4 1 68			106.8	
118									
110   111.1   42.65   110.9   43.13   110.7   43.61   110.5   44.15   120   112.0   43.00   111.8   43.49   111.7   43.9%   111.5   44.4%   111.5									
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ŕ	E1 0'   15'   30'   45'									
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1	100	Lat	Dep.	Lat	Dep.	Late	Dep.	Lat	Dep	
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ı	3	2.78	1.12	2.78	1.14	2.77	0.77	2:77	2.15	
ľ	4	3.71	1.50	3.70	1.51	3.70	1.53	3.69	1.55	
ı	5	4.64	1.87	4 63	1.89	4.62	1.91	4.61	1,93	
ı	6	5.56	2.25	5.55	2.27	5-54	2.30	5.53	2-32	
ı	7 8	7-42	3.00	7.40	3.03	7-39	3.06	7.38	3.09	
ı	9	8.34	3-37	8.33	341	8.31	3.44	8.30	3-48	
ĸ	10	9.27	3.75	9.26	3.79	9.04	3.83	9.22	3.87	
ľ	11	10.20	4.12	10.18	4-17	10.16	4.21	10.14	4-25	
ı	12	11.13	4.50	11.11	4-54	11.09	4-59	11.07	4.64	
ı	13	12.05	5.24	12.03	5.30	12.01	4-97 5-36	11.99	5.03	
ı	15	13.91	5.62	13.88	5.68	13.86	5.74	13.83	5.41	
R	16	14.83	5.99	14.81	6.06	14.78	6.12	14.76	6 19	
1	17	15.76	6.37	15.73	6.44	15.71	6.51	15.68	6 57	
1	18	16.69	6.74	16.66	6.82	16.63	6.89	16 60	6,96	
ı	19	18,54	7.12	17.59	7.19	17-55	7.27	18.44	7.35	
ı	21	-	7.87	-	7-95	19.40	8.04		8.10	
ı	22	19.47	8.24	19.44	8.33	20.33	8.42	19.37	list.	
ı	23	21 33	8.62	21.29	8.71	21.25	8.80	28.21	8.89	
ı	24	22.25	8.99	22.21	9.09	22.17	9.18	22-13	9/25	
ı	25	23.18	9.37	23.14	9.47	23 10	9.57	23.06	9.67	
ı	26	24.11	9.74	24 06	9.54	24-02	9.95	25.98	10.05	
ı	27	25.03	10.11	24.99	10,60	24.94	10.33	24.90	10.83	
ı	29	26.89	10.86	26.84	10.98	26.79	01.11	26.74	11,21	
ı	30	27:82	11.24	27.77	11.36	27.72	11.48	27.67	11,60	
ı	31	28.74	11.61	28.69	21.74	28.64	11,86	28.59	11.99	
ı	33	29.67	11.99	29.62	12.50	29.56	12.25	29.51	12:37	
ı	34	30.60	12.74	30 54	12.87	30.49	12.63	30.43	13.15	
ı	35	32.45	13.11	32.39	13.25	32-34	13.39	32 28	13.93	
R	36	33.38	13.49	33-32	13.63	33.26	13.78	33.20	13-91	
В	37	34.31	13.86	34.25	14:01	34.18	14.16	34.12	14.31	
ı	38	35.23	14.24	35-17	14-39	35.11	14-54	35.04	14.69	
ı	40	36.16	14.61	35.10	15.15	36.96	14.92	35.97 36.89	15:08	
R	41	38.01	15.36	37-95	15.52	37.88	15.69	37.8#	15.86	
R	42	38.94	15.73	38.87	15.90	38.80	16/07	38.73	16:24	
H	43	39.87	16.11	39.80	16.28	39-73	16.46	39.65	16.63	
H	44	40.80	16.48	40.72	10,66	49.65	16.84	40.58	17:02	
ı	45	41.72		41.65	_	41.57		41.50	17-40	
П	47	43.58	17.23	43.50	17.42	42.50	17.60	43.34	17.79	
ı	48	44.50	17.98	44.43	18.18	44-35	18.37	44.27	18.56	
ı	49	45-43	18.36	45.35	18.55	45.27	18.75	45.19	18.95	
Ą	50	46.36	18.73	46.28	18.93	46.19	19.13	46.13	19.34	
ı	51	47.29	19.10	47.20	19.31	47 12	19.52	47-03	19.72	
-	53	48.21	19.48	48-13	20.07	48.04	19.90	47-95	20.40	
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117	108.5	43.83	107.3	44.30	10%.1	4	10" 0	5
118		44.20	109.2	14 68		45 16	1.05.5	(4 - 4 - )
1119	110.3	44.58	110.1	45 06		45.54	1.39	10 13 1
120	111.3	44.95	111.1	45.44	115.4	15.00	11111-	1, 7, 1
1	1) p.	Lat	Dep	1.	1) 1	• • •	11.11	[11]
ا نخ	1 0	· ]	4.			<del>,</del>	1.	
1 9	<u>'</u>							
			67	DEGRI	565.			

	30 28 DEGREES.									
12	. 04	,		) <i>/</i>		)′	4.5	51		
Dist.	lai.	1). p.	l.a	Dep.	Lat	Dep.	l.a'	lki		
-	0.62	0.39	0.42	0 39	0.42	0.40	0.92	0.40		
2	1.84	i 5 "8	I 1.8.4	2.79	1.83	0.80	1.83	0.81		
3	3 68	1.17	2.76	1.13	1 2.75 1 3 6~	1.25	3 66	1.21		
1 +	1 300	1.56	3.65	1.58	4.59	1 49	4 58	2 C 1		
1	.1	2.34	5.51	2.37		2.39	5-49	2.42		
0	6.44	2 14	6.43	2.76	6.42	2.79	6.41	2. 2		
7 8	7.75	3.13	7.35	3.16	7.34	3 9	7.32	3		
9	8 28	3.52	8 27	3.55	8.25	3.59	8.24	3.6		
10	9.21	3.91	4 19	3.95	<u> </u>	3.99	9.15	45.		
11	15.13	4.3	10.11	. 4 34	10.69	+ 39	15.07	4.4,		
12	11.0; ":011	5.5%	11.53	++	11.92	4.~9 5.18	10.98	4.8 <sub>5</sub>		
1;	12.89	1 5 -	12 %	5.13	12 14	5.58	12.51	5.64		
15	1 1 3 8 1	5.86	138	5 92	13.76	5.48	13.73	6 04		
10	14.73	6.25	140	6.32	14.67	6.38	14.65	6 44		
15	15.65	6.54	15 02	6.71	15-59	6.78	15.56	6.85		
15	10.57	7 03	16 54	7.11	16.51	7.18	16.48	7.25		
1,3	18.41	7.42	17.46 18 38	7.50	17.42	7.58 7.98	17.39	7.65 8.05		
20		8.21		8.29						
21	19.33	8.60	19.29	8 68	19.26 20.18	8.37 8.77	19.22	8.46 8.86		
22 23	21 17	8.99	21 13	9.58	21,09	9.17	21.05	9.26		
24	22 09	9.38	22.05	9.47	22,01	9.57	21.97	9.67		
25	23.01	9.77	22.97	9 87	22.93	9.97	22.88	10.07		
26	23.93	10.16	23.89	10.26	23.84	10.37	23.80	10.47		
27	24.85	10 55	2.1.81	10.66	24.70	10.77	24.71	10.87		
28	25.7	10.94	25.73	11.05	25.68 26.59	11.16	25.63	11.28		
29 57	27.62	11.72	27.56	11.×4	27 51	11.96	27.46	12.08		
31	28.54	12 11	28.48	12.24	28.43	12.,6	28.37	12 49		
32	29.45	1350	20.40	12 63	20.35	12.76	29.29	12.89		
3;	\$5.58	12.89	3 - 32	13.63	30.20	13.15	30.21	13.29		
3 !	31.30	13.25	31.24	13.42	31.18	13.56	31.12	13.69		
1-3-	32.22	13 (8	32.16	13 82	32 10	13.96	3204	14.10		
33	33.14	14.0= 14.46	3,50	14 21	33.01	14 37	32 95	11.70		
3" 3'3	34.56 34.98	14.85	34.00	14.61	33.93	14.75 15.15	33.87	1.4 90 15.50		
39	3, 40	15.24	33.83	15.40	35.77	15.55	35.70	15.71		
4.5	36.82	15.63	56.75	15.79	30 68	15.95	36.61	16.11		
41	37,74	15.04	3".67	10.15	37.60	10 35	37 53 j	16.51		
42.	7, 00	10.41	35 59	16.58	38 52	16.75	38.44	16.92		
13	33.58	16.50	39.31	16 97	30 43	17.15	34.36	17.32		
44	41.42	17 58	43.43	17.70	42.35	17-54 17-94	45.27	18.12		
140	، نین ' ـــ 4 ز. 2 ئ	17 97	42.26	18.16	42.18	13 34	42 10			
	43 26	18.30	47.48	18.55	43.10	184	43.02	18.55 18.93		
45	41.15	18.76	44.10	18.95	44 52	19.14	43.93	19 33		
4.	45 13	19 15	45.02	19.34		19.54	44.85	19.73		
32	<u> </u>	19.54	_45.94	10.";	45 85	19 1/4	45	23 14		
5.1	46.65	14.95		25.13		25 34		20.54		
52 53	45.79	20.72	27.78 48.73	20.53	47 hg	20 74 31 13		20 (4 31 32		
54	49.71	21 15	1, 01	21 32		213		21.35		
_55	5.0;	26.54	5- 33	11.71		21.03		22.15		
50	51.55	218	`;i.·; !	22 11		22 ;3		22.55		
5-1	52.47	22.77	5 3.57	22.50	; 2. 2	2 2.1 3	52.17	22.1.6		
38	53.39	22.00	57:4	22 95		23.13		23.36		
i9 (-3	54.31	23.55 1 23.44 1	54.21   53.13	23.29 23.68		23.53		23.16		
	55.23	1.at.	25.13 Dep.		55 02 Dep.	23.92	54.92 Dep.	24.10		
ä	Dep 1	'	' -'	1 mt	_ '	Lat.		Lat.		
<u> </u>	Ū		45.	NECTO	504	'	15			

7	1 15/				1 3	0'	45'	
1 2	Lat	Dep.		D-p.	Lat	Dep.	Lat	' ⊢D.
61	56 15	23.83	11	24.05	·			24.,
62	57 07	24.23	56.05	24.33	55.94	24 32 24.72	55.83	24.J
1 .,	57.99	24.62	57.88	24 87	57 77	25.12	57 66	25
61	58.91	25.01	51.80	25.26	58.69	25.52		125.8
75	60.75	25.40	59.72	25.66	59 61	25.02	59.50	26.18
66	61.67	25.79 26.18	61 56	26.35	62.53 61.44	26.32 26.72	61 33	25 ja
68	62.59	26 57	61.48	26 84	62.36	27.11		27 ,
6.,	63.51	126.96	63.40	27.24	63.28	27.51	63.16	27 79
70	64.44	27 35	6433	27.63	64.19	27.01	64.07	28. : g
71 72	65. 0	127 74 124.13	66 15	28.03	65.03	28 31 28 71	64.79	29.05
1 -3	67.20	28.52	67 27	23.82	66.95	29.11	66.82	29.
74	58.12	28.91	67.99	29.21	6-86	29.51	67.73	29.80
75	69.51	29.30	68.91	29.61	6×8	29.91	64.6	30.21
76	69 96	29.70	69 83	3	69 "0	30 30	69,6	356
78	71.85	30.48	70.75 71 <b>.</b> 67	30.40 30.79		30.70 31.10	∻3.48   7139 }	31.4β1
-9	72.72	30.87	72,8	31.18	72 45	31.50	72.31	31 52
85	73.64	31.26	73.50	31.58	73.56	31 90	73.22	32
81	74 56	31.0,	74-42	3197		32.30	74.14	32.62
82 33	75.46	32.04	75.34 76.26	32.76		32.70   33.10	- 1	33.43 33.43
84	77.32	32.82	77.18	33.16		33.49		33.83
85	78.24	33.21	78.10	33-55	77.95	33.89		34.23
×6	79 16	33.60	79 32	33.45		34.29	78.72	3+0+
87 88	80.08	33 99	79.93	34-34		34.09		35-74
89	81.92	34.38 34.78	81.77	34.74		35.29   35 49	81.55	35.44
93	82.85	35 17	82 69	35.73		35.89		6. 25
1-11	83.77	35.56	83 61	3 ,.92	83.	30.24	13.29	36.65
92	84.69	35.95	84.53	36.32		36.68		37.55
93	85 61 86 53	36.73	85 45 86.37	36.71		37 28   37 48		37.40 37. 0
94 95	87 45	37 12	87.29	37.50		37.88		33 26
96	88.37	37.51	88.20	37.90		38.28		36 66
97	89.29	37.90	89.12	38.29		38.68		39.37
98	90.21	38.29 38.68	90.04	38.68 39.08		39.4%   39.4%		39·47 39·87
199	92.05	39.07	92.96	39.47		39.87	91.53	13.27
131	92.97	39 40	y2 to	39.87		13 27		10 6%
102	93.89	39.85	93.72	<b>4</b> 5.20		2 67	93.36	11.08
103	94.81	13.25	94.64	40.66		11.07		41.48
104	95.73 96.65	40.64 41.03	95.55	41.45		\$1.47 \$1.87		41 89   42.29
136	97.57	<del>11.42</del>	97.39	41.84		12.27	<del></del> ,	12.60
107	98.49	41.81	98.31	42.24		2.07		43.09
108	99.41	42.20	99.23	42 63	9904 .	\$3.07	1	دې.ډې
113	100.3	42.59 42.59	100.1	43.03 43.42		13.46 13.86		43.93 44.30
	102.2			43.82		14 26	101.6	
112		43 37 43 76		44.21		44 66	102.5	
1 3	101.0	14.15	1038	4461	103.6	\$5.06	103.4	45.71
114	104.9	44 54		45.00	104.5	15.46		17.91
115	105.9	14.93		45.40		15:86		46.73
116	105.8	45.32		45.79		16.25   16.65		47.12
118		46.11		46.58		7.05	108.0	47·56
119		15.50		46.97		7 45		47.93 1
120	110.5	16.89		<del>47 37</del>		17.85		48.33
ă	D p.	laiat.	D p 1	List.	1)cp	lat.		Lat.
<b>.</b> 5			45'		30'		15	

132				1 /د 1 30′				
Dist	0/			<b>'</b>	30	)'	45	
1 5 1	Lat.	Dep	Lat.	Dep.	Lat.	De.	List.	1:-p.
1	0.91	0.41	0.91	041	0.91	0.41	0 91	U.42
1 2	183	0.81	1.82	082	1.82	083	1.82	0.14
3	2.7.4	1.22	2.7+	1.23	2.73	1.24	2.72	1.20
4	3.65	1.63	3.65	164	3 64	1.66	3.63	1.67
5	4-57	2.C }	4.56	205	4.55	2 07	4.54	2.09
6	5.48	2.44	5-47	2.46	5.46	2 49	1 45	2.,1
7	6.39	2.85	6.38	2.88	6 37	2.90	6 36	2.93
8	7.31	3.25	7.29	3.29	7.28	3.32	7.27	3.55
9	8 2 2	3 66	8.21	3.70	8.19	3 ~ 3	8.17	3
10	914	4.07	9 1 2	4.11	9.10	4.15	9.08	4.1.
11	10.05	4.47	10.03	4.52	10.01	4.50	9 99	, 4.6.1
12	10 yń	4.58	10.94	4.93	10.92	4.98	10.93	5.02
13	11.58	524	11.85	5 34	11.83	5 9	11/91	5.4
14	12.79	5.69	12 -6	5.75	12 74	5.51	12.71	5.55
15	13.70	6.10	13.68	6.16	13.65	6.22	13.62	6.2
16	1462	651	14.59	6 5	14,6	6 64	14.53	6.0
17	15 53	6.41	15.50	6 98	15.47	7.05	15 44	7.12
18	16.44	7.32	1641	7 39	16 38	7.46	. 16.35	7-54
19	17 36	73	17.32	7.80	17 29	7.88 8 2 y	17.25	7.95
20	:8.27	8.13	15 24	8.21	18 50		18.16	8.37
21	19.18	8.54	19 15	5.63	19 11	871	19.07	8.79
22	20.10	8.95	20.06	9.04	20 02	9 12	1 y.y8 20 8 y	9.21
23 24	21.03	9.35	20.97	9.45 9.86	20 93 21 84	9.54	21.80	9.63
25	22 84	10.17	22.79	10.27	22.75	10.37	22 70	10.47
16	23.75	10.58	23.71	10 68		10 78		10 8y
20	24 67	10.98		11.00	23 66	11.20	23.61 24.52	11.30
28	25.58	11.39	25 53	11.50	24 57 25.48	11.61	i 25.43	11.72
29	26 49	11 80	26 44	11.91	26.39	1203	26.34	12.14
35	27.41	12 0	27.35	12 32	27 30	12.44	27.24	12 56
3	25 32	1261	28.26	12.73	28 21	12.86	28.15	12.98
3:	2., 23	13.02	29.18	13.14	29 12	13.27	29 00	13.43
33	35.15	13.42	ود هٔ ا	13.55		13.68	29.5	13 02
34	31.06	13.83	31.00	13.96	30 94	14 10	30 88	14.23
_35	31.07	14.24	31-41	14 35	31.85	14.51	31 78	1404
35	, ; 2 89	14.64	32.82	14.59	3: 6	14 93	32 00	15 57
37	338	15.65	33-4	1; 25	376-	15.34	33.60	15.49
38	34 "1	15.46	3100	1,61	34.54	15.76	34.51	15.41
34	35.63	15.80	35.56	16.03	35.44	10.17	35-42	10.33
4.	30.54	16.27	3': 47	10 43	36.40	16.59	36.55	10.73
.:1	37.46	16.68	3" 3	10.1	37 31	1705	3 .23	17.15
42	38 37	17.08	\$8.29	17.25	38.23	17.42		17.55
43	39.28	17 (9	39.21	17.06	39.13	17.53	39.05	18.00
44	40 20	17 93 18 (3	1 42 '2	18.07	40.01	18.24	39 90	12.42
			41.03	18 48	40 95	15.56	4	12.74
10	42.52	18 71	41 44	11 No	41.50	19.25	41.77	14, 25
48	47.94	19.12	42 35	14.35	<b>→</b> 77	Ly.ag	42 (8	19.58
49	1.15	19.42	43 -6	19 7 1	-(3.45	19.91 20.32	43.59 44.50	20.10 20.51
15	4	20.34	45.50	20 51	44-59	2 .73	44.72	2 3
52	1 7 34	25.74	41.50	20 65	46 4 i 47.32	21 15	45.52	21
53	41 42	21.59	4 11 4 2	2	41.23	21.98	47.22	21.77
	4. 33	21.50	49 24	22.18	40.14	22.34	49.34	2 3 3 4
		2: ;-	59.15	22 59	50 ° ;	32.81	49.4	2
-,-	51.	32.73	31.66	23 0	55 90	2; 22	<b>5</b> 0 6	<u></u>
5	52 27	23 18	51 97	23.41	51.07	23.64	51.70	2 0
1.58	\$2.59	23.59	52.55	2,.82	52.77	24.0	52 67	24 25
5.3	3.45	1.0	53.79	2 3	5:47.	34.47	43.48	2.4
	5181	14.0	5001	2.1	415	25.25	54.49	2 12
1 - 1	170	1!	- i - i	1		T. t.	Ta,	: l
1 5			-· .	,			1.5	
-			.,	Lare Ta			4.,	1

			24	DEG	REES. 13				
Dia	0	,	11	5'	, 3	io'	, 4	51	
-	Lat	d. ()	Lat.	Dep	Lat.	Dep	Lat.	Dep.	
61	55.73	2.4.81	55.62	25.05	55-51	25.30	55.40	25.54	
62	56 64	25.22	; 56.53	25.46	56.42	25.71	56 30	25.96	
63	57-55	25.62 26.03	57-44	26.20	57.33	26.13	57.21	26.38	
65	58.47	26.44	53.35	26.70	58 24	26.54 26.96	58.12	26 79 27.21	
66	60 20	26 84	60.18	27.11	60.06	27.37	59.94	27.63	
67	61.21	27.25	61.09	27.52	60.97	27.78	60.85	28.05	
68	62.12	27.66	62.00	27.93	61.88	28.20	61.75	28.47	
79	63.95	28.26	62.41	28.34	62.79	28.61	62.66	28 89	
1	61.86	28.86	63.82		63.70	29 33	63.57	29 31	
71 72	6;.78	29.23	64.74	29 16	64.61	29.44 29.86	64.48	30.14	
73	66.59	29.69		29.98	66.43	30.27	66.29	30.56	
74	67.60	30 13	67.47	30.39	67 34	30.69	67.20	30.98	
75_	68 54	20.51	68.38	30.80	68 25	31.10	68 11	31.40	
70	69 43	30. 1	69.29	31.21	69.16	31.52	69.02	31.82	
77 78	70.34	:31.32 : •73	70.21	31.63	70.07 70.98	31.93	69.93 70.84	32.24 32.66	
79	72 17	32.13	72.03	32.45	71.89	32.76	71.74	3,.07	
85	73.08	32.54	72 94	32.80	72.80	33.18	72.65	33.49	
81	74.00	32 45	73.85	33-27	73 71	33.54	73 55	33.91	
82	7491	33 35	74.76	33.68	7462	34.00	74-47	3+33	
83 84	75.82 76.74	33 76	75 68	34.09	75.53	34.42	75.38	34.75	
85	77.65	34 17 34-57	76.59 77.50	34.50 3491	76.44 77.35	34.83 35.25	76.23 77.19	35-17	
86	78.56	34 48	78.41	35.32	78.26	35.06	78.10	30.00	
87	79.48	35.39	79.32	35.73	79.17	36.08	79.01	36 42	
88	80 39	35 79	80 24	36.14	80 08	36.49	79.92	36.84	
89	81.31	36.20	81.15	36.55	80 gy	36.91	80 82	37 26	
90	82 22	36.61		36 96	81.90	37.32	81.73	37.68	
91 92	83.13	37.01		3: 38 37 79	82.81	37·74 38.15	82 64 83.55	38.10 38.52	
93	84 96	37 83		38.20	84.63	38.57	84.46	38.94	
94	85.87	38.23	85.71	38.61	85.54	38.48	85.37	39.35	
95	86.79	38.64	86.62	39.02	80 45	39.40	86.27	<u>39·77</u>	
96	87.70	39.05	87.53	39-43	×7.36	39.51	87.18	40.19	
97 98	88.61 89.53	39.45 39.86	88.44 89.35	39.54 40.15	80.27 89.18	40.64	88 og 89 oo	40 61 41 C3	
99	90.44	40.27		15 66		41.05	89 91	41.45	
100	91.35	40 67	91.18	417	ý i . <b>o</b> ó	41.47	95.Šī	41.87	
101	92.27	41.08	92 39	41.48	91.91	41.88	91.72	42.28	
102	93.18	11 49		41.89		42.30	92.63	42. 0	
103	94.10	41 89	93.91	42.71	93 73	43.71	93.54	43.12	
105	95.92	42.71		43.13	94.64	43.34	94 45	43·54 43·96	
106	96 84	13.11		+3-54	96.46	43.90	y6.16	44.38	
107	97.75	43.52	97.56	43.95	97.37	44.37	97-17	44.80	
108	98.66	43.93	98.47	44.36	98.28	44.79	98.08	45.22	
109	99.58	÷4-33		+4-77	99 19	45.20	98.99	45.63	
110	100.5	## #	1003	+5 18	100.1		99.90	40.05	
211		45.15	101.2	45.59 43.50	101.0	46.03 46.45	100.8	46.47 46.59	
113	103.3	45.90		46 41	101.6	46.86	102.6	47.31	
114	104-1	46 37	133.9	10.91	103.7	47 28	103.5	47 73	
115		46 77		+7.23	104 6	47.69	104.4	48.15	
116	106.0	47.18		47 04	105.6	48.10	105.3	48.56	
117	106.9	47.59 ; 48.00	100.7 107.6	48.05 48.46	106.5	48.52 48.93	106.3	48.98	
114	108.7	45.40	107.0	48.88		49.35	108.1	49.40	
120	109.6	40.61	109.4	49.29	109.2	49.76	109.0	50.24	
=	Dep.	Lish	Dep.	LaL	Dep	List.	Dep.	Lat	
Dist	0	,	451		30'		15	[	
					~				

7	0	1 0		1	5/	1 30	1	45'	
ļ	Dist.	Lat	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.
į	1	0.91	0.42	0.90	0.43	0.90	0.43	0.90	0.43
l	2	2.72	1.27	2.71	0.85	2.71	0.86 1.29	1.80	1.30
ı	3 4	3.63	1 1.69	3.62	1.71	3.61	1.72	3 00	1.74
۱	5	4-53	2.11	4.52	2,13	4-51	2.15	4.50	217
H	25	5.44	2.54	5.43	2.56	5.42	2,58	5.40	2-61
ı	7 8	7 25	3.38	6.33	3.41	7.22	3 01	7.21	3.04
ı	9	8.16	3.80	8.14	3 84	812	3.87	8.11	3.91
ı	13	9,06	4.25	9.04	4-27	9.03	4-31	9.01	4-34
ı	11	9.97	4.65	9 95	4 69	993	4-74	9.91	478
ľ	13	11.78	5.49	10.85	5.12	10.83	5.60	11.71	5.21
ı	14	12.69	5.92	12.66	5.97	12.64	6.03	12.61	6,08
ľ	15	13.59	6.34	13.57	6,40	13.54	6.46	13.51	6.52
Ī	16	14.50	6.76	14-47	6.83	14-44	7.32	14.41	0.95
ľ	18	16.34	7.61	16.28	7.68	15.34	7-75	16.21	7.39
	19	17.22	8.03	17.18	8,10	17.15	8.18	17.11	8 25
1	20	18.13	8.45	18.09	8.53	18.05	8.61	18.01	8,69
1	21	19.03	8.88	18,99	8.96 9.38	18.95	9 04	18.91	9.12
ı	23	20.85	9.72	20.80	9.81	20.76	9.90	20.72	3.30
ı	24	21.75	10.14	21.71	10.24	21.66	10.33	21.62	10:43
ı	25	22.66	10.57	22.61	10.66	22.56	10.76	22.52	10.86
ı	26	23.56	10.99	23.52	11.09	23.47	11.62	23.42	11.30
1	28	25:38	11.83	25.32	11.94	25.27	12.05	25.22	12.16
ı	29	26.18	12.26	26.23	12.37	25.18	12.48	25.12	12.60
ı	30	28.10	-	27.13		-	12.92	27.08	13.03
ı	31	29.00	13.10	28.94	13.22	27-98	13.35	27.92 28.82	13.47
ı	33	29.91	13.95	29.85	14.08	29.79	14-21	29.72	14:34
ı	34	30.81	14.57	30.75	14.50	30.69	14.64	30.62	14-77
١	35	31.72	14.79	31.66	14.93	31.59	15.07	31.52	15:21
ı	37	33.53	15.64	32.56	15.78	33.40	15.50	33-33	15.64
١	38	34-44	16 06	34-37	16.21	34/30	16.36	34-23	16.51
ı	39	35.35	16.48	35.27	17.06	35.20	17.22	35.13	15:94
ı	40	37.10	17-13	37.08	17:49	37.01	17.65	36.93	17.81
1	42	38.06	17.75	37.99	17.92	37.91	18.08	37.83	18.25
ı	43	38.97	18.17	38.89	18.34	38.81	18.51	38.73	18798
ı	44 45	39.88	18.60	39.80	18.77	39.71	18.94	39.63	19.12
ı	46	41.69	19.44	41.60	19.62	41.52	19.80	41.43	19.98
I	47	42 60	19.86	42.51	20.05	42.42	20.23	42.33	20.42
I	48	43.50	20.29	43.41	20.90	43,32	20,66	43.23	20.85
I	50	44.41	20.71	44.32	21.33	44-33	21.53	44-13	21.72
I	51	46.22	21.55	46 13	21.76	46.03	21.96	Mary Control	12.16
I	52		21.98	47.03	22 18	46.93	22.39	46.84	22.59
I	53	48.03	22.40	47.94	23.03	47.84	22.82		23.03
I	54	49.85	23.24	49.74	23,46	49.64	23.68		23.89
	56	50.75	23 67	50.65	23.89		24.11		14-33
	57	BLCOUNTS.	24.09	51.55	24.31	51.45	24-54	51.34	24.76
	58	52.57	24.51	52.46	24.74		24.97	53-14	15.20
1	60	54-38	25.36	54-27	25.59	54.16	25.83		26.07
A	St	Dep.	Lat.	Dep	Lat	Dep.	Lat.	Dep.	Lat.
L	Dist	0'		4.	5'	30	1-3	15	
			_			200		_	-

51	0' 1'				3	0'	45'		
Dist	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	
61	55.28	25.78	55-17	26.02	55.06	26.26	54.94	26.50	
62	56.19	26.20	56.08	26.45	55.96	26.69	55.84	26.94	
63	57.10	26.63	56.98	26 87	56.86	27.12	56 74	27 37	
64	58.00	27.05	57.89	27.30	57 77	27.55	57.64	27.80	
65	58.91	27.47	58.79	27.73	58.67	27.98	58.55	28.21	
116	50 82	27.89	59.69	28.15	59 57	28.41	59.45	28.67	
6-	60.72	28.32	60.60	28.58	60,47	28.84	60.35	29.11	
68	61.63	28 74	61.50	29.01	61.38	129.27	61.25	29-54	
69	62 54	29.16	62.41	29 43	62.28	29.71	62.15	29.98	
7.0	63.44	29.58	63 31	29 86	63 18	30.14	63.05	30.41	
-1	64.35	30.01	64.22	30.24	64.08	30.57	63.95	30.85	
72	65.25	30.43	65.12	30.71	64.99	31.00	64.85	31.28	
73	66.16	30 85	66.03	31.14	65.89	31.43	55.75	31.71	
74	67.07	31.27	66.93	31.57	66.79	31.80	66.65	32.15	
	67 97	31.70	-	31 99	67 69	32.29	67.55	32.58	
-6	64.88	32 12	68.74	32.42	68.60	32.72	68.45	33.02	
-7 -8	69.79	32.54	69.64	32.85	69.50	33.15	69.35	33-45	
79	70.69	32.96	70.55	33.27	70.40	33.58	70.25	33 89	
Xo	72.50	33.39	71.45	33.70	71 30	34.01	72.66	34.76	
81			-	3+13	_	-		-	
82	73.41	34.23	73.26	34-55	73 11	34.87	72.96	35.19	
83	74-32	34 65	74-17	34.98	74.01	35.30	73.86	35 62	
84	76.13	35.50	75 97	35.83	75.82	35.73	75.66	36.49	
85	77.04	35.92	76.88	36.26	76.72	36.59	76.56	36.93	
86	77.94	36.35	77.78	36.68	77.62	37 02	77.46	37.36	
87	78.85	36.77	78.69	37.11	78 52	37-45	78.36	37.80	
88	79.76	37 19	79.59	37-54	79.43	37.89	79.26	38.23	
89	80.66	37 61	80 50	37.96	80.33	38.32	80.16	38.67	
90	81.57	38.04	81.40	38.39	81.23	38.75	81.06	39 10	
91	82.47	38 46	82.71	38.82	82.14	39.18	81.96	39-53	
92	83.38	38 88	83.21	39 24	83.04	39.61	82.86	39.97	
93	84.29	39.30	84.11	39.67	83.94	40 04	83.76	40.40	
94	85.19	39.73	85.02	40.10	84.84	40.47	84.67	40 84	
95	86.10	40.15	85.92	40.52	85.75	40.90	85.57	41,27	
96	87.01	40.57	86.83	40.95	86.65	41.33	86.47	41.71	
97	87.91	40.99	87.73	41.38	87.55	41.76	87.37	42.14	
98	88.82	41.42		41.80	88.45	42.19	88.27	42.58	
99	89.72	41.84	89.54	42 23	89 36	42.62	89.17	43.01	
100	90.63	42.26	90.45	42 66	90.26	43.05	90.07	43.44	
101	91.54	42.68	91.35	43.08	91.16	43.48	90.97	43.88	
102	92.44	43.1 I	92.25	43.51	92.06	43.91	91.87	44.31	
103	93.35	43.53	93.16	43.94	92.97	44-34	92.77	44.75	
104	94.26	43 95	94.06	44.36	93.87	44.77	93.67	45.18	
_	95.16		94-97	44 79	94-77		94 57	45.62	
106	96.07	44.80	95.87	45.22	95 67	45.63	95.47	46 05	
107	96.97	45.22	96 78	45.64	96.58	46.06	96.37	46 49	
100	98.79	45.64	98.59	46.50	98.38	46.93	97.28	46.92	
110	99.69	46.49	99.49	46.92	99 28	47 36	99.08	47.79	
111		46.91				47.79	99.98	48.22	
112	101.5	47.33	100.4	47.78	100.2	48.22	100.0	48.66	
113	102.4	47.76	102.2	48.20	102.0	48.65	101.8	49.09	
114	103.3	48.18	103.1	48.63	102.9	49.08	102.7	49.53	
115	104.2	48.60	104.0	49.06	103.8	49.51	103.6	49.96	
116	105.1	49.02	104.9	49.48	104.7	49.94	104.5	50.40	
117	106.0	49.45	105 8	49.91	105.6	50.37	105.4	50.83	
118	106.9	49.87	106.7	50.34	106.5	50.80	106.3	51.26	
119	107.9	50.29	107.6	50.76	107.4	51.23	107.2	51.70	
120	108.8	50.71	108.5	51.19	108.3	51.66	108.1	52.13	
4	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	
Dist	0			5'		u' -		131	
-				-		-	1		

94 DEGREES.

Dist	1 0		F 1	51	1 30	01	. 43	1
87.	Lat.	Dep	Lat.	Dep.	Lau	Dep.	Lat-	Dep
1	0.90	0.44	0.90	0.44	0.89	0.45	0.89	0.45
3	2.70	0.88	2.50	1.33	2.68	0.89	2.68	0.90
4	3.60	1.75	3.59	1.77	3.58	1.78	3.57	1.80
5	4.49	2.19	4.48	2,21	4-47	2,23	4.46	2.25
6 7	5 39	3.07	5.38	3.10	5.37	3.12	6.25	3.15
7 8	7.19	3.51	7-18	3.54	7.16	3.57	7.14	3.60
10	8.09	3.95	8.97	3.98	8.05	4.02	8.04	4.05
11	8,99	4.38	9.87	4.87	9.84	446	9.82	4.50
12	9.89	4.82 5.26	10.76	503X	10.74	5.35	10.72	4-95 5-40
13	11.68	5.70	11.66	5.75	11.63	5.80	11.61	5.85
14	12,58	6.14	12.56	6.63	12.53	6.25	13.39	6.30
16	14.38	7.01	14.35	7.08	14.33	7-14	14.29	7.10
1 17	15,28	7.45	15.25	7.52	15.21	7.59	15.18	7.65
18	16.18	7.89	17.04	7.96	17.00	8.03	16.07	\$ 10
19	17.08	8.33	17-94	8.85	17.90	8.92	17.86	9.00
21	18,87	9.21	18 83	9.29	18.79	9.37	18.75	0.45
22	19:77	9.64	19.73	9-73	19.69	9.87	19.65	9.90
23	20,67	10.08	20.63	10.17	20.58	10.16	20,54	10.15
25	22.47	10 96	22,42	11:06	22.37	11.15	21411	Y 1425
26	23-37	11.40	23.32	11.50	23.27	11.60	23.22	11.70
28	24.27	11.84	24.22	11.94	25.06	12.05	25.00	12.15
29	26.07	12.71	26.01	12.83	25 95	12.94	25.90	13.05
30	2 6.96	13.15	26.91	13.27	26.85	13.39	26.70	13.50
31	27.86	13.59	27.80	13.71	27.74	13.53	27.68	13.95
33	28.76	14.03	29.60	14.60	29.53	14.72	29.47	14-40
34	30.56	14.90	30.49	15.04	30.43	15.17	39.36	15.30
35	31,46	15.34	31.39	15.48	31.32	15.62	31,45	15.75
36	32.36	15.78	33.18	15.92	32.22	16.06	33.04	16.00
38	34-15	16.66	34 08	16.81	34.01	16.96	33.93	17-10
39	35.05	17.10	34.98	17.25	34.90	17.40	34.83	17.55
40	35.95	17.53	36.77	18.13	36.69	18/29	35-72	18.46
42	37-75	18.41	37.67	18,58	37-59	18.74	37-51	(8.ga
43	38.65	18.85	38.57	19.02	38.48	19.19	38.40	18-35
44	39 55	19.73	39.46	19.46	39.38	20 08	39.29	19.10
46	41.34	20.17	41.26	20.35	41.17	20.53	41.08	20.70
47	42.24	20.60	42.15	20.79	42.06	20.97	41.97	21 05
48	43-14	21.04	43.05	21.23	43.85	21.42	45.76	21 60
50	44-94	21.92	44.84	22,11	44.75	22.31	44 65	12-50
51	45.84	22.35	45.74	22,56	45.64	21.76	45-54	22.95
52		22.80	46.64	23,00	46.54	23.20	40.43	芸芸
53		23.23	47.53	23 44	47-43	24.09		23-16 24-31
55	49.43	24.11	49.33	24.33	49.22	24-54		14.76
56	50.33	14-55	50.22	24.77	50.12	24.99		15.21
57		24.99	51.12	25.65	51.91	25.88		26.11
59	53.03	25.86	52.92	26.10	52.80	26.33	52.69	18.56
	53.93	26.30	53.81	26.54		26.77	53.58	27.01
Dist.	Dep.	Lat	Dep.	Latie	Dep.	Last	Dep.	Lan
9	. 0	-	45	DECHE	30	200	150	

9	0/	,	14	,	30	0/	4.5	7					
Dist	Lat.	Dep.	Lat.	D~p.	Lat.	Dep.	Lat	Dep					
61	54.83	26.74	54.71	26.48	5+59	27.22	54-47	27.46					
62	55.73	27.18	55.61	27.42	55.49	27.66	55.36 56.26	27.91					
64	56.62 57.52	27.62	57 40	27.86 28.31	56.38 57.28	28.56	57.15	28.81					
65	58.42	28.49	58.30	28.75	58.17	29.00	\$8.04	29.26					
50	59 32	28.93	59.19	29 19	59.07	29.45	58.94	2).71					
07	60.22	29.37	60.09	29.63	çy y6	29.90	59.83	30.16					
68	61.12	29.81	60.99	30.08	60.86	30.34	61 62	30.61					
69 70	62 02	30 25 30 64	61.88	30.52 30.96	61.75	! 30.79 ! 3 1.23	6251	31.51					
71	62.92	31.12	63.68	31.40	63.54	31.68	63 40	31.46					
72	64.71	31.56	64-57	31.84	64.44	32 13	64.29	32.41					
73	65.61	32.00	65.47	32.29	65 33	32.57	65.19	32.86					
74	66.51	32.44	66.37	32.73	66.23	33.02	66.08	33 31					
75	67.41	32 88	67.27	33.17	67.12	33.46	66 97	33.76					
76	68.31	33.32	68.16	33.61	68.02 68.91	33.91 34 36	67.87 68.76	34.21					
77 78	70.11	33.75	69.06 69.96	34.06 34.50	69.80	34.80	69 65	35.11					
79	71.00	34.63	70.85	34-94	70.70	35.25	70.55	35 56					
80	71.90	35.07	71.75	35.38	71.59	35.70	71.44	36.01					
81	72.80	35.51	7265	35.83	72 49	36.14	72.33	36.46					
82	73.70	35.95	73-54	36.27 36.71	73-38	36.59	73.22	30 y1 37 35					
83 84	74.60	36.38 36.82	74·44 75·34	37.15	74-28	37.48	7501	37.81					
85	76.40	37.26	76.23	37.59	76.07	37.93	75.90	38.26					
86	77 30	37.70	77.13	38.04	76.96	38.37	76.80	38.71					
87	78.20	38.14	78.33	38.48	, ,	38.82	77.69	39 16					
88	79.09	38.58	78 92	38.92	78.75	39.27 39.71	78.58	39.61					
89 90	79 99 80.89	39.01 39.45	79.82 80.72	39.36	79.65 80.54	40.16	80.37	40 51					
91		39.45	81.62	40.25	81.44	40.60	81.26	40.96					
91	81.79 81.69	40.33	82.51	40.69	82 33	41 05	82.15	41.41					
93	83.59	40.77	83.41	41.13	83.23	41.50	83.05	41.86					
94		41.21	84 31	41 58	84.12	41.94	83.94	42.31					
95	85.39	41 65	85.10	42.02	85.02	42.83	84.83	42.76					
96	86.28	42.08	86.10	42.46	85.91 86.81	43 28	85.73 86.62	43.21 43.66					
97 98		42.96	87.89	43.34	87.70	43.73	87.51	44.11					
99	88.98	43.40		43.79		44-17	88.40	44.56					
100	89.88	43.84	89.69	44.23	89.49	44.62	89 30	45.01					
101	90.78	44 28	90.58	44.67	90.79	.45.07		45.46					
102	9168	'44.71 ,45.15	91.48	45.11 45.56	91.28	45 51	91.68 91.98	45.91					
104	93.58	45.59	93.27	46 00	93.07	46 40	92.87	:6.81					
10;		46.03	94.17	46.44	93.97	46.85	93.76	1- 25					
106	95 27	46.47	95.07	10 88	94 86	47-32	44 66	47 7 !					
107	96.17	46.91	95.97	47.32	95.76	47 74 48.19	95.55	1 16					
108	97.07	47-34	96.86 97.76	47.77	96.65	18.64	95.44	48.61 19.06					
110	97.97 98.87	48.23	98.66	48.65	98 44	49.08	98.23	49.51					
111	99.77	¥8.66	99-55	49.09	99 34	49.53	99.12	49.96					
112	100.7	49.10	100 4	49.54	100.2	49.97	100.0	50.41					
113	101.6	49-54	131.3	49.98	101.1	50.42	100.9	50.80					
114	172.5	49.97	102.2	50 43 50 86	103.0	51.31	101.8	51.31					
115	103 4	50.41			103 8	51.76		11.76					
117	104 3	50.85	104.9	51.31 51.75	1047	52.21	103.6	52.21					
117	106.1	51.73	105.8	52.19	105.6	52.65	105 4	53.11					
119	107.0	52.17	106.7	52.63	106.5	, 3.10	106.3	1:7 55					
120	107.9	52 60	107.6	53.07	107.4	53.54	107.2	51.01					
Dist.	Dep	Lat	De p.	Lat	Dep.	, 1 <sup>-7</sup> f	Dep.	L					
	(	7	4.5	5/	30	<b>J</b>	1	j/					
3			63 DEGREES.										

-	0		15	5/	3	04	4.5	25
18)	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep
1	0.80	0.45	0.89	0.46	0.89	0.46	0.86	0.67
2	1.78	0.91	1.78	0.92	1.77	0.92	1.77	0.93
3	2.67	1.36	2.67	1.37	2.66	1.19	2.65	140
4	3.56	1.82	3.56	1.83	3-55	1.85	3-54	2-33
5	4.46	2.27	4.45	2.29	4-44	2 11	4:43	
6	6.24	3.18	5.33	3.21	6.21	3.23	6.19	3.16
7 8	7.13	3.63	7.11	3.66	7,10	3.69	7.08	3.72
9	8,02	4.09	8.00	4-12	7.98	4.16	7.96	4-19
10	8.91	4-54	8.89	4.58	8.87	4.62	8.85	4.66
110	9.80	4-99	9.78	5.04	9.76	5.08	9.73	5.12
13	10.69	5.45	11.56	5.49	10.64	5.54	10.62	6.05
14	12.47	6.36	12.45	6.41	11.42	6.46	12.39	6 52
15	13.37	6.81	13.34	6 87	13.31	6.93	13.17	6.98
16	14.26	7.26	14.22	7.33	14.19	7.19	1416	7-45
17	15.15	7.72	15.11	7.78	15.08	7.85	15.04	7.92
18	16 04	8.17	16.89	8.24	15.97	8.34	15.93	8.38
20	17.82	9.08	17.78	9.16	17.74	9.24	17-70	11.0
31	18.71	9 53	18.67	9.62	18.63	19.70	18.58	9.78
22	19 60	9.99	19.56	10.07	19.51	10.16	19.47	10.14
23	20.49	10.44	20.45	10.53	20.40	10.62	20.35	10,71
24	21.38	10.90	21.34	10.99	21.29	11.08	21.14	11.64
26	-	11.35	23.11	11.45	-	11.54	-	12-51
27	23.17	13.26	24 00	12.36	23.06	12.47	23.01	12.57
28	24.95	12.71	24.89	12.82	24.84	12.93	24.78	13.04
29	25.84	13.17	25.78	13.28	25.72	13.29	25.66	13.50
30	26.73	13.62	25.67	13.74	26.61	13.85	26.55	13.97
31	27.62	14.07	27.56	14.19	27.50	14.31	27-43	14-15
33	28.51	14-53	28.45	14-65	28.38	14.78	18.32	15:37
34	30.20	15.44	30 23	15.57	30.16	15.70	30.09	15.83
35	31.19	15.89	31.12	16.03	31.09	16 16	30.97	16.30
36	32,08	16 34	32.00	16.48	31.93	16.62	31.86	16.75
37	32 97	16.80	32.89	16.94	32.82	17.08	32.74	17-23
38	33.86	17.25	33.78	17-40	33.71	17.55	33-03	17-59
40	34.75	18.16	35.56	18.32	35.48	18.47	35,40	18.61
41	36.53	1861	36.45	18.77	36.37	18.93	36.28	19:59
42	37-42	19.07	37-34	19.23	37.25	19.39	37.17	19.55
43	38.31	19.52	38.23	19.69	38.14	19.86	38.05	20.02
44	39.20	19.98	39.12	20.15	39.03	20.78	38.94	20.49
46	-	20.88	40.89	21.06	40.80		40.71	21.42
47	40,99	21.34	41.78	21.52	41.69	21.24	41.50	21.83
48	42.77	21-79	42.67	21.98	42.58	21.16	42.48	11.35
49	43-66	22.25	43.56	22.44	43.46	12.63	43.36	22.82
50	44.55	22-70	44-45	22.89	44-35	23.09	44.25	13.28
51	45-44	23.15	45.34	23.35	45.24	23.55	45.13	93.75
52	45.33	24.06	46.23	23.81	46.12	24.01	46.90	24.21
54	48.11	24.52	48 01	24.73	47.90	24.93	47-79	25.14
55	49.01	24 97	48.90	25.18	48.79	25.40	48.67	24.61
56	49.90	25.42	49.78	25.64	49.67	25.86	49.56	26.07
57	50.79	25.88	50.67	26.10	50.56	20.32	50.44	26.54
50	51.68	16.33	51-56	26.56	52.33	26.78	51/33 52.0f	27-47
59	53.46	27.24	53 34	27-47	53.22	27.70	53.10	27-04
20	Dep.	Lat	Dep.	Lat.	Dep	Lat	Dep.	Lat-
Dist.	0			31	30	the second		51
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64   56.13   28.60   56.21   28.85   29.29   55.75   29.33   57.02   29.06   36.90   29.30   56.77   29.55   50.64   19.50   66.5   57.92   29.51   57.79   29.76   57.66   30.01   57.52   30.70   66.5   57.92   29.51   57.79   39.76   57.66   30.01   57.52   30.70   67.50   30.87   59.56   30.68   50.29   30.87   59.56   30.68   50.29   30.87   59.56   30.68   50.29   30.87   50.45   31.14   60.53   31.43   60.13   31.50   61.48   31.33   61.34   31.59   61.20   31.85   61.66   32.13   61.34   31.59   61.20   31.85   61.66   32.13   61.34   31.59   62.23   12.25   62.20   32.23   61.95   32.75   62.00   32.72   61.95   32.75   63.03   33.60   61.70   33.88   63.56   63.70   33.60   65.01   31.41   60.92   31.42   61.95   32.70   63.70   33.60   65.01   31.42   61.95   32.70   63.70   33.60   65.01   31.42   61.95   32.70   63.70   33.60   65.01   31.42   61.95   32.70   63.70   33.60   65.70   33.88   66.50   33.60   65.70   33.88   66.50   33.60   65.70   33.88   66.50   33.60   65.70   33.88   66.50   33.60   65.70   33.89   66.50   33.60   65.70   33.89   66.50   33.60   65.70   33.89   66.50   33.60   65.70   33.89   66.50   33.60   65.70   33.89   66.50   33.60   67.70   67.60   67.72   34.50   67.70   35.80   68.30   35.65   60.14   33.70   69.50   33.81   69.30   35.85   69.50   35.85   69.14   59.85   69.50   33.81   69.30   35.85   69.14   59.85   69.50   33.89   70.23   69.70   36.44   69.30   35.85   69.50   35.85   69.									
64   57.02   29.06   56.90   29.30   56.77   29.55   50.64   19.83   65.77   29.55   50.64   19.83   65.77   29.55   50.64   19.83   65.77   29.55   50.64   19.83   65.65   59.70   32.42   59.56   32.68   59.43   32.04   59.24   59.26   65.66   65.67   32.63   60.45   31.14   60.32   31.42   62.18   35.70   62.37   31.78   62.23   32.75   62.29   32.72   61.95   32.63   60.45   31.14   60.32   31.42   60.23   31.45   61.66   32.13   62.23   32.25   62.29   32.72   61.95   32.63   63.23   32.97   63.85   32.85   62.23   32.97   63.85   32.24   63.75   33.65   61.66   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   32.13   65.01   33.65   61.65   33.65   63.75   33.65   63.75   33.65   63.75   33.65   63.75   33.65   63.75   33.65   63.75   33.65   63.75   33.65   63.75   63.14   63.75   6									
58.81 29.96 58.68 30.22 58.54 30.48 58.41 30.73 65.75 59.13 30.44 59.39 51.20 65. 59.70 3.44 59.59 59.56 30.68 60.59 30.87 60.45 51.14 60.52 31.40 60.18 31.40 60.19 30.48 60.19 30.20 70.30 31.40 60.34 31.50 60.19 30.20 70.30 31.40 60.34 31.50 60.19 30.20 70.30 31.40 60.34 31.50 60.19 30.20 70.30 31.41 60.34 31.50 60.30 31.40 60.34 31.50 70.00 31.40 60.34 31.50 70.00 31.40 60.34 31.50 70.00 31.40 60.34 31.50 70.00 31.40 60.34 31.50 70.00 31.40 60.30 31.40 50.50 31.40 31.40 50.50 31.40 31.40 50.50 31.40 50.			29.06	56.90	29.30				
67	6;	57.92	24 51	59	39.76	57.66 30.01	57.52 (3).10		
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71   63.26   32.23   63.12   31.51   02.98   33.8   02.8   33.6   72.6   64.15   32.69   04.01   32.97   03.86   33.21   04.00   33.42   04.75   33.11   04.00   33.42   04.75   33.11   04.00   33.42   04.75   33.11   04.00   33.42   05.64   34.11   05.98   33.61   05.98   33.61   05.98   33.62   05.74   34.17   05.91   34.40   05.34   35.26   06.57   33.42   05.64   34.17   05.91   34.40   05.45   35.26   06.50   35.57   05.14   35.22   05.20   35.25   05.14   35.82   05.23   34.52   05.23   36.17   70.07   36.47   05.43   35.27   05.14   05.34   35.77   05.10   36.02   04.02   05.23									
72 64.75 32.69 04.01 32.97 03.86 33.21 04.00 33.42 05.00 33.43 06.00 33.45 06.									
23         65,04         3.14         64,07         33,48         65,79         33,48         65,79         31,48         65,79         31,48         65,79         31,48         65,74         31,14         66,79         31,48         65,74         31,14         66,73         31,45         65,71         31,14         66,73         31,45         65,71         31,41         66,73         31,45         65,71         69,19         36,02         69,23         31,41         33,42         66,18         31,41         69,34         35,77         69,19         36,02         69,11         30,82         69,11         30,88         70,96         36,44         70,87         70         70         70         35,87         70,29         36,67         70,96         36,44         70,80         37,28         37,29         37,68         73,79         38,03         73,09         37,68         73,79         38,00         73,62         38,33         37,45         38,46         74,44         38,14         74,08         38,46         74,51         38,79         73,42         38,33         37,45         38,46         74,51         38,79         73,43         39,11         76,14         39,47         76,14         39,72         74,51									
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66 83         3.105         6.147         31.34         66 53         31.65         65.7121.92           70         67.72         34.50         65.45         35.26         68.30         35.57         69.19         36.27         69.19         36.22         69.19         36.22         69.19         36.22         69.11         36.22         69.11         36.22         69.11         36.22         69.11         30.22         70.32         70.71         70.97         70.93         35.87         70.22         36.67         70.96         36.64         70.90         37.86         73.72         37.56         73.79         37.56         73.79         37.56         73.78         37.27         37.57         72.01         37.09         71.85         37.40         71.65         38.33         73.45         38.65         75.77         38.96         75.77         38.96         75.73         38.93         73.62         38.33         73.45         38.61         38.47         74.84         38.14         74.84         38.46         74.73         38.96         75.57         38.92         75.40         39.25         75.27         38.46         74.71         34.71         76.11         49.04         49.04         49.04         4					133.88				
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101   89.99   45.85   89.79   46.25   89.59   46.64   89.38   47.03     102   90.88   46.31   90.68   46.70   90.48   47.10   90.27   47.49     103   91.77   46.76   91.57   47.16   91.36   47.56   91.15   47.96     104   92.66   47.62   92.46   47.62   92.25   48.02   92.04   48.42     105   93.56   47.67   93.35   48.08   93.14   48.48   92.02   48.89     106   94.45   48.12   94.24   48.53   94.02   48.95   93.81   44.36     107   95.34   48.58   95.12   48.95   94.91   49.41   94.69   49.82     108   96.23   49.03   96.01   49.45   95.80   49.87   95.58     109   97.12   49.49   96.90   49.91   96.68   50.33   96.46   50.75     110   98.90   50.39   98.68   50.32   98.46   51.25   98.25     111   98.90   50.39   98.68   50.32   98.46   51.25   98.25     112   99.79   50.85   99.57   51.28   99.35   51.72   99.12   52.15     113   100.7   51.30   10.5   51.74   100.2   52.18   100.0   52.01     114   101.6   51.76   101.3   52.20   101.1   52.64   100.0   52.01     115   103.5   52.21   103.2   52.66   102.0   53.10   103.4   53.68     116   103.4   52.96   103.1   53.1   102.9   53.56   102.7   53.65     117   104.2   53.12   10.00   54.03   104.7   54.41   105.6   54.62   105.8     118   105.0   54.02   105.8   54.49   105.6   54.55   105.3   55.7     119   106.0   54.02   105.8   54.49   105.6   55.57   105.3   55.7     120   106.9   54.48   106.7   54.94   106.4   55.41   106.2   55.00     120   106.9   54.48   106.7   54.94   106.4   55.41   106.2   55.00     120   106.9   54.48   106.7   54.94   106.4   55.41   106.2   55.00     120   106.9   54.48   106.7   54.94   106.4   55.41   106.2   55.00     120   106.9   54.48   106.7   54.94   106.4   55.41   106.2   55.00     120   106.9   54.48   106.7   54.94   106.4   55.41   106.4   55.41   106.5   55.00     120   106.9   54.48   106.7   54.94   106.4   55.41   106.4   55.41   106.4   55.41   106.4   55.41   106.4   55.41   106.4   55.41   106.4   55.41   106.4   55.41   106.4   55.41   106.4   55.41   106.4   55.41   106.4   55.41   106.4   55.41   10									
102 90 88 46.31 90 68 46.70 90.48 47.10 90.27 47.49 103 91.77 46.76 91.57 47.16 91.36 47.56 91.15 47.96 104 92 66 47.22 92.46 47.62 92.25 48.02 92.04 48.49 105 93.56 47.67 93.35 48.08 93.14 48 48 92.02 48.89 106 94.45 48.12 94.24 48.53 94.02 48.99 93.81 49.36 107 95.34 48.58 95.12 48.99 94.91 49.41 94.69 49.82 108 96.23 49.03 96.01 43.45 95.80 49.87 95.58 50.29 109 97.12 49.49 96.00 49.91 96.68 50.33 96.46 50.75 110 98.01 49.94 97.79 50.37 97.57 50.79 97.35 51.22 111 98.90 50.39 98.68 50.32 98.46 51.25 98.23 51.62 112 99.79 50.85 99.57 51.28 99.35 51.72 99.12 52.15 113 100.7 51.30 100.5 51.74 100.2 52.16 100.0 52.01 114 101.6 51.76 101.3 52.20 101.1 52.64 100.0 52.01 115 103.5 52.21 103.2 52.66 102.0 53.10 102.9 53.56 12.27 53.15 116 103.4 52.06 103.1 52.11 102.9 53.56 12.27 54.91 117 104.2 53.12 10.00 53.77 103.8 54.02 103.1 53.4 105.6 54.02 105.8 54.03 104.7 54.41 12.54 54.4 105.6 54.02 105.8 54.03 105.6 55.00 105.8 54.03 105.8 55.00 105.8 54.03 105.8 55.00 105.8 54.03 105.	100								
103 91.77 46.76 91.57 47.16 91.36 47.56 91.15 47.96 104 92.66 47.22 92.46 47.62 92.25 48.02 92.04 48.42 105 93.56 47.67 93.35 48.08 93.14 48.48 92.02 48.89 106 94.45 48.58 95.12 48.99 94.91 49.41 94.69 49.82 108 96.23 49.03 96.01 44.45 95.85 49.87 95.58 50.29 109 97.12 49.49 96.00 49.91 96.68 50.33 96.46 50.75 110 98.01 49.94 97.79 50.37 97.57 50.79 97.35 51.22 111 98.90 50.85 98.68 50.32 98.46 51.25 98.23 51.65 112 99.79 50.85 99.35 51.72 99.12 52.15 113 99.79 50.85 99.57 51.28 99.35 51.72 99.12 52.15 115 100.7 51.30 100.5 51.75 100.2 52.01 101.1 52.64 100.0 52.01 114 101.6 51.75 101.3 52.20 101.1 52.64 100.0 53.08 115 103.4 52.00 103.1 52.1 102.9 53.57 122.7 53.08 116 103.4 52.00 103.1 52.1 102.9 53.57 122.7 53.08 118 105.1 53.57 104.0 53.57 104.7 54.41 105.6 54.02 105.8 54.03 105.6 54.02 105.8 54.03 105.6 54.02 105.8 54.03 105.6 54.02 105.8 54.03 105.6 54.03 105.6 54.03 105.7 54.04 105.6 55.57 105.3 55.71									
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107 95:34 48:58 95:12 48:99 94:91 49:41 94:69 449:82 108 96:23 49:03 96:01 49:45 95:80 49:87 95:58 50:29 109 97:12 49:49 96:00 49:91 96:68 50:33 96:46 50:75 110 98:00 50:39 98:08 50:32 98:46 51:25 98:23 51:68 112 99:79 50:85 99:75 51:28 99:35 51:72 99:12 52:15 100:7 51:30 100:5 51:74 100:2 52:18 100:0 52:01 114 101:6 51:75 101:3 52:20 101:1 52:64 100:0 52:01 115 102:5 52:21 103:2 52:66 102:0 53:10 101:8 53:58 115 103:4 52:06 102:0 53:10 101:8 53:58 115 103:4 52:06 102:0 53:10 101:8 53:58 115 103:4 52:06 102:0 53:10 101:8 53:58 115 103:4 52:06 102:0 53:10 101:8 53:58 115 103:4 52:06 102:0 53:10 101:8 53:58 115 103:4 53:58 103:0 53:58 1									
108         96.23         49.03         96.01         49.45         95.80         49.87         95.58         50.29           109         97.12         49.49         96.00         49.91         96.68         50.33         96.46         50.75           111         98.01         49.94         97.79         50.37         97.57         50.79         97.35         51.22           111         98.40         50.39         98.46         51.25         98.27         51.23         98.75         51.72         99.12         52.15           113         100.7         51.30         100.5         51.74         100.2         52.18         100.0         52.11           114         101.6         51.75         101.3         52.20         101.1         52.64         100.0         53.08           115         102.5         52.21         103.2         52.66         102.0         53.10         103.4         53.08           116         103.4         52.06         103.1         52.11         102.9         53.75         122.7         54.01           117         10.4         53.12         10.40         54.03         104.7         54.41         105.6         54.9									
109         97.12         49.49         96.90         49.91         96.68         50.33         96.46         50.75           110         98.01         49.94         97.79         50.37         97.57         50.79         97.35         51.22           111         98.90         50.83         98.68         50.32         98.46         51.72         99.12         51.75           113         99.75         51.28         99.35         51.72         99.12         52.15           114         101.6         51.76         101.3         52.20         101.1         52.64         100.0         53.08           115         103.5         52.21         103.2         52.66         102.0         53.12         103.9         53.08           116         103.4         52.06         103.1         52.11         102.9         53.67         122.7         53.08           117         10.42         53.12         10.0         53.57         103.8         54.02         103.7         54.91           118         105.1         53.52         105.9         54.03         104.7         54.41         105.6         54.95         105.3         54.94           120			,						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			, -			96-68 53.33	96 46 50 75		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	110	98.01	49.94	97.79	5237	97-57 50.79			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	111	98.90	50.39	98.58	53.32		95.23 51.68		
114         101.6         51.76         101.3         52.20         101.1         52.64         100.0         53.08           115         103.5         52.21         103.2         52.66         102.0         53.10         101.8         53.5           116         103.4         52.00         103.1         52.11         102.0         53.57         102.7         53.57         102.7         54.01           117         104.2         53.12         104.0         53.57         103.8         54.02         104.7         54.41         105.4         54.61           118         105.0         54.02         105.8         54.49         105.6         54.55         105.3         35.41           119         106.0         54.02         105.8         54.49         105.6         55.55         105.3         35.41           120         106.9         54.48         106.7         54.04         106.4         55.41         106.2         55.00	113			99 57	51.28		99.12 52.15		
t15         102.5         52.21         103.2         52.66         102.0         53.10         101.8         53.5           116         103.4         52.06         103.1         52.11         102.9         53.55         102.7         53.91           117         104.2         53.12         104.0         53.57         103.8         54.02         105.7         54.93           118         105.1         53.57         105.8         54.93         104.7         54.41         124.4         63.94           119         106.0         54.02         105.8         54.49         105.6         54.55         103.3         55.41           120         106.9         54.48         106.7         54.94         106.4         55.41         109.2         55.7									
116 103.4 : \$2.06 103.1 : \$3.1 102.9 \$3.55 102.7 : \$4.01 117 104.2 \$3.12 100 \$3.57 103.8 \$4.02 105.7 : \$4.4 118 105.1 \$53.57 105.8 \$4.03 104.7 \$4.4 105.4 \$4.04 118 105.0 \$4.02 105.8 \$4.03 104.7 \$4.4 105.4 \$4.04 119 106.0 \$4.02 105.8 \$4.49 105.6 \$4.05 105.8 \$5.05 105.8									
117 10,12 53 12 10,10 53,57 103 8 54,12 103.5 54,48 118 105 1 53 57 104.9 54,03 104.7 54,47 1254 54,04 119 106.0 54,02 105.8 54,49 105.6 54,55 103.3 55.41 120 106.9 54,48 106.7 54,04 106.4 55.41 106.2 55.0							· :		
118 105 1 55 57 105 9 54.03 104.7 54.41 125 4 53.04 119 106.0 54.02 105.8 54.49 105.6 54.55 173.3 55.41 120 106.9 54.48 106.7 54.04 106.4 55.41 106.2 55.00			-						
119 106.0 54.62 105.8 54.44 105.6 53.55 105.3 55.41 120 106.9 54.48 106.7 54.04 106.4 55.41 120.2 55.5									
120 106 9 54.48 136.7 54.94 106.4 55.41 136.2 55.6									
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2 / 0/ / 43/ ( 50)	ist		:;		<del></del>	<u></u>			
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ist.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lat	Dep.
11	0.88	0.47	0.88	0.47	0.88	0.48	0.88	0.48
2	1.77	0.94	1.76	0.95	1.76	0.95	1.75	0.96
3	3.53	1.41	3.52	1.89	3.52	1.43	3.51	1.92
4	4-41	2.35	4.40	2.37	4-39	2.59	4.38	2.40
6	5.30	2.82	5.29	2.84	5.27	2.86	5.26	2.89
7 8	5 18	3.19	6.17	3.31	6.15	3-34	6.14	3-37
9	7.06	3.76	7.05	4.26	7.03	3.82	7.01	3.85 4-33
10	8.83	4.69	8.81	4-73	8-79	4-77	8.77	4.81
TE	9.71	5.16	9.69	5.21	9-67	5.25	9.64	5-19
1(2)	10.60	6.10	11.45	6.15	10.55	6.20	10.52	5-77
13	12.36	6.57	12.33	6.63	12.30	6.68	12.27	6.71
15	13.24	7.04	13.21	7.10	13.18	7.16	13.15	7.25
16	14.13	7.51	14.09	7-57	14.06	7.63	14-03	7-70
17	15.89	7.98	14.98	8.52	14-94	8.11	15.78	8.18
19	16.78	8.92	16.74	8.99	16.70	9.07	16.66	9.14
20	17.66	9.39	17.62	9.47	17.58	9-54	17.53	9.62
21	18.54	9.86	18 50	9.94	18.46	10:02	18.41	10.10
22	19.42	10.33	19.38	10.41	19.33	10.50	20.16	11.06
24	21.19	11.27	21.14	11.36	21.09	11.45	21,04	11.54
25	23.07	11.74	12.02	11.83	21.97	1195.	21.92	12.01
26	22 96	12.21	22,90	12 31	22.85	12.88	22 79	12.51
27	23 84	13.15	24.06	12.78	23.73	13.36	25.67	13-47
29	15.60	13.61	25.55	13.73	25.49	13.84	25-43	13.95
30	26.49	14.08	26.43	14.20	16.36	14-31	26/30	14-43
30	27-37	14-55	28.10	14.67	27 24 28.12	44.79	28.06	14 151
33	29.14	15.49	20.19	15.15	39.00	15.27	28.95	15.39
34	30,02	15.96	29.95	16.09	29 88	16 22	29.81	15.35
35	30.90	16.43	30.83	16 57	30.75	16.70	30.69	16.83
36	31.79	16 90	33.59	17.04	31 64	17.18	31.50	17-33
37	33-55	17.84	33.47	17.99	33-40	18.13	33-32	18.28
39	34-44	18.31	34-35	18.46	34-27	18.61	34-19	18,76
40	35.32	18.78	35.24	18:93	35.15	19.04	35.07	19.24
42	36.20	19.25	36 t2	19.41	36.03	20.04	35-95 35.82	19.72
43	37.97	20.19	37.88	20.35	37.79	20.52	37.70	10.68
44	38.85	20.66	38.76	20.83	38.67	10.99	38 58	21.16
45	39 73	21.60	39.64	21.30	39.55	3 47	39:45	21.64
46	40.62	22.07	41.40	22.25	41.30	21.95	41.21	12.13
48	42.38	22.53	42.28	22.72	42.18	12 90	42.08	13 00
49	43.26	13.00	43.16	13.19	43 06	13 38	42.95	23 57
50	44.15	23.47	44.04	23 67	43.94	13.86	43 84	14.05
51	45:01	24.41	45.80	24.61	44.82	24-34	44-71	14 53
53,	46.80	14.88	46.60	25.09	46.58	25.29	46.47	15:49
54	47.68	25.82	47-57	26.56	47.46	25 77 26,24	47-34 48-11	15 97
99-	40.45	26.29	49-33	26.51	48.33	26,72	49-10	26 94
56	50.33	26.76	50.21	26.98	50.09	17.20	49-97	17:41
57	51.21	27.23	51.09	27.45	50.97	27.68	50.85	17 90 18.38
59 60	52.09	27.70	51.97	27 93 28.40	51.85	28.15	51.73	18.38 18.56
	Dep.	Lat	Dep.	Lat	Dep.	Las	Dep.	Lat.
Dist		_	-			No. of Lot	1	-
	-0' 45' 30' 1 15'							

61 DECHEES.

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Diet.	0		11	5'	30'	43/
.=	الندا_	: Dep	Lat	Dep_	Lat. Dp	Lat Dep.
61	54-35	27.69	54.23	27 93	54.11 28.17	53.98 28.40
62	55.24	28.15 28.60	55.12	28.39 28.85	54.99 28.63	54.87 28.87
63 64	56.13	24.06	56.90	29.30	56.77 29.55	56.64 29.80
65	57.92	2ý S I	57.79	29.76	57.66 30.01	57.52 30.10
66	58.81	29 96	58.68	30.12	58.54 30.48	58.41 30.73
6-	59.70	30.42	59.56	3 5.68	59.13 30.94	59.29 51.20
68 69		.30.87	60.45 61.34	31.14	61.20 31.45	61.26 32.13
70	62.37	31.78	62.23	32 05	62.09 32.32	61.95 32.59
71	63.20	32.23	63.12	3251	62.98 31.8	61.83 33.06
72	01 12	32.69	64.01	32.97	63.86 33.25	63.72 33.52
73	65.01	37.14 33.60	64.90	33.42 33.88	64.75 33.71	65.49 34.46
74	65.93 66.83	3105	6579	34.34	66 53 34 63	66 (7 131.92
75	6- 72	34.50	67 57	34.80	6-41 35 59	626 35 57
77	63.61	34 90	63.45	35 26	68.30 35.45	55.14 33.85
78	69.50	35.41	69.34	35.71	69.19 35.32	69.03 (0.32
79	70 39 71 28	35.87 36.32	70.23	36 17 36.63	70.07 36.48 70.96 36.94	69.91   30.78   70 ho   37.25
<u> 85  </u>			71.12		71 85 37.40	71.63 37.71
82		36.77 37.23	72.01	37.09 37.55	72.73 37.86	72 57 38 18
83	73-95	37.68	73.79	38.00	73.62 38.33	73.45 38.65
84	74.84	38 14	74.68	38.46	74.51 38.79	7.1.34 39.11 75.23 39.58
85	75-74	38.59	75.57	38.92	75:40 39 25	75.23 39.58
86 87	76.63	39.04	76.46 77.34	39.38	76.28 39.71 77.17 43.17	76.99 40.51
88	78.41	39.50 39.95	78.23	40 29	78.06 40.63	77.88 47 97
89	79.30	49.41	79.12	40 75	78-94 41-10	78.76 41.44
90	80.19	43.86	80.01	4121	79.83 41.56	79.65 41.91
91	81.08	41.31		41.67	80.72 42.02	80.53 42.37 81.42 42.84
93	81.97 81.86	41 77	81.79 82.68	42.12	81.61 .42.48 82.49 42.94	82.30 43.30
93	83.75	42.68		43.04	83 38 43.40	83.19 43.77
95	84.65	43.13	84.46	43.50	84.27 .43 87	84.07 44 23
96	85.54	43.58	85 35	43 96	85-15 44-33	84.96 44.70
97	86.43	44.54	86.23	44 41	86.04 44.79 86.93 45.25	86.73 45.16
98 99	87.32 88.21	41-19	88.01	44·87  45-33	80.93 45.25	861 40.10
100	89.10	45 42	88.yo	45.79	88.70 46.17	88.50 45.56
121	89.99	45.85	89.79	40.25	89.59 46.04	89.38 47.03
132	95 88	46.31		46.70	90.48 47.15	90.27 47.49
103	91.77	46.76	91.57	.47.16 :47. <b>6</b> 2	91.36 47.55	91.15   47.95     92.04   48.42
101	93.56	47.67	93.35	48.08	93.14 48 48	92.92 48.89
106	94.45	48.12	94 24	49.53	94.02 48.95	93.81 49 36
107	95.34	43.58	95.12	:48.99	94.91 49 41	94.69 49.82
128	96.23	49 03	96.01	49.45	95.80 49.87	95.58 150.29
109	97.12 y8.01	49.49	96.90	49.91 50 3-	95-68 50.33	96.46 50 75
		4 <u>9.94</u> 50.39	98.68	50.32	98.40 51.25	98.23 51 68
111	98.90 99.79	50.85	99.57	51.28	99.35 51.72	99.12 32.15
113	150.7	51.30	100 5	51.74	100.2 52.18	100.0 [42.01
114	101.6	51.76	101.3	52.23	101.1   52.64	103.9 53.08
115		52.21	123.2	52 66		·
116	103.4 104.2	53.12	103.1	57.57	102.9 (33.56	123.5   54.45
118		53 57	10.1.9	54.03	104.7 54.49	1344 5494
119	106 0	54.02	105.8	54-49	105.6 51.55	1253 355 01
120	106 9	15++8	105.7	54-24	106.4 55.41	1 20.2 55.
1 kg	De.	144.	Dep	l let.	Dep. La	Dep. Lst
Uist		<b>)</b> /	4.5	,	3.1.	1 1,4 
			6.1	DEGI	NUC	

li di	-	1 0	/	1 7	51	30'   45'				
	Dist	1	- British			Lat	Depa	-		
		Lat	Dep. 0.48	Lat.	Dep.	0.87	0.49	Lat	Dep.	
v	-	0.87	0.97	0.87	0.49	1.74	0.95	0.87	0.50	
в	3	2.62	1.45	-2.62	1.47	261	1,48	2.60	T-49	
и	4	3.50	1.94	3.49	1195	3.48	1,97	3.47	1,98	
п	5	4.37	2.42	4.36.	7.44	4-3.5	2,40	4-34	2.48	
и	6	5.35		5.24	2.93	5.22	2.95	5-21	2-98	
и	7 8	7.00	3 89	6.11	3.42	5.09	3-45	6.08	3-47	
п	0	7.87		7.85	4.40	7.83	443	7.81	4-47	
ш	10	8,75	4.85	8:73	4 89	8 10	4.92	8.68	4-96	
п	1.1	9.62	5.33	9.60	5.37	9 57	5.42	9-55	5-45	
и	12	10.50	6,30	10,47	6,35	10.44	6.40	11.20	5.95	
В	13	11.37	6.79	12,21	6.84	12.18	6.84	12.15	6.95	
в	115	13:12	7.27	13.09	7-33	13.06	7 39	13 D1	7:44	
в	16	13 99	7.76	13.96	7.82	13.93	7.88	13.89	7-94	
и	17	14.87	8.24	14.83	8.31	14.80	8.37	14.76	2 44	
п	18	15.74	9.21	16.58	9.28	16.67	9 36	16.50	943	
к	20	17.49	9.70	17.45	9.77	17-41	9.85	17-36	9.52	
н	21	18,57	10.18	18.32	10.26	18.28	10.34	18.23	10.42	
ш	22	19.24	10.67	19.19	10.75	19.15	10.83	19.10	10,92	
и	23	50.13	11,15	20.07	11.24	20,02	11.33	19-97	11.40	
и	24	20.99	12,12	20.94	11.73	20.89	12,31	21,70	11.91	
п	26	22.74	12.61	22.68	12/70	22.63	12.80	12.37	12.90	
п	27	23.61	13.00	23.56	13.19	28150	13.30	23.44	13.40	
ш	28	24 49	13.57	24:43	13.68	24137	13.79		13.89	
п	29	25.36	14:06	25/30	14-17	25.24	14.28	25,18	14-19	
н	30		14-54	26,17	-	25.11	14-77	-	14.89	
и	31	27.11	15.51	27.05	15.64	20.98	15.27	26.91	15.88	
ш	33	28.86	16 00	28.79	16.12	28 72	16.15		16.18	
и	34	29.74	16.48	29.66	16.61	29-59	16.74	I DOWNSON	16.87	
н	35	30161	16.97	30.54	17.10	30 46	17.23	30.19	17-37	
п	36	31.49	17-45	31.41	17.59	31.33	17.73	31.26	17.86	
н	37	33.24	18.92	33.15	18,57	32.20	18.71	32.12	18.55	
н	39	34.11	18,91	34.03	19.06	33-94	19.20	33.86	19.35	
N.	40	34.98	19.39	34.90	19:54	34.81	19.70	34-73	19.85	
н	41	35.86	19.88	35-77	20,03	35.68	20.19	35.60	10,34	
Ш	42	30,73	20,36	30:64	20.52	36,55	20 68		10,84	
ш	43	38 48	21/33	38.30	21-50	37 43 38.30	21.67		11,83	
1	45	39.36	21.82	39.26	11,99	39.17	22,16		22,33	
ľ	46	40.23	22.30	40.13	22.48	40.04	22.05		11.83	
1	47	41.11	22.79	41.01	22.97	40.91	23.14		3.52	
	48 49	41.98	23.76	41.88	23.45	42.65	23.64		15.51	
1	50	43-73	24-24	43.62	24 43	43.52	24.62			
1	511	44.61	24 73	44.50	24-92	-	25,17	44.18	5,51	
	52	45.48	25.21	45-37	\$5.41	45.26	25.61	45.15	15/80	
1	53	46.35	25.69	46.24	25.90		26.10		6.80	
1	54 55	48.10	26.66	47-11	26.87		27.08		7,29	
1	56	48.98	27.15	48.86	27.36	-	27.58	-	7 79	
I	57	49.85	27.63	49-73	27.85	49.61	28,07	49.49	8.48	
	58	50.73	28,12	200000	28,34		28 56		5.75	
	59 60	51.60	28.60	52.35	28.83		29.05		9.23	
-	_	Dep.	Lat.	Dep.	Lat	Dep.	Lat	Dep.	Eate	
1	Dist.	Dep. 1	tott.	45		30/		400 100		
-	-	0			WGRE			- 10		

60 DEGREES,

				13' 1 30'					
Digt	(/						4.5		
	_Lat_	Dep.	Lat.	Dep	Lat.	Dep	Lat.	Dep.	
61 62	53.35	129.57 30.06	53.22	29.81 30.29	53.09 53.96	30.54	52.96	30.27   30.27	
63	54.23	30.54	54.97	30.29		31.02	54.70	30.77	
64	\$5.98	31 03	55 84	31.27	55.70	31.52	55.56	31.70	
65	56 85	31.51	561	31.76	56.57	32.01	56 43	32.25	
66		32.00	57.58	32.25	57 44	3 - 50		32.7;	
67	58.60	32.48	53.40	32 74		132.99		33-25	
68 69	59 47 60 35	32.97 33.45	59-33 60.20	33.23	59.18 60.05	33.48	59.04	33-74	
70	61.22	33 94	61.07	34 20	60.92	34.47	60.77	34.74	
71	62.10	34.42	61.95	34 69	b1.80	34.96	61.64	35.23	
72	62 97	34.91	62.82	35.18	62.67	35-45		35.73	
73		35.39	63.69	35.67	63.54	35.95	63.38	36.22	
74   75	65.60	35 88	64.56 65.44	36.16	64.41 65.28	·36.44 36.43	65.11	30.72	
76	66.47	36.85	66.31	37.14		342	65.98	37.71	
77	67.35	37.33	67.18	37 62	67.02	3 92	66 85		
78	68 22	382	68.05	38.11	67.89	38.41	67.72	38.70	
79	69 09	38.30	68.93	38.65		38.90	68 59	30.20	
80	69.97	38.78	69 80	39 09	69.63	39.39	69.46	34 70	
81	71.72	39.27	70.67	39 58	70.50 71.37	39.89 40 38	70.32	40.19	
83	72.59	39.75	72 42	40.07	72.24	40.87	71.19	41 19	
84	73.47	10 ~2	73.29	41.64	73.11	41.36		4168	
85	7+3+	41.21	74-16	41.53	73.98	41.86	73.80	4: 18	
86	75.22	41 60	75.03	42 02	74.85	42.35	-4.6-	42.67	
87 88	76.09	42.18	75.91	42.51		42.84	73.53	43 17	
Sg	-6.97 -7.84	43.15	77.65	13.40	77.46	143.83	77.27	143.07 144.16	
9ó	78.72	43.63	-8.52	43.98	49	144.32	78.14	44.66	
91	79 59	44.12	-9.40	44.46	79.20	44 81	79.01	45.10	
92	80 47	44 65	80.27	44-95	83 O7	45.30	79.87	45.65	
93	81.34	45.09	81.14 82.01	45.44	81.81	45.80	85.74 C. 4:	46 15	
94 95	82 21 83.09	45.57	82.89	45.93		146.29	81.61 82.48	46.64	
96	8; 46	46 54		16 91		4- 2-	83.35	j~ 64	
97	84 84	47.03	ـ ن م ا	47.40		14	84.22	48.13	
98	85.71	47.51	85.50	4- 88	85.29	48.26	_	48.63	
99 '	1.0.19	4 <sup>1</sup> .00		48.37		148.75		140.13	
100		48.48	87.25	48.86	87.04	49.24		149.62	
101 102	88.34	48.97	85.12 88.99	40 35	87.91 88.78	,49.73  50.23	87.69 88.50	50.12	
103	90.09	49.45	89.87	50.33	89.65	50.72	89 42	51.11	
104	92.96	50 42	90.74	50 82	90.52	51.21	93.29	51.61	
105	91.84	50.91	91.61	51.31	91.39	51 70	91.16	52.17	
106	92.71	51.39		51.79	92 26	52.20	9203	52 60	
107 158	93.58	51 87   52 36	93.36	52.28	93.13	52.69 53.18	92.90	53.59	
109	95 33	52 84	95 10	53.26	94.87	53.67	94.63	54.09	
110	96 21	53.33		53.75	95.74		95.50	54 58	
111	97.08	53.81	96.85	54.24	96.61	54 60	96 37	55.08	
142	996	54.30	97 72	54.73	97.48	55.15	97.24	55.58	
113	98.83	54.78	98.59	55 21 55.70	98.35	55.64 56.14	98.11	56.C7	
115	100.6	55.75	100.3	56.19	100.1	56.63	99.84	57.00	
116	101.5	56.24		56.68	101.0	57.12	100.7	57.56	
117	102.3	56.72	102.1	157-17	131.8	57.61	101.6	58.06	
118	103.2	57 21		57.66	102.7	58.11	152.4	58.55	
119   120	104.1	57.69 58.18	-	58.15 58.63	103.6	58.00	103.3	59.05	
. 20			104.7	-	104.4	59.09	104.2	59.55	
	Dep.	· Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	
Dist.	<del></del> -	<del></del>	45		30	, 1	15		

-	0		F 15	,,	1 30	P	45			
Dist	Lat.	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.		
	0.87	0 50	0.86	0.50	0.86	Q-SI	0.86	0.51		
1 2	1.73	1.00	1.73	10.1	1.72	1.02	1.72	1,02		
3	2.60	1.50	2.59	1.51	2,58	1.52	2.58	2.53		
4	3.46	2.50	3.46	2.02	3:45	2.03	3-44	2.05		
6	5.20	3.00	5.18	3.02	5.17	3.05	5.16	3.07		
7	6,06	3 50	6.05	3-53	6.03	3.55	602	3-58		
7 8	6.93	4.00	6.91	4.03	6.89	4.06	6,88	4.60		
10	8.66	5.00	7-77	5.04	7:75 8.62	5 08	8.59	5.11		
11	9.53	5.50	9.50	5.54	9.48	5.58	9.45	5.62		
12	10.39	6.00	10.37	6.05	10.34	6.09	10.31	6.14		
13	11.16	7.00	11.23	7.05	11.30	7-11	12.03	7-16		
14	12.99	7.50	12.96	7.56	12.92	7.61	12.89	7-67		
16	13.86	8.00	13.82	8.06	13.79	8.12	13.75	8.18		
17	14 72	8.50	14.69	8.56	14.65	8.63	14.61	8.69		
18	15 59	9.60	15.55	9.07	16 37	9.64	15.47	9.74		
20	17.32	10.00	17.28	10.08	47.23	10.15	17.19	10.23		
21	:8.19	10.50	18.14	10.58	18.09	10.66	18.05	10.74		
22	19.05	11.50	19.87	11.08	19.82	11.67	18.91	11.75		
23	20.78	12 00	20.73	12 09	20.68	12.18	20.63	12.27		
25	21 65	12.50	21.60	12.59	21 54	12.69	21.49	12.78		
26	22.52	13.00	22.46	13.10	22.40	13.20	2234	13.29		
27	24.25	13.50	23.32	14.11	23.20	13.70	24.06	13 80		
29	25.11	14.50	25.05	14.61	24 99	14.72	23 92	14.83		
30	25.98	15.00	25.92	15.11	25.85	15.23	25.78	15-24		
31	26.85	15.50	26.78	15 62	26.71	15.73	26.64	115.85		
32	28.58	16.00	28.51	16.12	27-57	10.75	28.36	16.30		
34	29.44	17.00	29.37	17.13	29.30	17.26	29.11	17-38		
35	30,31	17.50	30.23	17.63	30 16	17.76	30.08	17.90		
36	31.18	18.00	31.10	18.14	31.88	18.27	30.94	18.41		
37	32.91	19.00	32.83	19.14	32.74	19.19	32.66	19-43		
39	33-77	19.50	33.69	19 65	33.60	19.79	33-52	19-94		
40	34 64	20.00	34-55	20.15	34-47	20.30	34.38	20.45		
41 42	35.51	20.50	35.42	20.65	35.33	21 32	35.24	20.90		
43	37.24	21.50	37.14	21.66	37.05	31.82	36.95	2t.99		
44	38 11	22.50	38.01	22.67	37 91 38.77	22.33	37.81	22.50		
46	39.84	23.00	39.74	23.17	39.63	23:35	39.53	23.52		
47	40.70	23.50	40.60	23.68	40 50	23.85	40.39	24.03		
48	41 57	24.00	41.46	24.18	41.36	24.36	41.25	24-54		
49	43.30	24.50	42-33	24.68	43.08	24.87	42.97	25.05 25.56		
51	44.17		-	25.69	-	25.88	43.83	16.08		
52	45:03	26.00	44.92	26.20	44.80	26.39	44 69	26.59		
53	45.90	26.50	THE RESIDENCE	26.70	45.67	25.90	45-55	27.10		
54	47.63	27.50	46.65	27-71	47.39	27.91	47-27	28.12		
56	48.50	28.00	48.37	28.21	48.25	28.42	48.13	28.61		
57	49.36	28.50	49.24	28.72	49.11	28.93	48.99	29.14		
50	51.10	29.00	50.10	39.72	49 97	29.44	49.85	39.65		
59	51.96	30.00		30 23		30.45	51.56	30.68		
	Dep	Lat.	Dep.	Lat.	Dep.	Lat	Dep.	Lat		
Dist.	0/		45		30	A STATE OF	15			
1	59 DEGREES.									

15	-	=	n:	1	137	1	30"		400
		Lat	] Oct	LA		La		-	43'
6	= 1	CE.ST			-				Dep
15		13.5	CIII DOUBLE			3 53.4		DESCRIPTION OF THE PERSON NAMED IN	
6		54-51		54.4	2 31.7	4   54.2	8 81.9	7 54.14	32.24
6		55-43						100 100 100 100 100 100 100 100 100 100	32.71
60	==	57.11				-	and in column 2	The second second	33.23
5		58.00	THE PERSON	100 000					33-75
6		58.89	-		ALL ROMAN	The second second	-	1 58.44	34.77
75		50 76	-					100 100 100	35.28
21		61.40			-	in the second		- Contraction	30.32
1 92		02.35		61.10	36.2	62.0	36.54		36.81
1		3.22							37.52
74		4.00	37.00	THE RESERVE OF THE PERSON NAMED IN		64.6			37.84
56		6.82	38.00	2		0 5.46	CO MARKET		38.86
77	1	6 68	38.50		-	66.3	39.08		39 37
78	1 6	7 58	39.00	1000000					39.88
79 Bo	-	3,42	39,50	69.11					40.39
81		21.0	40.50	THE REAL PROPERTY.		in the same of	41.11	and the same	THE REAL PROPERTY.
80	7	1.01	41.00	70.83	41.31	70.65	41.62		41.93
1 81		1.88	41.50		13.81			71133	47.44
\$4 85		3.51	42.00	73.45	42.32		III MATERIA	72,19	43.46
86		4 48	43.00	1	Contract of the last	-	column		43-97
82		5.34	43.50	75.15	43.83		44-10	74-77	44-48
#8 #6		7.08			44-33	10000000		1000	44-99
90		7.94	45.00	77-71	45-34	77.55	1000	77-35	45.51
gr	72	8.81	45.50	78.61	49.84	78.41	46.19	78.21	46.53
92		9.67	46,00		40.35		46 69	79.07	47.04
12		1.41	40.50		40.85		47-71		47.55
45		27	47.90	82.06	47.86		48.22		48.57
100	83	114	48 00	82.93	48.36	\$2.72	48.72	82150	49.08
97	-	.00	48.50	8179	48.87	100000	49-23	1 4000	49.60
20		87	49.60	84.00	49-17	85.30	149.74		50.61
30		6.60	(0.00	65 38	50 38	86 16	59.75	BURNS OF THE PARTY	\$1,13
191		42	50.50	87.45	50.88		51 26		51.64
122		33	\$1.00	88.97	\$1.38	87.39	51.77	1000	52.15
104		.07	\$1.50	89.84	51 89	89 61	53.78	0 0	53.17
195	40	93	\$2 50	90.70	51.90	90.47	\$3.29		53.69
1.36		83	53.00	91457	51.40	91.33	53.80		54.20
103	100	-53	\$4.00	93.43	54.90	93.19	54.81	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	56.22
rai		40	54.50	94.16	54-91	93-92	55-32	Sec. 20. 15	\$5.73
CHA	95	.26	\$4.00	95.02	\$5.42	94.78	55-83		6.24
330			54.50			95.64		95-39	
113						97-36		95.15	
104				98.43		98-23		97.97	8.29
113		59	57.50	99.34	57.93	99 09	58.37	98.81	8,80
110			58.00	100.2		99.95	58,87		9.31
118	10	1211	E4.50			100.5		100.6	
tig	10	5.00	59050	102.8		102.4	69.40	102.1	0.84
125	103	19	00/00	-	00 45	The state of the s	firings.	1031	100
3	Me	1000	Lat.	Dep	Let	March Co.	Lui	Acres de la companya	Bati
Dis	-	01	- 11	45	-	30		15	

10	140 SI DEGILLES										
1	Dist	0	1	1 1	51	1	301	1 4	151		
1	735	Lat	Dep.	Lat.	Dep.	Lat	1 Days	Lat	Dep		
н	1	0.86	0.51	0.85	0.52	3	0.52	0.85	0.63		
	2	1.71	1.03	1.71	1.04	1.71	1.04	1.70	1.05		
п	3	2.57	1.55	2.56		2.50		1 255	1.58		
	4	3.43	2.06	3,42		3.41		3.40	2.10		
1	5	4-29	2.58	4.27	2.50	4.26	-	4,25	2.63		
	6	6.00	3,09	5.13	3.11	5.12	3.13	5.10	3.68		
п	7 8	6.86	4.12	6.84	435	5.97		6,80	4-21		
п	9	7-71	4.64	7.69		7.67		7.64			
ı	10	8.57	5.15	8.55	5-10	8.53	5.11	8.50	5 26		
1	11	9.43	5.67	9.40		9 38	5.75	9-15	5.79		
Н	13	10.19	6.18	10,26		10,23		10.20	631		
н	13	11.14	7-21	11,11	7.26	11.08		11.05	2-37		
1	15	13.86	7.73	12.82	7.78	12.79	7.84	1 12.76	7-89		
п	16	13.71	8.24	13.68	8,30	13.04	8. 36	13.61	8.42		
	17	14-57	8,76	14.53	8.82	14 49	0.00	14.46	8.95		
1	18	15.43	9.27	15.39	9.34	15.35	9.40	15.31	9-47		
	19	16.29	9.79	15,24	9.36	16.20		16.16	10.00		
1	20	47-14	10.30	17.10	10.38	17.05	10.45	17.01	10.52		
ı	21	18.00	10.82	18.81	10.89	17.91	10.97	17.85	11.05		
1	22	19.71	11.85	19.66	11.93	18.76	12.02	19.56	12.10		
ı	24	20:57	12.36	20.52	12.45	20.46	13.54	20.41	12.63		
u	25	21.43	12.88	21 37	12-97	21.32	13.06	21,26	13.15		
ı	26	22.29	13.39	22.23	13.49	22 17	13.59	22/11	13.68		
п	27	23.14	13.91	23.08	1401	23.02	14.11	22,96	14-11		
п	28	14.00	14.42	23.94	14.53	23.87	14.63	23.81	14-22		
ı	30	25.71	14.94	24.79	15.04	25.58	15.15	25.51	15.79		
ı	31	26.57	15.97	26 50	16.08	26.43	16 20	25.36	16.31		
ı	32	27143	16.48	27.36	16.60	27.28	16.72	27.21	16.84		
1	33	28, 29	17.00	28.21	17.12	28,14	17.24	28.06	17.57		
н	34	29.14	17 51	29.07	17.64	28,99	17.77	28.91	17.80		
H	35	30.00	18.03	29.92	18.15	29.84	18.29	29.76	18.42		
н	36	30.76	18.54	30.78	18 68	30,70	18.81	30.61	18,94		
п	31	31.72	19.06	31.63	19.19	31,55	19.33	31,40	19.47		
п	39	33.43	20.00	33-34	20.23	33.25	20.38	33.16	20.52		
L	40	34-29	20,60	34.20	20.75	34.11	20.90	34.01	21.01		
	41	35.14	21.12	35.05	31.27	34.96	22.42	34.86	21.57		
	42	36.00	21.63	35.91	21.79	35 81	21.94	200	22.10		
	43	36.86	22.15	37.62	22 31	36.66	12.47	30.57	21.63		
	45	38.57	23.18	38 47	23.34	37.52	23.99	37 42 38.27	21.68		
-	46	39.43	23.69	39:33	23.86	39.22	14.03	39.12	24.21		
	47	40.29	24.21	40.18	24 38	40.07	24.56	39.97	24.73		
Ŧ.	48	41.14	24.72	41.04	24 90	40.93	25.08	40.82	25.25		
	49.		25 24	41.89	25.42	41.78	25.60		25.78		
15	50		25.25	42.75	25.94	42.63	26.12	-	6.11		
1	51	No.	26.27	43.60	26.46	43,48	26.65		20.84		
	53		26.78	44.46	27.50	44-34	27-17		17.8g		
	54	46.29	27.81	46.17	28:01	46.04	28,21	45-92 1	18.41		
	55	47-14	28.33	47.02	28.53	46 90	28.74	46.77	8,94		
1	56	48.00	28.84	47.88	29.05	47.75	29,26	and the same of the	19-47		
1	57		29.36	48.73	29.57	48.60	29.78	48.47	9-99		
	03		29.87	49.58	30.09	49.45	30.30		0,52		
10	59		30.39	51.29	30 61	51.16	30 83		1,57		
	_	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.		Late		
1	Dist	13ch. 1		Married Married	STREET, SQUARE, SQUARE			15°			
-		-0'	-	45	DECR	30		19.	- 0		

100				DEGRE				14
2	0	-	15		3	0,	4.5	f
1 7	Lac	Don-	Late	Dep	Lat	Dep-	Late	Oup.
61	52/29	31.42	52/15	31.65	52.01	31.87	51.87	32.10
52	53.14	31-93		32 10	32.86		52.72	1000000
53	54.00	32.45	53.E6	31.68	(3.72	32.92	53:57	
64	54.86	33.48	54-71	33.30	54 57	33-44	54 42	34.20
66	56.37	33.99	50.42	34.24	\$6,27	\$4.48	50/12	34-79
67	57 47	34.91	57.28	34.76	57743	35.01	56.98	35-20
68	\$8,29	35.02	58.13	31.25	57:98	35 53	\$7.82	34.25
69	59 14	35-54	58.99	33.80	12.21	36.05	38.67	36.31
70	60.00	36.25	59.84	30.34	59.68	36.57	59.52	36 4
21	61.73	30 57	60.70	36.83	61.30	37.10	61,23	37.36
72 73	62.57	37,60	61.55	37.35	62.24	38.64	62.08	37.14
74	63-43	38.11	63.26	38,39	62.10	38 56	62.93	39.94
75	64 29	38.63	64-12	38.91	63.95	39-14	63.78	34.47 6
75	55.14	39.14	64.97	39.43	64.80	39.71	04:03	39-99
77	66.00	39.66	65.81		65.65	45.43	65:48	42 53
78	66.86	42.17		40.46	67-36	41.28	65 33	41.07
79	66.57	41.20	68,39	41.50	68.21	41.80	68.03	48.10
81	69 43	44.72	09.25	42.02	69.05	42.32	68.88	41.01
82	70.29	42.23		42.54	69.91	42.84	69-73	43.15
83	71.14	42.75	70.96	43.08	70.77	43-37	70.58	43.55
84	72'00		COLUMN TWO IS NOT THE OWNER.	43.58		43.89	71.43	14.11
85	72.86	43.78	72.07	44.10	72.47	44.41	72.28	4522
85	78.74	44.29	73-52 74-38	44.61	73-33	44-93	73.98	45-78
88	75-43	45.32	25/23		75.03	43.98	74-83	46 38
89	76.29	44.84	70.09	46.17		46.50	75-68	+6.83
90	27.15	46 35	76-94	46,69	16.74	47 02	76.53	47.33
91	78.00	46.87		47 21	77/39	47.55	77.38	47.59
92	78.86	47-38		47-73	79.44	48.07	78,23	45.41
93	79-74 80.58	47.90	79:51 80:30	48.20	79 33	48.59	79.08	49-47
94	81.43	48.03	81,22	19.28	\$1.00	49.64	80.78	19.99
90	82.29	49.44	82.07	64.30	81.85	50.10	81,61	90.92
97	83.15	19.96	82.93	50 34	82.72	52.68	82,45	51.04
98	84.00	59.47	83.78	50.84	83 56	51.20	¥1.35	91.57
199	84.86	50.99	84.64	51 36		51.73	85.04	52.13
100	85.72	51,50	85.49	\$1.88	85125	52.25	THE REAL PROPERTY.	52.5b
101	86.57	\$2.53	86.33	52.91	80.17	53.19	86.74	55.15
103	88,29	53.05	88.06	\$3.43	37 82	53.81	87.59	54.10
104	89.15	53.56	88.91	53.95	88.67	54-34	88,44	5475
105	90.00	5408	89.77	54-47	89-53	54-40	89.29	55.25
106	95.88	54-59	90,62	54 99	90.38	55.38	40.14	53-73
137	91.72	55.11	91.48	55.51	91.21	55-91	90.99	\$6.30
108	92.57	55.02	92.33	50.03	92.09	50.43	92.69	57.30
110	99.29	\$6.65	94.04	57,00	93.74	57.47	93.54	57.88
ELE	95.15	57.17	THE RESERVE	\$7.58		\$8,00		58.41
212	96.00	57 68		58.10	95.50	58.52	95.24	58.94
713	96 86	58,20			90 35	59.04	96.09	59.40
1.14	97.72	58,71			97:20	59-50	95.94	59.99
TIE	98.57	59-23	4813 E	59.66	98.05	00.09	97-79	60. (1
115	99.43	59-74		60.18	98.91	61.13	98.64	61.57
117	101.1	60.77		61.42	100.6	61.65	100.3	61.09
119	101.0	61 29		61.73	1Dis	52.18	101.2	62,62
120	102.9	61.80	The Personal Property lies	62.15	102.3	62.70	102.0	02.13
7	Dep.	Lat	Dep a	Lat.	Dep.	Kish.	Dep	Late
Dist	0	-	43		30	7	15	-
-		1	59 0	EGRE	0.2		-	

峼		-	-			-		200	
ı	7	0	STATE OF	15	1	30	1	45	AD THE
-	6	Lat.	Dep	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
м	10	No. of Persons	-	_		SHOW SHAPE	-		
п	2	0.85	0.53	0.85	0.53	0.84	0.54	0.84	0.54
	2	1.70	1.06	1.69	1.07	7.69	1.07	1.68	1.08
	3	254	1-59	2/54	1.60	1-53	1.64	2.52	1.62
м	4	3.39	2112	3.38	2113	3 37	2.15	3.30	2.16
8	5	4.24	3.65	4.23	1.67	4.32	2.09	4.21	2.70
u	6	5.09	3118	5.07	3.20	5.06	19.22	\$.05	3.45
ш		5 94	3.71	5.92	3-74	5.90	3:76	5.89	3.79
ш	7 8	6.78	4.24	6.77	4-27	6.75	4.10	6.73	4-33
в	9	7.63	4-77	7.61	4-80	7:59	4.84	7.57	4.87
	10	8.4%	5.30	8.46	5.34	8.43	5.37	Bigt	5-41
			-	Street, Square,		The second second			
	11	9.33	5.83	9.30	5.87	9.28	5.91	9.15	5.95
ш	12	10,18	6:36	10.15	6.40	10.12	6.45	10,09	6149
	13	11.02	6.89	10.00	6.94	10.96	6.98	10.93	7103
	14	11.87	7:42	11.84	7-47	11.51	7.53	16.77	7157
=	*15	12.72	7.95	12.69	8.00	11,05	E.06	12.62	8 11
	16	13.57	8.48	13.53	8.54	13:49	8.60	13.40	8.66
	17	14.42	0.01	14.38	9.07	14.34	9.13	14-30	0.20
	18	15.26	9.54	15.22	9.61	15.18	9.67	15.14	9.74
	19	16 11	10.07	16.07	10:14	15.01	10.21	15.98	10 28
	20	16.96	10 60	16.91	10.67	16.87	10.75	16.82	10.52
ш	21	17.81		17.76	11.21		11/28	17.66	11.56
	THE REAL PROPERTY.	18,66	11.13	18.61	The second second	17 71	11.82	18.50	
	22	ALL CARLES	12.19	Contract Contract	11.74	18.55	12.36	19.34	15.44
	23	19.51		19.45	12.81	100000000000000000000000000000000000000			man and
	24	20.35	12.72	20.30		20.24	12.90	20,18	12.98
	25	21.20	13.25	21 14	13.34	21.08	13.43	21,03	13.52
ш	26	2205	13.78	21 99	13:87	21.93	15:97	21.87	14:07
	27	21.00	14.31	12.83	14.41	22.77	14:51	22-71	14.61
	28	23.75	14.84	23.68	14.94	23.61	15.04	23.55	15119
	29	24.50	15.37	24.53	15:47	\$4.46	15 53	\$4.39	15.59
	30	25.44	15.90	25.37	16.01	25.30	16.12	15.23	16.11
	31	26.29	10.43	26.22	16.54	26 15	16.66	16.07	16.77
	32	27-14	16.96	27.06	17.08	26.99	17-10	16.91	17-31
п		27 99	17.49		17.61	27.83	17-73	27.75	17.85
80	33	28.83	18.02	28.75	18.14	28.68	18.27	18.60	18.39
	34	29.68	18.55		18.68	100000000000000000000000000000000000000	18.81	29.44	18.01
	35	-	-	29.60	-	29.52		-	
	36	30 43	19.08	30.45	19:21	30.36	19.34	30.18	19-48
	37	31.38	19.61	31.29	19-74	31.21	19.88	31.10	10/01
	38	32.23	20.14	32 14	20.28	32.05	20 42	31.90	20.50
	39	33.07	20.67	32 08	20.81	32.89	20.95	32.80	21.10
90	40	33.92	21.20	33.83	21.34	33.74	21.49	33.64	31.64
24	41	34-77	21.73	34.67	21.88	34.58	22.03	34.48	12.18
1	42	35.62	12.26	35-52	29.41	35 42	22 57	35-32	12.72
	43	36.47	22.79	30.37	22.05	30.27	23.10	36.46	23 26
1	44	37.31	23 32	37.21	23.48	37.11	23.64	37-01	23.80
	45	38.16	23.85	38.06	14.01	37.95	24.18	37.85	14-34
		-	-			Street, Square, or other Designation, or oth			
	46	39 01	=4-38	38.00	24-55	38.80	24.72	38,69	24.88
	47	39 86	74-91	39.75	15.08	39.64	29.25	39.53	25 43
	48	40.71	25.44	40.59	25.61	40.48	25.79	40.37	25.97
	49	41.55	25.97	41:44	26.15	41.33	26.33	41.21	20.51
18	50	42.40	26 50	42,29	26.68	42,17	26.87	42.05	07.05
	51	43.25	27.03	43.13	27.21	43.01	27.40	42.80	17-59
-	52	44.10	27 56	43.98	27.75	43.86	27-94	43-73	28.13
	53	44-95	28.09	44.82	28.28		28.48	44 58	28.67
7	54	45.79	28.62	45.67	28.82	45.54	29.01	45.42	29.21
	55	46.64	29.15	46 52	29 35	46.19	19.55	46.20	20.75
-	56	47.49	29.68	47.36	29.88	47.23		47.10	_
- 1		48 34	30.31	48 21	30.42	48.07		47.10	10.84
1	57	49 19	30.74	49.05		48.92		47-94	31.38
		50.03	31.27	49.90	30.95	49.76	31.70	49.62	31.92
	59 60	50.88	31.80	50.74	31-40			50.46	
-1		-			-	50.60			30.40
	Dist.	Dep.	Lat	Dep	Lat.	D <sub>F</sub> p	Lat	Dep	Lat.
	6	0		41	F - 5	30/		15	-
	-		-	_	DECK				

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Dis	0	3	7.0	Die	31		45	-	ı
346	Lat	Dep.	Lat	Dap	Lat	Dep.	Lat.	Dep.	ı
61	51.73	32.33	51.59	32.55	51.45	32.78	52.14	33.00	ı
63	53:43	33.38	53.28	33.62	53.13	33.85	52.99	34.08	ı
64	54.28	33-91	54-13	34-15	53.98	34-39	53.83	34.62	ı
65	55.12	34-44	54.97	34.68	54.82	34.93	54.67	35.16	ı
66	55-97	34-97	55.82	35.22	55.66	35.46	55.51	35.70	ı
68	56.83	35.50	57.51	35.75	57-35	36.00	56.35	36.25	ı
69	58.52	36.56	58.36	36.82	58.19	37.07	58.03	37 33	ı
70	59.36	37.09	59.20	37-35	59.04	37.61	59.87	37.87	ı
72	60.21	37.62	60.05	37.89	59.88	38.15	59.71	38.41	ı
72	61.06	38.15	60.89	38.42	61.57	38.69	61.40	38.95	ı
73	62.76	39.21	62.58	39.49	62.41	39.76	62.24	39.49	ı
75	63.60	39.74	63.43	40,00	63.25	40 30	63.08	40.57	ı
76	64-45	40.27	64.28	40.55	64.10	40.83	63.92	4ERL	ı
77	65.30	40.80	65.12	41.09	64.94	41.37	64.76	41.66	ı
78	66.15	41.33	66.81	41.62	66.63	41.91	66.44	42.74	ı
80	67.84	42.39	67.66	42.69	07-47	41.98	67.28	43.48	ı
81	68.69	42.92	68.50	43.12	68.31	43.52	68.12	41.82	ı
82	69.54	43.45	69-35	43-76	69.16	44.06	69.97	44.36	ı
83	70.39	43.98	70.20	44.82	70.00	44.60	70.65	44.90	ı
84	71.24	45.04	71.89	45.36	71.69	45.67	71.49	45.44	ı
86	72.93	45-57	72.73	45.89	72.53	46.21	72.33	40.52	ı
87	73.78	46.10	73.58	46.42	73.38	46.75	73-17	47.06	ı
88	74-63	46.63	74.42	46.96	74.32	47.18	74.01	47.61	ı
90	75.48	47.16	75.27	47-49	75.06	47.82	74.85	48.15	ı
91	77-17	28.22	76 96	48.56	76.75	48.89	76.53	49.23	ı
92	78.02	48.75	77.81	49.09	77.59	49-43	77.38	49.77	ı
93	78.87	49.28	78.65	49.63	78.44	49.97	78,22	50.31	ı
94	7972	49.81	79.50	50.16	80.12	51,04	79.06	51.39	ı
95	80 56	50:24	81.19	51,23	80.97	51.58	80.74	51.93	ı
96	82.26	51.40	22.04	51,76	81.81	52.12	81.58	52.47	ı
198	83.11	51.93	\$2.38	\$2,29	82.65	52.66	82.42	53.02	ı
99	83.90	52 46	83.73	52.83	83.50	53-19	84.10	53.56	ı
100	84.10	52.99	84.57	53.36	84 34	53-73		54-10	ł
101	85.65	53-52	86.25	53.93	85.18	54-27	84.94	54.64	ı
103	87.35	54.58	87.11	54.96	86.87	55-34	86.63	55.72	ı
104	88.20	55.11	87.96	55.50	87.71	55.88	87-47	56.26	ı
105	89.04	55.64	88.80	56.03	88.50	50.42	88.31	56.80	1
100	89.89	56.17	89.65	56.56	90.24	57-49	89.15	57.34	ı
108	91.59	57 23	90.49	57.10	91.00	58.03	90.83	58.42	ı
109	92.44	57.76	92,18	58.16	91.93	58.57	91.67	58.97	ı
110	93 29	58.29	93.03	58.70	9277	59.10	92.51	59-51	ı
933	94.13	58.82	93.88	59.23	93.62	59.64	93.36	60.05	١
113	94.98	59.35	94-72	59.76	94.46	00.71	95.04	60.59	I
114	96.68	60.41	96.41	60.83	96.15	01.25	95.88	61.67	1
115	97-53	160.94	97-26	61.37	96.99	61.79	96.72	62.21	I
116	98.37	61.47		61.90	97.83	62.33	97.56	62.75	1
327	99.22	62.00	98.95	62.43	98.68	62.86	98.40	63.29	1
118	100.1	61.53	100.6	63.50	100.4	63.40	100.1	64.38	I
120	101.8	163.59	101-5	64,03	101.2	64.48	100.9	64.92	1
1 2	Dep.		Dep.	Lat.	Dep	Lat	Dep.	Lat	1
Dist		0'	- 45	1	30	)/	1	5'	1
-		_			S CP CP CP CP				-

1	1 0	1/	1-	15/	1	30/	1	(50)
1 8	Lat	Dep.	Lat	Dep.	Lat	Dep-		Dep
100	The second second		-1	The same	-		The real Party lies	
13	and the second	1.09	1:67	1.10			1.66	0,56
1 3	W 3000	1.63	2.51					1.67
1 4	40 1000 1400	2 18	3.35	2.19			3.33	2.11
103		2/72	4 18	2-74	4 17		4.16	2.78
1 6		3.27	5.02	3.29	5.00	3.31	4-99	3-35
1 2		3.81	5.85	3.84	5.84	3.86	5.82	3.89
_		436	6.69	4-39	6.67		6.65	4-44
9		4.90	7.53		7.5		7.48	5.00
10	_	5-45	8.56	5.48	8.34	-	8.31	5.56
1 33		5.99	9.20	6.03	9.17		9.15	6.67
13	ST STREET, ST.	7 08	10.87	7.13	10.84		10.81	7.22
14		7.62	11.71	7.68	11.67		11.64	7-78
15		8.17	12.54	8.22	12.58	8:48	12.47	8.33
16	13.42	8.71	13.38	8.77	13.34	8.83	13.30	8.89
1 17		9.26	14.22	9.32	14.18	9.38	14-14	9-44
18	15.10	980	15005	9.87	15:01	9.93	14.97	10.00
19	15.93	10.35	15.89	10.42	15.84	10.49	15,80	10.56
20		10.89	16.73	10.97	16.68	11 04	16 63	ILII
21	17.61	11.44	17.56	11,51	17/51	11.59	17.46	11.07
22	18.45	11.98	18.40	12.61	18.35	12.14	18.29	12.78
1 44	20.13	12.53	20.07	13.15	19.18	13.25	19.12	13.31
25	20.97	13.62	20.01	13.71	2018 5	12.80	20.79	13.50
26	21.81	14.16	21.74	14.26	21.68	14:35	21.62	14:44
27	22.64	14.71	22.58	14.80	23.55	14.90	22.45	15.00
28	23.48	15.25	23.42	15.35	23 35	15.45	23.28	15.50
20	24.32	15.79	24 25	15.90	24.18	16,01	24-11	15.11
30	25.16	16 34	25.09	16.45	25.02	16.56	24.94	16.07
31	26.00	16.88	25.92	17.00	25.85	17:11	25.78	87.22
32	26.84	17.43	26.76	17:55	26.68	17.66	26.61	7178
112	27.68	17.97	27.60	18.09	27.52	18.11	27:44	18.33
34	28.5t	18.52	28.43	18.64	28.35	19.32	28.27	19-44
		-			-	-	-	20.00
35	30.19	20.15	30.11	19.74	30.02	19.87	30.76	20.56
38	31.87	20.70	31178	30.84	31.69	20.97	31.60	21111
39	32.71	21.24	32.62	21/38	32.50	2L53	32 43	21.67
40	33-55	21.79	33.45	21.93	33 36	22.08	33-16	22.22
41	34-39	22.33	34.29	22,48	34.19	22.03	34.00	22.78
42	35-32	12 87	35.12	23,03	35.01	23.18	34.92	93.33
43	36.06	23.42	35.96	23.58	35.86	23.73	35.75	13.59
44	36.90	23.96	36.80	24.12	36.69	24.29	36.58	24-45
45	37-74	24 51	37.53	24.67	37.52	24-84	37-92	13.00
46	38.58	25.05	38,47	25.22	38.36	25.39	34.29	25.56
47	40.26	25.60	39-31	25.77	40 03	25.94	39.91	26.11
49	41.09	20.69	40.98	26.87	40.86	27.04	40.74	27.33
50	41.93	27.23	41.81	27.41	41.69	27.60	41.57	17.78
51	42.77	27.78	42.65	27.96	42.53	28.15	42.40	28.33
54		28.32	45.49	28.51	43.36	28.70	43.24	28.89
53	44-45	28.87	44-32	29.06	44.20	29.25	44.07	19 45
54	0.00	29 41		39.61	45.03	29.80	Interest Control of the Control of t	30.00
55	Section 2 is	29.96	40.00	30,16	45.86	30.36	-	30.55
56		30.50		10.70	46.70	30.91		31.11
57 58		31.04		31.25	47-53	31.46	1000	11-07
59	The second second	31.59		32.35	48.37	33.01		12.22
60		32.68		32.90	50.03	33.12		3-33
4	Dep.	Lat.	Dep.	Lat	Dep.	Lat	Dep.	Lat.
3	0/		45		30	-	Treat	-
	-			DECE			107	Second 1

	0/		15	,	30	<u>,,</u>	1 4.	37
Dist	Lat.	Dep.	Lat.	lk:p.	Lat	Dep.	lat.	Dep.
		33.22	51.01	33:45	50.8	33.07		33.84
61	51.16 52.50	33.77	51.85	33 99	51.70	34 22	51.55	34.45
63	52.84	34.31	52.64	34 54	52 53	34	52 34	15.00
64	53.67	34.86	53-52	35.39	53.37	35.32 35.8	(3.21	35 56
65	54.51	35.47	54 36			39.43	54 05 54 05	36 67
66 6;	55.35	35.45 36.49	55.19 56.03	36 19 36 74	55.57 55.87	36.95	54.88	322
68	57.03	37.04	56.8-	3- 28	56.70	3-53	56.54	3>
69	587	37.58	57.70	37.83	57-54	38.08 38.64	57.37	38.31
70	58.71	38 12	58.54	38.38	54.;-			· — <u>-</u>
71 72	59 55 60.38	34.6~ 39.21	59.38 60.21	34.43 39.43	59.21 65.04	39-19 39-7	59 č. 59 8-	40.00
-3	61.22	346	61.35	:223	65.5-	45.29	65 73	40.56
74	62 06	40.33		;3.57	611	10.84		41.11
75	62.43	42.85	622	11 12	62 54	41 40	62 35	11.6-
76	63.74	41.39	63.56 64.59	.;1.67 ;2.22	64.38	41.95	63.19 64.02	42.22 42.78
77 78	64.58	41 94	04.39	42.77	650+	43 05		: 43-33
79	66.25	13.03	66.37	13.32	65.88	43 65	65 67	43.84
8ó	609	43.57	66 92	43.86	661	11.16	66.52	14 45
81	67.93	44 12	67.74	4441	67.54 68.38	44.71 45.26	67.35 68.18	45.00
82 83	64.77 09.61	41.66	68.58 69.41	44.96 45.51	69.21	45.20		45.56  46.11
84	72.45	45.75	70 25	≟6 <b>5</b> 6	-50;	16 36	69 84	15.57
85	71.29	46.29	71 28	<del>46.60</del>	-2 88	46.91	70 6-	47.22
86	72.13	46.84	71.92	47.15	71.71	+7 47	71.51	47.78
87	72.96	438	72 -6	47.70	72 55	48.57	72.34 73.17	48.89
88 89	73.80	4~-93 48.4~	73.59	48.50	7,22	49.12	74 00	÷9.45
90	75.48	19.02	75.27	49-35	75.55	49.67	7483	50.00
91	76.32	49.56	76 31	19.84	75.88	50.23	75.66	50.56
92	77.16	50.11	75.94	50.44	76.72	50 78	76.50	51.11
93	78.00	50 65	77.77	50 99	77.55 78.39	51.33	77.33 78.16	51.67
94 95	79 67	51.74	79-45	52.00	79.22	52 43	78.99	528
96	80.51	52.29	80.28	52.64	80.05	52.99	79.82	53-33
97	81.35	52 83	81.12	53.18	80.89	53-54	80.65	13.89
98	82 19	53-37	81.96	54.28	812 82 55	54.64 54.64	81.4S 82.32	14.45
100	83.03 83.87	53 92	83.53	54.83	83.37	55.19	83.15	15 56
101	84.71	55:01	84 46	55 38	14 22	55.75	83.98	56 11
102	85.54	55-55	85.30	55.93	85 06	56.30	84.81	56 67
103	86.38	56.10	86.14	56.47	85.89	56 85	85.64 86.47	57.22
104	87.22 88.06	519	86.97 87.81	57.57	856	57 40 57 95	8- 30	57.78 58.33
106	88.90	57.73	83.65	53.12	88 39	58.51	88.14	58.89
107	89.74	58.28	89 48	58.67	89.23	59 CG	88 97	59 45
108	90.58	58.82	90.72	54.22	95.56	59.61 60 16	89.80	60.00
1109	91.42	59.37	91.10	59.76 60.31	95.89	60.71	90 63 91 46	60.56
111		60.45	92 83	60.86	92.50	61.26	92.29	61.67
1112	93.09	61.00	93.66	61.41	93.40	61.82	93.12	62.22
113	94.77	61.54	94.50	61.96	94 23	62 37	93 96	62.78
114	95.61	62.63	95.34	63.51	95.06	62.92	94 79	63.34 63.89
115	96.45	63.18	97.01	63 60	96.73	64.02	95.62	64.45
1116	97.29	63.72	97.85	164.15	97.56	64.58	9".28	65.00
118	98.96	64.27	98.68	64.70	98.40	65.13	98.11	65 50
119	99.80	18.40	99.52	65.25		65.68	98.94	. 66 11
120	100.6	65.36	100.4	lat	100.1	Lat	11	
뙲	Dep.	late	Dep.		Dep. 30			
12	1	) <i>'</i>	76 76			,		

1 5	. 0	,	1 1	51	7 9	0'	45	-
Dist.	Lat.	1 Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.81	0.56	0.83	0.56	0.82	0.57	0.81	0.57
1 2	1.66	1.12	1.65	1.13	1.65	1.13	1.64	1.14
3	3.33	1.68	3.31	1 69	3.30	2.27	3.19	2.38
5	4.15	2,80	4.13	2.81	4.12	283	4.11	2.85
6	4-97	3.36	4.96	3.38	4-94	3.40	493	3-42
7 8	5.80	3.91	5-79	3.94	5.77	3.95	5.75	3-99
9	7.46	5.03	7.44	5.07	7.43	4.53	7-39	4-56 5-13
10	8.29	5.59	8 27	5.63	8.24	5.66	8,22	5.70
71	9.12	6.15	9.09	6.19	9.07	6.23	9.04	6,27
13	9.95	7.27	10.75	7-32	9.89	7.36	9.86	7.41
14	10.14	7.83	11.57	7.88	11.54	7.93	11.50	7-98
15	12.44	8,39	12.40	8.44	12 36	8.50	12:32	8.55
16	13.26	8.95	13.23	9.57	14.01	9.06	13:15	9.12
17	14-92	10.07	14.88	10.13	14.83	10.20	14.79	10.25
19	15.75	10.61	15.71	10.69	15.66	10.76	15.61	10,53
20	16.58	11.74	16.53	11.82	17.31	11.89	17.24	11,4D
21	17.41	12 30	17.36	12.38	18.13	12.46	18.08	1 L-97 1 h-54
23	19.07	12.86	19.01	12.94	18.95	13.03	18.90	13.11
24	19.90	13.42	20.66	13.51	19.78	14.16	19-72	13.68
26	21 55	14.54	21.49	14.63	21.43	14-73	21.36	14.82
27	22 38	15.10	22.32	15.20	22.25	15.29	22 18	15.39
28	23.21	15.66	23.14	15:76	23.08	15.86	23.85	15.96
30	24.04	16 78	23.97	16.88	23 90	16.99	24.65	17-10
31	15.70	17.33	25.62	17.45	25.55	17.56	25 47	17.67
32	26.53	17.89	26.45	18.01	26.37	18.13	26.29	18-24
33	27.36	18.45	27.28	18 57	27.20	18.69	27.11	13.81
35	29.02	19.57	28 93	19 70	28.84	19.82	28.76	19.95
36	29.85	20.13	29.76	20.26	29.67	20.30	29.58	20.52
37	30.67	20.69	30,58	20.82	30 49	10.96	30.40	21.00
39	32.33	21.81	33.24	21.95	32.14	22.09	31.04	11.23
40	33.16	22.37	33.06	22.51	32-97	22.66	31.87	22.80
41 42	33 99 34.82	23.49	33.89	23.64	33-79	23.22	33.69	23-37
43	35.65	24.05	35-54	24.30	35.44	24.36	34-51	24-11
44	36.48	24.60	36.37	24-76	36.26	24.92	36.15	25.08
46	37-31	25.16	37.20	25.33	37.09	25.49	36.97	25.65
47	38.14	25 72 26.28	38.02	25.89	37-91	26.62	37.80	25.79
48	39-79	26.84	39.68	27.01	39.56	27.19	39-44	47-36
49	40.62	27.40	40.50	27.58	40.38	27.75	40.16	27-93
51		28.52	41.33	28.70	42.03	28.59	-	19.07
52	43.11	29.08	42 98	29.27	42.85	29.45		39.64
53	43.94	29.64	43.81	29.83	43.68	30.01	43-55	30.21
54	44-77	30.20	44.64	30.95	44-50	30.59	45.19	30.98
56	46.43	31.31.	46.29	31.52	_	31.72	46.01	11 92
57	47.26	31.87	47-12	32.08	46.98	32.29	46.83	32.49
50		32.43	47-94	32.64	47.80	32.85	47.66	13.06
57 58 59 60		33-55	49.60	33-77	Decision 1	33.98	49.30	4 10
Dist.	Dep.	Lat	Dep.	Lat	Dep.	Lac	Dep.	Lat.
5	01	1	4			0,	F 72	
	_		63	DEG	REES.		37000	

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110	-	,	-	134	1	20.		45"	-1
1 35	Lan	Dep		Dep	Lat:	D-D	Let	Dep.	4
	1 5257		50.41						ı
16	52.23	34 57	1208				50 94		1
6.		35.29	\$190				52.59	III PORTON	н
10	5 53.80	36 35	\$3.73	35.58	53-57	35,84	53 41	137.05	а
	54-72		10000			-	54/23		п
61	THE RESERVE	37-47					55.87		ı
6		38 18		A Property of	1000000		36.69		п
1 36	The state of the s	39.14	0.00				57.92		4
7:	58.86	39:10					38,34	40 47	1
1 23		40.26			59-14		39 39		ı
74	61.35	41.38	60.14	41.65			59.98 60.80		Ł
25		21.94	61.99	42.25	100		Dr.ba		ı
10	63:01	42 50	62.82	44.77	64.63	43.05	SE45	43-32	н
12		43.00			61,46				1
78					64 15		Baux	95.07	1
179	III DOMESTIC OF THE PERSON NAMED IN	44.74		45-92	\$4.01	45.31	65473	45.60	1
Si		1000	66.05	No.	100.12	45.88	60.55	46.12	ı
1 80	67 98 .	45.85	67.58	40.45	47-58	48.45	62-17	46.74	1
130	18.20	DATE OF THE PARTY	68.61	46.71	65.40	47.01	68,10		ı
84	70.47	40.97 47.57	70.26	47.83	70.05	47-58	69.84	47.88	ŧ.
86		48.00	71.09	The second second	70.87		70 66		u
B#	72.13		71.91	48 46	71 70	49 28	71.48		н
1 38	(2.00)	_	72.74		72 52	49.84	72,30	500000000000000000000000000000000000000	ı
80	73.78	49.77	73 57	50.05	73.35	\$0.41	73.13	\$7.7.E	ı
92		502.58	75.52	51.22	75.00	91.54	74-77	100	D
91	and the second	\$0.89 \$1.45	76.05	51.78	75182		25:59	\$5.00 \$7.46	н
93	77.10		76.87		76.64	52.68	76.41	53:01	н
94		72 96	177.70		77-47		77-23	53 5E	и
95		51.12	78 53		78.29	55.81	78:00	54.15	а
90	ALCOHOL: N	53 68	49.35		79194	54.94	79.70	55.00	я
98	The second second second second	C4.80	2101		30.76	55.51	80.53	22 86	9
99		\$ 8.36	15 t. K3		81.59	36.07	81/34	59-43	П
100	Print makes	55 02	81,66	56.28	82.45	56.64	152 16	57.483	ľ
101		(5.43 ) (7.0a	Bags	56.84	34.00	37.21	82.99	57-57	
103		CT.60	Sping .			58 34	84.63	58.71	
104	86.22	58.10	8 0.47	38.53	85.74	58.91	85-45	59.28	
105	THE RESERVE OF	58.72	86.74	39.09	86.55	59 47	86.27	39.85	
107		9 27	86 az	69 66	\$7.36 \$8.18		E7-09	60.41	
108	Total Control of the	19.83 12.50	89 37		89.01	61.17	88.74	60.99	
100			90.10	61.35	89 83	61.74	89.56	61 13	
210		1 61	67.02	6.1104	90.65	B± 30.	00.38	61.70	
Ett		207		62.47	91.48	61.87		63.17	
EI3		2.63	92.58		92.30	64.00		54.41	
114			94.41			64.57	93.67	64.98	
reg		111		04.72	94-77	65.04		65.55	
215	DESCRIPTION OF THE PERSON NAMED IN	437		05.29		05.70	95-31	06.72	
117		5 43		5685	90.42	66.27		00,69	
EIG I		6.54		56.97		65,84		67.83	
120		2.10		7.54		67.97		68 40	
14	minima many in	Luci	Dep	Lat.	Dep.	1.00	Dep.	Test	
3	07	1	457	-	30	T	-	51	1
		-		DEGR				-	=

	-	751		-		700		- 45	-
1 0	1	0,	-	100		30		- 65	-
1		_fat	Dep	Lat	Dep.	Lat	Dep.	Lat	Dep
1	1	0.82	0.57	E.82	0.58	0.81	0.58	0.81	0.55
1	4	1.64	1.15	1-03	1.65	1.63	1.10	2,62	BART
п	1	240	1.75	2.45	1-73	2,44	1.74	243	149.8
ш	4	9.28	2 29	3,27	131	3.20	3-33	3:25	514
14	3.1	4-10	2.87	4.08	2,39	4-07	1.90	4.00	2.02
и	0	4.91	3.44	4.90	3.40	4.55	3.48	487	3:51
и	7	5.73	4101	5.72	4.04	510	2,06	5,68	4.09
ш	8	0 55	4-59	6.53	4.63	7:33	4.65	7930	4/07 5/20
ш	0	7:37 8:10	5-10	7.35	5:15	8.14	5.23	8,42	3.84
	-		5.74		$\overline{}$	8.96	-	-	bal
		9.01	0.88	8.98	6.93		6.39	8,93	7401
_	3	10.65	7.46	10.62	7.50	9.77	7-55	9.54	7.60
	4	11:47	8.03	11.43	808	11.40	8.13	11.76	8.18
	15	12.29	8.60	12,25	8.66	12.71	8,71	12 17	8.76
	16	13.11	9.18	13/07	9.23	13.03	0.30	12.00	9/35
	17	13.93	9.75	13.88	0.81	13.84	9.87	13.20	9:93
	18	14:74	10.32	14.70	10.39	14.65	10.45	14.61	10.48
	10	15056	10.90	15.52	10.97	15147	10.03	115-42	11.10
	10	10:18	11.47	16,33	11.54	16,28	11.61	16.23	11.69
1	11	17.20	12.05	17 15	12 12	17.10	12.19	117:04	12.27
	12	18,02	12.62	17.97	11.70	17.91	12.78	17 85	12.85
12	1	18.84	13.19	18.78	13.27	18.72	13.36	18.67	73.44
	24	19.66	13.77	19.50		19:54	13.94	19.48	14.03
	15	20.48	14-14	20.42	14.43	20.19	14.52	20 19	14 fit
ı	ê	21.30	14.91	21.23	15.01	26,17	15.10	21.10	15-19
	17	22,12	15.49	22.05	15.58	21.98	15.68	21.91	19.77
	18	22.94	16.06	22.87	16.10	12.80	16 26	22.71	10-35
	10	13 76	16.63	23.63	15.74	23.61	16.84	23-54	18-54
	30	34-57	17.21	24:50	17-31	24-42	19.42	14:15	17-13
	91	25.39	17-78	25.32	17.89	25:24	18 00	35.10	18.11
	12	26.21	18.35	26.13	18.47	26.05	18.58	35.0*	1 K 10
	33	27.85	18.93	16.95	19.62	20.87	19.16	26 78	19 28
	14	18 67	20.08	27.77	20.20	28.4-1	19.74	27 59	19.86 10.45
-			-		1				
	36	29.49	20 65	29.40	20.78		20 91	29.21	21.03
	37	31.13	21.22	31 03	21.93	30.04	21.07	30.84	31.61
	39	31.95	22.37	31.85	22 51	3175	22.05	31.65	22.79
	10	32.77	22.94	32 67	23.09	32.56	23.23	33.46	23.37
	_	33-59	27.52	33.48	23.66	33.38	23 81	33-27	28.85
	11	34-40	24.09	34-30	24 24	34.19	24.50	34.09	20.54
	43	35.22	24.00	35 12	24.82	34.01	124.07	34.90	25.12
	14	36.04	=5.24	35.93	25.39	35.82	25.55	35.71	25.71
	4.5	36.86	25.81	36 75	25-97	36.64	26.11	36.52	16129
	16	37.68	26.38	37-57	\$0.55	37-45	26.71	37-31	26.88
	+7	38.50	26.96	38.38	27,13	38.26	27.29	38.44	27.46
	48	39 32	27.53	\$9.40	27.70	39.08	27.57	138-46	25 04
	49	40.14	28.11	40.02	28.28	39.89	28:45	39-7.7	35.63
1	50	40.96	28.68	40.83	25.86	40.51	29.04	40.5%	29.21
	51	41.78	29.25	41.65	19.43	41.52	19.62	41:30	29.50
1	52	4.2.60	29.83	41.47	30,01	42/33	30,20	42,20	30 38
100	53	43.42	30.40	43.28	30,59	43.15	30.78	43.01	30,97
18	54	44.23	30.97	44.10	31.17	43-95	31 36	43.83	31.55
	55	45.05	31,55	44193	31.74	44.78	31.94	44.64	32.13
	50	45.87	32.12	45473	32,30	45-59	32.50	45.45	32.72
1	57	40.69	32.09	46.55	11.90	45-40	33.10	46.46	33-30
1	58	47.51	33.27	47:37	33-47	47.22	33,68	47.07	33.89
1	59	49.15	33.84	48 18	34 63	48.85	34.84	47.88	34-47
_			Married Woman or		THE REAL PROPERTY.				15.06
	Dist	Dep	Lut.	Dep.	Lati	Dep	Lat	Lep.	Lat.
1	R	0			5"	30		1 15	1
			-	_	- NAME OF STREET	MNE			

55 DEGREES.

1	-	-		_	_			-	
	12	1-0	ν.	1 13		-	30/	1 - 4	5
	No.	Late	I Dep	Lat	Dept.	List.	Thip	Lat.	Degi
п	61	89-97	36-99	89.62	39 24	49.56	75-42	09-51	15.64
п	62			50.63		I STARK	28.00	1 99.11	20.12
в	by	E1.61	26.14	5X45		51.29	24.58	Stat	36,51
ш	64	52.43	28/21	68-97	39-94	58.90	27-16	SLOS	37-39
8	65	53-84	23.08	93.94		62.42	17-75	21.12	37-91
в	100		37.86	4140	BLOW	53.73	28.32	43-49	38.16
п	59	34.55	35.45	64-71	38.67	14-55	Lat	54-18	39-14
ш	56	55.00	39.00	55-53	39-35	\$5.35	79-49	\$5.19	139.71
М	fiè		39-58	54.75	Zh-Ez	SE 17	40.07	\$/L00	417.31
u	90	57/54	40.15	\$7.10	40.40	45.49	40.65	56.51	417 00
п	71	SEIN	49.72	£7-08		57780	41,33	57.61	4648
0	72	58.44	41,30	AR SO		59.61	41,81	58-43	142,07
8	73	54.80	44,57	Egiot		59.43	44.39	59-14	47.65
3	73	50.61	42-44	60.45		50,24	92.97	fsp.06	杨级
н	75	61,44	13,01	61,05	43/39	61,05	42.75	60.87	43.72
п	7.5	62,26	43-39	61.06		61,57	49:13	01.55	141.40
и	7.7	63.07	44-17	fib.EE	45-44	61.09	44.78	62.49	44-99
8	78	63,89	44:74	49.70	45.003	65.50	45-29	61.10	145-17
ı	79	64-71	45.31	fielgi	45-59	64.32	44,45	64.11	45.16
в		85153	45-89	165-33	45.17	65 13	46.46	64.45	46.74
и	81	66.35	46.46	66.15	46.75	65.94	47.04	65.74	4 31
н	81	67,17	41.03	60.46	47/33	66.76	47.62	66.55	47.04
в	83	48.81	47.61	65.78	45.48	67.57	48 10	67 15	48.49
в	84	69.63	48.75	59.41	49.05	66 Ig 60 00	48.78	68.17	49.6h
н			-	1			49.36		
и	86	70.45		70.23	49.63	T0.01	49-94	60.80	50.17
и	88	71.09	49.90	71.05	30.21	71.64	50.53	70,61	SOUTH
п	23	72.90	51.05	72.63	30.79 S1.37	72.46	51.68	74-42	52.00
и	93	73.74	51.62	73.50	SLOF	73.27	52.26	75.04	52.58
н			58-80	1000				73 85	(A) (S)
ı	91	74-54	LOCATION	79-51	52.51	74.08	53,84	74.66	53-75
۰	93	76.13	53-94	75-13	\$3.67	74.90	59.42	75.48	54-11
п	94	77-60	53.92	76.76	54-25	76.53	54-59	76.29	24-91
и	95	77.82	54-49	77.58	54 83	77-84	55-17	77-10	55-50
1	46	78.64	55.00	78,40	\$5-41	78.16	55.75	77.91	50 Du
и	97	79-40	55.64	70 21	55.48	78.07	56.33	78.73	56.67
и	98	80.28	56.21	80.03	50.56	79-78	56 92	79.53	57-46
п		81.10	56.78	80.85	\$7.14	80.60	57-49	80.35	57.84
1	100	\$1.92	57 36	81.66	53 (21	81.41	58 27	81.16	38.42
п	DE	82.73	57-93	82.48	58.29	Na.ar	58.65	\$L97	54.01
	EDE	83.55	58 50	83 30	58.87	82.04	50.23	82.78	59-10
н	03	84-37	59.08	84.14	59-45	\$3.85	59.8L	83.59	60.18
	04	85.19	59.65	84.93	60,D#	\$4.67	60.39	84.40	60.90
1	05	86:01	60.13	85.75	60,60	85.48	60 97	85.22	61-41
	06	36.83	60.80	86.46	DL.18	86.30	61.55	86.03	1911
	97	87.65	61.37	87.18	51:75		62.14	86.84	D1 61
	08	88.47	51,95	88.20	5133	87.92	62.72	87.65	03.08
	00	89.29	62.52	S9.04	62.91		63.30	88.46	54.57
10	10	90.11	63,09	89.83	63.49	_		-	personal services
	11	90.93	63:67	40.65	64.06		64 46	The second second	04.55
	63	91.74	64 44	91.46	64.64		65.04		00.02
	3	92.56	64.81	92.28	65.22		66.20	02.72	00.00
	14	93.18	65 39	93.10	66.37		66.78		57 19
16			65.96	93.94	and in case of Females,		-	44 FA 1	13/46
	10	95:02	06.53	94-73	66.95		67.36	94-14	N 26
	17		67.11	95.55	68 10		68.52	94.77 5	State
	18		67.68	96 36	68.10		69.10	95 58 6	9.83
	19		68 83	98.00	69.26	97.69	69.68	97.39 7	C II
	-	-	-	1kp	Lat.	Dep	Lak.	Dept	Lan
	1	Dep.	Lati		_		-	15	
	3.	0,	-	43		30'	The same of the		
	-	-		26.0	END CLERK	APRIL TO SERVICE			

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1 21	1 0	1-	1	5/	30	7	1 4	-
1	Lat	Dep	Lat.	Dep	Inti	Depi	Lat	
-	1000		-		0.80			Dep-
1 :	1.62	0.59 E-18	1.61	1.18	1.61	1.14	0.80	1.00
3	2.43	1.76	2.42	1.77	2.41	1-78	2.40	670
4	3.24	2:35	3.23	2.37	5-11	2.38	3 20	110
5	4:05	2.94	4-03	2:96	4.92	297	501	2-99
6	4 85	3-53	4.84	3.55	4.82	3.57	+81	3-19
7 8	5 66	4.11	5.65	4-14	5.63	4.70	5.61	4.19
9	7.38	5.29	7.26	5-32	7/23	5.35	7,21	4-70 5-50
10	8.00	5.88	8.06	10.3	8.04	5.95	8,01	5/05
11	8.90	6.47	8.87	6.50	8.84	6.54	8.81	6.58
12	9.71	7.05	9 68	7-10	9.65	7.14	9.61	7.11
13	10.52	7.64	10.48	7.60	10.45	7/13	10.41	7-78
15	11:33	8.23	11.10	8.28	11.25	8.92	12.02	8.92
16	12.94	9.40	11.90	9.46	12.86	0/50	12.52	-
17	13.75	9.90	13.71	10.05	13.67	10.11	15.60	9:57
18.	14.56	10.58	14.52	10.64	14.47	19.71	14.42	10.77
19	15:37	11.17	15.51	11.23	19.27	11 10	15.22	11.57
20	16,18	11.76	16.17	13.83	10.08	11.60	16.03	11/97
21	16.99	12.34	16.94	12-92	16.88	12.49	16.83	1256
22	17.80	12.52	17.74	13.01	17.68	13.50	17.03	13.76
24	19.42	14:11	19.35	34.19	19.29	14.28	19 ==	14:30
135	80,23	14.69	20.16	14.78	20.10	14.87	20.03	24.90
36	21.03	15.28	20,91	15-37	20.90	15:47	20.83	15.55
27	21,14	15.87	21/17	15.97	21,70:	16.06	21.67	16.35
28	22,65	16 46	21.58	16.56	12.51	10.05	22.44	16.75
30	23.46	17.05	13.39	17:45	25.31	17-25	24.04	17-35
_	25.08	18.22		17.74	24.10		-	17.95
31 32	25.80	18.81	25.00	18.33	24.92	18:44	25.64	15:35
33	26.70	19-40	26.61	19.51	26.53	19.63	20.44	19.74
34	27.51	19.98	27.42	20.10	27,33	10.21	80.84	10.14
35	28.32	20.57	28.23	1070	18.15	10 83	SK.04	20.92
36	29 12	21.16	19 03	21-29	28.94	21.41	25.55	24.34
37	29.93	21.75	29.84	21.28	20:74	22.01	29.55	22.14
38	31.55	22,34	30,04	22 47	30.55	22,60	31-25	27.74 23.33
40	32.36	23.51	32,26	23.65	32.15	23.70	1200	23495
41	33 17	24-10	11.06	24.24	32.96	24.59	32.84	=4.53
42	33.98	24.69	11.87	24.83	33.76	14.98	35-65	15.15
43	34.79	19 27	34.68	25.43	34-57	25.58	34.45	28-72
44	35,00	25.86	35.48	26,02	35.37	26.17	35-36	26.150
45	30.41	26.45	36.29	26.61	36.17	26.77	36406	u6.gz
40	37.21	27.04	37.10	27.20		27 36	36:86 37:56	27,52
48	38.83	28.21	38.71	28.38		27.96 18.55	3846	28/22
49	39.64	28.80	39.52	28.97		29.15	39.26	19.51
50	40.45	29.39	40.32	29.57		29.74	40.06	29.42
51	41.26	29-98	41-13	30.16		19.34	40.86	30.41
52	42.07	30 56	41.94	30.75		30.93	41.00	SERE
53	43.69	31.74	47.74	31.34		31.53	42.47	31.71
54	44.5D	32.33	44-35	32,52	44-21	32-51	44.02	12.31
56	45.30	32.92	45-16	33,41		33-31	44.87	35-51
57	46.11	33.50	45.97	33-70		33.90		34-10
57 58	46:92	34.00	45.77	34.30	46,62	14.50	40.47	34.70
59 60	47-73	34.68	47.58	34-89		35.09		35-30
	48.54	35.27	48.39	35.48	48.23	35.69		15:40
Dist	Dep.	Lat.	Dep.	Late	Dep.	Lat	Bep.	Lat.
- E	0.		45	WC DO	30	'	15	1

A Company	and the same				100 M	-		
21	01	-	1.5	55	3	1/	45	A CHILD
5	Lat	Dep.	Lat	Dep	Late	Dep.	Late	Dep.
-	-	Department of	-	-	-	-	48.83	-
61	49.34	15.85	49 19	36,07	49.04	10.28	III. Married	\$6.70
61	50,16	30.44	50,00	36,66	50.64	37-47	49.6X	37.69
64	59,97	37.03	51.61	17.84	51:45	38.07	51.28	38.59
05	54150	3820	(B)4B	18:44	52.25	18.66	SEOR	38.80
200	The same of the		-	1	-		-	The second second
66	53:40	35.79	53-21	34.93	53005	39.36	52.88	19-40
68	54/30	29:35	54173	40.11	51.86	30.35	53.68	40.00
50	55101	19.97	55.00	40.80	55-97	41.04	55.29	41.28
90	(6.61	41/14	56145	41.39	56,22	41.64	50.04	41.88
10000		11041	57/10	100000	_	43.33	-	2100000
72	57:44	47.32	58,00	42.57	57.88	42.83	50.89	42.98
73	59.06	42.91	\$8,87	43-17	100000	43.42	58.49	
74	59.37	43.50	30.05	43.76		44.02	59.29	
75	60.68	44.08	60:48	44-35	60,29		60:09	44.87
76	61140	-	61.29	44-94		45.21	6a.ga	
70	62.29	44.07			51 90		61-70	45:47
78	63.10	45.85	61.90	49.12			62 50	
79	67.91	46:43	63.71	40.71			63.30	47.27
80	64.72	47 03	64.52	47-30	04.31		64 10	47.87
81	65.53	47.61	65.32	47.99	64.11	48.18	64.90	48.46
82	66,34	48:30	66.13	48.49	65.92	48.78	69.70	49.00
82	67.14	48.79	66.93			49.37	66.50	49.66
84	67.96	49-57	67.74	49.67	67-52	49-97	67-38	40. ati
35	68 77	49.96	68.55	40.26	68.33	59.56	68 LL	50.86
86	69 48	50.95	69.35	50.85	69:13	51.15	68.41	\$1.46
87	70.38		79.16	1000	69.94	51.75	69.71	20.52
88	74.19	51.73	79.97	52,04		52.34	70.51	\$2.65
89	72,00	52 31	71127	\$2.63	71.54	52-94	7031	53.25
90	7231	51.90	72168	\$3.32	72.35	53.53	72.11	\$4.85
91	73.62	53-49	73-39	53.81	73.84	54-13	72/91	98 45
92	74-43	54.08	74.19		73.95	5472	73.72	55-00
93	75/14		75.00		7470	55.32	74.52	55.64
1 94	78.05		75.81	15-58	75.56	\$5.94	75-32	\$0.24
95	76.86	55.84	76.61	56.17	76.37	56.51	76.12	56 84
96	77.67	56.43	-77,42	46.77	77417	57.10	76.94	57:44
197	78.47	57.92	78.23	97.36	27/97	197.70	77.72	58.04
98	79/28	57.60	79.03	57.95	78.78	28.29	78.52	58 mg
99	80.09	58.19	79.84	58.54	79.5%	98.89	79.32	59.23
100	80.90	58.78	80.64	59.13	80.39	59.48	80-13	59.87
101		59-37		59.72	\$1.19	60.68	80.93	60.43
	82.52	59.95		60.31	81.99	62.67	81,73	61,01
	83.71	60.54		69.90	81,80	61.27	82 53	61.63
104		61.13		61.50	31.00		81-13	61.23
105	34.95	61.72	The latest designation of	51 04	24.41	-	34-13	Q5.83
106	85.70	62.31		61.68		65.05		5142
	86.56	100000000000000000000000000000000000000	86.29		55 01	61.69		64 01
	87-37	63.48		63.86			86.54	04.02
	81.88	64.66	87.90		88,42		87-34	04.22
	88.99		10000	65.04	-	05.45	1	Ser Loncoln
111	89.80	65.24		65.64	89.23	66.03		66 41
112	90.61	65.83		66.23	90,03	00.02		67.04
112	91-42	66.42		60.81	60.84	67.22		67.64
114	93.04	67.60		05.00	92.44	68 40	91 14	68.21 68.81
1	Allenania.	-	-		-		92 14	1
116	93.85	68.18	100000	68.59	93/25	69 00	92,95	69.41
117	94-65	68.77	94-35		94.05	69.59	93-75	70.00
1118	95.27	69.36	95.16	69.77	94.86	70.78	94-55	70.60
110	97.08	70.53	95.97	70.45	96.46	71.38	95.35	71.80
1	THE REAL PROPERTY.	The same of	1		17000000	The same of	-	1.
1	Dep.	Late	Dep.	Lat.	Dep.	Lat	Dep.	
8	1		4	31	30		13	27

50	11 0	)/		51		101		50	1
1 ste	Lat	[ Dep.	Lat	Dep.	Late	Dep-	Lat.	Dep.	A
-	0.80	0.60	030	0.61	0.79	0.61	P-70	01.61	i
_	1,60	1.20	1159	1101	1159	1.22	1.58	1 2.22	ı
	1,00	1.81	B.39	1.82	1 x138	1,83	2:37	1.84	ı
113		3.01	3.98	3.05	3.97	1.04	3.16	3.06	ı
H		3.61	4 78	3.63	476	1.65	474	3.47	1
		4.24	5-57	4.24	5-55	4.26	5-53	4-19	ı
	and the same of	4.81	6.37	4.84	6.35	4-87	6.33	4.90	ı
20		5.42	7.16	5.45	7.14	5.48	7-12	5:57	ı
T T	-	6.62	8.76	6.66	8.73	6.70	8.70	6.73	1
100	9.58	7.22	4.55	7.26	9.51	7-31	9-49	7-35	1
1 33		7.82	10.35	7.87	10.31	7.91	10.08	7-96	1
110		9.03	11.14	9.08	11.11	9.13	11.86	9.18	۱
16		963	12.74	9.68	12.60	9.74	12.65	1 0.50	1
127	13.58	10.23	13-53	10.29	15:49	10.35	13-44	10.01	ı
12	14-38	10.83	14-33	10.90	14-28	10.96	14-13	11,01	
15		12-04	15.22	11.50	15.57	11.57	15.81	13.00	
100	the second second	12.64	16.72	12.71	16.66	12:78	15.60	12.86	
2.0	12.57	13.24	17.51	13.30	17-45	13.39	17.40	13.47	
23		13.84	18.31	13-94	18.45	14.00	18.19	14.79	ı
24		15.05	19.10	14.53	19.01	15.82	19.77	15-31	ı
26		15.65	20.70	15.74	20.52	1583	30.55	15.92	ı
27	21 56	16.25	24-49	16.34	21.42	16.44	21.35	16.53	ı
28		16.85	22.29	16.95	23.01	17.05	22.93	17 14	ı
4 30		18.05	23.88	18.16	23.80	18.26	25.72	18.87	ı
31	No. of Concession, Name of Street, or other Designation, Name of Street, or other Designation, Name of Street,	18.66	24 68	18.76	24.59	18.87	24-51	Zg.Zi	ı
32	25.56	19.26	25.47	19.37	25.39	19.48	35.30	19-10	ı
33	26.35	19.86	26.27	19.97	26.18	10.70	16.039	20,20	ı
35	27.15	21.06	27.86	21.1g	27-77	21.11	27.67	24142	ı
136		21.67	23.66	11.79	28.56	21.92	28.46	27.04	ı
37	29.55	22.27	29-45	22.40	29.35	22.52	29.26	12.95	ı
38	30.55	23:47	30.25	23,61	30.15	23.75 23.74	30.05	23.88	ı
40	31.95	24.07	31.84	24.21	31.5	448	1461	24.40	
41	32.74	24.67	32.64	24.82	32-53	24.96	11-41	25.10	N
44	33 54	25.28	33-45	25 42	35-32	25.57	33.27	35.73	
43	34-54	15.88	34.23	26.63	34.11	26.18	34-79	26.95	
45	35.94	27.08	35.82	27.24	35-70	27 39	35.58	77.55	
46	36.74	27.62	36.62	27.84	36.49	28,00	36.37	18 16	
47	37-54	28:29	37.41	18.45	37.29	18,61	37.16	18.77	
49	38.33	28.89	39.00	29.05	38.08	29.52	37-95	10.00	
50	39.93	30.09	39.80	30.26	39.67	3044	39-53	10.01	
51		30.69		30.87	42.40			11.02	
53	41.53	31.29	41.39	31,48	41.25	31.66		1184	
54		32.50		32.08	41.05	32.00		13.05	
55	43.93	33.10	43-78	33.29	43.63	33.48	43-49	13.67	
56	44-72	33.70	44.58	33.90	44-43	34 09	04.28	14.28	
57	THE RESERVE OF THE PERSON NAMED IN	34.30	45-37	34-50	45.80			34.90	
10		34.91		35-71		35-31		35.31	
59		36.11	47-76	36.38	47.60	36.53	47-44	16.73	
lig.	Dep.	La	Dep.	Lat	Dep	14	Den	Lat.	
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100	48.72	36 71	48.56	30.42	48.19	37//3	48.23	37-35	я
63	49-52	37 11	49-35	37-63	49-19	3- 74	49,01	37.95	
\$ 63	50,31	37-91	50:15	38-13	49.95	38.35	49 81	38.57	
0.4	SUM	36.52	50 04	38-74	50,77	38 46	50.60	34.18	
0.5	\$1,91	39.13	51,04	39.34	5,1187	39-57	51.59	39-79	1
66	5274	36.11	52-54	19-95	52.30	(Q. 12	52.14	40.41	
67	53-51	40.32	53-83	40.55	53:43	40.74	£2-48	41-02	
68	纤斑	40.93	54-13	4L10	53-95	61.42	\$3-77	41 03	
69	3511	41.53	54.92	45/77	59.74	41,00	54.69	42.74	
79	55.40	4413	55:72	42.37	55-53	42.61	55-35	41.86	
7.6	\$6,70	42.73	50 52	4198	56-33	45.44	55.14	93-47	
7#	57 50	43-33	57:35	43-58	57412	43.83	50 43	44.58	
7.3	58 TO	43 93	58.11	44.19	57.91	44-94	57-72	44-61	
74	59 10	44-53	38.90	44-79	58.71	45.05	58-51	45-32	
1.75	69.90	45.14	59.70	45-40	59-50	45.00	54.30	±5102	
76	60,70	45.74	60.50	46.00	60v29	46.27	60.00	46193	
77	61 49	46.34	61.19	46.61	61.09	46.87	60.88	47114	
3 28	62.29	45.94	62.09	47 BE	61.58	47 48	61.67	47-79	
7.9	63.09	47-54	61.83	47.82	62-67	28.09	61.46	48.37	
80	63.89	48.15	63.68	48-49	63.47	48.70	63.20	48.48	
SI	64.69	48.75	64-48	49.03	64.26	49.31	64.05	49-59	
82	65-49	49-35	65.27	49.63	85.05	49.91	64-84	50.20	
1 83	66.39	49.95	65.07	50 24	65.85	50.53	65.63	50.84	
1 84	67.09	50.55	66.86	50.84	65.64	51.14	66 41	51.43	
85	67.88	51.15	67.66	54-45	67-43	51:74	67 21	\$3.04	
86	68.68	51.76	68.40	52.00	68.23	52.35	68.00	52.65	
4 87	69-48	\$2.36	69.25	51.66	69.02	52.96	68.79	53.26	
88	70.28	53.96	69.05	53-27	fig. 8:	53-57	69.58	53 RE	
89	71.05	\$3.56	70 84	53.87	70.61	54-18	70.37	54-49	8
90	71 88	54.16	71.64	54.48	71.40	54-79	71.16	55.10	
92	72.68	\$4.77	72.44	55.08	72.20	55.40	71.95	55.71	2
92	73-47	55-37	73.23	55.69	72.99	50.01	7274	50.11	
93	74-37	55-97	74.93	56.29	73-7%	56.61	73-53	36.94	
94	75.07	56.57	74.82	56.90	74-58	57.22	74.32	57-55	
95	75.87	57.17	75.62	57.50	75-37	57.83	75.12	58.16	
96	76.67	\$7-77	75.43	58.11	76.16	58.44	75-91	58.77	
97	77-47	58.38	77.21	58.71	-6.96	59.05	76.70	59-39	
98	78.27	58.98	78.01	59.32	77-75	59.66	77-44	60.00	
1.00	79.06	59.58	78.80	59.92	78.54	60.27	78.28	60.61	
100	19.86	60.18	79.60	60.53	79-34	60.88	79.07	61 22	
101	8b.66	60.78	80.40	61.13	80.13	61.48	79.86	61.83	
103	81.46	61.39	BILIG	61.74	80:92	62.09	80.65	6145	1
103	81.25	61,99	81.99	62.35	81.72	62.70	81.44	63,06	
104	83-05	-62 50	82.78	61.95	82 51	63.31	80.23	63.67	
100	83.85	63.19	83.58	63.55	83 30	63.92	87.01	64 28	
106	1 84.66	03.79	84-18	64.16	84.10	64.53	53.81	64.89	
107	85.45	64.39	85.16	64.77	84.89	65.14	84 60	PRODUCTION AND	
803	86.25	65.00	85.07	65.37	85.68	B\$175	85.39	66,11	
LDG	\$7.05	65.60	86.76	65.98	86.48	66.16	86.19	66.73	
110	87.85	66.20	87.56	66.58	87 27	66,96	86 93	67.34	
Att	85.65	66.80	1			67.57		THE REAL PROPERTY.	
1113	39.45	67,40	88.36	67.19	88.06	68.18	87.77	67.96	
1113	90.25	68.11	89.95	68.40	39.85	68-70	88.56	68.57	
114	91.04	68.61	90.74	69.00	90.44	69.40	89.35	69.79	
115	91.84	69.21	91.54	69.61	91.24	70.01	90,14		
							90.93	70.40	
116	91.64	69.81	91-35	70.21	9203	70.01	91.72	71.02	1
117	93-44	70.41	93.13	The second second	92.52	71.23	92.51	71.63	
Itg	99-24	71,63	95.93	21-43	93.63	71167	93.10	72-24	
100	95.84	73 38	94.72	7103	9441	72.47	94.09	72.85	
			93.52	22.64	95.20	71-05	94.88	73.47	
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1 26		30,41		601	20,47	_	16.10	п	20.35		10.10	П	ZD(2)		1	
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32		35,22		2.70	25-13		9.81		15.04		9.91		24.96		1001	
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38	п	30,94		40	30.63		4-14		9.74		4.28		19.64 19.42		3170	1
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42	1	33.10		.86	12.95	12	6,00		2.87		6.15		2.70		6.24	
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61	48.07		47.90		47.74		47-57		
63	49.64	38.79	49.47	38.38	48.52		49.13		
64	50.43		50.26		50 09	39.84	49.91		
65	51.22	40.02	51.05		50.87	40 46	50.69	40 58	
66	52.01		51.83	40.86	51.65	41.09	51.47	41.31	
67	52.80		52.62		52 43		52.25	41.94	
68	53.58		53.40			42.33	53.03	42.56	
70	54-37 55-16	42.48	54-19	42.72	54.00	+2 95 +3.58	53 81	43.19	
71	_		54-97		55.57	44.20	55.37		
72	55.95	43.71	56.54	44-57	56.35	44.82	56.15	45 07	
73	57.52	44-94	57 33	45.19	57.13	45.44	56 93	45.69	
7.4	58.31	45 56	58.11	45.81	57.91	45 07	57 71	40 32	
75	59 10	46.17	58.90	46 43	58.70	46.69	58.49	49.94	
76	59.89	46.79	59.68	47.0,	59.48	47.31	59.27	47.57	
77	65.68	47.41	60.47	47.67	60.26	47.93	60.05	48.20	
78	61.46	48.64	61.25	48.29	61.04	48.56	60.83	49.45	
80	62.25	49.25	62.83	49.53	62.61	49.80	62 39	50.07	
81	63.83	49.87	63.61	50 15	63.39	50 42	63.17	50.70	
82	64.62	50.48	64.40	50 77	64 17	51.05	63.95	51.33	
82	65.40	51.10	65.18	51.38	64 96	51.67	64 73	51.95	
84	66.19	51.72	65.97	52.00	65.74	52.29	65.51	52.58	
85	66.98	52-33	66.75	52.62	66.52	52.91	66.29	53,20	
86	67.77	52.95	67.54	53.24	67.30	53.54	67.07	53 K3	
87	68.56	53.56	68.32	53.86	68.09	54.16	68.63	54.46 55.68	
89	70.13	54-18	69.89	54.48	69.65	55.40	69.41	55.71	
90	70.92	55 41	70.68	55.72	79.13	56.03	70.19	56.33	
91	71.71	56.03	71 46	56.34	71.24	56 65	70.97	50.46	
92	72.50	56.64	72.25	56 96	72.00	57.27	71.75	57.58	
93	73.28	57.26	73.03	57.58	71.78	57.89	72.53	58 21	
94	74.07	57.87	73-82	58 19	73-57	58,52	73.31	58.84	
95	74.86	58.49	74.61	58.81	74.35	59 14	74.09	59.46	
96	75.65	59.10	75.39	59-43	75.13	59.76	74.87	60.09	
97	76.44	59.72	76.96	60.05	75.91	61.01	75.65	61.34	
99	78.01	62.95	77-75	61.29	77.48	61.63	77 21	61.97	
00	78.80	61.57	78.53	61.91	78.26	62 25	77-99	62.54	
10	79.59	62.18	79.32	62.53	79.04	62.87	78.77	63.22	
02	80.38	62.80	80.10	63.15	79.83	63.50	79-55	63.84	
03.	81.17	63.41		63.77	80.61	64.12	80.33	64.47	
04	81 95	64.64		6,00	81.39	64.74	81.11	65.10	
-		-		65 62	82.96		82.67		
06	83.53	65.26		66.24	83.74	66.61	83.45	65.47	
08		66.49		66.86	84.52	67.23	84.23	67 60	
09	85.89	67.11	85.60	67.48	85.30	67.85	85.01	68.25	
10	86.68	67.72	86.38	68.10	86.09	68.48	85.79	68.85	
11	87.47	68.34		68.72		69.10	86.57	69.48	
12	88.26	68.95		69 34	87.65		87.35	70.10	
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Dep. Lat. Dep. Lat. Dep. Lat. Dep. Lat.	11	59	45.85	37.13	45.60	37-33	45-53	37-53	45.36	37,73	81
1 01 421 301 12.		-00				2000	-	-			
		181	Dep	-	. Deb		Deb		Detr	Lat	1
	-	0	1	01	-		-	_	1	72.	-

1-	,	0,		5'	1 7	υ,	4	
Dist	Lat.	Dep.	Lat.	Dep.	- :	Dep.		Dep
61		38.39	47.21	38.60	-	18.30		9.51
62	47.41	39.02	48.01	39 23	47.84			5,.65
63	48.96	39.65	48.79	39.86	4861	40 07	48.44	¦ນ.ຊ8ົ [
64	49.74	40.28	49.56	40.49	49.38	40.71		12 92 T
65	50.51	40.91	50.34	41.13	50.16	41.35		11.50
66 67	51.29 52.07	41.54	51.71	41.76	50.93	41.98	1	12.84
68	52.85	42.79	52.66	43.02	52.47			3 48
69	53.52	43.42	53-43	43.66	53.24	43.89		14.12
70	54.40	44.05	54 21	41.29	54.01	44.53	· ! - : ·	4. 6
71	55.18	44.68	54.98	44 92	54 79	45.80		15.40
72 73	56.73	45 94	56.53	46.19	56 33	46.43	56.13	
74	57.51	46 57	57-31	46 82	57.10	47.07	56 89 1-	17.32
75	58.29	47.20	58.08	47.45	57 87	4	'-	116
76	59.06	47.83	58.85	48.09	58.64			8.40
77 78	59 84 60.62	49.09	59.63	48.72	59 42	48.98		19.24
79	61.39	49.72	61.18	49 98	60.96	50.25	60 74 5	52
80	62.17	50 35	61.95	5062	61.63	50.84	61.51	1.16
81	62.95	50.97	62.73	51.25	6 - 50	54.52		1.79
82 83	63.73	51.60	63.50	51 88	63.27	52.16		2.43
34	65.28	52 86	65.05	53.15	64.83	52.79	1	3.C7
85	66.06	53.49	65.82	53.78	65.59	54.07	1	4.35
86	66.83	54.12	66.60	54-41	66.36	54. 0	1	4.99
37	67 61	54.75	67.37	55.05	67.13	55-44		3.63
88	68.39	55.38	68.15 68.92	55.68 56.32	68.67	55.97		6.9T
90	69.94	56.64	69.70	56.94	69.45	57.25	69.20 5	
91	70.72	57.27	70.47	57.58	70.23	57.88		8.19
92	71.50	57.90	71.24	58.21	70.99	58.52	70.73 15	4.83
93	72.27	58.53	72.02	58.84	71.76	59.16		y ÷7
94 95	73.05	59.16	72.79	59.47	72.53	59.79 63 <sub>43</sub>		275
96	74 61	60.41	74-34	65.74	74.08	61.00		1.39
97	-5.38	61.04	75.12	61.37	74.85	61.70		2 - 3
98	76.16	61.67	75.89	62.01	75.62	62.34		2.66
100	76.94 77.71	62.30 62.93	76.60 77.44	62. <b>6</b> 4 63.27	76.39	62 97		3.32
101	78.49	63 56	78.21	63.90	77.93	64.24		1.58
102	79.27	64.19	78 99	64.54	73.71	64.88		5.22
103	80.05	64 82	79.76	65.17	79.48	65.52	79.19 6	;.86
104	80.82 81.60	65.45 66.08	80.54 81.31	65.80 66 43	80.25 81.02	66.15		5.50
106	82.38	66 71	82.0y	67.07	81.79	65.79		.14
107	83.15	67.34	82.80	67.70	82.56	68 c6		.78
108	83.93	67 97	8363	68 33	83.34	68.70		.06
109	84.71	68 60	84.41	64.96	8411	69.33		o
110	86.26	69.23	85.18	69.60	84.88	6y.97		2-14
112	87.04	69.85 72 48	85.96 86.73	70 23 70.86	85.65 86.42	70.60		.98
113	87 82	71.11	87.51	71.50	87 19	71.88		.62
114	88.59	71.74	88.28	72.13	8- 97	72.51	87 65 72	90
215	89.37	72.37	89 06	72.76	88.74	73.15	88.42 73	
117	90 15	73.00	89.83	73.39	59 51	73 79		17
118	92 93	73.63   74.2 <b>6</b>	93.63	74.03 74.66	90.28	74.42	89.95 74	.51
119	92 48	74.89	1	75 29		75.69	91.49 .76	50
120	93.26	75.52	92.93	75.92	92.59	76.33	92 26 76	.73
<u>ئ</u> د	Dep.	Lat.	Dep.	Lt.	Der.	11		1.11.
is a	0'		45	<u>'</u>	1 3	U'	/ J.	, /
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8 1	0/	-	1.54	1	30	,	45'	-1
Dist.	Lat.	Dep	Lat	Dep.	Lat.	Dep.	Lat.	Dep.
1	0.77	0.64	0.76	0.65	0.76	0.65	0.76	0.65
2	1.53	1.29	2.20	1.29	2,18	1.30	2,27	1.95
3	3.06	2.57	3.05	2 58	3.04	2.60	3.03	2.61
5	3.83	3.21	3.82	3.23	3.80	3.25	3-79	3,25
6	4.60	3.86	4.58	3.88	4.56	3 90	4 55	3.92
7 8	6.13	4.50	5.34	4.52	6.08	4.55	6.06	4-57 5-22
9	6.89	5.79	6.87	5.17	6.84	5.84	6.82	5.87
10	7,66	6.43	7.63	6.46	7.00	6.49	7.58	6.53
IL	8.43	7.07	8.40	7 11	8.36	7.14	8.33	7.18
12	9.19	7.71	9.19	7.75	9.12	7.70	9.09	7.83
13	9.96	9.00	10.69	9.05	9.89	0.00	10.61	9.14
15	11.49	9.64	11.45	9.69	11.41	9.74	11-36	9-7#
16	12 26	10.28	12.21	10.34	12.17	10.39	12.12	10.44
17	13,02	10.93	12.97	10.98	12.93	11.04	12.38	11.10
18	13.79	12.21	13.74	12-28	13.69	11.09	14.39	12-40
20	15.32	12.36	15.26	12.92	T5.21	12.99	15.15	13.06
21	16.09	13.50	16.03	13.57	15.97	13.64	1591	13-71
22	16.85	14.14	16.79	14.21	16.73	14.29	16.67	1436
23	17.62	15:43	18 32	14.86	17.49	15.59	17.42	19.67
25	19.15	16.07	19.08	16.15	19.01	16.24	18.94	16.31
26	19.92	16.71	19.84	16.80	19.77	16.89	19.70	16.97
27	20.68	17.36	20.61	17.45	20.53	17.54	20.45	17.61
28	21.45	18.64	21.37	18.09	22.05	18.18	21.21	18.23
30	22.98	19.28	32.90	19.38	22.81	19.48	22.73	19.58
31	23.75	19.93	23.66	20,03	23-57	20,13	23.48	20.24
32	24.51	20.57	14.42	20,68	24.33	20.78	24.24	20.89
33	25.28	21.85	25.19	21.32	25.85	21 43	25.76	21,54
35	26.81	22.50	26.71	22.61	26.61	22.73	26.51	22.85
36	27.58	23.14	27.48	23.26	27.37	23.38	27.27	23.50
37	28.34	13-78	28.24	23.91	28.12	24.03	28.03	14 15
38		25.07	29.77	24.55	28.90	24.68	28.79	24.82
40	The state of the state of		30.53	25.84	30 43	25.98	30.30	26.11
41	200	26.35	31 29	26.49	31:18	26 63	31.05	26.76
42		27.00	32.06	27.14	31.94	27.28	31.81	17.42
43			32.82	28.43	32.70	27.93	33.33	28.07
45		28 93	34 35	29.08	34.22		34.09	29.37
46		700	35.11	29.72	34.98		34.85	30.03
47		30.21	35.87	30.37	35.74	30.52		30.68
48			36.64	31,01	36.50			31.33
50			37.40	32,31	38.02	32.47	37.88	32.64
50	39.07	-	1		38.78		-06.	13.29
57	39.83	33-4 ×	39.69	33.60	39.54	. 33-77	39.39	33-94
53		THE CANADAS IN		34 24				34 60
54			41.98	1000	1 0			35.25
31				-	-			36.55
5	49.66	36.64	43.50	36.83	43-34	37.02	43.18	37.24
5			and the second			37.67	43-94	
6	9 45.26						44-70	
_	-	_	A Add Annual	-				Lat
Dist	4	0 +	-	450	1-	30'	1	721
			-		WEGNE	200		-

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Dist.		Dep.	Lat.	Dep	Lat.	Dep.	Lat.	Dep.
61	46.73	39.21	46.56	39.41	46.38	39.62	46.21	39.82
62	47-49	39.85	47.32	40.06	47.15	40.27	46.97	40.47
63		40.50	48.08	40.71	47.91	40.92	47.73	41.12
64 65		41.14	48 85 49.61	41.35	48.67 49.43	41.56	48.48	41.78
66	50.56	12.12	50.37	42.64	50. 19	42.86	50.00	43.08
67	51.32		51.14	43.29	50.95	43.51	50.76	43.73
68	52.09	43.71	51.95	43.91	51.71	44.16	51.51	44-39
69		44-35	52.66	44.58	52.47	45.46	52.27	45.04
70	;	45.64	53.43	45.87	53.23	46.11	53.03	46 35
71	54.39 55.16	46.28	54.19	40.52	53.49 54.75	40.76	53.79 54.54	47.00
73		46.92	55.72	47.17	55.5 L	47 41	55.30	47.65
74	56 69	47.57	56.48	47.31	56.27	48.06	56 06	48.30
75	57.45	48.21	57.24	48.46	57.03	48.71	-56.82	48 96
76 77	58.22 58.99	48.85 49.49	58.01 58.77	49.11	57-79 58 55	49.36 50.01	57·57 58.33	49 61 50.26
78	59.75	50.14	59-53	50.40	59.31	50.66	59.09	50.92
79	60.52	50.78	60.30	51.04	60.07	51.31	59.85	51.57
80	61.28	51.42	61.06	51.69	60.83	51.96	60.61	52.22
81	62 05 62.82	52.07	61.82	52.34	61.59	52.61	61.36	52.87
82	63.58	52.7 L	62.59	52.98	62.35 63.11	53.25 53.90	62.13	53.53
84	64.35	53.99	64.11	54.27	63.87	54.55	63.64	54.83
85	65.11	54.64	64.87	54.92	64.63	55.20	64.39	55.48
86	65.88	55.28	65.64	55-57	65.39	55.85	65.15	56.14
87 88	66.65 67.41	55.92	66.40	50.21	66.16 66.92	56.50	65.91 66.67	56.79
89	68.18	56.57 57 21	67.93	57 50		57.15	67.42	57-44 58.10
90	68.94	57.85	68.69	58.15		58.45	68.18	58.75
91	69.71	58.49	69.45	58.80	69.20	59.10	68.94	59.40
92	70.48	59.14	70.22	59.44		\$9.75	69 70	60.05
93	71.24 72.01	59.78 60.42	70.98	60.09	70.72 71.48	61.05	70.45 71.21	60.71 61.36
95	72.77	61.06	72.51	61 38	72.24	61.70	71.97	62.01
96	73-54	61.71	73.27	62 03	73.00	62.35	72.73	62.66
97	74.31	62.35	74.03	62.67	73.76	63.00	73.48	63.32
98	75.07	62.99	74.80	63.32		63.65	74.24	63.97
99	76.60	64.28	75.56 76 32	63.97	75.28 76.05	64.94	75.00 75.76	64.62
101	77:37	64.92	77.09	65.26	76.80	65.59	76.51	65.93
102	78.14	65.50	77.85	65.90	77.56	66.24	77.27	66 58
103	78.90	66.21	78.61	66.55		66.89	78.03	67.23
102	79.67 80.43	67.49	79.38 80.14	67.20	79.08 79.84	67.54 68 19	78.79 79-54	68.54
106	81.20	68.14	80.90	68.49	80 60	68.84	80 30	
107								69.19
	81.97	68.78	81.67			69.49	81.06	69.8c I
103	81.97 82.73	68.78 69.42	81.67 82.43	69.14	81 36 82.12	69.49 70.14	81.82	69.85 70.50
109	81.97 82.73 83.50	68.78 69.42 70.06	81.67 82.43 83.19	69.14 69.78 72.43	81 36 82.12 82.88	69.49 70.14 70.79	81.82 82.57	70.50 71.15
109	81.97 82.73 83.50 84.26	68.78 69.42 70.06 70.71	81.67 82.43 83.19 83.96	69.14 69.78 79.43 71.07	81 36 82.12 82.88 83 64	69.49 70.14 70.79 71.44	81.82 82.57 83.33	70.50 71.15 71.80
109	81.97 82.73 83.50 84.26	68.78 69.42 70.06 70.71 71.36	81.67 82.43 83.19 83.96	69.14 69.78 70.43 71.07	81 36 82.12 82.88 83 64 84.41	69.49 70.14 70.79 71.44 72.09	81.82 82.57 83.33	70.50 71.15 71.80 72.46
109	81.97 82.73 83.50 84.26	68.78 69.42 70.06 70.71 71.36 71.99 72.64	81.67 22.43 83.19 83.96 84.72 85.48 86.25	69.14 69.78 79.43 71.07	81 36 82.12 82.88 83 64	69.49 70.14 70.79 71.44	81.82 82.57 83.33	70.50 71.15 71.80
108 109 110 111 112 113	81.97 82.73 83.50 84.26 85.03 85.80 86.56 87.33	68.78 69.42 70.06 70.71 71.36 71.99 72.64 73.28	81.67 82.43 83.19 83.96 84.72 85.48 86.25 87.21	69.14 69.78 70.43 71.07 71.72 72.37 73.01 73.66	81 36 82.12 82.88 83 64 84.41 85.17 85.93 86 69	69.49 70.14 70.79 71.44 72.09 72.74 73.39 74.04	81.82 82.57 83.33 84.09 84.85 85.60 86.36	70.50 71.15 71.80 72.46 73.11 73.76 74.41
108 109 110 111 112 113 114	81.97 82.73 83.50 84.26 85.03 85.80 86.56 87.33 88.10	68.78 69.42 70.06 70.71 71.36 71.99 72.64 73.28 73.92	81.67 82.43 83.19 83.96 84.72 85.48 86.25 87.31 87.77	69.14 69.78 70.43 71.07 71.72 72.37 73.01 73.66 74.30	81 36 82.12 82.88 83 64 84.41 85.17 85.93 86 69 87.45	69.49 70.14 70.79 71.44 72.09 72.74 73.39 74.04 74.69	81.82 82.57 83.33 84.09 84.85 85.60 86.36 87.12	70.50 71.15 71.80 72.46 73.11 73.76 74.41 75.07
108 109 110 111 112 113 114 115	81.97 82.73 83.50 84.26 85.03 85.80 86.66 87.33 88.10	68.78 69.42 70.06 70.71 71.36 71.99 72.64 73.28 73.92	81.67 82.43 83.19 83.96 84.72 85.48 86.25 87.27 88.54	69.14 69.78 72.43 71.07 71.72 72.37 73.01 73.66 74.30 74.95	8: 36 82:12 82:88 83:64 84:41 85:17 85:93 86:69 87:45	69.49 70.14 70.79 71.44 72.09 72.74 73.39 74.04 74.69 75.34	81.82 82.57 83.33 84.09 84.85 85.60 86.36 87.12	70.50 71.15 71.80 72.46 73.11 73.76 74.41 75.07
108 109 110 111 112 113 114	81.97 82.73 83.50 84.26 85.03 85.80 86.56 87.33 88.10	68.78 69.42 70.06 70.71 71.36 71.99 72.64 73.28 73.92 74.56 75.21	81.67 82.43 83.19 83.96 84.72 85.48 86.25 87.31 87.77	69.14 69.78 72.43 71.07 71.72 72.37 73.01 73.66 74.30 74.95 75.60	8: 36 82:12 82:88 83:64 84:41 85:17 85:93 86:69 87:45 88:21 88:97	69.49 70.14 70.79 71.44 72.09 72.74 73.39 74.04 74.69 75.34 75.99	81.82 82.57 83.33 84.09 84.85 85.60 86.36 87.12 87.88 88.64	70.50 71.15 71.80 72.46 73.11 73.76 74.41 75.07 75.72 76.37
108 109 110 111 112 113 114 115 116 117 118	81.97 82.73 83.50 84.26 85.03 85.80 86.56 87.33 88.10 88.86 89.63 90.39 91.16	68.78 69.42 70.06 70.71 71.36 71.99 72.64 73.28 73.92 74.56 75.21 75.85 76.49	81.67 82.43 83.19 83.96 84.72 85.48 86.25 87.77 88.54 89.30 90.06 90.82	69.14 69.78 72.43 71.07 71.72 72.37 73.01 73.66 74.30 74.95	8: 36 82:12 82:88 83:64 84:41 85:17 85:93 86:69 87:45 88:21 88:97	69.49 70.14 70.79 71.44 72.09 72.74 73.39 74.04 74.69 75.34	81.82 82.57 83.33 84.09 84.85 85.60 86.36 87.12 87.88 88.64 89.39	70.50 71.15 71.80 72.46 73.11 73.76 74.41 75.07 75.73 76.37 77.03 77.68
108 109 110 111 112 113 114 115 116 117 118	81.97 82.73 83.50 84.26 85.03 85.80 86.56 87.33 88.10 88.86 89.63 90.39 91.16 91.93	68.78 69.42 70.06 70.71 71.36 71.99 72.64 73.28 73.92 74.56 75.21 75.85 76.49 77.13	81.67 82.43 83.19 83.96 84.72 85.48 86.25 87.77 88.54 89.30 90.06 90.82 91.59	69.14 69.78 72.43 71.07 71.72 73.01 73.66 74.30 74.95 75.60 76.24 76.39	81 36 82.12 82.88 83 64 84.41 85.17 86.99 87.45 88.21 88.97 89.73 90.49 91.25	69.49 70.14 70.79 71.44 72.09 72.74 73.39 74.04 74.69 75.34 75.99 76.63 77.28 77.93	81.82 82.57 83.33 84.09 84.85 85.60 86.36 87.12 87.88 88.64 89.39 90.15 90.15	70.50 71.15 71.80 72.46 73.11 73.76 74.41 75.07 75.72 76.37 77.03 77.68
108 109 110 111 112 113 114 115 116 117 118	81.97 82.73 83.50 84.26 85.03 85.80 86.56 87.33 88.10 88.86 89.63 90.39 91.16	68.78 69.42 70.06 70.71 71.36 71.99 72.64 73.28 73.92 74.56 75.21 75.85 76.49 77.13 Lat.	81.67 82.43 83.19 83.96 84.72 85.48 86.25 87.77 88.54 89.30 90.06 90.82	69.14 69.78 72.43 71.07 71.72 72.37 73.01 73.66 74.30 74.95 75.60 76.24 76.39	81 36 82.12 82.88 83 64 84.41 85.17 85.93 86.99 87.45 88.41 88.97 89.73 90.49	69.49 70.14 70.79 71.44 72.09 72.74 73.39 74.04 74.69 75.34 75.99 76.63 77.28 77.93	81.82 82.57 83.33 84.09 84.85 85.60 86.36 87.12 87.88 88.64 89.39 90.15	70.50 71.15 71.80 72.46 73.11 73.76 74.41 75.07 75.73 76.37 77.03 77.68

	-	-	1 15/		- 20	-	- 15	,
Dist	0	-			30		45	
-	Lat.	Dep.	Lat	Dep.	Lat	Dep.	Lat	Dep.
1 3	0.75	1.31	0.75	1.32	1.50	0.66 1.33	1.49	1.35
3	2.26	1.97	2.26	1.98	2.25	1,99	2.24	200
100	3.02	2.62	3.01	2.64	3.00	2.65	2.98	206
5	3.77	3.28	3.76	3 30	3-74	3.31	3.73	3:33
6	4 53	3.94	4-51	3.96	4-49	3.98	4.48	4,00
8	6.04	5.25	6.01	5-27	5.24	5.30	5.22	4.66
9	6.79	5.90	6.77	5-93	6.74	5.96	6.71	5.90
10	7.55	6.56	7.52	6,59	7.49	6.63	7.46	6.66
11	8.30	7.22	8.27	7.25	8 24	7 29	8-21	732
12	9.06	8.53	9.02	7,91	8.99	7.95	8.95	7.99
13	9.81	9.18	9.77	9.23	9 74	9.28	10.44	9.31
14	11.32	9.84	11.28	9.89	11.23	9.94	11.19	9-99
16	12.08	10.50	12.03	10.55	11.98	10.60	11.95	10.05
17	12.83	11.15	12.78	11.21	12.73	11.26	12 68	21.32
18	13.58	11.81	13.53	12.53	13,48	11.93	13.43	11.99
19	14.34	13.12	15.04	13.19	14 98	13.25	14.92	13-32
21	15.85	13.78	15.79	13.85	15.73	13.91	15.67	13.98
22	16.60	14-43	16.54	14.51	16,48	14.58	16.41	14.65
23	17.36	15.09	17.29	15.16	17.23	15.44	17.16	15.42
24	18.11	15.75	18.04	15.82	17.97	15.90	17.91 18.6¢	15.98
25	19.62	17.06	19.55	17-14	19.47	17.23	19 40	17.31
26	20.38	17-71	20.30	17.80	20.22	17.89	20.14	17.98
28	21.13	18.37	21,05	18.46	20.97	18.55	20.89	18.64
29	21.89	19.03	21.80	19.12	21.72	19 22	21.64	19.98
30	22.64	19.68	22.56	19.78	22-47	19,88	22.38	
31	23 40	20.34	23.31	20.44	23.22	21 20	23,13	31.31
32	24.91	21.65	24.81	21.76	24.72	21.87	24.62	21.97
34	25.66	22.31	25.56	22 42	25.46	22.53	A5-37	22.61
35	26.41	22 96	26.31	23.08	26.21	23.19	16,11	23.31
36	27.17	23.62	27.07	23.74	26.96	23.85	17.60	23.97
37	27.92	24.93	28.57	24.40	28 46	24 52	28.35	25.30
38	29.43	25.59	29.32	35.71	29.31	25.84	19.10	85.97
40	30.19	26.24	30.07	26.37	29.96	26.50	29.84	26.64
41	30.94	26.90	30.83	27.03	30.71	27 17		27 30
42	31.70	27.55	31,58	27 69 28.35	31.46	27.83		27.97 28.61
43	32.45	28.87	33.08	29.01	32.95	29.16	The Control of the Co	29.30
44	33.96	29.52	33.83	29.07	33.70	29.82	33.57	19.97
46	34-72	30 18	34.58	30.33	34.45	30.48	-	10.63
47	35-47	30.83	35:34	30.99	35.20	31.14		11.30
48	36.23	31.49	36.84	31.65	35.95	31.81		1.63
49	37-74	32.80	37-59	32.97	37:45	33.13		3 29
51	-	33.46	-0	33 63	-	33-79	-	3.95
52	39.24	34.12	39.10	34-29	18.95	34.46	38.79 3	4.63
53		34-77	39.85	34.95	39.69	35.12		5.49
54	40.75	35.43	40.60	36.26	40.44	35.78		6.61
55	42.26	36.74	42.10	36.92	41.94	37-11	-	7.29
56		37.40	42.85	37 58	42 69	37-77	42-53 1	7 96
57 58	43.77	38,05	43.61	38.24		38,43		8.62
59	44-53	38.71	44.36	38.90	44-19	39.09		9.29
	Dep.	Lat.	Dep	Lat	Dep.	Lat	Dup.	Late
Dist	Dep. 1	Late	15 45	-	30		150	-
-	-	-		DEGRE		-	- 10	

-	-		-		JEGRE	-		45'		
п	2	01	-	15/	-	1	0'	-	-	
Ш	F	Lat	Dep.	Lat.	Dep	Lat	Dep.	Lat	Dep.	
	61	46.79	40.68	45 86 46.61	40.88	45.09	41.08	45.51	40.62	
	63	47.55	41.33	47.37	41-54	47.18	41.75	47.00	41.95	
и	64	48.30	41.99	48.12	42.20	47.93	42.41	47.75	42.62	
и	65	49.06	4264	48.89	42.86	48.68	43.07	48.49	43.28	
ł	66	49.86	43.30	49.62	43 52	49.43	43.73	49.24	43.95	
п	68	50.57	43.96	50 37	44.18	50.18	44.40	49.99	44.61	
и	69	52.07	45/27	51.88	45-49	51.68	45.72	51.48	45.95	
ı	70	51.83	45.92	52.63	46 15	52 43	46.38	52.22	46.61	
П	78	53 58	46.58	53.38	46 81	53 18	47.05	52.97	47.28	
н	7=	54-34	47 24	54.13	47 47	53.92	47.71	53.73	47-94	
ı	73 74	55.85	48.55	54,88	48 13	54.67	48.37	54.46	49.28	
ı	75	56.60	49.20	56.39	49-45	56 17	49.70	55.95	49.94	
ı	76	57-36	49.86	57.14	50.11	56,92	50.36	56.70	50,61	
1	77	58.11	50.52	57.89	50.77	57.67	51.02	57.45	51.27	
1	78	58.87	51 17	58.64	5E.43	58.42	51.68	58.19	51-94 52.60	
и	79	59.62	51 83	59.40	52.75	59.17	52.35	58.94	53.27	
1	81	61.13	53-14	60,90	53.41	60.67	53.67	60.43	53.94	
ı	82	61.89	53.80	61.65	54.07	61.41	54-33	61.18	54.60	
1	83	62.64	54-45	62.40	54-73	62 16	\$5.00	61.92	55.27	
и	84	64.15	55.11	63.15	55.38	62.91	55.66	62.67	55.93	
ı	86	64.90	55.76	64.66	56.04		56.32	63.41		
ı	87	65.66	57.08	65.41	55.70	65.46	57.65	64.91	57.27	
п	88	66.41	57-73	66.16	58.02	65.91	58.31	65.65	58.60	
М	89	67.17	58.39	66.91	58.68	66.66	58.97	66.40	59.26	
а	90	67 92	59.05	67.67	59.34	67-41	59.64	67.85	59.93	
ı	91	68.68	59.70	68,42	60.66	68.15	60.30	68.64	61.29	
п	91	70.19	61.01	69.17	61.32	68 90	61.62	69.38	61.93	
п	94	70.94	61.67	70.67	61.98	70.40		70.13	61.59	
	95	71.70	62.33	71.42	62.64	71.15	62.95	70.88	63.26	
ĸ	96	72.45	62.98	72.18	63.30	71.90		71.62	63.92	
ı	97	73.21	64.29	72.93	64.62	72.65		72.37	65.16	
R	99	74.72	64.95	74.43	65.28	73.40	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN COLUMN TWO PERSON NAMED IN COLUMN TRANSPORT NAMED IN COLUMN TWO PERSON NAMED IN CO	73.86	65.92	
R	100	75.47	65.61	75.18	65 93	74.90			66.59	
B	IOI	76.23	66.26	75-94	66.59	75.64	66.92	75.35	67.25	
ĸ	102	76.98		76.69		76.39		76.10	67.92	
	103	77.74		77.44		77.14		76.84		
	105	79-24	1 - m m	78.94	69.23	78.64		78.34	69.92	
14	106	80,00		79-70	-	-		79.08	-	
	107	80.75	70.20	80.49	70.55	80.14	1 70.90	79.83	71.25	
	108	81.51	20.85	81-20			ARREST DESCRIPTION			
	110	82.20	ALC: NO.	81.99						
	III	83 77		834		and in column 2 is not	- To . Sec. 2			
	112									
	113	85.28	74.13	84.9	74-51	84.6	3 74.88	84.30	75.24	
	114		74-79					85.04		
	115			-		-				
	115							1 2 2	77.24	
	118									
	Lry	89 8	1 78.07	1 89.4	7 78.40	5 89.1	3 78.8	1 88.71	79.24	
	120	-	_	-	-	-				
	S. C.	Dep		Del	-	. De		. Dep	Lat.	
	Dist	1	0'	1	451	die	30'	1	15'	
	100	-	-	100	48 DE	BREES.		-	-	

6	100	-	-	33.5	DEGRE				
r	6	1 0	1	1	5/	1 3	0,	45	
B	381	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat	Dep.
8	-	-	0.66	-	0.66	0.75	0.60	-	0.67
r	3	1.51	1.31	1,50	1.32	1.50	1.33	0.75	1,33
0	2	2.26	1.97	2.26	1.98	2.25	1.99	2.24	2.00
u	7 4	3.02	2.62	3.01	2.64	3.00	2.65	2.98	2.66
ĸ	5	3,77	3.28	3.76	3 30	3.74	3.31	3 73	1-33
В	6	4 53	3.94	4-51	3.96	4-49	3.98	4.48	4.00
и		5.28	4.59	5.26	4.62	5.24	4.64	5.22	4.66
ĸ	7 8	6.04	5.25	6.01	5.27	5.99	5.30	5.97	5-31
н	9	6.79	5.90	6.77	5.93	6:74	5.96	6.71	5-99
u	10	7.55	6.56	7.52	6,59	7.49	6.63	7.46	6.56
ı	11	8.30	7.22	8.27	7.25	8 24	7 29	8-21	7.12
	12	9.06	7.87	9.02	7.91	8.99	7:95	8.95	7.99 3.66
	13	9.81	8.53	9.77	8.57	974	8.61	9.70	
ĸ	14	10.57	9.18	10.53	9.23	10.49	9.28	10.44	9.33
	25	11.32	9.84	11.28	9.89	11.23	9.94	11.19	9.99
1	16	12.08	10.50	12.03	10.55	11.98	10.60	11.94	10.65
	17	12.83	11.15	12.78	11.21	12.73	11.26	12 68	11.32
	18	13.58	12.47	13.53	12.53	13.48	11.93	13-43	11.99
1	19	14-34	13.12	15.04	13.19	14 98	13.25	14.92	13.32
1	20	15.85	13.78	_	13.85			15 67	63.9B
1	21	16.60	14.43	15.79	14.51	15.73	13.91	16.41	14.05
1	22	17.36	15.09	17.29	15.16	17.23	15.24	17.16	15-33
в	24	18.11	15.75	18.04	15.82	17.97	15.90	17.91	15.98
п	25	18.87	16.40	18 80	16.48	18.72	16,57	18.65	16.65
в	26	19.62	17.06	19.55	17-14	19-47	17.23	19 40	17.31
н	27	EQ. 38	17.71	20.30	17.80	20,11	17.89	20.14	17.98
п	28	21.13	18.37	21.05	18.46	20.97	18.55	20.89	18.64
ĸ	29	21.89	19.03	21.80	19.12	21.72	19 22	21,64	19.31
ı	30	22.64	19.68	22.56	19.78	22:47	19.88	22.38	19.98
в	31	23.40	20.34	23.31	20,44	23.22	20.54	23.13	20.64
п	32	24 15	20.99	24.06	21-10	23.97	21 20	23.87	21.31
ĸ	33	24.91	21.65	24.81	21.76	24.72	21.87	24 62	21.97
ĸ	34	25.66	22.31	25.56	23.08	25.46	22.53	25.37	23.31
п	35	26.41	22 96	-	-		23-19		200
н	36	27.17	23.62	27.07	23.74	26.96	23.85	26.86	23.97 24.64
u	37	27.92	24.93	28.57	24.40	28 46	24.52	The second second	25.30
и		29.43	25.59	29.32	25.71	29.21	25.84		25.97
u	39	30.19	26.24	30.07	26.37	29.96	26.50		26.64
ш	40	30.94	26.90	30.83	27.03	30.71	27 17		27 30
п	41	31.70	27.55	31.58	27 69	31.46	27.83		27.97
п	42	32.45	28.21	32,33	28.35	32.21	28.49		28.63
1	44	33.21	28.87	33.08	29.01	32.95	29.16	32.83	29.30
1	45	33.96	29.52	33.83	29.67	33.70	29.82	33.57	19 97
1	46	34.72	30 18	34-58	30.33	34-45	30.48	34-32	10.63
1	37	35-47	30.83	35.34	30.99	35.20	31.14	35.06	1.30
I	48	36.23	31.49	36.09	31.65	35.95	31.81		1.96
1	49	36.98	32.15	36.84	32,31	36.70	3247		2.03
1	50	37.74	32.80	37-59	32.97	37.45	33:13		3 29
I	51	38.49	33.46	38.34	33 63		33.79		3.95
1	52	39.24	34.12	39.10	34.29	38.95	34.46		4.63
1	53		34-77	39.85	34.95		35.12		5-29
1	54	40.75	35.43	41.35	35.60	40.44	35.78		5.96
1	55	41.51		-	STREET, SQUARE, SQUARE,		-		
1	56	42.26	36,74	42.85	36.92 37.58		37-11		7,29
1	57 58		37.40	43.61	38,24		37.77		7-90
1	58		38.71	44.36	38.90	44-19	39.09		9.29
1	59		39.36	45.11	39.56		39.76		9.95
ŀ	-	Dep.	Lat.	Dep	Lat.	Dep.	Lat		Lat.
1	Dist	0'	-	4		30	-	150	-
-	9	0		-	_			130	-
				48	DEGI	LEVELD			

					<del></del>		<del></del>	
Dist	04			5'		)′	1 - 4	
.۳	Int	Deb.	list	D-p	Let.	Dep	lat_	Den.
61	45 33	10.82	45.15	11.01	44.97	41.21	44.79	\$1.41
62	46.37	41.49	45.89	41.69	4571	41.89	45.53	42 00
63	46.82	42.16	45.63	42.36	46.45	12.56	46.26	42.76
64	47.56	42 82	43.11	43.03	47.19	+3.24	47.73	13 41
65	<u> </u>	43.40		13.70	-47.92	43.91		4 1 1 2
66	49 05	44.16	48.85	14.38	48.66	44.50	484"	41.85
6-	49.79	45.50	49 59	4,.05	49 40 50.13	5.26	49.20	45.48
68	50.53 51.28	46.17	50.33 51.0-	45.74		45.04	50.07	16.81
69 70	52.02	16.84	51.82	40-		47.20	51.40	45
1		47.51	52.55	47.74		47.07	52.14	. 8.14
71 72		48.18	53.30	48.41	53.08	48.64	52.87	1,8 5-
73	54.25	48.85	51.04	4.7.08	53.82	4.) 32	53 64	49.55
74	54 99	47.52	548	49.76	54.56	49.99	54-34	\$5.23
- 5	55."4	50.18	55.52	50 13	55.30	50.77	1 (1.0-	52.91
76	56.48	50.85	50.26	51.10	50.03	51.34	55 61	11 59
	57.22	51 52	57.00	51.77	56.77	\$2.02	50.54	12 37
78	57.97	52.19	57.74	52.44	57-51	52.70	, · · · ·	17.0
79		52.86	58.4×	53 12	58 24	53 37	58.01	
8o	59.45	53 53	59.22	53.70	5º 98	54.05	5× -5	(3) 33
81	60.19	54.20	59 46	54.46	59 72	54.72	59.18	154.9
82	60.04	54.87	60.70	55.13	62.46	\$5.40	62.21	35 %1 36 34
83	62.42	55.54	62.18	55.81	61.19	56.75	61.68	15° 34 15° 22
84	63.17	56 88	62 92	57.15		157.43	62.42	;,
	63.91	'57.55	63 66	582	63.41	58 10	63.13	5.5 38
86 87	64.05	58.21	64.40	54.50		58.78	63.80	59.0h
88	65.40	\$8.88	65 14	59.17		59 45	6162	;y3
89		59.55	65.58	59 84	65.62	60.13	0, 35	63.41
90		60.22	66 62	60 51	66.35	60.80	66 00	6. 10
91	67.62	65.89	67 36	61.19	67 Og	61.48	66.82	61.77
92	68.37	61 56	68.10	61.86	6-83	62 15	6;.,6	62.45
93	69.11	62.23		62 53	68.57	62 83	68.29	63 13
94	69.86	62.40		63 20	6g. zo	63.51	69.53	03.81
95	~2 65	63 57	70.32	67.87	70.04	64.18	69 70	64.49
96	71.34	64.24	71.06	64.55	70.78	64.80	70.49	65 16
97		64.91	71.80	6 5.22	71 52	65 53	71 23	05.X4
98		65 57	72.54	65.89	72.25	66.21	71.96	65 32
99		66.24	73 28	66 56	72.99	66.88	72.5	67 88
100	74.31				73.73	67.56		
101	75.06	67.58 68.25	74.76	[67.91 [63.58]	74.40	6X 23	74.17	65 56
102		69.92	76.24	69.25	75.20 75.94	68.91	74.90 75.64	69.24
104	77.29	69 59	76.98	69 93	76.68	69 59	76.37	1-0 65
105	78.03	70.20	77:2	- 5.60	77.41	70.94	77 13	-1 27
106	78.77	170.93	78.46	71.27	78.15	71.61	77 84	195
107	79.51	71 60	79.20	1.94	78.89	72.29	78 57	1-2.63
108	80.26	72.27	79.94	72.62	79.63	72.96	79.31	73 31
109	81.00	72.94	80.68	73.29	80.36	73.64	80.04	1-3 49
110	81.75	73.60	81.42	73.96	81.10	74 31	80 78	46-
111		74 27	82.16	74.63	81.84	74 99	81.51	73.35
112	×3.23	74-94	82 90	75.31	82.57	75.67	82 24	76 3
1113	83.98	75.61	83.64	5.93	83 31	76.3‡	8 - 98	6.5
.114		76.28	84.38	70.65	84.25	.77.92	83.71	/ X
115	85.46	76.95	85 12	7.32	_X+ 79_	60	84 15	3
116		77.62	85.47	77.99	85.52	78.37	85 13	78 74
317	86 95	,78.29  78.46	86 61	-3 07	86.96	79.74	8,02	19.43 33.15
811	87.69   88.43	79.63	86 00	(19.34 (2).01	87 33	79.72	86.65	80.10
122	89 19	180 30	88 43		87.74	80.45 181.07	85.12	81.46
. —	Dep	Lat.	1) -)	Tat.		; <del></del>	D(p.	
ist.			!	: :	D.:p	ļ. <b>1</b> 77	-'" '-	·,
. <del>.</del> .		١,		י	, ,		1	

47 DEGREES.

(	11	0/	1	1 15/		307		451		
1 0	La		ep. L		ep. La		ep. L	at-	Dep	
	1 0.7			_		74 0.		73	0.68	
	2 1.4	9 1.	34 1.	48 1.	34 1.	47 1.	35 I	47	1.36	
	3 2.2			COLUMN TWO IS NOT THE OWNER.	01 2.	CATALON BOOK		20	1.04	
	3.7		COLUMN TO SERVICE STATE OF THE PARTY OF THE		69 2.1			67	3.39	
	5 4.4			44 4				41	4.07	
	5.2			18 4	71 5.1	6 4.	3 5	14	4-75	
				66 6.0				87	5.43	
10	-			COLUMN TO SERVICE AND ADDRESS OF THE PARTY O		-	200		6.79	
1									7-47	
12				CONTRACTOR OF THE PARTY OF				_	8.15	
13									9.50	
25				-			DESIGNATION OF THE PARTY NAMED IN		0.18	
26	_		11 11.1	84 10.7	6 11.8	0 10.8	1 11.	75 1	0.16	
17	-								1-54	
18					COR MICHAEL			-	1.90	
20						1000			3.58	
21	15.61		5 15.5	4 14.1	2 15.4	8 14.1	9 15-	42 4	4-25	
22	16.35			MILE BOLDE		THE RESERVE TO SERVE	-		4-93	
23	17.84					- 2 2			5.61	
25	18.58					ALC: UNKNOWN			197	
26	19.32						19.0		.65	
27	20.06			- 20 20					33	
29	21 55		AND DESCRIPTION OF						69	
30	22.29								15	
31	23.04	20.7				SIII Edward A			.04	
32	23.78	21.4					MI DOWN		-72	
34	25.27	22 7							OH	
35	26.01	23.42	25.9	23.53					76	
36	26.75	24.00	-			24.32			44	
37	27-50	25-43							70	
39	28 98	26.10	28.87	26.22	28.75	26 35	28.6			
40	29.73	26.77		26.89	29.40	27.02		_		
41	30.47	27.43			30.23	27.70	30.84			
43	31.21	28.77			30.97	29.05	31.58			
44	32.70	29 44	32.57	29.58	32.44	29.73	32.31	29		
45	33 44	30.11	3	-	33.18	30.40	33.04			
46	34.18	30.78	34.05		33.91	31.08	33.78			
47	35.67	32,12	35-53	32.27	35.39	32.43	35.25	32.	8	
49	36.41	32.79	36.27	32.95	36.13	33.10	35.98			
50	37.16	33.46	37.01	33.62	36.80	33.78	36.72	33.5	14	
52	37.90	34.13	37.75	34.29	38.34	34.46	37.45	35-3	6	
53	39-39	35.46	39.23	35.64	39 08	35.81	38.92	35-9	8	
54	40.13	36.13	39-97	36.31	39.81	36.48	39.65	36.6	_	
55	41.62	36.80	40.71	36.98	40.55	37.16	41.12	38.0		
57	42.36	37-47	41.45	37-65	41.29	38.51	41.86	38.6		
57	43.10	38.81	42.95	39.00	42.76	39.18	42.59	39-3	2.1	
59 60	43.85	39.48	43.67	39.67	44.24	39.86	43.32	40.0		
	Dep.	Lat	Dep.	40.34 Lat.	Dep.	1,at.	Dep.	Lat	Trans.	
Dist.	Dep. 0/			51	30		-	5/	2	
-	0		4	7000	GREES		1	-	310	

è	1	-	_	-	-	-	M .	-		ì
I	2	0	-	36715		1 300	-	- 4	-	ı
H		Lat	Dep	Lat	Dep.	Lat	Dep.	Lat.	Dep-	I
1	61	45.34	41.60	44.43	41.80	44-25	41.99	44-79	42.87	ı
ı	63	46.08	42.97	45.89	43-17	45.70	43-37	45.51	43-57	ı
ł	64	46.81	43.65	46,61	43.85	46.43	44.05	46.33	44.26	ı
1	65	47.54	44-33	47-34	44-54	47-15	44-74	46.95	44-95	ł
۱	66	48.27	45.01	48.80	45.91	47.87	45-43	47.68	45.04	ı
1	68	49.73	46.38		46.59	49-33	46.81	48.40	47,02	ı
ł	69	50.46	47.06		47-28	50.05	47.50	49.84	47-71	ı
ı	70	51.19	47-74	50 99	47-96	50.78	48,18	50.57	48.41	ı
ı	71	51.93	48.42	51.71	48.65	51.50	48.87	51.19	49.10	ı
1	73	53.39	49-10	52 44	49-33	52.23	49.56	52.01	50.48	۱
ı	74	54-12	50.47	53.40	50.70	53.68	50.94	53.45	51.17	۱
Į,	75	54-85	51.15	54.63	51.39	54 40	51.63	54:18	51.86	ı
II	76	55.58	51.83	55,36	52.07	-55.13	52.31	54.90	52.55	ı
ı	77	56.31	52.51	56.81	52176	55185	53.00	56.61	53.35	ı
1	78	57.78	53.88	57-54	58-44	57.30	53.69 54.38	57.07	53-94	
1	80	58.51	54-56	58.27	54.81	58.03	55.07	57.79	55.32	
H	81	59 24	55.24	59.00	55.50	58,76	55.76	58.5)	56.01	ı
1	82	\$9.97	55-92	59-73	56.18	59.48	56.45	59-23	56.70	
1	83	61.43	57-29	61,18	56.87	60.21	57.82	59.96	58.00	ı
1	85	62.17	57-97	61.91	58.24	61.66	58.51	61.40	58.78	ı
ı	86	62.90	58.65	62.64	58.93	62.38	59.20	6212	59-47	ı
ı	87	63.63	59-33	63.37	59.61	63.11	59.89	61.85	60.16	ı
1	88	64.36	60,02	64.10	60.30	63.83	60.58	63.57	60.85	ı
ı	90	65.82	61.38	65.55	61.67	65.28	61.05	64.29	61.54	ı
1	91	66.55	62.06	66.28	62.35	66.01	62.64	65.74	62 93	i
ı	92	67.28	62.74	67.01	63.04	66.73	63 33	66 46	63.62	ı
Н	93	68.03	63.43	67.74	63.72	67.46	6402	67.18	64 31	ı
ı	94	68.75	64.79	68.47	65.09	68.19	64.71	68.62	65.60	ı
ł	95	69.48		69.20	65.78	_	66.08	-	OWNERS OF TAXABLE PARTY.	l
1	96	70.21	65.47	70.65	66.46	70.36	66.77	70.07	67.08	ı
И	98	71 67	66.84	71.38	67.15	71.09	67.46	70.79	67.77	ı
ı	99	72 40	67.52	72.11	67.83	71.81	68.15	71.51	68.46	ı
ũ	100	73.14	68.20	72,84	68.51	72.54	68 84	72.24	69 15	ł
R	101	74.60	68.88	73-57.	69.20	73.16	70.21	72.96	70153	I
ĸ	103	75-33	70.25	75.02	79.57	74-71	70 90	74.40	71.23	ı
1	104	76.06	70.93	75.75	71.26	75.44	71.59	75.13	71.91	Į
V	105	76.79	71.61	76.48	71.94	76.16	72.28	75.85	72.61	١
	106	77.52	72.29	77-94	72.63	77.61	72-97	70.57	73.30	١
	108	78.99	73.66	78.66	74.00	78.34	74-34	78.01	74.68	I
	100	79.72	74-34	79-89	74.68	79.07	75.03	78.74	75 37	ı
	110	80,45	75.01	80.12	75-37	79.79	75.72	79.46	76.78	I
	III	81.18	75-70	80.85	76.06	80.52	76.41	80.18		۱
	113	81.91	76.38	81.58	76.74	81.24	77-10	80.90	77-45	1
	114	83.37	77.75	83.03	78.11	82.69	78.47	82.15	78.83	1
	115	84.11	78.43	83.76	78.80	83.42	79.15	83.07	79 32	1
	116	84.84	79.11	84-49	79.48	84.14	79.84	83.79	80,33	
	118	85-57	79.79	85.22	80.17	84.87	81.13	84.52 85.04	80.91	
	itq	86.30	81.16	86.68	81.54	85.59	81.91	85.90	82.84	
	120	87-76	81.84	87.40	82.22	87.04	82,60	-86.68	82.98	
	1 2	Dep.	Lat	Dep.	Lat.	Dep.	Lat.	Dep.	LINE	
	Dist	1 0	)/	1 4	5'	_	0/	transition in	154	
	-				BE THE	PANHE	-	_		

ī	8	0	Sparing S	15	1	30		4	51
١	18	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.
۱	1	0.73	0.68	0.73	0.69	0.73	0.69	0.71	0.69
ı	1	1.46	1.36	1.46	1.37	1.45	2.38	1.44	1.38
ı	3 4	2.19	2.73	2.19	2.06	2.18	2.75	2.80	2.77
ı	5	3.66	3.41	3.64	3-43	3.63	3-44	3.61	3.46
ı	6	4-39	4.09	4.37	4:11	4-35	4-13	4-33	4-15
ı	7 8	5.12	4.77	5-10	4.80	5.08	4.82	5.05	4.84
۱	9	5.85	6.14	5.83	5.48	5.80	6.20	6.50	6.22
R	10	7-31	6.82	7.28	6.85	7.25	6.88	7.22	6.92
ľ	III.	8.04	7.50	8.01	7-54	7.98	7-57	7.95	7.61
ı	12	8.78	8.18	8.74	8.22	8.70	8.26	8.67	8.30
9	13	9.51	9455	9.47	8.91	9.43	8.95	9.39	8.99 9.68
8	15	10.97	10.23	10.93	10.28	10.88	10.33	10.84	10.37
ı	16	11.70	10.91	11:65	10.96	11.61	11.01	11.56	1 LOS
	17	12.43	11.59	12.38	11.65	12.33	11.70	12/28	11.76
1	19	13.16	12.28	13.11	12.33	13.00	13.08	13.00	13.45
	20	14.63	13.64	14-57	13.70	14.51	13.77	14-45	13.83
1	21	15.36	14.32	15.30	14-39	15.23	14.45	15.17	1451
	22	16.09	15.00	16.02	15.07	16.68	15.14	15.89	15.21
ı	23	17:55	15.69	16.75	16.44	17.41	16/52	15.61	15.00
ĸ	25	18.28	17.05	18.21	17.13	18.13	17:21	18,06	17.29
ĸ	26	19.02	17:73	18.94	17.81	18.86	17.90	18.7%	17.98
B	27	19.75	18.41	19.67	18.50	19.59	18.59	19.50	18.07
ı	28	20.48	19.10	20.39	19.87	21.04	19.27	20.23	20.05
R	30	21.94	20.46	21.85	20.56	21.76	20.65	21.67	20.75
ı	31	22 67	21.14	22.58	21.24	22.49	21.34	22.39	\$1.44
ı	32	23 40	21.82	23.31	21.93	23.21	22.03	23.12	22.13
N	33	24.13	23.19	24.04	23-30	23.94	12.72 13.40	24.56	23.51
ĸ	35	25.60	21.87	25.49	23198	25.39	24.09	25.28	24,20
H	' 36	26.33	2455	26.22	24.67	26.11	24.78	26.01	24.89
R	37	27.79	25.23	26.95	25135	26.84	25.47	26.73	15.59 16.28
ı	38	28.52	26.60	28.41	26.72	27.56	26.85	28.17	26.97
ø	40	29.25	27.28	29.13	27.41	29.01	27.53	28.89	27.66
F	41	29.99	27.96	29.86	28.09	29.74	28.22	29.62	18.35
9	42	30.72	28.64	30.59	28.78	30 47	28.91	30.34	19.04
1	43	31.45	30:01	32.05	30.15	31.19	30.29	31.06	30.43
1	45	32.91	30.69	32.78	30.83	32.64	30.98	32.51	31.12
1	46	33.64	31.37	33.51	31.52	33-37	31,66	33-23	31.81
1	47	34-37	32.05	34.23	32.20	34.09	32.35	33.95	32.50
1	49	35.84	33.42	35.69	33-57	35-54	33-73	35:40	33.88
1	50	36.57	34.10	36.42	34 26	36.27	34-42	36.12	34-58
1	51	37.30	34.78	37.15	34.94	36.99	35.11	36.84	35.17
1	52	38.03	35.46	37.88 38.60	35.63	37.72	35.79 36.48	37.56 38.ag	35.96
1	53	39 49	36.83	39-33	37.00	39.17	37.17	39.01	37-34
1	55	40,22	37.51	40.06	37.69	39.90	37.86	39-73	38 03
I	56	40.96	38.19	40,79	38.37	40.62	38.55	40.45	38,72
1	57	41.69	38.87	41.52	39.06	41.35	39.24	41.17	39.42 40.18
1	50	43.15	40.24	42.97	40.43		40.61		40.80
1	59 60	43,88	40.91	43.70	41.11	43.52	41.30	43-34	41.49
1	Dist.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.
1	9	0		45	DECE	30		154	

) is	1	0'	<u> </u>	15'	_	30'	_ 1	45'	
1	Lat.	D~p.	Lat	i. De	p La	it. 1)	ep. la	at.   I he	ep. L. D.
61	43.×8	42.37	43.64					.32 42.	
52	44.60	43.07	44-41					.03  43.	
63	45.32	43.76	45.13					74 44	
61	46.76		46.56						
66	47.48	-	47.28						
	48.20		47.99						*,   .
64	48.92		48.71	47.4	5 43.5	0 4	66 43.	29 47.5	37 48.5
69		47.93	49.42					, .	
70		48.63	50.14	-	-   -			j	
71	51 07	49.32	50.86	1					
73	51.79	50.71	52 29	50.24					
74	53.43	51.40m	53.01	516				55 52.1	0   52.55
75	53.95	52.10	53.72	52.33	53-4	9 52.9	7 53.	26 52.8	o ¹ <u>53</u> ⊙,
76	54.67	52 79	54 44	53.03	54.2	1 53.2	7 53.9	7 :53-5	1 53-7
77	55 39	53.49	55.16	53.73					
78	56.11	54.18	55 87	54.43					
79 80	56.83	55-57	56.59	55.82	56 3				
81	57.55	56.27	58.02	56.52	_,	-1			
×2	58.99	56.96	58.74	57.22	57 77			2 57.0; 4 57.7;	
83	59 71	57.66	59.45	57.92	59 20				
84	60.42	58.35	60.17	58.61	59.91		\$ 59.6	6 .59.14	59 40
85	61.14	59 C5	60 89	59.31	60.63	_			60.13
86	62.86	59.74	61.60	60 01	61 34			,	
87 88	62.58	61.13	62.32 63.03	60.71	62.05	61 68			
89	64.02	61.82	63.75		63 48				
yo	64.74	62.52	64.47	62.80	64.19	63.08		2 :63.36	
9!	65.46	63.21	65.18	63.50	64 91	63.78	_		-
42	66.18	63 91		64.20	65.62	64.48	65.34	64.77	65 05
43	66.90	64.60	66.62	64.89	66 33	65.18	66.0	:65.47	65.76
94	67 62	65 30	67.33 68 05	65.59	67.76	65.89			66.47
95		65.99				67 29	-1		67.18
96 97	69.06 69.78	66 bg    67.38	68.76 69.48	66 yy 67.69	68.47	67 99			67.88
98	70.50	68 08		68. 38	69.90	68.69			69.30
99	71.21	68 77	70.91	69.08	70.61	69.39	70.51	69.70	70.00
103	71 93	69.47	71.63	69.78	71 33	70.09	71.02	70.40	70.71
101	72 65	70.16	72.35	70 48	72 04	70.79	71 73	71.11	71.42
102	73-37	70.86	73.06	71.17	72.75	71.49	72.44	71.81	72.12
103	74.09 74.81	71.55	73.78	71.87 72.57	73 46	72.19	73 15	72.51	72.83
125	-5.53	72.94	75.21	73 27	74.89	73.60	74.57	73 23	73-5-1
126	76.25	73.63	:	73.97	75 60	74.30	75.28	74.6	74.95
127	76 97	74 33		74.66	76.32	75.00	75.99	75.33	75.00
108	77.69	75.02		75.36	77.03	75.70	70.70	76.0	70.37
110	78.41	75.72		76 06	77.74	76.40	77-41	76.74	77.07
-	79.13			76.76	78.46	77.10	78.12	77.44	77.78
112	79.85 80.57			77-45	79.17	77.80	78 83	78.15	78.49
113	81.29			79.85		79.20	79.54	78.85	79.23 79.90
114	83.00	79.19	81.66	79 55		79.93	80.25 80.96	79.55	80.01
115	82.72	79.89	82 37	80.25		80.65	81.67	80.26	81.32
116				80.94	82.74	81.31	82.38	81.67	82.02
117			83. <b>8</b> r 8	81.64	83.45	82.01	83.00	82.37	82-7
118				32.34	04 10 .	82.71	83.80	83.07	83
120	86.32			3 04	84 88 . 85.59 1		84.51	3.78	84
l!	Dep.		Dep.	1.at.		8.4.11	85.22	84.48	.84
Dist.	0'		45'			Lat.	Dep.	lat.	سا
=			45'		30		1.	5	0
				45 D	EGREF.	S.			

MEAN REFRACTION.

I to the state of	-	-
App. Refr App. Refr. App. Refr. App. Refr.	App.	Helt.
Alt. Alt. Alt.	Ait	-
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0 0 33 0 5 0 9 54 10 0 5 15 20 0 2 35	34 9	1 24
0 5 32 10 5 5 9 46 10 10 5 10 20 10 2 34	34 30	1 13
0 10 31 22 5 10 9 38 10 20 5 5 20 20 2 32	35 9	1-11
0 15 30 35 5 15 9 30 10 30 5 0 20 30 2 31	35 30	1 20
0 20 29 50 5 20 9 23 10 40 4 56 20 40 2 29	36 0	1 18
0 25 29 6 5 25 9 15 10 50 4 51 20 50 2 28	36 30	E 17
0 30 28 23 5 30 9 8 11 0 4 47 21 0 2 27	37 0	1 -16
0 35 27 41 5 35 9 1 11 10 4 43 21 10 2 26 0 40 27 0 5 40 8 54 11 20 4 30 21 20 2 25	37 30	17 34
	38 0	F 33
0 45 26 20 5 45 8 47 11 30 4 34 21 30 2 24	38 30	1:31
0 50 25 42 5 50 8 4: 11 40 4 31 21 40 2 23	39 0	1 10
TO SECURE AND ADDRESS OF THE PARTY OF THE PA	39 30	THE REAL PROPERTY.
0 55 25 5 5 55 8 34 11 50 4 27 21 50 2 21 2 0 24 29 6 0 8 28 12 0 4 23 22 0 2 20	40 0	1 9
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1 20 22 15 6 10 8 3 12 40 4 9 22 40 2 16	44 0	0 59
1 25 21 44 6 25 7 57 12 50 4 6 12 50 2 15	45 0	0 57
1 30 21 15 6 30 7 51 13 0 4 3 23 0 2 14	46 0	D 55
1 35 20 46 6 35 7 45 13 10 4 0 23 10 2 13	47 0	0 53
	-	1
CANCELLO DESCRIPTION OF THE PROPERTY OF THE PR	48 0	0 51
- 13 3 3 3 13 1 23 2 2 3 1 3 21 3 2	49 0	0 49
	50 0	0.48
	51 0	0 46
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	53 0	0 43
THE RESERVE OF THE PARTY OF THE	54 0	0 41
ROBERT STREET,	55 0	0 40
	50 0	0 38
THE REAL PROPERTY OF THE PARTY	57 0	0 37
	58 0	0 35
2 35 16 4 7 35 6 49 15 10 3 28 25 10 2 1	59 G	0.34
2 40 15 45 7 40 6 45 15 20 3 26 25 20 2 0		D 33
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	63 0	0 29
	64 0	0 28
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3 10 14 4 8 10 6 22 16 20 3 12 26 20 1 55	66 0	0 25
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	68 o	0 23
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	70 0	0 21
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A STATE OF THE PARTY OF THE PAR	72 0	0 18
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4 42 22 22 2 2 2 2 2 2 2 2 2 2 2 2 2 2	4 0	0 6
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THE PROPERTY OF THE PROPERTY O	0 0	0 0
4 55'10 21 9 551 5 18/19 501 2 37/33 301 1 2019	G G1	52 D

Sun's	Paral-		TAB of the	Hori		Dip at differ. Distances
lax	in Alt.	leight	Dip.	Height	Dip	from the Observer.
Altit	-	Feet	111	Feet	1.1	Fee'
0			0 58	19	4 11	111 23/ 34/45/157/ 68
_		2	1 21	20	4 17	The last last last last
0	9	3	1 40		4 23	1 . 9 12 15 10 22
10	9	4	1 56	22	4 30	1.   2   5   0   12   12   12
20	8	5	2 9	23	4 36	0.4 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2
30		6	2 21	24	4 42	
40	7	7	2 33		4 52	1.4 2 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
50	6	8	2 44	28	5 5	
55	5	9	2 53	30	5 15	
	4	10	3 2	35	. 5 39	3 2 3 4 5 6 7
65	4	11	3 10	40	6 4	
70	3	12	3 19	45	6 27	5 2 3 4 5 5 6
75	3	13	3 27	50	6 46	3 4 4 5 0
80	2	14	3 36	60	7 25	0.2.3.4.4.515
85	1	15	3 42		8 1	4
90	0	16	3 50	80	8 34	
		17	3 57	90	9 6	5
		18	4 4	100	9 35	S -4

TABLE 10.

The Semi-diameter of the Sun.

the second	Day.	Sun's	Month	Day.	Sun's	뒫	Day.	Snn's
Month	Ā	Semi-di.		Ä	Sun's Semi-di	ş	Ā	Sun's Semi-di-
January.	1 7 13 19 25	16' 19' 16 19 16 19 16 18 16 17	May.	1 7 13 19	15/54" 15 53 15 52 15 51 15 50	September. Month	7 13 19 25	15'55" 15 56 15 58 15 59 16 1
February.	7 13 19 25	16 16 16 15 16 14 16 13 16 12	June.	7 13 19 25	15 49 15 48 15 47 15 47 15 47	October.	1 7 13 19 25	16 3 16 4 16 6 16 8 16 9
March.	7 13 19 25	16 10 16 9 16 7 16 6 16 4	July.	7 13 19 25	15 47 15 47 15 47 15 48 15 48	December. Nov ember.	1 7 13 19 25	16 11 16 13 16 14 16 15 16 16
April.	1 7 13 19	16 2 16 1 15 59 15 57 15 56	August.	25 7 13 19	15 49 15 50 15 51 15 52 15 53	December.	1 7 13 19	16 17 16 18 16 18 16 19 16 19

## TABLE II.

# Apparent Time of Transit of Pole Star.

This table is adapted to leap year, particularly 1808. In order in make it serve for other years, the time of transit must be taken for the day following that given in the months of January and February. For the first year after leap year, one minute is to be added to the time of transit given in the table; two minutes for the second, and three minutes for the third after leap year,

Again, to reduce this table to a different meridian than that to which it is adapted, viz. Greenwich; if the longitude is between 45° E, and 45° W, there is no correction to be applied. If the longitude is between 45° and 185° E, one minute is to be added; but if it is between 45° and 185° W, one minute is to be subtracted. If the longitude is between 135° E, and 180°, two minutes are to be added, but subtracted if the giret longitude is between 135° W, and 180°.

This table is useful to find the time when the altitude of the pole to ought to be observed, to find the latitude by its meridian altitude; it is also useful in finding the variation of the compass by the pole star-

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TABLE 10.

The Semi-diameter of the Sun.

Month	Day.	Sun's Semi-di.	Month	Day.	Sun's Semi-di.	Month	Day.	Sun's Semi-di-
2	7 13 19 25	16' 19' 16 19 16 19 16 18 16 17	May.	1 7 13 19	15/54" 15 53 15 52 15 51 15 50	September. Month	7 13 19 25	15'55" 15 56 15 58 15 59 16 1
	7 3 19 5	16 16 16 15 16 14 16 13 16 12	June.	7 13 19 25	15 49 15 48 15 47 15 47 15 47	October.	1 7 13 19 25	16 3 16 4 16 6 16 8 16 9
March.	7 3 9 5	16 10 16 9 16 7 16 6 16 4	July.	7 13 19 25	15 47 15 47 15 47 15 48 15 48	December, Nov ember.	1 7 13 19 25	16 11 16 13 16 14 16 15 16 16
April.	7 3 19	16 2 16 1 15 59 15 57 15 56	August.	7 13 19	15 49 15 50 15 51 15 52 15 53	December.	1 7 13 19 25	16 17 16 18 16 18 16 19 16 19

Sun's Declination for the Years 1808, 1812, 1816, 1820.

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10	22	5	14	37	4	2	8	0	17	39	23	2	22	15	15	34	4	55	6	42	17	12	22	57
	21	56	14	17	3	39	8	22	17	55	23	6	22	7	15	16	4	32	7	4	17	20	23	2
12	21	47	13	58	3	15	8	44	18	10	23	10	21	59	14	58	4	9	7	27	17	45	23	71
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15	21	17	12	57	2	4	9	49	18	54	23	20	21	32	14	3	3	C	8	34	18	33	23	13
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# EXPLANATION AND USE OF THIS TABLE.

The Declination of the Sun is an arch of a meridian contained between its centre and the equinoctial, which arch is reckoned in

degrees, minutes, &c.

In the first quadrant of the ecliptic, from about the 21st of March, to the 21st of June, the Sun's declination is North, and increasing; and in the third quadrant, between the 22d of September and 21st of December, the Sun's declination is South, and increasing. In the second quadrant of the ecliptic, from about the 21st of June to the 22d of September, the Sun's declination is North, and decreasing; and in the fourth quadrant, between the 21st of December and the 21st of March, the Sun's declination is South, and decreasing; which will be readily perceived by inspecting the table.

In this table, the Sun's declination is given, from the year 1808 to 1823 inclusive, calculated for the instant of noon, each day, at

Difference of Altitude of the Pole Star and the Pole, at different distances of the Star from the Meridian.

As the pole star is generally known, that no opportunity, therefore, may be lost for determining the latitude, this table is inserted, the use of which is as follows:—

Find the interval between the time of observation of the altitude of the pole star, and that of its passing the meridian, and take out the corresponding equation from the table; which added to, or subtracted from the true altitude of the pole star, will give the latitude of the place of observation.

#### EXAMPLES.

I. Let the corrected altitude of the pole star be 46° 10' N, observed 8h. 30' before its passage over the meridian. Required the latitude?

True altitude of the pole star 46° 10' N
Equation from table 12 to 2h. 30' + 1 5

Latitude 47 15 N.

II At 1h. 10' after the passage of the pole star over the meridian, its altitude corrected was 58° 51' N. Required the latitude?

True altitude of the pole star - 58° 51' N. Equation from table 13 to 1h. 10' - 1 42

Latitude - 57 9 N.

#### TABLE 12.

Difference of Altitude of Pole Star and Pole.

Argument. Distance of the Star from the Meridian, in Sidereal Time Subtract.

Min.	0	Hour.	1	Hour.	8	Hours.			41	lours.	5 I	lours.	T
0	ī	46'9	1	43.3	1,	32,6	10	15'6	00	53.4	0"	27.7	60
. 5	1	46.9		42.7	ı	31.4	ı	13.9	0	51.4	0	25.4	55
10	I	46.8	1	42.0	1	30.2	1	12.2	0	49-4	0	23.2	50
15	1	46.7	!	41.2	1	28.9	I	10.5	10	47.3	0	20.9	45
20	I	46.5	ī	40 4	1	27.6	1	8.7	0	45.2	0	18.6	40
25	1	46.3	1	39.6	1	26.2	1	6.9	0	43. L	0	16.3	35
30		46.0	ı	38.8	1	24.8	1	5.1	0	40.9	0	14.0	30
35	1	45.7	1	37.9	١.	23.4	1	3.2		38.8	0	11.6	25
40	1	45.3	1	36.9	t	21.9	L	1.3	0	36.6	0	9.3	20
45	1	44.9	ı	35.9		20.4	٥	59.4	0	34-4	0	7.0	15
50	1	44-4	I	34.8	1	18.8	0	57.4	0	32.2	၁	4.7	10
55	I	43.9	2	33.7	1	17.2	0	55.4	0	29.9	0	2.3	5
60	ı	43.3	E	32.6	1	15.6	0	53.4	0	27.7	0	0.0	0
	īī	Hours	10	lours.	9 1	iours.	8 H	lours	7 F	louts.	6 H	ours.	Min.

Sun's Declination for the Years 1810, 1814, 1818, 1822.

DI	Jan	1. ]	Fe	b. I	31	ar.	Api	ril	M	ay.	Jui	ne.	Jul	y.	Au	g.	Se	pt	Oc	1	No	Y.	Dec	1
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3	22	52	16	37	6	57	5	10	15	33	22	16	23	1	17	39	7 4	43	3	48	14	58	22	4
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6	22	33.	15	43	5	48	6	19	16	26	22	37	22		16	51	6 .	37	4	58	15	53	22 2	я
17	22	26	15	24	5	24	6	41	16	42	22	44	22	39	16	34	ю	14	5	21	16	1.4	27 3	6
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II	1000	52	14	8	3	51	8	II.		47	1000		22	43	25	25		44	6	53	37	20	#3.0	9
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33	19	31	9	57	0	53	12		20	10051	23		20		II			6	11	17	20	18	23 1	7
24	19	17		35	1	17	-	44	20	1000	23	27	19	59	II	16	0	18	11	38	20	30	=1 :	7
25	19	3	9	13	4	40	13	4	20	53	23	25	19	47	10	56	0	41	11	59	40	42	23 3	5
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30	_	45		100	3	37	14	39	21				18	_		-	2	30	13.	40	21	37	23	4
31	17	28			4		1	I	21	52	1	1	18	24	8	49	1	11	14	0			43	L

of refraction and parallax upon the distance; it is also necessary to calculate the apparent time from an obsered altitude of the sun at a distance from the meridian, the latitude being given; or to compute the time of the sun's setting or rising; which, though a less accurate method than the former of obtaining the time, may yet be useful when that cannot be had. For any of these purposes the sun's declination must be found to the time given nearly, reduced to the meridian of Greenwich, making proportion according to its daily increase, or decrease, by the help of table 14, as in the following examples.

1st Required the Sun's Declination at noon in New-York, in

Longitude 740 8' West, on the 1st of April, 1811.

Dec. for April 1st, 1811, at Greenwich, in Tab. 13 = 4\* 18' N. Equation for Long. Table 14. = + 4 50"

Required Declination = 4° 22' 50".N.

Sun's Declination for the Years 1809, 1813, 1817, 1821.

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100	23	2	17	7	7	37	14	30	15	2	22	3	23			6		22	3	7	14	24	21	49
1 3	100	ge es		50	м	14	4	53	15	20		-	23	_	17	50		0		31	14	43	21	58
3	22	SEA.	16	33	6	51	5	16	1000		22		100		17	35		.38		1000	15	2	22	7
Ш	22	2.8	15	15	6	28	56	39		13	22		22	100.00		19	6	54	4	17	15	21	22	23
113	-			320	1~		6	7				-		-		- 19	6		1	400		40	-	
107	22	31	15	39	20.00	45	6		16	46	22	39	22		16	47	6	31	5	27	16	58	22	30
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the Meridian of Greenwich, or the meridian, at which we begin to reckon the Longitude. It is to be taken out with the month at the top, and the day in the left hand column, at the same time, noting whether it be North, or South, as expressed at the top of each column. The declination being here given to the nearest minute, it will be found sufficiently exact for the most common

and useful problems, wherein it is concerned.

The sun's declination is necessary to find the latitude, whether at sea or land, from the meridian abitude observed; it is also requisite for finding the latitude from two abitudes observed with the interval of time measured by a watch; it serves for computing the sun's azimuth, having his altitude and the latitude of the place given, in order to find the variation of the compass; it is required, jointly with the latitude of the place and the sun's horary angle, to compute his altitude, if neglected to be observed at the time of taking the moon's distance from the sun for finding the longitude, being useful to facilitate the calculation of the effect

When Sun's dec. increases.

Add in W. lon. | Add af noon. | Sub. in W. lon. | Sub. af noon. | Sub. in E. lon. | Sub. be. noon. | Add in E. lon. | Add be. noon. |

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### Sun's Declination for the Years 1811, 1815, 1819, 1823.

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N. B. To find the equations in Table 14,—seek the Sun's declination to the nearest degree in the top line of the table; then, under this declination and against the given Lon. in the left hand column, is found the equation for Lon. and in the same column with the dec. and against the given time from Noon, in the right hand column, is found the equation for time; both which equations must be added, or subtracted, according to the directions at the head of the Table.

2d Required the Sun's Declination on the 1st of May, 1811, at 6 h. 48 min. P. M. in Longitude 72° W.

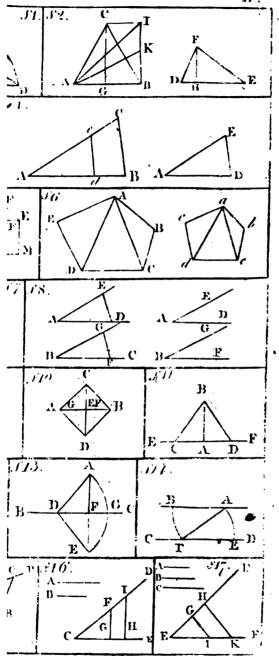
When Sun's dec. increases.

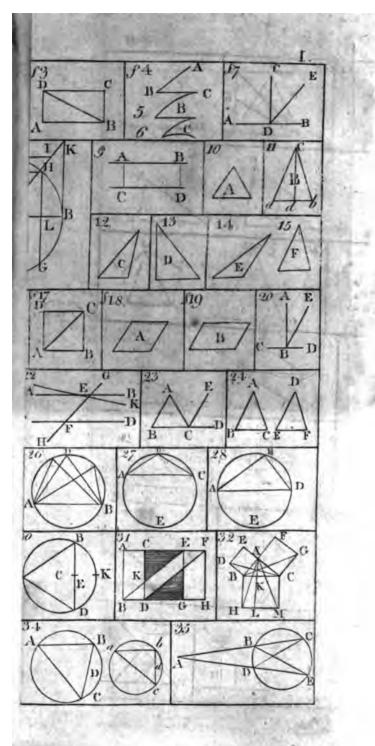
When Sun's dec. decreases.

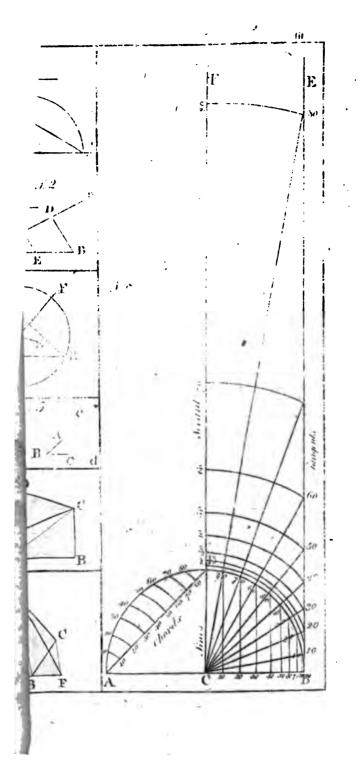
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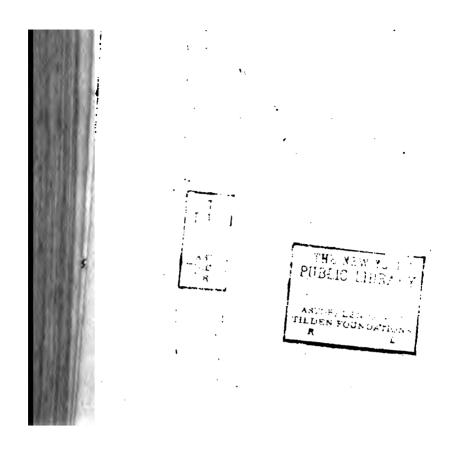


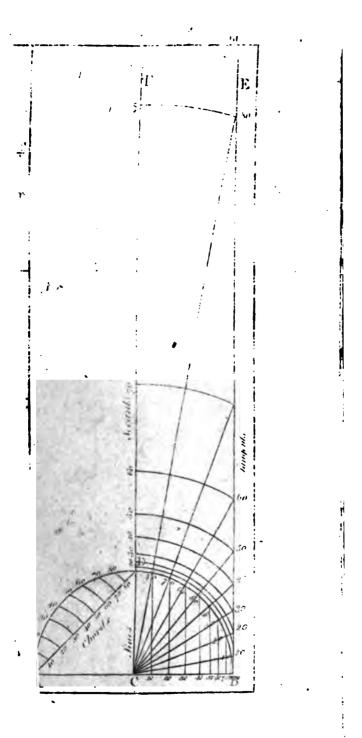


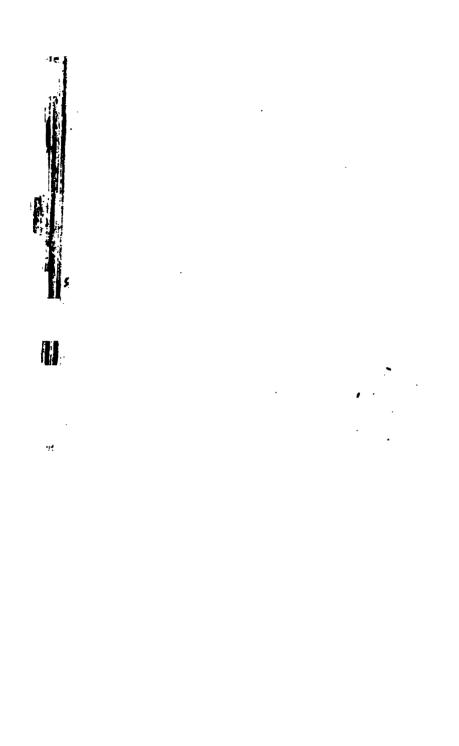
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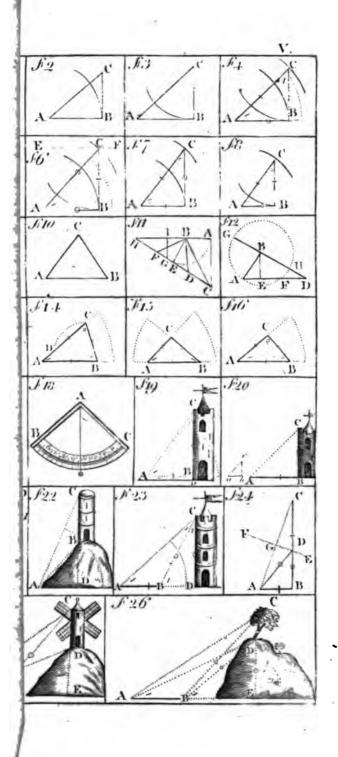
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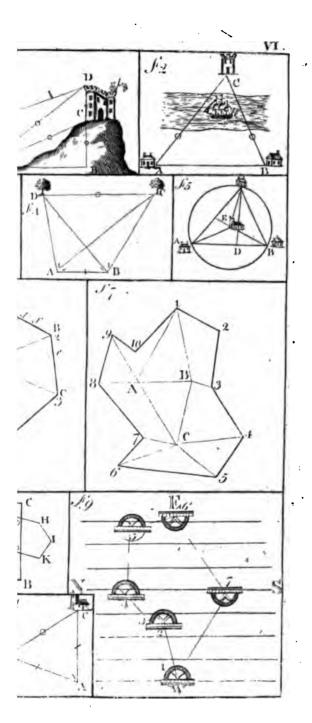


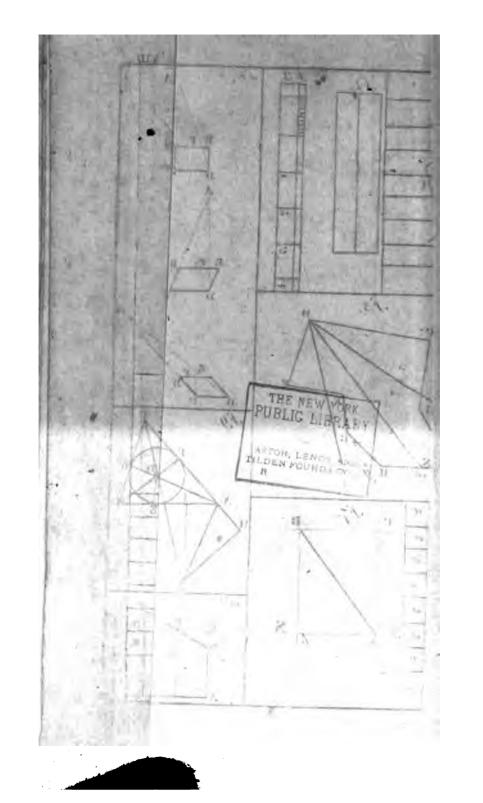


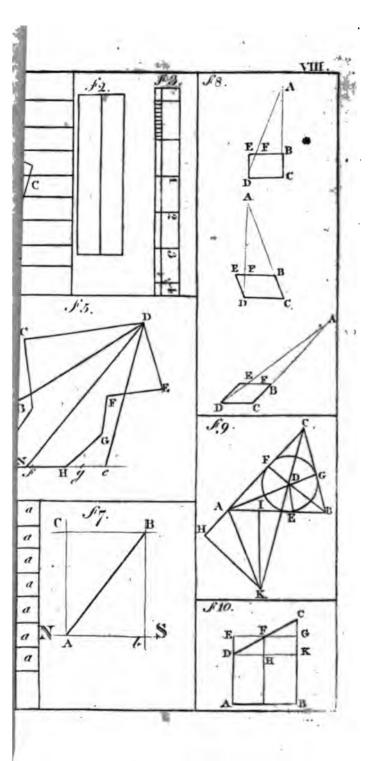








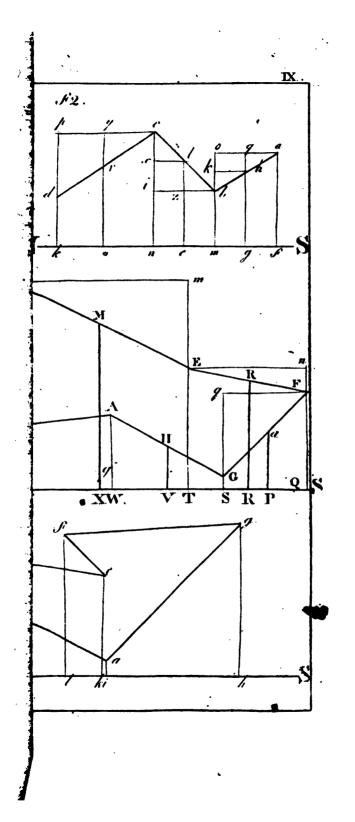




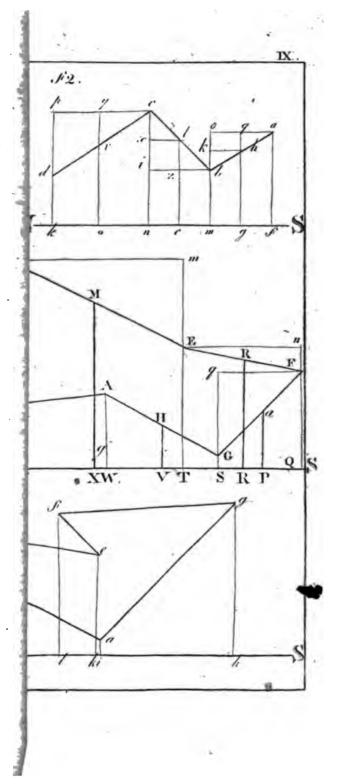
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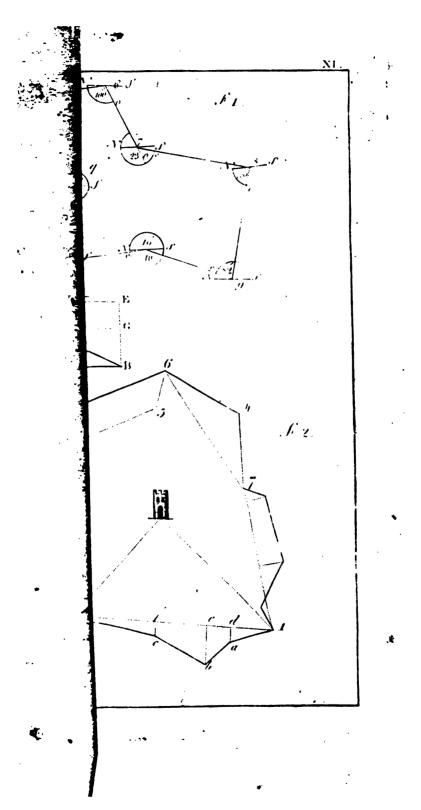




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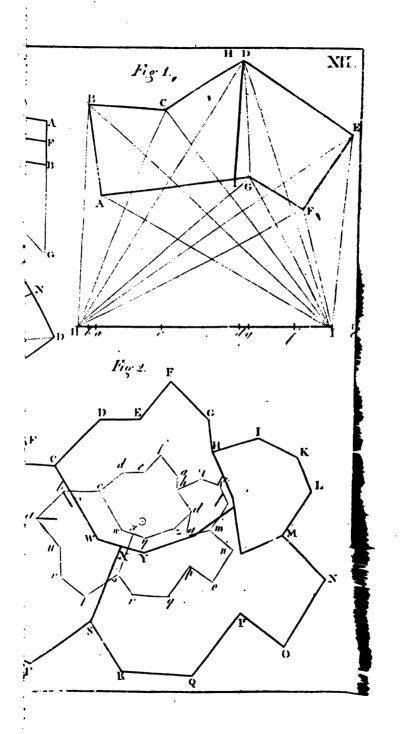
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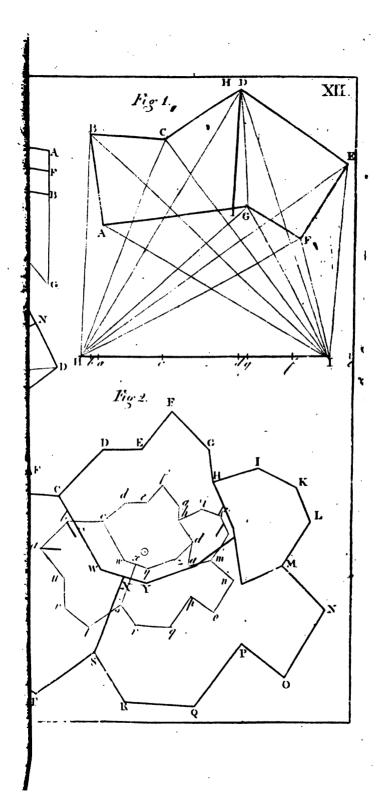




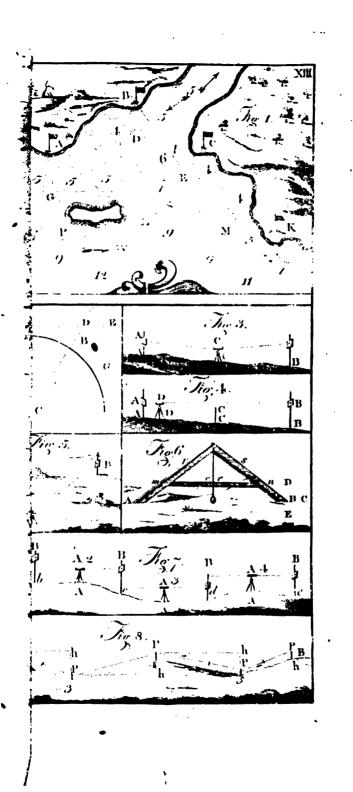


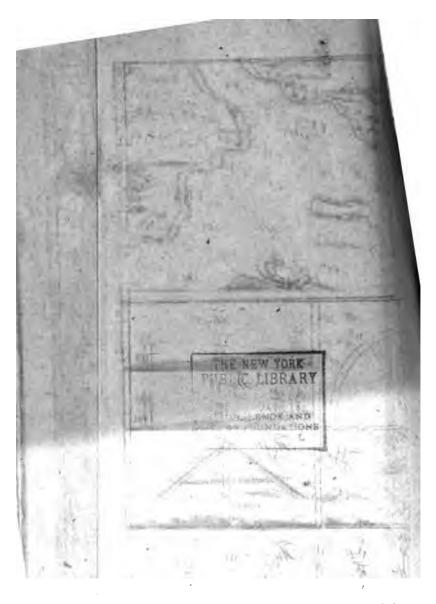




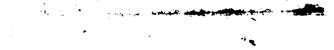




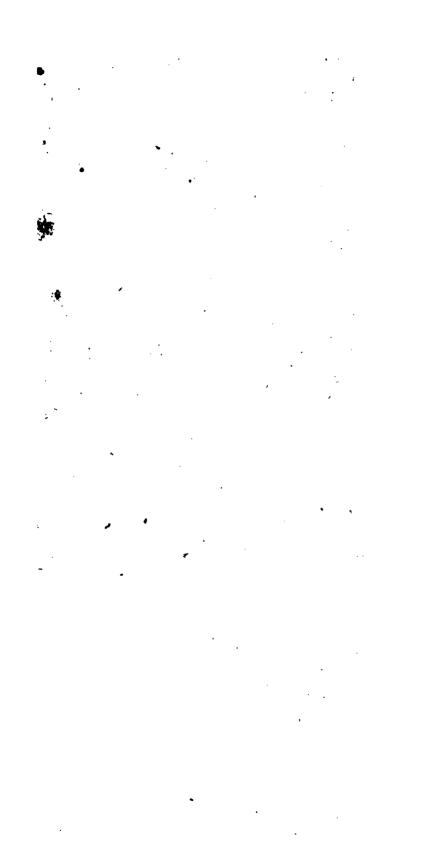




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